Burner Test Report

WOOD Foster Wheeler Energy Ltd. for BOC/Hunstman in Teeside, United Kingdom

P.O. No.: 20105669

Witness Test Date: September 23rd, 2020

Equipment Tested: CUBLF-6W-PSA

Honeywell Callidus UOP Technologies

CallidusTechnologies, LLC

7130 South Lewis, Suite 500 Tulsa, OK 74136-5488 Phone (918) 496-7599

Project: B-9050770

Revision 0

Oct 1st, 2020



This burner witness test was conducted at the UOP Callidus Manufacturing and Testing Facility located at 2499 Highway 16 Beggs, OK 74421-9581 (918) 267-4920

ATTENDEES DURING TESTING

| Peter Holsgrove | WOOD |
|--------------------|-----------|
| Richard Spires | WOOD |
| Shyam Pillalamarri | WOOD |
| James Percy | Linde/BOC |

CALLIDUS TEST FACILITY PERSONNEL

| Name | Title |
|---------------|-----------------|
| James Dickson | Test Engineer |
| Teresa Thomas | Project Manager |

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I. BURNER TEST

A. INSTALLATION

The burner was installed in Test Furnace #3, mounted in the center of the furnace against the firing wall (opposite the tube wall). (Information about Test Furnace #3 can be found in Appendix C)

B. EXECUTIVE SUMMARY

The burner for this project was originally designed and optimized to meet guarantee criteria in accordance with Callidus burner project B-9011196. The burner tested was a field burner delivered from the customer site. No changes to the burner design were made to affect performance.

The purpose of this project was to demonstrate the effects on emissions using a fuel with less inert CO2 in PSA fuel than was used in the original performance test. The agreed to test points performed can be found in the test procedure located in Appendix A. A complete set of all burner parameters captured during testing can be found in Appendix B

C. CONCLUSION

The burner was tested across various site conditions on forced air preheat. The final burner configuration ran stable across all operating points and was optimized to meet all design criteria.

Test point 1 was performed as specified. During testing, it was clarified that emissions for this point could not clearly be compared to the original burner test. The overall heat release for this point is comparable to that of the minimum heat release of the original test. Typically, during burner performance tests, minimum heat release points are performed with air settings remaining set at normal heat release conditions to give a worst-case condition for stability. Because of this, high excess O2 along with a cold firebox provide and a diluted NOx sample and is not corrected for in calculation. Thus, no point from the original test can easily be compared for test point 1.

Test point 2 was performed as indicated and did show a marginal increase in NOx (44.22 mg/Nm² corrected to specified site conditions) emissions compared to that of the original fuel (as expected) but did not exceed the guarantee of 146 mg/Nm³.

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A third test point was requested during testing to demonstrate the effect of higher excess O2 on NOx emissions. Firing rates remained unchanged from test point 2, but draft was increased to bring excess oxygen to approximately 4%. NOx emissions did increase at this point (as expected) to 53.35 mg/Nm^3 (corrected to same site conditions as test point 2) but again, did not exceed the original emissions guarantee.

Noise data was taken at both test points 1 and 2. Both test points measured below the guarantee of 80 dBa. Background noise was not measured nor removed from noise reading due to raw noise readings being below that of the guarantee.

