# H1 CONTROLLED WATERS RISK ASSESSMENT - POINT SOURCE EMISSIONS TO SURFACE WATER FROM AD PROCESS

Whitwick Manor, Lower Eggleton, Herefordshire, HE8 2UE

### **STL Energy Limited**

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# 1 Introduction

### 1.1 General

- 1.1.1 Oaktree Environmental was commissioned by STL Energy Limited to prepare a H1 Controlled Waters Risk Assessment. This assessment has been undertaken to assess the potential impacts from emissions to surface water associated with an anaerobic digestion (AD) process to be undertaken at the site, Whitwick Manor, Lower Eggleton, Herefordshire, HE8 2UE. This assessment is prepared in support of an application for an environmental permit to operate an anaerobic digestion plant at the site.
- 1.1.2 The EA H1 Screening Tool has been used to assess potential impacts due to the discharge of fully treated AD effluent on the system of surface water drainage receptors. This document outlines the method used and results from the assessment. A copy of the completed H1 screening tool showing inputs and outputs is included within Appendix I.
- 1.1.3 The site will be constructed and operated in accordance with the requirements of the WRAP Quality Protocol specifying the end of waste criteria for the production and use of quality outputs from anaerobic digestion of source-segregated biodegradable waste dated January 2014 and the PAS 110:2014 Specification for whole digestate, separated liquor and separated fibre derived from the anaerobic digestion of source-segregated biodegradable materials dated July 2014. Any solid or liquid output (referred to in this assessment as the thick fraction and thin fraction respectively) will therefore comprise a material and not a waste until such point as the holder either discards it or is required to discard it.
- 1.1.4 Due to the ongoing recording of elevated nutrient levels in the River Wye and its tributaries it is proposed that the liquid output from the AD process is treated to reduce the nutrient concentrations within the output to levels which will not cause further deterioration in water quality in the River Wye catchment. Any liquid effluent produced by the AD process will be re-circulated back into the process in the first

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instance following treatment as appropriate. Only where liquid effluent can not be re-used and re-circulated will the effluent be treated and discharged in accordance with the concentration and volume limits set out in this assessment.

1.1.5 The discharge point W1 as shown at Appendix I will be the only discharge to surface or groundwater as part of the site operations. Two package treatment plants will be used to treat domestic sewage arising from the weighbridge offices and the grain store which will discharge to the drainage system consistent with the general binding rules for domestic sewage discharges and as such will be exempt from the need for an environmental permit.

### 1.2 **Site Location**

- 1.2.1 The site is located at an approximate National Grid Reference SO 60660 45744 and is located off the A417. The proposed site is currently in agricultural land use and is bounded to the north and north east by the A417 with agricultural land beyond. To the east lies agricultural and with the A417 beyond and to the south and west lies agricultural land.
- 1.2.2 It is the intention that the solid material generated by the AD process will be exported as a material. Notwithstanding the liquid fraction being PAS110 compliant, it is unlikely that any liquid effluent will be exported from the site for use on the land due to the potential for such as use to cause a further deterioration in water quality in the River Wye catchment.
- 1.2.3 Neither the thick fraction nor the thin fraction will be discharged to surface water due to the lack of a public sewer in proximity to the site operations. Any liquid effluent which can not be re-used and surface water generated at the site will be treated and discharged to the surrounding surface water drainage system.

### 1.3 **Development Proposals**

- 1.3.1 The development comprises an anaerobic digestion facility and an associated grain store. The development is presented in the Environmental Statement (Report Reference 2102-003-B). The plant will be capable of processing up to 176,000 tonnes/annum of feedstocks. These will comprise 100,000 tonnes/annum poultry manure, 16,000 tonnes/annum apple pomace and 60,000 tonnes/annum of liquid waste from dairy units and drinks industry processes etc.
- 1.3.2 The results of these processes are the production of biogas, which consists predominantly of methane (CH<sub>4</sub>) and carbon dioxide (CO<sub>2</sub>) and digestate product.
- 1.3.3 The proposals will allow for the construction of an anaerobic digestion plant as shown on Drawing No. 2102-006-02. All waste handling treatment operations will take place on a sealed drainage system with an impermeable base or will take place within covered areas or within the sealed vessels or tanks. The proposals also include reed and buffer lagoons for further treatment of liquid digestate and a network energy facility and compressor to export generated biogas to the National Grid, a CO<sub>2</sub> and dry ice manufacturing plant, two combined heat and power plants and an emergency flare. Energy generated in the combined heat and power plant will be used to dry grain in the proposed grain store.

# 1.4 **Hydrological Setting**

1.4.1 The site is in the catchment of the River Wye. The drainage system in respect of the operation will discharge to the field drainage system under the control of the operator as shown on Drawing No. 2102-006-03. The boundary of the operator's land comprises the drainage ditch running parallel with and to the north of the Herefordshire and Gloucestershire Canal which comprises an unnamed tributary of the Withington Marsh Brook. The Withington Marsh Brook comprises a tributary of the River Little Lugg which in turn comprises a tributary of the River Lugg discharges to the River Wye.

# 2 **Operations**

### 2.1 **Overview**

- 2.1.1 The H1 Screening Tool has been used to assess potential impacts from the discharge of fully treated water from the anaerobic digestion (AD) process to the River Lugg via a settlement lagoon and unnamed tributary. The following sections describe and justify the input parameters which have been used in the H1 Screening Tool.
- 2.1.2 The site layout is shown on Drawing Reference 2102-003-03 which is presented at Appendix I along with a flow-chart schematic of the process which is presented at Appendix II. The discharge from the site will comprise only fully treated water from the AD process and rainfall runoff generated on the site surfaces discharged from the site drainage system. The mass balance calculations on which this assessment is based are presented also at Appendix II.
- 2.1.3 Liquid digestate from the anaerobic digestion process will be retained for as long as possible within the primary digesters. Digestate from the primary digesters will be pumped to the secondary digester to allow further gas collection which will maximise insofar as possible the methane gas yield. Only in the scenario where the digestate can not be re-used within the process with or without treatment.

# 2.2 **Feeders**

2.2.1 There will be 4 walking floor feeders of approximately 100m³ capacity, sufficient for 12 hours. These will be filled twice a day, morning and evening.

# 2.3 **Pre-treatment**

2.3.1 There will be three hydrolysis/pasteurisation tanks, each being 1,000m³ in volume to allow for the feedstocks to be pre-processed by hydrolysis, pasteurisation and deammoniafication. Approximately 55% of the ammonia is removed before the digestion process to prevent the nitrogen from inhibiting the digestion process and to extract

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55% of the Nitrogen into a concentrated Ammonium Sulphate solution which can be sold as a fertiliser. A large 6,250m<sup>3</sup> Ammonium Sulphate storage tank is provided for.

## 2.4 **Anaerobic Digestion**

2.4.1 The pre-treated material is pumped into 4 primary digesters, each 6,250m³ in volume and then into two secondary digesters, also providing 6,250m³ of volume. These will be maintained at over 40 degrees Celsius for the digestion process and fully stirred. The biogas that is produced will bubble up to the headspace in the double membrane roofs. The roofspace has support straps and a de-sulphurisation net as well as a flexible gas membrane and air-blown outer weather membrane. The resultant biogas is around 55% CH<sub>4</sub> and 45% CO<sub>2</sub> and is piped via desulphurisation tower(s) for use in the Combined Heat and Power (CHP) units and the biomethane plant.

# 2.5 **Nutrient Recovery**

2.5.1 The phosphate recovery and treatment process document is presented at Appendix V. The digestate overflow will be treated to extract nutrients in a multi-stage process where the majority of the remaining Nitrogen, Phosphates and Potassium are removed. These processes collect the nutrients in a concentrated form including ammonium sulphate, calcium phosphate, which can be easily transported and then applied as available fertilisers where and when agronomically required.

# 2.6 **Digestate Separation**

2.6.1 The low nutrient digestate is then separated with screw presses and/or decanter centrifuges into a benign solid soil improver and a liquid stream. The liquid stream is still around 1% solids so requires further processing through a reverse osmosis membrane / ion exchange plant to create a liquid stream suitable for re-circulation or final polishing in a reed bed before discharge.

- 2.7.1 An area of around 5.3ha has been allocated for a reed bed system which further cleans the run-off water. A buffer storage lagoon has been provided for to allow for maintenance and process control. A second lagoon has also been provided for to capture rain from the site which can be used in the AD process or discharged to the local ditch network. The layout of the reed bed system is shown on Drawing No. 2102-006-02 presented at Appendix I.
- 2.7.2 Water from the reed bed is discharged into the storm water lagoon which is discharged via a restricted outlet to the surrounding surface water system. The sampling point inf respect of Emission Point W1 will be located immediately downstream of the flow restriction device as shown on Drawing No. 2102-006-02 presented at Appendix I. The fully treated discharge will then be conveyed through ditches under land controlled by the operator to the drain running parallel with the Herefordshire and Gloucestershire Canal as shown on Drawing No. 2102-006-03.

# 2.8 **Site hydrological setting**

- 2.8.1 The site is in the catchment of the Withington Marsh Brook which is in the catchment of the River Lugg. The site and wider area are recorded as being in the operational catchment of the River Arrow, Lugg and Frome. The Withington Marsh Brook flows generally north east to south west along the northern boundary of the site. The confluence between the Withington Marsh Brook and the River Little Lugg is approximately 3km west of the site.
- 2.8.2 The sites is within flood zone 1 which is defined as land having less than 1 in 1,000 annual probability of flooding from rivers or sea. The site generally has a very low (less than 1 in 1,000 year annual probability of surface water flooding except within the areas immediately surrounding the ponds and watercourses at the site which is consistent with the site's topographic and hydrological setting. The site is not at risk

due to canal flooding, with the nearest canal comprising a disused section of the Herefordshire and Gloucestershire canal.

