

PRIMARY & SECONDARY CONTAINMENT REPORT WITH BUND CAPACITY CALCULATIONS

FOR

**PROPOSED ANAEROBIC DIGESTION PLANT** 

AT

HORSE CLOSE,

ON BEHALF OF



Project ref:		GGP/29384/Horseclose/Bund Calcs	
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#### Appropriately Qualified Person Statement:

This report has been prepared and written by Jeremy Collins BSc (Hons) MCIWEM, Civil Engineer. Who has Over 18 year's industry experience across reinforced concrete, water retaining structures, building & structures, SuDS & Highway design and detailing. In addition, Jeremy has designed and detailed over 30 Anaerobic Digestion plants been fully compliant to CIRIA C736 & EA (BAT) Guidance.

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01	09.07.2024	First Issue	JHC
02	06.12.2024	Construction Issue	JHC
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# 1.0 <u>Brief</u>

GGP Consult has been requested by Acorn Bioenergy Ltd Limited to prepare containment calculations for the proposed Anaerobic Digestion Plant for Horse Close (Courteenhall).

The calculations demonstrate the philosophy behind the bunding of the site and how a tank failure event would be contained within the site boundary.

### 2.0 <u>Description</u>

The proposed bund will contain 3 main digester tanks of similar sizes, and a few smaller "tanks".

A drawing has been provided showing the proposed site layout with tank sizes indicated.

This can be seen in Appendix I.

# 3.0 Design Philosophy

The AD plant shall be bunded with a reinforced concrete wall, a full internal concrete slab and underlay with a HDPE membrane.

The report design approach will be determining if the proposed designed wall height of 121.800m AOD (Concrete Bunds) & 122.800m AOD (Earth Bunds) will provide sufficient containment volume in line with thew requirements set out in CIRIA C736.

All tanks shall operate with a "high" alarm and max fill overflow pipes. Therefore, it is technically impossible for these tanks to be overfilled. These levels can therefore be adopted in accordance with *CIRA C736, Section 4.3.2. "However, where the tank is fitted with a physical overflow, the capacity at which the tank would overflow may be taken."* 

Max fill capacity levels will be taken for all tank and not operational levels. This will be referred to as "fill level" within this report.

Further design points are the 10% margin has been interpreted by industry and regulators to cover a range of factors including,

- Prevention of overtopping of the bund in the event of a surge of liquid caused by catastrophic failure of the primary tank.
- Prevention of overtopping, which may be caused by wind-induced wave action during the time that the bund is full, following a failure of a primary tank.
- An allowance for firefighting agents, including a foam blanket on the surface or firefighting water.
- Protection against overfilling.
- An allowance for rain that might collect in the bund and reduce its net capacity, or for rain that might fall in coincident with, or immediately following, the failure of the primary containment.

Based on the above, providing the bund can contain the 110%, no further action is required to justify an increase wall height of any of the above points.

However, for the purpose of this report a quantitative assessment of these assumptions will be provided in section 9.0.

As part of the quantitative assessment, the 100% volume will always be taken and compared against.

#### Design Standards:

The bund capacity will be calculated in line with CIRA C736, Section 4.2.1

"Where two or more tanks are installed within the same bund, the recommended capacity of the bund is the greater of:"



- 1. 110% of the capacity of the largest tank within the bund.
- **2.** 25% of the total capacity of all the tanks within the bund, except where tanks are hydraulically linked in which case they should be treated as if they were a single tank.



# 4.0 Bund Capacity

4.2

# 4.1 <u>110% of the largest Tank Capacity</u>

The largest proposed tank is one of the digester tanks at 45m Diameter with a wall height of 9.0m. The tank will have an available fill height of 8.5m.

Inner Tank Volume (26m DIA x 8.5m High) =	= 4,512m <sup>3</sup>
Outer Tank Volume (45m DIA x 8.5m High) – (Inner +	- Wall) = 9,000m <sup>3</sup>
Total Volumes	
Inner Ring	= 4,512m <sup>3</sup>
Outer Ring	= 9,000.00m <sup>3</sup>
Tank Volume	= 13,512.00m <sup>3</sup>
110% Volume	= 14,863.20m³
25% of Total Tank Capacity	
For all tank capacities see appendix 1.	