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II. Appendix



A. Test Procedure

| | Honeyw U | vell Call op Tecl | idus hnologie | es | | | BURN | ER TI | EST P | ROCE | DURE | | Rev 1 | | Sheet 1 of 1 |
|-----------|--------------------------------|----------------------|------------------|--------------------------|---------------|-------------|--------------------------|-------------|---------------|-----------------------------|-------------------------------|---------------|--|-----------------|-------------------|
| 7130 S. L | ewis | | | Project Er | aineer | | | | | Date Prepa | red | | | | |
| Tulsa, Ol | | | | Teresa The | • | | | | | September | | | | | |
| | 918) 496-7597 | | Test Engi | | | | | | Test Date | | | | | | |
| Telephor | ne (918) 496-75 | 599 | | James Dic | kson, Godfr | ey Wanyam | а | | r — | September | 24, 2020 | | | | |
| Cust. | WOOD F | oster Wheele | r Energy Li | mited | Burner | CU | BLF-6W-PS | SA | Dwg: | B-90 | 11196 - 301 | Cap. | . Curve: | B-90 | 11196 - 181 / 182 |
| PO no. | | 201056 | | | Job no. | | B-9050770 | | User: | BOC | / Huntsman | n Site: | <u>: </u> | | Teeside, UK |
| | nce Guarante | | | | | | | | | | | | | | |
| | Guarantees: | | | | C: 100 ppn | | se: 80 dBA | | | Delat O | | | T . (40000C | | |
| | s Recording (e recorded at | | sis: For te | St Point 1, C | correct emis | SIONS TO BW | 1 01 890-0 | and 3% di | y OZ; FOF I | est Point 2, | correct emis | SIONS TO BAN | 1 01 1020-0 | and 3% dr | <u>y 02</u> |
| Х | Gas Pressure Gas Temp | | X X | Amb Air Te Comb Air 1 | | X X | DP Across Air Registe | | X X | Barometric Flame Dime | | X CO X NOx | | Box Temp O2% | X Heat Release |
| | (VOL %) | Aux Fuel (NG) | PSA-30% HMU | HMU | | | | | - | | | | | | |
| | Gas | A | B | C | | | | | - | | | | | | |
| | Nat Gas C3H8 | 100 0 | 12 0 | 13 0 | | | | | | | | | | | |
| - | H2 | ů 0 | 65 | 50 | | | | | | | | | | | |
| | CO2 | 0 | 23 | 37 | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | - | | | | | | |
| MIA | 1187 | 47 40 | 10.00 | 11.78 | <u> </u> | | | | | Site Tempera | | | | | |
| MJ/kg | LHV SG | 47.49 0.619 | 19.06 0.470 | 11.78 0.680 | <u> </u> | | | | | | e Available: 2 | :00 kPa(g) | | | |
| <u> </u> | Wobbe | 50.4 | 18.4 | 13.6 | | | | | | Fuel Temper Fuel Pressur | ature: 25°C e Available: 1 | 15 kPa(o) | | | |
| Target | | 50.4 | 18.4 | 13.5 | | | | | | | astal/Sea Le | | e Relative H | lumidity: 909 | % |
| | Aux Heat | PSA Heat | | Comb | | | | • | • | · | | | | | |
| Test | Release | Release | PSA | Comb. Air | O2 vol% | ΔP | | | | | | | | | |
| Point | MW | MW | Fuel | Temp. | dry | mm H2O | | | | Commen | ts | | | | |
| | | | | | | | | | | | | | | | |
| TP1 | 0.338 | 0.351 | В | 130°C | 8.0% | TBD | HMU Oper | ation at 30 | % capacity | · Record No | ise; Emissio | ons Correctio | ons as state | d above | |
| | 0.000 | 0.001 | | 100 0 | 0.070 | | | | , o capacity, | , 11000101110 | | | no do otato | 4 45010 | |
| TP2 | 0.292 | 1.191 | с | 350°C | 1.9% | TBD | | ation at 86 | % canacity | · Record No | ise; Emissio | ons Correctio | ons as state | d above | |
| 112 | 0.232 | 1.131 | | 330 0 | 1.370 | 100 | TIMO Open | | 70 capacity, | | 136, 11113310 | | 113 83 31810 | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | - | - | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| - | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | Sito F | Fuel Det | aile | | | | | | |
| | | E | A | DOA 00 | DOA 00 | | | | 1 | DOA 00 | DOA 00 | | | | |
| | | Fuel (Vol%) | Aux | PSA 30 | PSA 86 | | Fuel | Units | Aux | PSA 30 | PSA 86 | | | | |
| | | CH4 | 85.37% | 16.56% | 16.54% | | LHV | MJ/kg | 46.20 | 18.03 | 11.26 | | | | |
| | | C2H6 | 8.31% | | <u> </u> | | HHV | MJ/kg | 51.11 | 20.44 | 12.60 | | | | |
| | | C3H8 | 2.42% | | <u> </u> | | SG | | 0.656 | 0.544 | 0.779 | | | | |
| | | C4H10 | 0.60% | | | | MW | | 18.93 | 15.70 | 22.47 | | | | |
| | | C5H12 | 0.16% | | | | Wobbe | | 50.4 | 18.4 | 13.5 | | | | |
| | | CO | - | 8.66% | 12.94% | | | | | | | | | | |
| | | CO2 | 2.06% | 20.66% | 34.40% | | | | | | | | | | |
| | | N2 | 1.07% | 1.00% | 0.74% | | | | | | | | | | |
| | | H2 | <u> </u> | 52.02% | 34.58% | | | | | | | | | | |
| | | H2O | | 1.10% | 0.80% | | | | | | | | | | |
| | | TOTAL | 100% | 100% | 100% | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| NOTES: | | | | | | | | | | | | | | | |
| 1) Beggs | Natural Gas co | mposition: 899 | % CH4, 8% | C2H6, 1% | C3H8, 2% N | 12 | | | | | | | | | |
| L | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| Reviewer | /Approved | | | | | Date | | | | Witnesse | d/Approved | | | | Date |
| | | | | | | Date | | | - | | | | | | |
| L | | | | | | | | | | | | | | | |