- 2.8.3 The land at the site falls generally towards the north west in the north and to the south in the south of the site. The site will be re-profiled as shown on Drawing No.s 0113-00-C Whitwick Manor Sheet 02 (site plan). Rainfall incident to the proposed concrete area in the current situation drains to the north to an unnamed tributary of the Withington Marsh Brook as discussed above. The drain discharges to the Withington Marsh Brook approximately 2.77m south west of the site.
- 2.8.4 Following the proposed development, rainfall incident to the impermeable concrete surface in the north of the site will drain to the storm water lagoon to the south of the proposed concrete surface as shown at Appendix I.
- 2.8.5 Based on the above and taking into account the general historic and current land uses at and in the area surrounding the site, it is considered that the hydrological receptors at the site and in the surrounding area have a low degree of sensitivity to the proposed operations at the site.

# 2.9 Flow in River Lugg and tributaries

2.9.1 Based on information presented on the National River Flow Archive Website<sup>1</sup> the Q95 within the River Lugg at Lugwadine is the closest river gauging station to the site. The median discharge rate or Q<sub>MED</sub> for this period is 6.78m<sup>2</sup> and the average 95<sup>th</sup> percentile exceedance discharge is 1.62m<sup>3</sup>/s. Based on information presented of the FEH online website, the catchment area of the River Lugg at Lugwadine is reported as 844.66km<sup>2</sup>. The catchment area of the drainage ditch to the north of the canal downstream of the

<sup>&</sup>lt;sup>1</sup> https://nrfa.ceh.ac.uk/data/station/meanflow/45003

area at Kymin is approximately 6.30km<sup>2</sup>. The Q95 value at Kymin based on the catchment area is therefore:

$$1.62 \text{m}^3/\text{s} \text{ x} (6.30 \text{km}^2 / 182.2 \text{km}^2) = 0.0115 \text{m}^3/\text{s}$$

2.9.2 The  $Q_{95}$  flow at the outfall from the STL AD facility to the unnamed tributary of the River Little Lugg is therefore modelled as  $0.0115m^3/s$ .

# 2.10 **Effluent flow rates**

- 2.10.1 The mass balance calculations supplied by the technical provider, including the flow rates are presented at Appendix III. The discharge rate from the AD process is calculated as 478 tonnes / day which is 5.53l/s. The discharge of fully treated effluent from the AD process will not exceed this volume.
- 2.10.2 In order to provide a worst case assessment it is assumed that there will be no surface water discharged from the lagoon concurrently with the fully treated effluent from the AD process. It is likely that the fully treated effluent will be diluted further within the lagoon prior to discharge in comparison to the scenario modelled.
- 2.10.3 The discharge is also modelled assuming conservatively that the full discharge from the process is fully treated and then released to the unnamed tributary of the River Little Lugg. A proportion of the water within the process will be re-circulated back to the primary digestor tanks depending on the water demand within the process hence the modelling of the constant discharge of fully treated effluent equal to the output of the AD process is a worst case assumption.

# 2.11 Risk assessment

2.11.1 The discharge from the after storage tanks will be controlled so that it does not exceed an average of 5.53l/s.

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2.11.2 The temperature of the surface water discharged from the site will be ambient due to the time spent in the reed beds and lagoon prior to discharge.

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# 3 H1 risk assessment

- 3.1.1 There is the potential for the fully treated effluent from the process and the drainage at the site to contain ammoniacal nitrogen and phosphate. Notwithstanding the assumed removal of ammoniacal nitrogen and phosphate from the discharge both in the pre digestion treatment and the post digestion water treatment, the assessment and monitoring in the site discharge of ammoniacal nitrogen and phosphate concentrations will serve to verify the effectiveness of treatment process and confirm that the operations will not have an unacceptable impact on the water environment.
- As discussed above the pH of the digestate is likely to be neutral to slightly alkaline therefore it is considered that the ammoniacal nitrogen present in the water within the treatment process is likely to be present almost exclusively as ammonium. It is therefore considered that the positively charged ammonium ions are likely to partition within the process towards the negatively charged clay and organic matter particles within the thick fraction of the process and sorb to the negatively charged clay surfaces within the clay filters and reed bed substrate. The negatively charged phosphate ions will be removed as struvite crystals through a process of ion exchange involving calcium, magnesium, ammonium and phosphate. The ammonia and phosphate removal processes will therefore be mutually complementary hence any malfunction within the treatment process will be readily detectable allowing for prompt identification and rectification.
- 3.1.3 Biochemical oxygen demand and chloride concentrations are assessed and will be monitored also in order to verify that the redox conditions and the total dissolved solids of the fully treated effluent are consistent with the assumptions made as part of the design of the process.
- 3.1.4 The elevation of the receiving watercourses in respect of the site discharge is less than 80m AOD and the background alkalinity recorded in the River Lugg at Wergins Bridge approximately 7.8km west south west of the site between January and September 2022 ranges between 130mg/l and 230 mg/l with and average of approximately

184mg/l. It is therefore considered that the receiving watercourse comprising the unnamed tributary of the River Little Lugg should be classified as Type 5 as set out in Table 1 of the Water Framework Directive (Standards and Classification) Directions (England and Wales) 2015 as amended.

- 3.1.5 The overall water quality classification for the Withington Marsh Brook to the conference with the River Lugg is poor with a poor ecological class. The Withington Marsh Brook to its confluence with the River Lugg fails its chemical classification.
- 3.1.6 A H1 screening assessment is presented at Appendix III in which the likely impact due to the site discharge on water quality in the River Little Lugg.

# 3.2 **Parameters modelled**

3.2.1 The parameters used in the H1 assessment are as follows:

PARAMETER	UNIT	VALUE	JUSTIFICATION
Ammonia concentration in discharge	mg/l μg/l	0.13 130	Typical analytical detection limit assuming complete removal of ammoniacal nitrogen from water discharging from process.
Phosphate concentration in discharge	mg/l μg/l	0.05 50	Typical analytical detection limit assuming complete removal of phosphate from water discharging from process.
Biochemical oxygen demand	mg/l μg/l	6.5 6,500	Background concentration needed to achieve 'Moderate' standard for Type 5 rivers consistent with approach set out in Environment Agency H1 Annex D2 which would cause no deterioration in the catchment of the Whithington Marsh Brook whose current overall status is 'poor'.
Chloride concentration in discharge	mg/l	30	Estimated background concentration based on mean electrical conductivity of 441.2µS/cm, (converted using a factor of 1.9 to 232 mg/l) minus avarage alkalinty

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PARAMETER	UNIT	VALUE	JUSTIFICATION
			of 184mg/l converted to chloride using a conversion factor of 17/28.
Effluent flow rate	l/s m³/s	5.53 0.00553	Output from AD process presented at Appendix II.
Q95 flow in River Lugg	I/s m³/s	11.5 0.0115	See paragraph 2.3.1 of this assessment
EQS for Ammonia concentration in discharge	mg/l μg/l	0.2 200	Used in the H1 assessment tool and is identical to that set out for ammonia (as N) for a high water quality watercourse below the elevation of 80m with a hardness greater than 50mg/l CaCO <sub>3</sub> (Type 3 or 5 watercourse) as set out in Reference <sup>2</sup>
Phosphate concentration in discharge	mg/l μg/l	0.05 50	Typical analytical detection limit assuming complete removal of phosphate from water discharging from process.
Biochemical oxygen demand	mg/l μg/l	6.5 6,500	Background concentration needed to achieve 'Moderate' standard for Type 5 rivers consistent with approach set out in Environment Agency H1 Annex D2 which would cause no deterioration in the catchment of the Whithington Marsh Brook whose current overall status is 'poor'.
Chloride concentration in discharge	mg/l	30	Estimated background concentration based on mean electrical conductivity of 441.2µS/cm, (converted using a factor of 1.9 to 232 mg/l) minus avarage alkalinty of 184mg/l converted to chloride using a conversion factor of 17/28.

<sup>&</sup>lt;sup>2</sup> Water Framework Directive (Standards and Classification) Directions (England and Wales) 2015 as amended

### 3.3 **Results**

- 3.3.1 The results of the H1 assessment at Appendix IV show that the modelled BOD is equal to the EQS specified above which is in turn lower than the background concentration in the River Lugg catchment. BOD therefore screens out on this basis.
- 3.3.2 The chloride release concentration is greater than 1% of the EQS and the process contribution of chloride is calculated as 3.9% of the EQS. The chloride contribution therefore screens out at Test 2.
- 3.3.3 The release concentration of ammoniacal nitrogen is greater than 1% of the EQS and the process contribution is greater than 4% of the EQS. The predicted environmental concentration minus the background concentration is less than 10% of the annual average EQS, and the predicted environmental concentrations are less than both the annual average and maximum allowable EQS values. Therefore, tests 3, 4a and 4b are passed and further consideration or modelling in respect of the risk posed due to ammoniacal nitrogen emissions are not necessary.
- 3.3.4 The release concentration of phosphate is greater than 1% of the EQS and the process contribution is greater than 4% of the EQS. The predicted environmental concentration minus the background concentration is less than 10% of the annual average EQS, and the predicted environmental concentrations are less than both the annual average and maximum allowable EQS values. Therefore, tests 3, 4a and 4b are passed and further consideration or modelling in respect of the risk posed due to phosphate emissions are not necessary.