Digester 1 Inner	= 4,512.00m <sup>3</sup>	x 1No.	= 4,512.00m <sup>3</sup>
Digester 1 Outer	= 9,000.00m <sup>3</sup>	x 1No.	= 9,000.00m <sup>3</sup>
Digester 2 Inner	= 4,512.00m <sup>3</sup>	x 1No.	= 4,512.00m <sup>3</sup>
Digester 2 Outer	= 9,000.00m <sup>3</sup>	x 1No.	= 9,900.00m <sup>3</sup>
Tertiary Digester	= 7,444.00m <sup>3</sup>	x 1No.	= 7,444.00m <sup>3</sup>
Pasteurisation Tank	= 25.00m <sup>3</sup>	x 3No.	= 75.00.00m <sup>3</sup>
Dirty Water Tank 1 - 2	= 402.00m <sup>3</sup>	x 2No.	= 804.00m <sup>3</sup>
Digestate Buffer Tank	= 402.00m <sup>3</sup>	x 1No.	= 402.00m <sup>3</sup>
Liquid Feed Tank 1	= 402.00m <sup>3</sup>	x 1No.	= 402.00m <sup>3</sup>
Total tank Volume			= 36,151.00m <sup>3</sup>
25% Volume			= 9,037.75m³ < 110%

THEREFORE 110% CAPACITY WILL BE USED FOR THE BUND VOLUME



# 5.0 Available Bund Volume – Design Stage

A detail assessment of the bund proposed levels has been undertaken. A 2D/3D model has been generated to provide an accurate available volume within the bund. See appendix II.



The model has taken the proposed internal bund levels and excluded all tanks / equipment within the bund up to the design retaining wall level.

From the model an available liquid volume within the bund has been calculates to be 17,010.00m<sup>3</sup>.

The proposed bund capacity requirements have confirmed that the 110% volumes shall be taken as concluded in section 4.0.

#### The final available liquid volume within the bund for the 110% scenario will be 17,010.00m<sup>3</sup>

It has therefore been demonstrated that the available bund volume based on a top of wall height no less than 121.800m AOD provides more than sufficient volume to contain the 110% volume.



# 6.0 Quantitative Assessment for the 10% Arbitrary Allowance

In accordance with the CIRA C736, guidance, the following section shall review the 10% increase.

The largest tank capacity based on max fill level equates to.

#### 14,863.20m<sup>3</sup>

Based on the detailed assessment undertaken using a 2D model, an available volume equates to

#### 17,010.00m<sup>3</sup>

Rainfall shall now be considered.

### 6.1 Rainfall Allowance

At the time of a failure, it can be assumed that the drainage system will be empty providing an allowance is made for rainfall equal to a 1:10 year return period 24hr duration before & 8 days' duration after a failure event (*CIRA C736, Section 4.3.3, page 43 & 44*).

For a first estimate fig 4.2 average rainfall depths (from HR Wallingford, 1986) shall be used.

Based on the below table (see following page), a total rainfall depth of 97mm (32mm + 64mm) should be accounted for.

32mm of rainfall occurred across the site dirty water area 24hr before a failure event, equating to 418.00m<sup>3</sup> (13,057x0.032=418.00).

Based on the above the bund will have sufficient capacity to contain the first 41mm.

14,863.20m<sup>3</sup> + 418m<sup>3</sup> = 15,281.20m<sup>3</sup> < 17,010.00m<sup>3</sup> - **PASS** 

Now to consider 8 days of rainfall be 64mm.

64mm of rainfall occurred across the site dirty water area 8 days after a failure event, equating to 836m<sup>3</sup> (13,057x0.064=836).