B. Test Data

| | Honey | well Jop | Calli Tech | idus nnolog | gies | | | | |
|--|---------------------|--|---|--|------------|-----------|---|---|--|
| Client | WOOD FOSTER WHEELER | | Work Ord | der | B-9 | B-9011196 | | | |
| Date | 9/24/2020 | | Furnace | # | F3 | | | | |
| Burner Description | CUBLF-6W-PSA | | | | | | | | |
| Variable Name Test Point # Time | Units | 1 10:09 AM | | | r | | | | |
| | omposition | 10.05 AN | 11.55 AW | 12.05 P M | | I | | | |
| Total Burner Heat Release | MW | 0.64 | 1.48 | 1.49 | | | | | |
| Fuel Gas 1 Name | | В | c | с | | | | | |
| Heating Release - LHV | MW | 0.35 | | | | | | | |
| Heating Value | kj/Nm^3 | 10931 | 9710 | 9738 | | | | | |
| Specific Gravity | ~ | 0.471 | 0.684 | | └── | | | | |
| CO NG | % | 0.00% | 0.00% | 0.00% | <u>├──</u> | | | | |
| NG H2 | % | 65.00% | 49.80% | 50.05% | | | | | |
| СЗН8 | % | 0.00% | | 0.00% | | | | | |
| CO2 | % | 22.97% | 37.24% | 36.98% | | | | | |
| Eval Cap 2 Name | | <u> </u> | | | г <u>г</u> | | | | |
| Fuel Gas 2 Name Heating Release - LHV | MW | A 0.29 | | | | | | | |
| Heating Value | kj/Nm^3 | 35692 | | 35692 | | | | | |
| Specific Gravity | | 0.622 | | 0.622 | | | | | |
| со | % | 0.00% | 0.00% | 0.00% | | | | | |
| NG | % | 100.00% | 100.00% | 100.00% | | | | | |
| H2 | % | 0.00% | 0.00% | 0.00% | | | | | |
| C3H8 CO2 | % | 0.00% | 0.00% | 0.00% | | | | | |
| | | 0.00 / | 0.0070 | 0.0070 | | | | | |
| Pres | ssure | | | | | | | | |
| Fuel Gas 1 Tip Pressure | kPag | 0.124 | | | | | | | |
| Fuel Gas 1 Tip Pressure @ 77°F Fuel Gas 2 Tip Pressure | kPag kPag | 0.128 | | 1.225 | | | | | |
| Fuel Gas 2 Tip Pressure @ 212°F | kPag | 4.610 | | 6.014 | | | | | |
| Airside Pressure Drop | mm W.C. | 3.2 | | | | | | | |
| Airside Pressure Drop Corrected to Site | Conditions mm W.C. | 3.2 | | 10.3 | | | | | |
| Damper Position Temp | erature | wo | wo | WO | | | | | |
| Ambient Air Temperature | C | 26.6 | | | | | | | |
| Combustion Air Temperature | c | 125.0 | | | | | | | |
| Upper Furnace Temperature | <u>с</u> с | 734.1 | | 1026.2 974.1 | ├─── ┼── | | | | |
| Floor Temperature Fuel Gas 1 Temperature | C | 16.4 | | | | | | | |
| Fuel Gas 2 Temperature | <u> </u> | 15.5 | | | | | | | |
| | sions | | | | • | • | · | · | |
| Actual O2 % (Dry) | | 8.05 | 2.01 | 3.92 | | | | | |
| Raw NOx | PPMV | 18.38 | | 25.19 | | | | | |
| NOx @ *** BWT | PPMV | 28.65 | | 24.94 | └── | | | | |
| NOx @ 3% O2 | PPMV | 25.54 | | 26.54 | ├ | | | | |
| NOx @ 3% O2 & *** BWT NOx @ 3% O2 & *** BWT & *** CAT | PPMV PPMV | 39.83 40.03 | | | | | | | |
| NOX @ 5% 02 & BWT & CAT NOx (HHV) @ *** BWT | mg/Nm^3 | 81.64 | | | | | | | |
| NOx (HHV) @ *** BWT & *** CAT | mg/Nm^3 | 82.06 | | | | | | | |
| Raw CO | PPMV | 0.00 | | | | | | | |
| CO Corrected to 3% O2 | PPMV | 0.00 | 0.00 | 0.00 | | | | | |
| Flame Di | mensions | | | | | | | | |
| Flame Height | m. | 1.2192 | 1.524 | 1.524 | | | | | |
| Flame Width | m. | 0.4572 | 0.4572 | 0.4572 | | | | | |
| Notes | | Emission | Emission | Emission | | | | | |
| Damper Position are listed in number of *** BWT and CAT temperature correctio | | Corrections: BWT: 890 ℃ CAT: 130 ℃ | Corrections: BWT: 1020 °C CAT: 350 °C | Corrections: BWT: 1020 °C CAT: 350 °C | | | | | |
| | | Honeywell - | Confidential | | | | | | |