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3.3.5 The discharge therefore passes the screening tests set out in the UK Government surface water pollution risk assessment for your environmental permit guidance<sup>3</sup> hence it is concluded that the proposed discharge will not have an unacceptable adverse impact on the water quality in the River Lugg.

<sup>&</sup>lt;sup>3</sup> https://www.gov.uk/guidance/surface-water-pollution-risk-assessment-for-your-environmental-permit

# 4 <u>Compliance limits in respect of the discharge to surface water and monitoring</u>

4.1.1 The following compliance limits are proposed in respect of the discharge to surface water:

DETERMINAND	LIMIT
Volume (Discharge from treatment process)	5.53l/s
Volume (Discharge at emission point W1)	12.9l/s
Chloride	30mg/l
BOD	6.5mg/I (O)
рН	Between 6 and 9
Phosphorous	0.05mg/I (P)
Ammoniacal Nitrogen (as N)	0.13 mg/l

4.1.2 It is proposed that monthly samples are collected from emissions point W1.

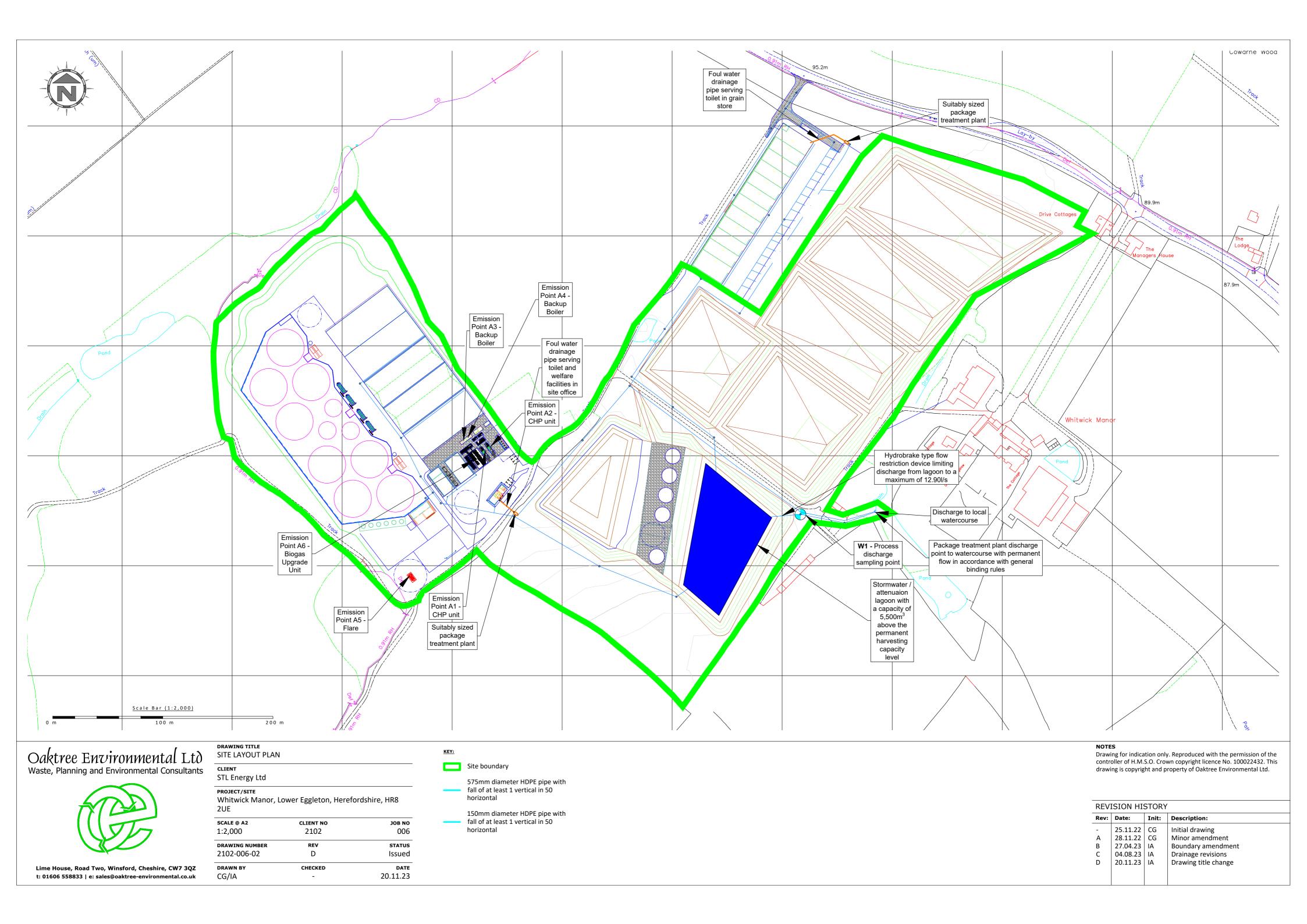
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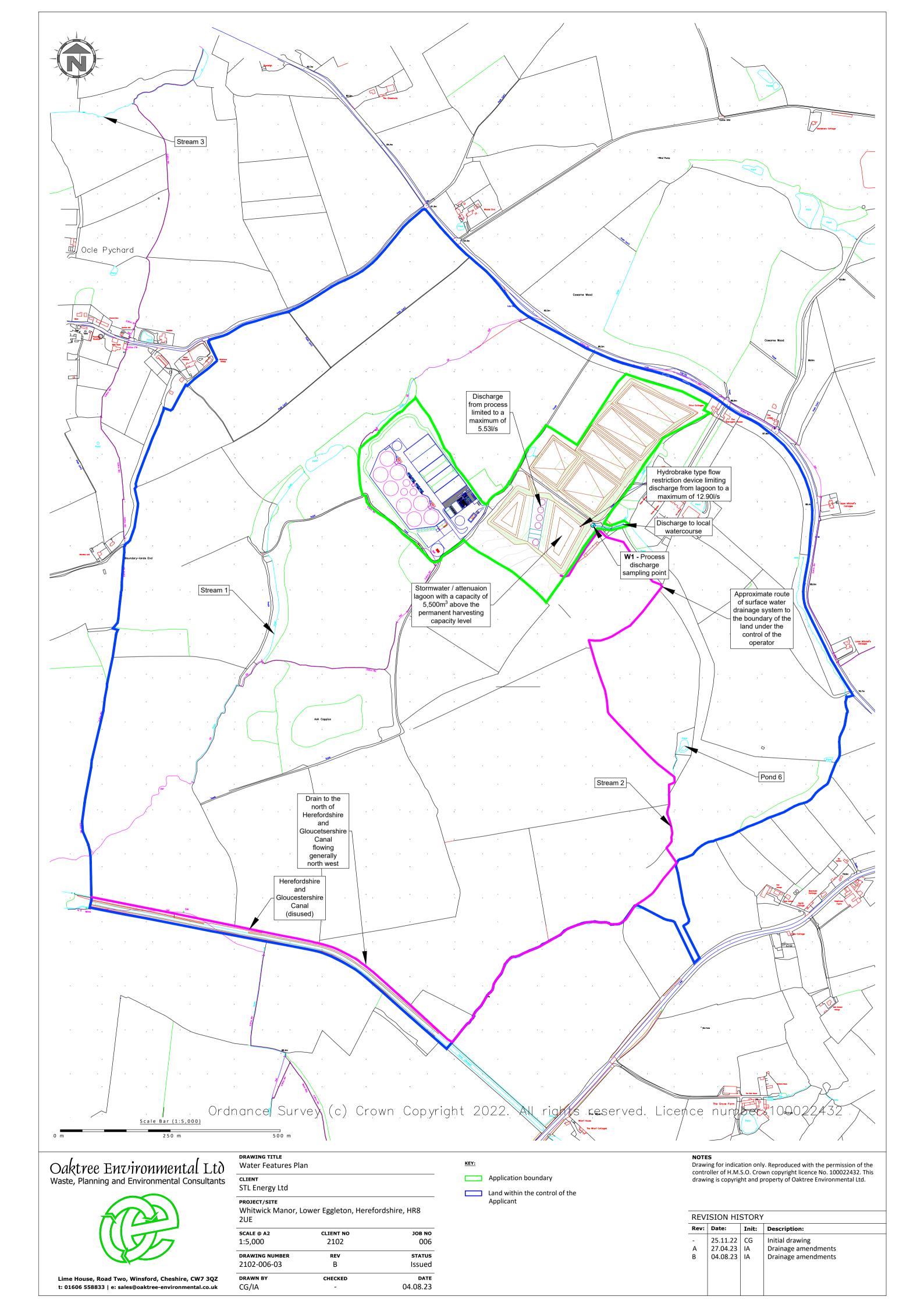
# 5 <u>Conclusion</u>

5.1.1 It is concluded that the site fully treated effluent from the AD process can be discharged to the surface water treatment system without posing a significant risk to the water quality within the River Lugg including the unnamed tributary of the Withington Brook and the River Little Lugg.