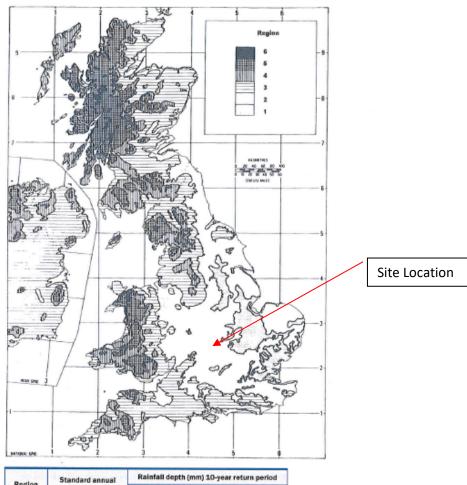
Based on the above the containment will have sufficient capacity to contain the first 32mm plus the additional 64mm.

14,863.20m<sup>3</sup> + 418m<sup>3</sup> + 836m<sup>3</sup> = 16,117.20m<sup>3</sup> < 17,010m<sup>3</sup> - PASS

It can now be concluded that the bund will have sufficient capacity to contain a failure event including rainfall.

Freeboard & dynamic effects shall now be considered.





Region	Standard annual	Rainfall depth (mm) 10-year return period		
Region	average rainfall (mm)	24-hr duration	8-day duration	
1	<600	29	54	
2	600-800	32	65	
3	800-1200	41	95	
4	1200-1600	52	120	
5	1600-3200	88	231	
8	3200	105	288	

Notes

It should be stressed that Figure 4.2 should only be used to derive a first estimate for considering containment This is for two reasons:

 The figure is based on Flood studies report (Institute of Hydrology, 1975) deta produced up to 1986.
 Climate change effects since the publication of HR Wallingford (1986) will have resulted in different annual rainfall figures. De

ailed design should therefore be based on the output of the FEH rainfall.

Figure 4.2 Average rainfall depths (from HR Wallingford, 1986)

Based on the above table at total rainfall depth of 97mm (65mm + 32mm) should be added to the bund wall height.



# 6.2 Freeboard & Dynamic Effects

An allowance for freeboard in bund and dynamic effects should be added to the final bund height required for the worse case failure i.e. 110%.

#### Freeboard / Firefighting Foam

The tank contents are not of a flammable nature and therefore the allowance for firefighting foam is not considered necessary for this development.

### Surge

CIRA C736, Section 4.4, page 53 & 54. fig 4.7.

### Table 4.7 Surge allowance (in the absence of detailed analysis)

Type of structure (see Part 3)	Allowance
In situ reinforced concrete and blockwork bunds	250 mm
Secondary containment tanks	250 mm
Earthwork bunds	750 mm

Based on the above table at total surge allowance of 250mm should be added to the reinforced concrete bund wall height along the north, east, south containment elevations.

To the west are part of the south containment, the walls are made up of earth retaining, which shall adopt the higher surge requirements of 750mm.

As the lowest containment level is located within the reinforced concrete section 250mm will be considered.

Surge shall be considered at the time of failure.

The available bund volume at time of failure will be 17,010.00m<sup>3</sup>.

100% volume = 13,512m<sup>3</sup>.

13,512.00 LESS 17,010 = 3,498m<sup>3</sup>.

Wall available surge height = 3,498 / area (13,057) = 0.267m

Therefore, based on the above and the proposed wall height of 121.800m AOD will comply with the surge allowance required set out in table 4.7 above.

# 7.0 Jetting Failure

The failure of a storage tank through a rupture or corrosion of the side wall, could result in the escape of a jet of liquid. This is referred to as jetting.

The risk of jetting cannot be designed out, however maintenance of the tank through internal inspections can assess the condition of the tank. However, this is not always practical or feasible.

Additional protection measures have been included by all tanks being covered in insulation & cladding. The cladding system will add a secondary protection measure to jetting failures, with the likely event forcing AD material to run down the internal face of the cladding panels.

This is considered as an acceptable protection measure.