| | Honey | well Jop | Calli Tech | idus nnolog | gies | | | | |
|--|---------------------------------|---|---|---|--------------|----|--|----------|---|
| Client | WOOD FOSTER WHEELER | | B-: | B-9011196 | | | | | |
| Date | 9/24/2020 | | Furnace | # | F3 | F3 | | | |
| Burner Description | CUBLF-6W-PSA | | | | | | | | |
| Variable Name Test Point # Time | Units | 1 10:09 AM | | | | | | | |
| | omposition | 10.09 AW | 11:33 AW | 12.09 PW | | | | | |
| Total Burner Heat Release | MMBtu/hr | 2.20 | 5.06 | 5.08 | | | | | |
| | | | | | | | | | |
| Fuel Gas 1 Name Heating Release - LHV | MMBtu/hr | B 1.20 | | C 4.07 | | | | | |
| Heating Value | Btu/SCF | 293.4 | | 4.07 261.4 | <u> </u> | | | | |
| Specific Gravity | | 0.471 | | 0.681 | | | | | |
| со | % | 0.00% | 0.00% | 0.00% | | | | | |
| NG | % | 12.04% | 12.96% | 12.97% | | | | | |
| H2 | % | 65.00% | 49.80% | 50.05% | └── | | | | |
| C3H8 | % | 0.00% | | 0.00% | ├ | | | | |
| CO2 | % | 22.97% | 37.24% | 36.98% | | | | | |
| Fuel Gas 2 Name | | A | A | A | | | | | |
| Heating Release - LHV | MMBtu/hr | 1.00 | | | | | | 1 | |
| Heating Value | Btu/SCF | 958.0 | | 958.0 | | | | 1 | 1 |
| Specific Gravity | | 0.622 | 0.622 | 0.622 | | | | | |
| со | % | 0.00% | 0.00% | 0.00% | | | | | |
| NG | % | 100.00% | 100.00% | 100.00% | | | | | |
| H2 | % | 0.00% | 0.00% | 0.00% | | | | | |
| C3H8 CO2 | % | 0.00% | 0.00% | 0.00% | | | | | |
| | | 0.00% | 0.00% | 0.00% | | | | | |
| Pres | ssure | | | | | | | | |
| Fuel Gas 1 Tip Pressure | Psig | 0.018 | 0.2 | 0.2 | | | | | |
| Fuel Gas 1 Tip Pressure @ 77°F | Psig | 0.019 | | 0.2 | | | | | |
| Fuel Gas 2 Tip Pressure | Psig | 0.5 | | | | | | | |
| Fuel Gas 2 Tip Pressure @ 212°F | Psig | 0.7 | | | | | | | |
| Airside Pressure Drop Airside Pressure Drop Corrected to Site | in. W.C. Conditions in. W.C. | 0.13 | | 0.41 | | | | | |
| Damper Position | | 0.13 WO | | | | | | | |
| Temp | erature | | | | II | | | 1 | I |
| Ambient Air Temperature | F F | 79.9 | | 87.7 669.6 | ├───┼── | | | | |
| Combustion Air Temperature Upper Furnace Temperature | F F | 1353.4 | | | ├ | | | | |
| Floor Temperature | F F | 1353.4 | | 1879.2 | <u>├───</u> | | | | |
| Fuel Gas 1 Temperature | F | 61.6 | | 100.4 | | | | 1 | |
| Fuel Gas 2 Temperature | F | 59.8 | | | | | | | |
| | sions | | | | | | | | |
| Actual O2 % (Dry) | | 8.05 | | 3.92 | ├ | | | <u> </u> | |
| Raw NOx NOx @ *** BWT | PPMV PPMV | 18.38 | | 25.19 24.94 | ├───┼── | | | | |
| NOX @ ³ BW I NOX @ 3% O2 | PPMV PPMV | 28.65 | | 24.94 26.54 | ├ | | | | |
| NOX @ 3% 02 NOX @ 3% 02 & *** BWT | PPMV | 39.83 | | | | | | | |
| NOx @ 3% O2 & *** BWT & *** CAT | PPMV | 40.03 | | | i i | | | | |
| NOx (HHV) @ *** BWT | lb/MMBtu | 0.0600 | | | | | | | |
| NOx (HHV) @ *** BWT & *** CAT | lb/MMBtu | 0.0603 | | | | | | | |
| Raw CO | PPMV | 0.00 | | | | | | | |
| CO Corrected to 3% O2 | PPMV | 0.00 | 0.00 | 0.00 | | | | l | L |
| Flame Di | mensions | 1 | | | | | | | |
| Flame Height | ft. | 4 | 5 | 5 | | T | | | |
| Flame Width | ft. | 1.5 | | 1.5 | i i | | | | |
| Notes | | Emission | Emission | Emission | | | | | |
| Damper Position are listed in number of *** BWT and CAT temperature correctio | | Corrections: BWT: 1634 °F CAT: 266 °F | Corrections: BWT: 1868 ℉ CAT: 662 ℉ | Corrections: BWT: 1868 ℉ CAT: 662 ℉ | | | | | |
| | | Honeywell - | Confidential | | | | | | |