# **Appendix I**

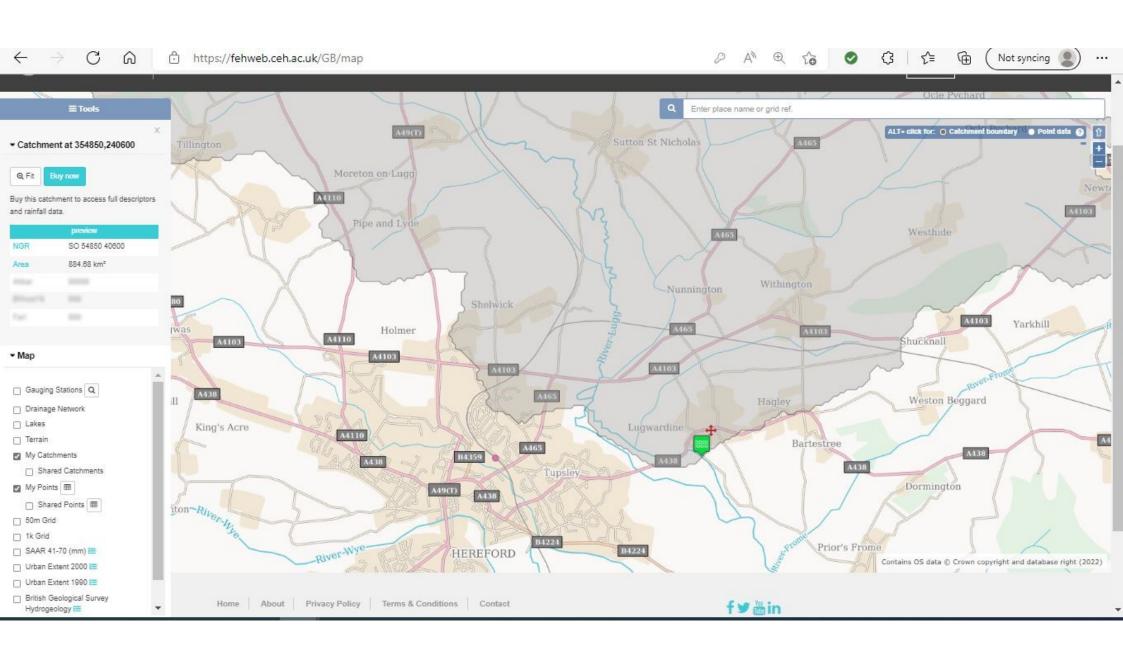
# **Drawings**

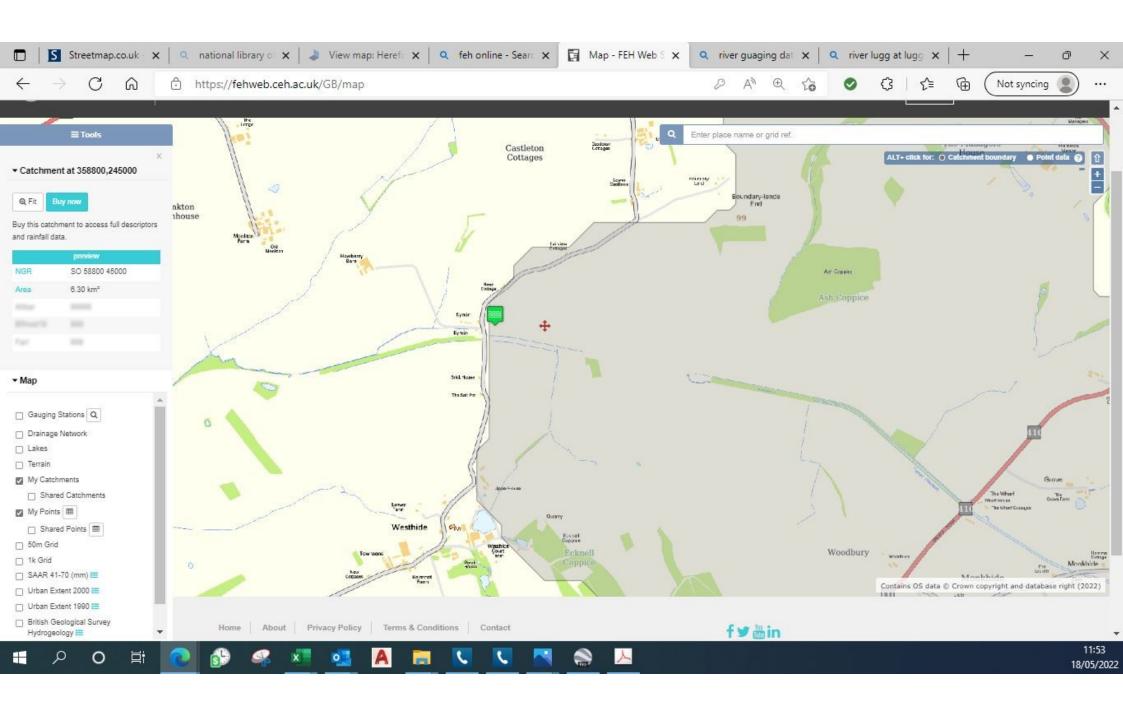




# **Appendix II**

# **Catchment areas of receiving watercourses**





# **Appendix III**

# Mass balance information

#### STL2 Whitwick Manor Farm **Process Flow Diagram** Solid Feeder 1 200 m3 Pasteuriser 1 1000 m3 Nitrogen Extraction 1 Primary Digester 1 6250 m3 6250 m3 Nitrogen Phos Ex. 1 695 T/d Stage 1 Centrifuge / Separation Fibrous Soil Improver 114 T/d Secondary Digester 1 Low nitrogen reduced P 40% DM Soil conditioner Primary Digester 2 Secondary Digester 2 Nitrogen Phos Ex. 2 581 T/d 41,610 pa Solid Feeder 2 Pasteuriser 2 1000 m3 Nitrogen Extraction 2 6250 m3 6250 m3 Output Liquid Solid Feeder 3 Pasteuriser 3 Primary Digester 3 55% N 1000 m3 6250 m3 Residence Time 21 d Approx Extraction Stage 2 Centrifuges/press Phosphate concentrate 39 T/d 25% DM 1 T/d Solid Feeder 4 533 T/d Min Residence Time Approx Extraction 55% % 6250 m3 Output Liquid 60 min at 70 DegC 811 T/d 14,600 pa throughput Feedstocks 1 batch per day approx Residence Time Reed bed system Hydrolysis / Past 3000 m3 COD removal 274 T/d Poultry Manure Primary 25000 m3 Secondary 12500 m3 Converted to Biomass and Liquid inputs Apple Pommace 44 T/d Transperation Digestate 96 T/d Digestate 96 T/d Total 40500 m3 Liquid Waste 68.5 T/d Liquid Waste 68.5 T/d 478 T/d 0 T/d 0 T/d Output Liquid Water Water 328.8 T/d 329 T/d Recirculate Recirculate Available Phosphate 138.758 kg P205/d 811.3 T/d 493 T/d Total Total input to plant Ammonium Sulphate 32% 4838 m3/y Clay media Adsorbed in clay pellets Ammonium Sulphate 32% 33.804167 T/h 1088 m3/y Water/liquid store 6250 m3 6250 m3 478 T/d nmonium Sulphate Store Output Liquid Feedstocks 482.5 T/d Water/recirc 328.8 T/d 329 T/d Recirculation Rainwater captured and used as part of recirculation Output Am. Sulphate Soln. 16 T/d Water to discharge 149 T/d Poultry Manure 100,010 T/yr Apple Pommace 16,060 T/yr Digestate 35,040 T/yr

Liquid Waste

25,003 T/yr

# **Appendix IV**

# **H1** Assessment





### **Welcome to the H1 Software**

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If you find the screen fonts in the H1Tool too small to read you can use the Windows zoom feature at any time to magnify the screen by holding down the 'Windows' key and '+' key. To cancel the feature hold down the 'Windows' key and 'Esc' key.

#### Introduction

This version of the tool accompanies the Horizontal Guidance Note H1 and the eleven supporting technical annexes.

### **Important Notes:**

With the exception of Annex I (Landfill) and Annex J (Groundwater) this software tool can be used to complete risk assessments within the technical annexes which support H1. However, further information may need to be provided in the following areas:

- detailed assessment of fate and effects, where required
- decision-making trails for the comparison and ranking of options

This software provides a general structure for assessing costs and environmental impacts. You may need to decide the best way to apply this structure to fit the nature and pattern of your operation, in particular:

- where load is variable, such as seasonal or demand-led operations
- where a number of processes are conducted at the same time, such as integrated operations
- where a number of products are made, with possible differences in unit operations and release points employed
- where fugitive or potential emergency releases are of particular interest

Information in this database will be used to determine your EPR permit, therefore to get the most from this software tool, you should:

- read the H1 Overview document, to understand the basic principles, module structure and methods
- use the HELP boxes and refer to the H1 guidance as you progress to ensure that the data you input is representative and accurate
- use the comments boxes to clarify assumptions and data sources

This software will also output annual emissions data to an OPRA profile(s), which you can select on the Summary Tables page.

On line instructions on using this tool and on the H1 Methodology itself are available on Gov.UK (click here)



In conjunction with:

www.ability-software.co.uk

# **Facility Reference Information**

Please complete the following information:

Company Name: STL Energy Limited

Location: Whitwick Manor, Lower Eggleton, Herefordshire, HE8 2UE

Permit Number:

If you have data already stored in a previous version of the H1 software you may import it by pressing the button to the right.