# 8.0 Design Summary

- 110% of the largest tank volume has demonstrated to be the worst-case design option when compared against 25% of the all the tanks.
- Analysis of the proposed structural slab levels has demonstrated an available volume equal to 17,010m<sup>3</sup> based on the proposed minimum wall level of 121.800m AOD & earth bund level of 122.800m AOD
- Surge allowance of 250mm has been incorporated within the as- built minimum wall level in accordance with the CIRIA guidance.
- The design level of 121.800m AOD (Concrete Bund) & 122.800m AOD (Earth Bund) has been demonstrated to provide additional capacity to the requirement containment volume. The wall height shall be review and refined during the detail design phase of the project.



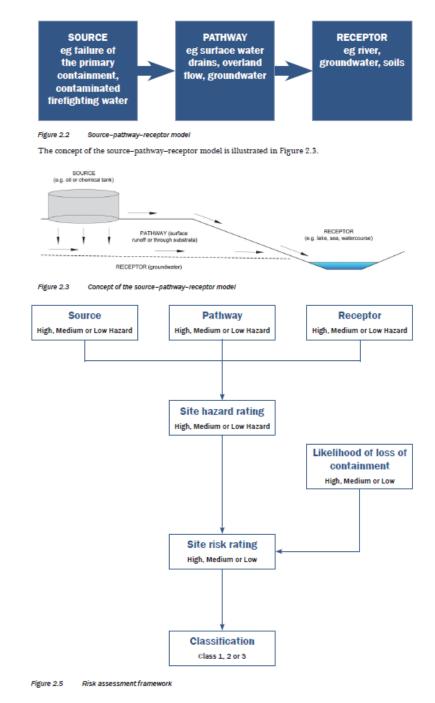
### 9.0 <u>Site Classification</u>

The following section shall follow the risk assessment methodology set out within CIRIA C736.

This will be done as a three-tier risk-based classification system for secondary and tertiary containment.

The outcome of this will provide a standard of construction, or level of performance in accordance with each of the three levels of risk.

The following diagrams set out the methodology of the risk assessment to determining the Classification.





### 9.1 <u>Source</u>

The source material is energy crops and digestate. This is an organic rich material.

The material is classified as non-hazardous.

Given the above, it has been deemed the material shall be classified with a **LOW** environmental hazard rating.

#### 9.2 Pathway

The following pathways shall be considered, as part of these pathways the main receptors location in relation to the site shall also be considered.

- 1. Overland flows.
- 2. Existing sewers.
- 3. Ground Conditions
- 4. Below Ground Pipework
- 5. Watercourse

### 9.2.1 Overland Flows

The tank farm benefits from a perimeter bund, made of reinforced concrete walls, which shall been construction in accordance with CIRIA C736.

The internal area has a mixed surface finish of hard and gravel soft finishes. The bund has a full HDPE membrane located under the internal surface lapped into the external bund, providing a full water retaining containment cell.

Overground flow will therefore be contained within the confines for the perimeter bund.

Surge has been considered as part of the bund calculations with compliance with the requirements set out in the CIRIA guidance.

#### The risk from overland flows is therefore considered LOW

#### 9.2.2 Existing Sewers

The site has no existing sewer connection.

No local sewers are present on the site or the surrounding area.

#### The risk from sewers is therefore considered LOW

#### 9.2.3 Ground Conditions

Infiltration test have been carried out at formation of the earthworks package demonstrating no infiltration within the clayey strata.

Ground improvement layers has then been placed above the strata with a minimum thickness of 0.6m up to 2.0m. This improvement ground has been stabilised using cement providing an impermeable manmade strata above the existing impermeable clay.

Both strata will provide an adequate protection to any potential ground pathway.

It shall be considered, the risk to the ground water shall be taken as Low.

#### Therefore, the risk of ground contamination is considered LOW.



# 9.2.4 Below Ground Pipework

The existing strata along with the ground improvement strata shall provided to layers of impermeable strata with the additional of a HDPE membrane.

Any below ground pipework within the containment area shall be placed above the HDPE membrane.

All process pipework shall be placed above ground with only drainage pipes below ground. These shall be CCTV's before use and air tested.