C. Noise Data

Honeywell UOP Callidus Technologies

| J T T | Burner Type: Job Number: Time: Test Pt: Fuel: | 10:09 AM | CUBLF-6 | | | | | Testedler | 1 | |
|-------------|---|------------|-----------|--------------|----------|---|-----------|----------------|-------|--------------|
| T | Time: Test Pt: | | | 70 | | | | Talata di buru | 1 | |
| Т | Test Pt: | | | | | | | Tested by: | James | s Dickson |
| Т | Test Pt: | | | | | | | | | |
| | - | | - | Time: | 11:33 AM | | | | A | Fuel Blend % |
| F | Fuel: | TP1 | <u>.</u> | Test Pt: | TP2 | | | | N.G. | 100 |
| | - | A/B | - | Fuel: | A/C | | | | | |
| | | | | | | | | | | |
| Scale , | / Frequency | | Sca | le / Frequen | су | | | | | |
| F | A Scale | 77.4 | dBa | A Scale | 78.8 dBa | | | | | |
| | 31.5 | 36.5 | dB | 31.5 | 36.4 dB | | | | в | Fuel Blend % |
| | 63 | 44.2 | dB | 63 | 45.6 dB | | | | N.G. | 12_ |
| | 125 | 49.3 | dB | 125 | 49.9 dB | | | | H2 | 65 |
| | 250 | 54.3 | dB | 250 | 56.5 dB | | | | CO2 | 23_ |
| | 500 | 60.1 | dB | 500 | 59.7 dB | | | | | |
| | 1000 | 62.3 | dB | 1000 | 63.5 dB | | | | | |
| | 2000 | 66.7 | dB | 2000 | 67.6 dB | | | | с | Fuel Blend % |
| | 4000 | 76.3 | dB | 4000 | 77.9 dB | | | | N.G. | 13_ |
| | 8000 | 65.3 | dB | 8000 | 66.1 dB | | | | H2 | 50 |
| | 16000 | 57.9 | dB | 16000 | 57.8 dB | | | | CO2 | 37_ |
| | | | | | | | | | | |
| Meter: | : | Quest Tec | hnologies | , SoundPro | SE/DL | | | | | |
| Notes: | : | | | | | | | | | |
| - | | | | | | | - | | | |
| | | | | | | | | Burner | | |
| Muffle | Type: | None, Flat | t, Shoebo | ox, Snorkel | | А | D | amper | Е | |
| Distan | ice From Burr | ner Openin | g | 3 Feet | | В | E | C |) | |