Please note that before the import can take place any data that already exists in this copy of the tool will be removed. Please also note that any 'Operating Mode' information you had entered in your Air and Water

inventories will defer to the default of 100% on data import

#### NOTE ON MICROSOFT ACCESS SECURITY WARNING

Depending on your security settings, you may get a security notice appearing each time the import routine connects to a table in your source database. You need to click 'Open' on this message for the Import routine to be successful. There are 18 tables to connect to in total but if you place your cursor over the 'Open' button you will be able to repeatedly click your mouse to make this process execute quickly and without too much frustration. We apologise for this inconvenience but it is an aspect of Microsoft Security provisions that are beyond our control.

Import Utility

#### Step 1

### **Introduction to Step 1**

#### **Step 1: Describe the Scope and Options**

The aim of this step is to:

- state the OBJECTIVES of the assessment
- in the case of ENVIRONMENTAL ASSESSMENT of the whole facility, describe the scope of the activities to be included in the assessment;
- in the case of OPTIONS APPRAISALS, identify candidate options for BAT by considering all relevant techniques to prevent and minimise pollution and the scope of activities covered by the techniques.

Depending on the reason for the assessment, you will need to complete different modules of the guidance. The software will automatically select the required modules according to the responses you enter.

NOTE: If you are going to complete more than one assessment or appraisal, make sure that you create a copy of the H1 file for each new assessment BEFORE you begin to input data. This is because Microsoft Access automatically saves changes to the current file you are using, rather than allowing you to save your changes at the end of your work.

TO CONTINUE WITH STEP 1, PRESS "NEXT".

# Water Discharge/Release Details and Flow Data

Please define your Release Points for Releases to Water

Number	Description	Location or Grid Reference	Activity or Activities	Final Discharge Point	Discharge via Sewer?	Mean Effluent Flow Rate* m3/s	Max Effluent Flow Rate* m3/s
1 W	/1	Discharge point from Whitwick	Discharge to surface water	1 Unnamed tributary of River Little Lugg	No	0.0055	0.0055
			is conservatively assumed that rocessf is occurring in the site dr	no dilution of the treated water from ainage system	the AD	* When operat	ing

### **Describe the Objectives**

Depending on the reason for the assessment you will need to complete different parts of the tool.

#### Select the type of assessment:

• a) to carry out an ENVIRONMENTAL ASSESSMENT of the releases resulting from the facility as a whole

Do Steps 1, 2 and 3 only

 $\bigcirc$  b) to conduct a costs/benefits OPTIONS APPRAISAL to determine BAT or support the case for derogation under the Industrial Emission Directive.

Do Steps 1,2, 3 and 4 and continue with 5 and 6 if necessary

1.1 Briefly summarise the objectives and reason for the assessment in terms of the main environmental impacts or emissions to be controlled:

Discharge of fully treated water from AD process to an unnamed tributary within the River Lugg catchment

Scope of Environ	mental Assessme	nt		
List the activities included in the a	ssessment			
Number Activity				
Use the 'Add' button at the bottom le	ft to create a new activity			
1 Discharge of fully treated	water from AD process to R	River Lugg.		
	Comments:			

### **Describe the Candidate Options**

#### Identify all reasonably applicable options of techniques

You should include:

- a) a brief description of individual control measures or configurations of control measures seleted for each option, and the activities with which they are associated (the existing base-case may conveniently be the first option).
- b) justification why any techniques generally applicable to the regulated facility have not been selected for assessment. (see relevant H1 annex) (This should be based on regulated facility-specific technical, not economic reasons).
- c) for new projects, whether any initial environmental assessment that was done at the project evaluation stage, or any screening of technology or process routes prior to this assessment, particularly where this has a bearing on environmental performance. (see H1)

In the case of b) or c) please enter your Comments here:

It is considered that if possible, the fully treated water from the AD process should be discharged to surface water hence returned to the water environment rather than being treated elsewhere.

Option Number Title

Description

1 Base-Case	Discharge of treated water to unnamed tributary of River Little Lugg
2 Tankering off site	Collection and removal of all site drainage for treatment at an off site facility is prohib

Once a series of options have been generated for the proposed project, it is recommended that the Operator discuss these with the local Regulator to check both parties agree that the options are satisfactory. This may save the Operator from spending resources on assessment of options which are unlikely to meet the required environmental performance.

List the main activity or activities to which the release control options are applicable and any other activities that will be affected by the candidate control option on the main activity:

#### Step 2

### **Introduction to Step 2**

#### **Step 2: Emissions Inventory**

The aim of this Step is to produce an inventory of sources and releases of polluting substances from each option. This is used as the basis for the subsequent evaluation of environmental impacts.

For this Step you will require information on:

- release points and sources of emissions to air, water (inc. sewer) or land
- concentration and mass rate of released substances
- frequency and duration of releases and how these relate to long term and short term effects

#### **IMPORTANT NOTES**

- you may need to consider a suitable method for assessment of groups of pollutants, such as VOCs, heavy metals, uncharacterised liquid effluents, etc (see "Grouping air emissions" in Annex F).

TO CONTINUE WITH STEP 2, PRESS "NEXT".

	Receiving Water Body(s)								
Please define the Final Discharge Locations for Releases to Water									
Are th	nere any discharges to surface waters?	Yes							
For o N.B. indi		nt where the sewage works discharg Estuary) you only need enter the R ext page. For discharges to TRaC	es to a surface water iver description and flow once. Further details of waters, seperate Discharge Locations must be added for						
Numl	per Description	Final Discharge Category	Freshwater Q95 flow rate						
1	Unnamed tributary of River Little Lugg	R	River Flow (m3/s): 0.0115						

### Release Concentrations of Substances Present in Discharges to Water

Please list all Substances released to Water for each Release Point identified in the previous page.

, , ,	of assessment method are you using? ox & H1 Annex D for information)	Continue with the method below.
Method:	Chemical Specific	
Reference:		

			Operating	Average Concentration in the Effluent (AA)		Maximum Conc Effluen			Significant
Numbe	r Substance	Meas'ment Method	Mode (% of	Conc.	Meas'ment Basis	Conc.	Meas'ment Basis	Annual Rate	Load (PHS Only)
				μg/l		μg/l		kg/yr	kg/year
1		Continuous	100.0%	130	Annual Avg	130		22.6712304	3
	>50mg/l (90 %ile)	1							
2	Chloride	Continuous	100.0%	30000	Annual Avg	30000		5298.048	
3	Phosphate	Continuous	100.0%	50	Annual Avg	50		8.83008	
4	Biochemical	Continuous	100.0%	6500	Annual Avg	6500		1133.56152	
	Oxygen Demand (Poor)								

### **Water Temperature**

Where relevant, please enter temperature of effluent for each release point.

This table is to check that the effluent is acceptable, i.e. within the required temperature range. It is not used to make relative judgement between options.

			High	High Peak Rate	Max Temp. Difference	Ber		
Discharge Location	Release Point	Measurement Method	Normal Rate			Max Summer	Max Winter	Max Temp
1 Unnamed tributary of Riv	1 W1	Continuous				21.5	10	2

### Water pH

Where relevant, please enter pH of effluent for each release point.

This table is to check that the effluent is acceptable, i.e. within the required pH range. It is not used to make relative judgement between options.

			High	High	Low	Low	pH of	Do artificial variations
		Measurement	Normal	Peak	Normal	Peak	Receiving	caused by effluent
Discharge Location	Release Point	Method	Rate	Rate	Rate	Rate	Water	exceed 0.5pH units?

1 Unnamed tributary of Riv 1 W1 Continuous 9 9 6 6 7.94 No

### **Raw Materials**

Please list all Raw Materials Consumed:

Annual

Number Material Consumption Units

1	Non-potable Water	tonnes/year	
2	Potable water	tonnes/year	

Pe	Performance Indicators								
inter consum	ption data to d	etermine you	r performance indi	icators					
Which of the	following parar	neters do you	use for calculating y	your performance Produ	ct				
Please descr	Please describe and justify your choice:								
Basic Consur									
	Name Annual Quantity Units								
Amount of P	Product:								
Main Raw M	laterial:				Produc	tion Efficiency:		1	
Potable Wat	ter:			m3	Potable Water:			m3	
Non Potable	e Water:			m3	Non Po	table Water:		m3	
Energy:				MWh	Energy:	:		MWh	
Waste: Ine	ert:			tonne	Waste:	Inert:		tonne	
Haz	zardous:			tonne		Hazardous:		tonne	
Stal	ble Non-reactiv	e Hazardous:		tonne		Stable Non-reactive Hazardous:		tonne	
Biod	degradable Nor	n-hazardous:		tonne		Biodegradable Non-hazardous:		tonne	
Oth	er Non-hazardo	ous:		tonne		Other Non-hazardous:		tonne	

Step 3

### **Introduction to Step 3**

### **Step 3: Quantify Impacts**

The aim of this Step is to quantify the effects on the environment of the releases listed in the inventory in Step 2. The guidance provides methods for assessing the eight main environmental considerations of most relevance to the EPR regime. Your releases may not result in effects to all eight of these considerations, and this tool allows you to screen out any that are not relevant.

The emissions you entered in Step 2 are automatically brought forward for assessment into each environmental consideration that is relevant for that type of release (e.g. a release may have more than one type of effect).

This part of the tool allows you to screen out any releases that are insignificant, and to identify those releases where further, detailed assessment of the potential environmental impact may be required.

#### IMPORTANT NOTE

This software tool only completes part of the requirements for Step 3, as described above. Depending upon the degree of risk to the environment presented by the releases, the operator may need to do further, detailed assessment of the potential effects using methodologies that are not provided here. This information should be submitted separately, as indicated within this part of the tool.

TO CONTINUE WITH STEP 3, PRESS "NEXT".

Identify	v Re	levant	Im	pacts
Idelitii	y itc	ovant		puoto

Identify any environmental impacts that are not relevant to this assessment by deselecting from the list below:

Releases in Part 2?		Justification for omission
No	Air	N/A
No	☐ Deposition from Air to Land	N/A
Yes	<b>✓</b> Water	
No	Waste	N/A
No	☐ Visual	N/A
No	Ozone Creation	N/A
No	☐ Global Warming	N/A

If you have deselected an environmental impact as not relevant to this assessment,

no further assessment of this impact will be carried out

### **Local Environmental Quality**

### **Describe the Quality of the Environment:**

Provide a brief description of the main local factors that may influence the importance of the impact of emissions in the surrounding environment

### Air Quality

Are there any Environmental Quality Standards relating to substances released from the activities, which may be at risk due to additional contribution from the activity? (Environmental Quality Standards for air and water are described in EPR Technical Guidance Notes)

Are there any Local Air Quality Management Plans applicable to releases from the activity?

### Water Quality & Resources

Are there any Environmental Quality Standards relating to substances released from the activities, which may be at risk due to additional contribution from the activity?

Are proposals to abstract water satisfactory in order to obtain an abstraction licence?

Is the activity located in a groundwater vulnerable zone (for activities with direct releases to land only)?

### **Proximity to Sensitive Receptors**

Is public annoyance likely to be an issue for noise, odour or plume visibility ?

Are there any wildlife habitats, eg Special Areas of Conservation, or Special Protection Areas, likely to be affected by releases from the activity? (Description of requirements of Habitats Directive is provided in EPR Technical Guidance Notes)

lone		

None

N/A

### **Water Impacts - Fresh Water Releases**

Apply Test 1 (See Guidance) and Calculate Process Contributions of Emissions to Water

This table applies Test 1 and also estimates the Process Contribution for Freshwater releases, this is calculated after dilution into the relevant surface water type for each emission to water listed in the inventory, according to the release point parameters input earlier. If you have more accurate data obtained through dilution modelling, this may be entered as indicated and will be used instead of the estimated PC. Any releases which 'Pass' Test 1 are screened out at this point.

-	A	nnual Avg EQ	S	MAC EQS	
Substance	Release	EQS	Release conc <	Release MAC	Release conc <
	μg/l	μg/l	10% EQS	β μg/l μg/l	10% EQS
			Test 1		Test 1
[W1] Ammonia CaCO3 >50mg/l (90 %ile) (Unnamed tributary of River Little Lugg)	130.0000	200.0000	Fail	130.0000	N/A
[W1] Biochemical Oxygen Demand (Poor) (Unnamed tributary of River Little Lugg)	6500.0000		N/A	6500.0000	N/A
[W1] Chloride (Unnamed tributary of River Little Lugg)	30000.0000	250000.0000	Fail	30000.0000	N/A
[W1] Phosphate (Unnamed tributary of River Little Lugg)	50.0000	120.0000	Fail	50.0000 120	Fail

Note that the Process Contribution shown for each substance is the sum of the individual process contributions of each point from which the substance is emitted. Process Contributions obtained from modelling data should incorporate all relevant release points and flow conditions.

\* If you have valid dispersion modelling data available - please enter it here

### Water Impact Screening - Fresh Water Releases

Apply Test 2

This page applies Test 2 and displays the Process Contribution as a proportion of the EQS. Emissions with PCs that are less than 4% of the EQS can be screened from further assessment as they are likely to have an insignificant impact.

		Annual Avg EQS ————								
Substance	Annual Avg EQS	PC	Modelled PC	F % PC of EQS	PC < 4% of EQS?	MAC EQS	PC	Modelled PC	% PC of MAC	PC < 4% of MAC?
	μg/l	μg/l		%	Test 2	μg/l	μg/l		%	Test 2
Ammonia CaCO3 >50mg/l (90 %ile) (Unnamed tributary of	200	42.2137		21.11	Fail		42.2137		-	Pass
River Little Lugg)										
Chloride (Unnamed tributary of River Little Lugg)	250000	9,741.6324		3.90	Pass		9,741.6324		-	Pass
Phosphate (Unnamed tributary of River Little Lugg)	120	16.2361		13.53	Fail	120	16.2361		13.6	Fail
	Comme	nts:								

### Water Impact Screening (Predicted Environmental Concentration) - Fresh Water Releases

Apply Tests 3 and 4 and identify which releases may need more Detailed Modelling of Emissions/Discharges to Water

This page applies Tests 3, 4a and 4b and displays the Predicted Environmental Concentrations in relation to the backgound pollutant levels and the AA or MAC EQS. Any substances that pass all 3 of these tests can be screened out. Substances failing any of the tests must be modelled. Note that releases that have passed Tests1 and 2 are insignificant are not shown as they are already screened out.

				Annual Avg EQS			_		MAC* E	QS —		
Number	Substance	Bkgrnd Conc. µg/l	PC µg/l	PEC μg/l	(PEC - BC)/ EQS	PEC -BC >10% AA EQS	% PEC of EQS %	PEC >100% AA EQS	PC µg/l	PEC µg/l	% PEC of MAC %	PEC >100% MAC
		μg/1	μдл	µg/1		Test 3	70	Test 4a	49/1	μул	70	Test 4b
	Ammonia CaCO3 >50mg/l (90 %ile) (Unnamed tributary of River Little Lugg)	72	42.3	90.9	9.4%	Pass	45.5	Pass	42.3	0	-	Pass
3	Phosphate (Unnamed tributary of River Little Lugg)	76.6	16.3	68.0	-7.2%	Pass	56.7	Pass	16.3	68.0	56.7	Pass

<sup>\*</sup> MAC = Maximum Allowable Concentration

Describe source of background information or reference to relevant documentation here:

### **Water Impact Modelling Assessment**

See guidelines in H1 Annex D and respond to the following

Describe here the justification for whether detailed modelling is, or is not required for any of the releases. Refer to the quidelines in H1 Annex D.

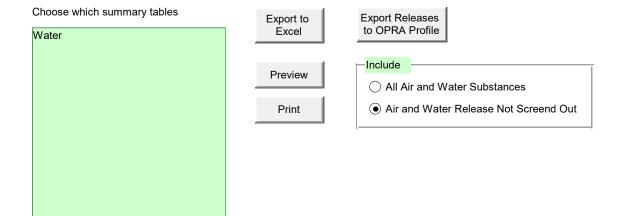
Detailed modelling not requried as none of the process contributions in respect of the determinands modelled due to all substances modelled screening out at Tests 1 or 2 or passing Tests 3, 4a and 4b

Describe source of background information:

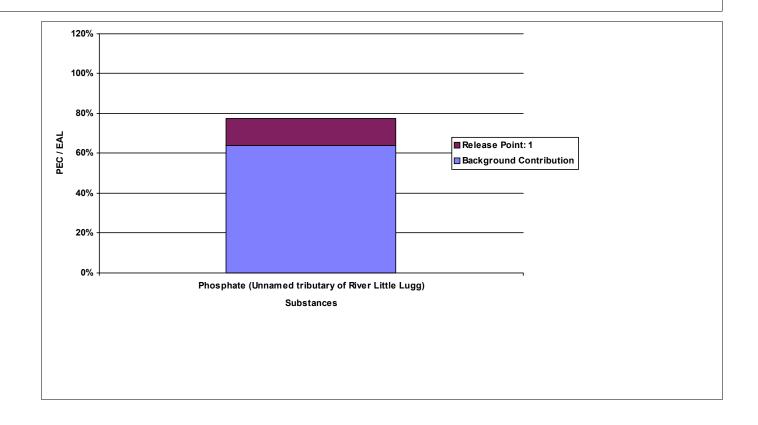
Describe location of detailed modelling work:

N/A N/A

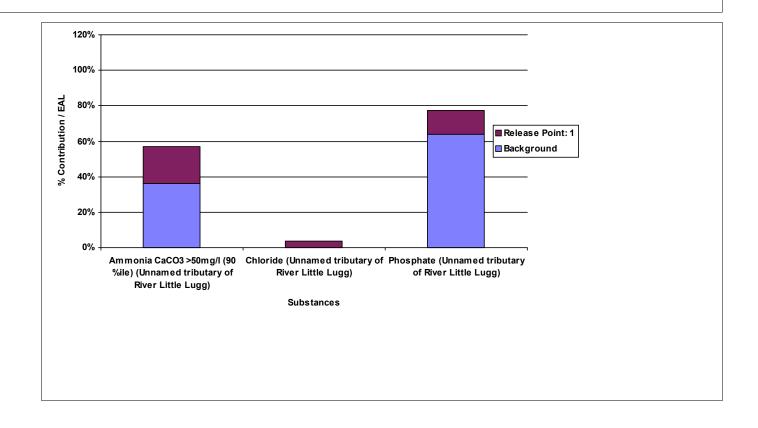
	Summary Tables
Print or Pre	eview summary tables:



### **Short Term Water - Substance Comparison**



### Water Long Term Effects - Comparison by Substance



### **Summary of Environmental Assessment**

You have now completed all of the steps in this software for the environmental assessment. This will provide you with:

- an inventory of all emissions sources and substances emitted from your activities
- an information trail of how the impacts of these emissions have been assessed
- a summary of the impacts

You now need to use this information to confirm whether the emissions are acceptable, i.e. that they do not cause significant pollution to occur, by responding below:

Do any of the emissions exceed any of the following	
Do any of the enhasions exceed any of the following	
	e substances concerned and improvements that are needed to at attacked at a calculation and are needed to at a calculation.
(air and water): investigate whet	e substances concerned, the contribution from the activities and her further detailed fate and effect modelling and/or pollution ded. Ensure that the relevant EQS reference conditions are applied.
	e substances concerned, the contribution from the activities and her further detailed fate and effect modelling and/or pollution controls
Use the box below to provide further information on any of the abo	ve to which you have responded 'Yes':

Finally, print all of the information and submit with your application. Remember to include any supplementary information and reports that you have had made reference to during the assessment procedure.