D. Test Equipment

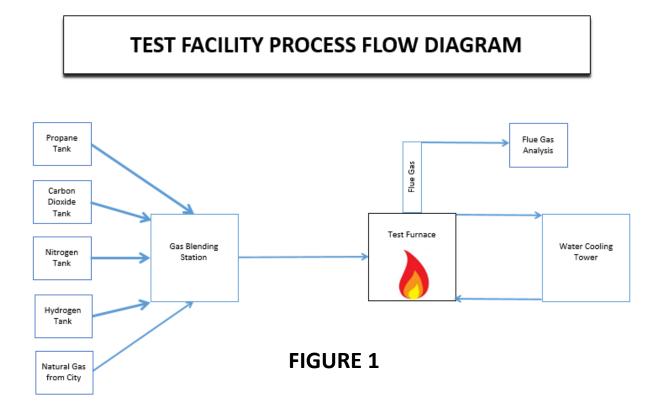


A. Test System Configuration

The general layout for any test includes test fuel gas storage, test fuel gas blending station, a furnace, a cooling water circulation system, and a flue gas sample system.

Test Fuel gas is blended to adequately simulate site fuel gas by metering and measuring each component gas, mixing in a fuel header and delivering to the test burner. Each test fuel gas is calculated to simulate as best as possible the site fuel gas using wobbe number, heating value, and specific gravity. The burner is mounted in the most appropriate test furnace as close to the field mounting configuration as possible with regards to overall burner duty or combined burner duty. Water is circulated through process tubes in the furnace to remove heat. The temperature of the furnace is controlled as close to the design temperature as possible through insulation of the cooling tubes.

Various pressure, temperature, and differential pressure transmitters are placed in this system for measurement of all critical parameters. A vacuum pump draws a sample of the flue gas at the exit of the radiant section and delivers the sample to gas analyzers located in the Central Control Room (CCR.)

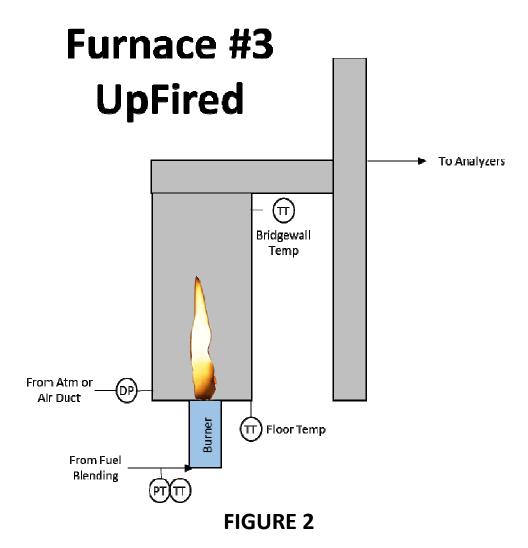




B. Test Furnace

Furnace 3: The test furnace itself is rectangular in section, measuring 6 ft. each side with an overall height of 22.5 ft. inside. Test burner is mounted in the center of the floor of the furnace firing upwards. The furnace is equipped with a 2' I.D. stack with an overall height of 50 ft. above the floor. Cooling tubes are located adjacent to one wall to simulate process tubes in a fired heater. Refractory covers the interior surfaces. Ceramic fiber is used on the walls and castable refractory covers the floor, roof, and stack. A draft connection is located at the floor and in the combustion air duct (if present for forced air applications). A temperature connection is provided at the top of the radiant section.

A suction pyrometer is located near the exit of the radiant section. A Flue Gas Sample Port is located just after the exit of the radiant section. Note: there is no convection section on this furnace. The draft across the burner is measured via a differential pressure. The downstream pressure tap is located at the roof of the furnace. The upstream pressure tap is located at the roof of the burner for forced draft applications, or is open to atmosphere in natural draft applications. See FIGURE 2 for Furnace Layout



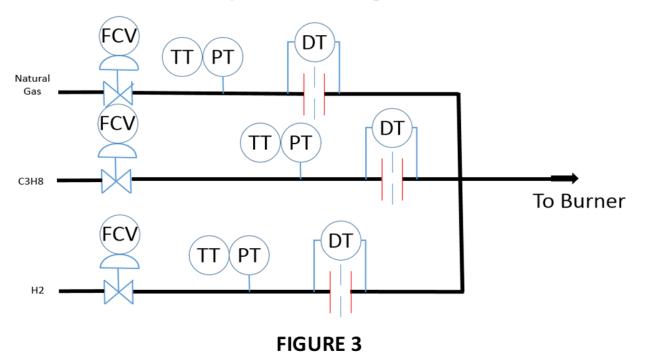


C. Instrumentation

Each component of the test fuel is controlled by automated flow control valves and measured by the use of an individual orifice run, which conforms to American Gas Association (AGA) specifications. Orifice plates are selected to provide accurate ranges of flow. Fuel temperature, orifice differential pressure and operating pressures are transmitted to the Honeywell Distributed Control System (DCS) which calculates individual component flow rate, specific gravity, and heating value. These values are totaled up and recorded to define the overall characteristics of the Test Fuel Blend. **See FIGURE 3**

A Suction Pyrometer, mounted at the end of the radiant section, measures the temperature of the radiant section / bridgewall temperature. Honeywell Wireless pressure, differential pressure, and temperature transmitters monitor furnace draft across the burner, fuel pressure, fuel temperature, and furnace temperature, all of which are transmitted wirelessly to the DCS. **Reference FIGURE 2**

Flame dimensions are ascertained visually and recorded manually unless otherwise stated.



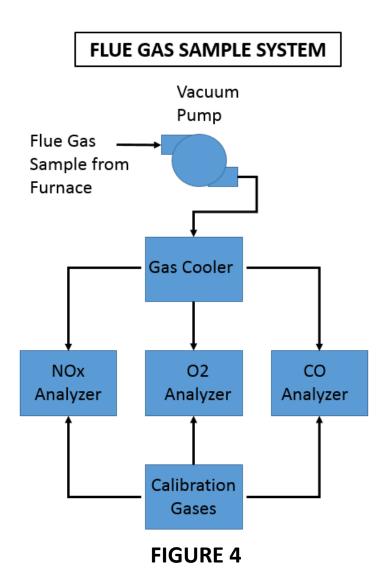
Example Blending Station



D. Flue Gas Sampling

Flue gas samples are drawn from the end of the radiant section through a heated stainless steel line by the use of a Vacuum Diaphragm Pump. Water is removed from the sample gas via a Thermoelectric Gas Cooler of make and model common in refinery CEMS, then delivered to analyzers for analysis.

 NO_X content is measured using Chemlumonescence detection. Excess Oxygen content is measured using Paramagnetic detection. Carbon Monoxide content is measured using Infrared detection. All of the instruments are calibrated using certified zero and span gases in the operating range of the test facility. Calibration of the meters are done before and after each test, and at any time that there is questionable data. See FIGURE 4





E. Data Acquisition and Reduction

All field instruments and flue gas analyzers transmit to a Honeywell Distributed Control System. These process variable signals are converted from analog to digital then to engineering units in the DCS. All flow calculations are also made by the DCS. The converted and calculated process variables then populate a spreadsheet specifically designed to calculate critical values that cannot be measured directly, such as Fuel Heating Value, Specific Gravity, percentage (%) of total flow for each fuel, etc.

The spreadsheet also calculates corrected values for NO_x and CO based on deviation from design Excess Oxygen, site Furnace Temperature, and site Combustion Air Temperature. Correction for Excess Oxygen is performed using EPA methods. Correction for Furnace Temperature and Combustion Air Temperature are performed using empirical, proprietary curves and equations developed specifically for each type of Callidus burner through extensive testing. These curves are similar to those found in API 535.

Pressure Loss (Draft) across the burner is corrected for deviation from design site elevation (atmospheric pressure), site humidity, and combustion air temperature. Fuel pressure is corrected for deviation from design fuel temperature.

Data is acquired by the system every one (1) second. The DCS provides a ten (10) second rolling average to the spreadsheet. When equilibrium is attained for a particular operating condition, the data is saved.