#### tep 4

### **Compare Impacts between Options**

The aim of this Step is to compare the overall performance of each option for all of the environmental considerations assessed in Step 3, in order to identify which option represents the lowest impact on the environment as a whole.

### **IMPORTANT NOTE**

Unless the best option is self-evident (i.e. results in the lowest impact for all considerations), you will need to use professional judgement to decide which option is the best overall. This judgement should be made taking into account the considerations described in the H1 guidance notes and may require decisions about the relative importance of environmental considerations. The operator should submit a response to the Regulator that describes how the decision has been made. The following page provides a structure which may be used to summarise the decision-making process.

TO CONTINUE WITH STEP 4, PRESS "NEX

	Compare the Options		
Review t	he graphs and summary date to rank the options according to environmental impac	t	
	Is the best Option self-evident? i.e. results in the lowest impact in all environmental considerations	Yes	
	Are you going to implement the option that is self-evidently the best? If yes, no further assessment is necessary and you may end here.	Yes	
	Compare the Options		
Review t	he graphs and summary date to rank the options according to environmental impac	t	
	Is the best Option self-evident? i.e. results in the lowest impact in all environmental considerations	No	

No

Are you going to implement the option that is self-evidently the best? If yes, no further assessment is necessary and you may end here.

### **Resolve Cross Media Conflicts**

<b>Environmental Cons</b>	sideration	Importance	Comments / Justification
Releases to Air	Long Term:		
	Short Term:		
Deposition to Land:			
Releases to Water	Long Term:		
	Short Term:		
Visual:			
POCP:			
GWP:			
Disposal of Waste:			

### Provide a description of how cross media conflicts have been resolved:

This will require reasoned judgement, with reference to any decisions or assumptions made over the relative importance of different environmental impacts. See H1 for requirements, guidelines and examples to assist in the process. You may submit this information

Location or reference to information on resolution of cross media conflicts:

### Present a summary of the final ranking of options in the table below:

Number	Title	Ranking
1	Base-Case	
2	Tankering off site	

### **Resolve Cross Media Conflicts**

**Environmental Consideration** 

Importance

Comments / Justification

Releases to A	ir Long Term:											
	Short Term:											
Deposition to I	Land:											
Releases to W	Vater Long Term:											
	Short Term:											
Visual:												
POCP:												
GWP:												
Provide a des	scription of how cross		ts have been resolved:									
Provide a des This will requir environmental	scription of how cross re reasoned judgement, I impacts. See H1 for re	, with reference to equirements, guid	to any decisions or assum delines and examples to a	otions made over t	he rela s. You	ative ma	impo	ortan nit t	ıce o	<sup>:</sup> differ	ent tion	
Provide a des This will requir environmental	scription of how cross	, with reference to equirements, guid	to any decisions or assum delines and examples to a	otions made over t ssist in the process	he rela s. You	ative ma	impo	ortan	ıce o	<sup>:</sup> differ	ent	
Provide a des This will requir environmental Location or ref	scription of how cross re reasoned judgement, I impacts. See H1 for re ference to information c	, with reference of control of co	to any decisions or assum delines and examples to a cross media conflicts:	otions made over t ssist in the process	he rela s. You	ative ma	impo	ortan	ice o	<sup>:</sup> differ	ent	
Provide a des This will requir environmental Location or ref Present a sur	scription of how cross re reasoned judgement, I impacts. See H1 for re ference to information o	, with reference of control of co	to any decisions or assum delines and examples to a cross media conflicts:	ssist in the process	he rela	ative	impo	ortan mit t	ice o	<sup>:</sup> differ	ent	
This will requirenvironmental Location or ref  Present a sur  Number T	scription of how cross re reasoned judgement, I impacts. See H1 for re ference to information c	, with reference of control of co	to any decisions or assum delines and examples to a cross media conflicts:	otions made over t ssist in the process	he rela	ative ma	impo	ortan nit t	ice o	<sup>:</sup> differ	ent	

### **Summary of Option Appraisal**

You have now completed all of the steps in this software for appraisal of BAT.

Finally, print all of the information and submit with your application. Remember to include any supplementary information and reports that you have had made reference to during the assessment procedure.

## **Appendix V**

## **Phosphate Recovery and Treatment Process**

# STL2 Whitwick AD

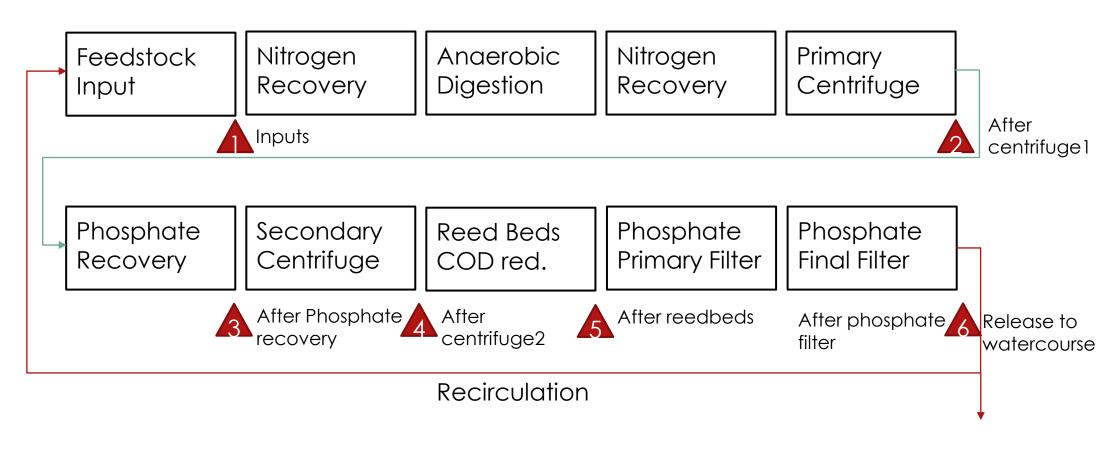
PHOSPHATE RECOVERY AND TREATMENT PROCESS JANUARY 2023

# Phosphate in Agriculture

- Phosphate is one of the three essential plant nutrients ("NPK") used as fertiliser in agriculture
- Poultry manure contains significant quantities of this valuable resource
- ▶ Historically the application of poultry manure to land has resulted in too much Phosphate ( $P_2O_5$ ) being applied relative to the other plant nutrients especially Nitrogen ("N")
- This excess Phosphate has resulted in pollution of watercourses such as the River Wye

**The solution** is to remove Phosphate from poultry manure and transform it into products that can be appropriately and safely used as fertiliser in agriculture.

## STL2 Whitwick Phosphate Recovery Process Flow



Key process analysis points

# 1 – Total Plant Inputs

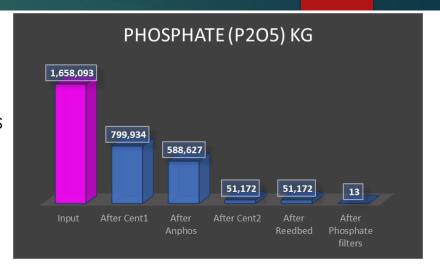
## Total Feedstock Inputs

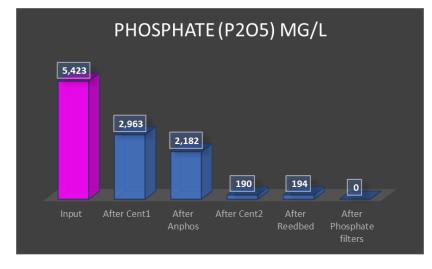
- 100,000 tpa\* Poultry manure delivered by covered truck, stored under cover and fed quickly to plant
- 16,000 tpa Apple pomace transported locally by lorry and stored in clamp; then fed over 12 months to balance feedstock mix. Runoff captured and fed directly into digester
- 25,000 tpa Digestate from Hampton Bishop delivered daily and fed directly into sealed tanks
- 35,000 tpa Liquid waste delivered daily and fed directly into sealed tanks
- 170,000 tpa Recirculated water from end of process avoids water extraction

## Whitwick Process

- The feedstock mix is kept as stable as possible to promote a consistent biological process
- Due to pre-digestion Nitrogen stripping, liquid inputs are reduced by around 100,000 tpa
- Liquid inputs are pumped directly into sealed storage tanks from sealed delivery vehicles
- Solid inputs are fed into feed hoppers and incorporated into the sealed anaerobic (i.e. without air) digestion process
- Total Phosphate Input:

1,658,093 kgs Phosphate per year





<sup>\*</sup> tpa = tonnes per annum

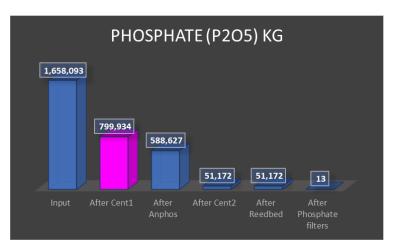
# 2 – Post Digestion and Centrifuge 1

## Typical AD Process

- Most AD plants use a single stage screw separator to remove a small proportion of solids to facilitate spreading of liquids to land
- The solid fraction is typically only 22% dry matter and contains significant soluble Phosphate and is also subject to leaching and runoff during field storage
- Both the solid and liquid including all the Phosphate are then spread to land

- The first Decanter Centrifuge produces a high quality soil improver with dry matter between 40-45%
- Approximately 35,000 tpa of this soil improver captures 830 t of very slow release insoluble, mineral Phosphate
- The balance of Phosphate remaining in the liquid fraction is: 799,934 kgs Phosphate per year





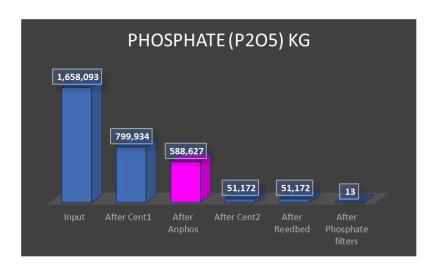
# 3 – Soluble Phosphate Recovery

## Struvite Recovery System

This technology is not usually deployed at AD plants and has been developed primarily for



- Proven Struvite
  recovery technology
  uses Magnesium
  Hydroxide to make
  Struvite (Magnesium
  Ammonium
  Phosphate)
- This process captures
   Ammoniacal Nitrogen
   and 90% of the
   remaining soluble
   Phosphate for use as a
   fertiliser
- Remaining Phosphate: 588,627 kgs Phosphate per year



# 4 – Centrifuge 2

## Centrifuge Stage 2

During trials at STL1\* the second stage centrifuge achieved a significant total Phosphate reduction (the results of the trials showed a 99% capture rate)

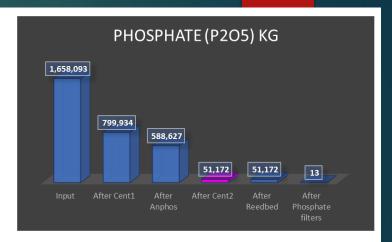


\*STL1 – STL Energy's existing AD plant at Hampton Bishop

## Whitwick Process

- At STL2 this process is split into three steps to optimise Phosphate recovery.
- Centrifuge2 is the third step prior to the reed beds. The design has been based on 95% Phosphate removal whereas in STL1 trials 99% was achieved.
- Approximately 1,300 tpa of solids are produced for use as fertiliser
- Phosphate remaining after Centrifuge2:

51,172 kgs Phosphate per year



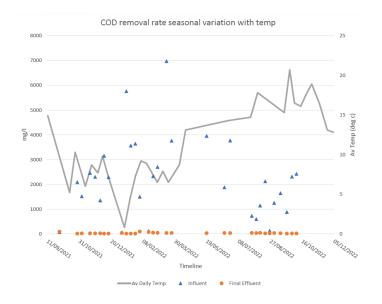
# Further processing of liquid to allow discharge to watercourse

- The intensive Phosphate capture processes will remove in excess of 99% of the Phosphate from the input materials (including poultry manure)
- The remaining liquid stream coming from Centrifuge 2 still contains small concentrations of Phosphate, organic matter, plant nutrients and trace elements
- The remaining processes to treat these consist of:
  - Reed beds to remove organic matter, measured as Chemical Oxygen Demand (COD) potential
  - Phosphate filters in series, after the reed bed to reduce the Phosphate concentration to minimal levels allowing the treated water to be discharged to the watercourse

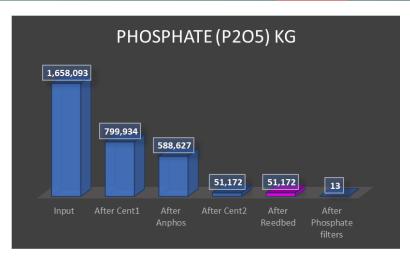
## 5 – Reed Beds COD reduction

## Typical Reed Bed

Reed beds COD\* removal efficiency over the year



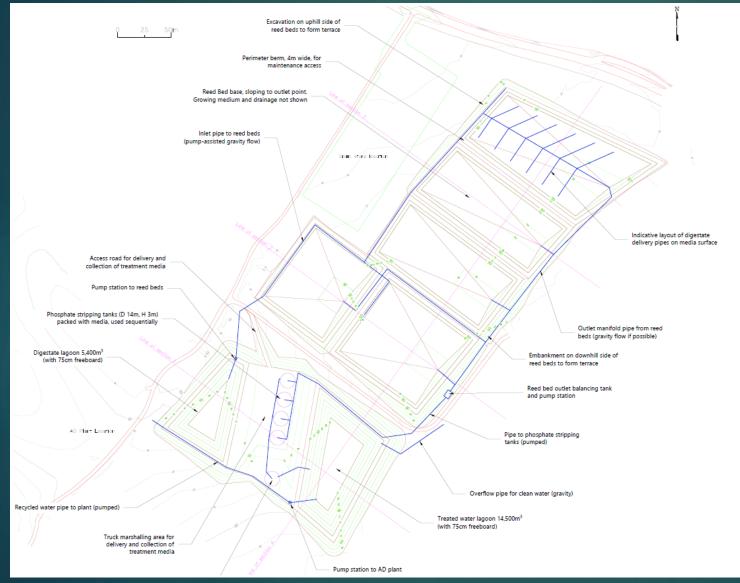
- Nitrogen and Phosphorous recovery and organic solids separation in previous processes minimises the COD loading on the reed beds.
- The reed beds are primarily designed to remove the remaining COD
- Phosphate remaining after the reed bed:
   51,172 kgs Phosphate per year





<sup>\*</sup>COD - Chemical Oxygen Demand

# 5 (cont.) - Reed bed layout



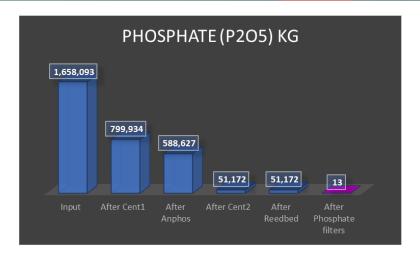
- There are five vertically fed reed beds in parallel to cope with the hydrological water loading.
- This allows for one red bed to be taken out of service in turn, for cleaning or replanting as necessary
- Treatment area is: 3.5 ha
- Phosphate remaining after the reed bed: 51,172 kgs of Phosphate per year

# 6 – Phosphate Filters

## Phosphate Filters

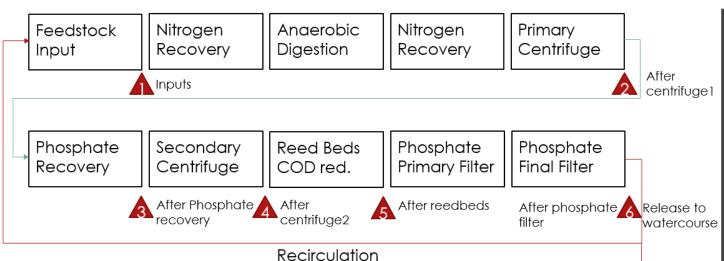
- The filters are a simple upflow adsorption filter with the ability to bypass or add units in series
- The Phosphate levels will be monitored both before and after each unit to detect when the media is becoming saturated
- When a filter becomes saturated it will be bypassed emptied and refilled with new media
- The specific media has been developed and then tested with the Environment Agency

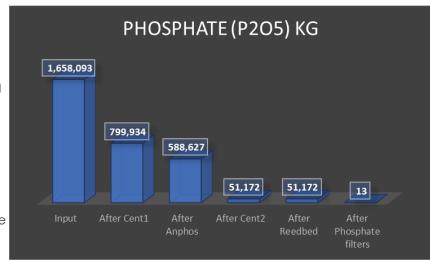
- The system has four main processing filters and a spare, to allow for cleaning and refilling or to provide extra protection if one of the upstream processes is undergoing maintenance
- When saturated, the Phosphate saturated media may be used as a slow release fertiliser
- The STL2 plant design allows for the additional final filter, to have a very low loading
- Phosphate remaining for release to watercourse:
   13 kg of Phosphate per year or <0.05mg(P205)/litre</li>





# Phosphate reduction





- A typical house in the Wye catchment area produces around 0.5 kgs. Phosphate per year or an acre of farmland 0.9 kg per annum.
- The STL2 plant will release less than 4.5 kgs per year of Phosphate to the watercourse, less than the amount of Phosphate produced by 5 hectares of farmland
- The phosphate release to the watercourse will be less than 0.039mg/I of Phosphate the minimum level detected at the nearest River Lugg measuring station

- The balance of Phosphate remaining in the liquid fraction released to the watercourse is:
- <5.5 kg of Phosporous (<13kg Phosphate P205) per year
- The phosphate removed during the whole STL2 process will be in formats suitable for transport and use as fertiliser or for further processing in fertiliser manufacturing plants
- The concentration of Phosphate released to the lagoon will be: <0.05 mg/l of Phosphate where it will be then further diluted by rainwater from the catchment