#### Therefore, the risk of ground contamination is considered LOW

#### 9.2.5 <u>Watercourse</u>

The site is bond by a watercourse to the North, with the site been elevated means a potential overground flow pathway to the watercourse.

The site shall have primary and secondary containment systems designed to be compliant with CIRIA C736, taking into account rainfall, surge and freeboard.

Secondary containment shall consist of reinforced concrete wall to the perimeter of the tanks, constructed to water retaining standards. During the construction phase a Construction Quality Control procedures shall be carried out by the contractor and a Civil Engineer to ensure the construction works follow and comply with the design drawings.

Failure of the primary & secondary containment is not considered likely.

#### Therefore, the risk to the watercourse is considered LOW / MEDIUM.

#### 9.2.6 Pathway Risk Consideration

From the above the pathways is deemed to be Medium risk. these do however relay on the integrity of the perimeter bund & hardstanding.

#### 9.3 Receptor

The receptors are;

1. Watercourse

The watercourse is environmentally sensitive and located downhill in a flow path of containment bund.

The site shall be constructed with a concrete hardstanding, reinforced concrete bunding all compliant to CIRICA C736, this secondary containment system will from a second line of defence.

Based on an unlikely failure event the risk shall be considered as High, however in normal operation the site is considered to be low risk to the receptors.

It can therefore be concluded for this particular event, the risk to the receptor shall be considered medium taking a conservative approach between the two events.

In the event of an unlikely failure event the tank & the bunding. The watercourse would become engulfed with contaminated material.

Given its unlikely event, it is not recommended that further actions are taken to help / protect against such events. However, it is noted that an HDPE membrane has been included under the full containment bund plan area which will offer a third level of containment. Would normally be considered for this reason.

It is therefore essential that the bund integrity forms a vital part of the plant maintenance and inspection schedule, with all reported defects responded to as a matter of the highest importance.

#### Therefore, after reviewing all the receptors, an overall risk has been concluded as HIGH.



## 9.4 Site Hazard Rating

The site hazard rating shall be assessed using the below table from CIRIA C736, with the following ratings, derived as above.

- 1. Source Low
- 2. Pathway High
- 3. Receptor High

Box 2.1 Suggested combinations of hazard ratings to give overall site hazard rating

Environmental hazard ratings H = High rating		
M = Moderate rating L = Low rating		
Source	Pathway	Receptor
(hazard rating)	(transport potential)	(damage potential)
May be H, M or L	May be H, <mark>M</mark> pr L	May be H M or L
Possible combination of ratings:		Suggested consequent overall site
HHH or HHM or HMM		hazard rating:
HHL or MMM or HML		HIGH
MML or HLL or MILL or LLL		LOW

Therefore, an overall site hazard rating has been considered and concluded as MODERATE.

# 9.5 Site Risk Rating

The site risk rating considers the site hazard rating and the risk of loss of containment.

The site hazard rating has been deemed moderate.

The risk of loss of containment shall now be considered and this is done by using the below table.

Table 2.3 Frequency of loss of containment

Risk of loss of containment	Annual probability of loss of containment per site	
High	Greater than 1% (1 in 100)	
Medium	Between 1% (1 in 100) and 0.001% (1 in 1 million)	
Low	Less than 0.001% (1 in 1 million)	

The following simple table has been formulated considering events and their probability in relation to the above table from CIRIA C736

	High	Medium	Low
Small Spills	Х		
Pump failure	Х		
Pipe Failure		Х	
Localised Flooding		Х	



Site-wide Fires	X
Whole vessel failure	X
Major flooding	X
Vandalism	X
Subsidence	X
Terrorism	X
Plane Crash	X
Earthquake	X

From the above table it has been concluded a likely risk of loss of containment shall be taken as medium to be conservative.

These two risks shall now be put into the following table to conclude a Site Risk Rating.

Box 2.2 Overall site risk rating as defined by combining ratings of site hazard and probability of containment failure

Site hazard ratings May be high (H), moderate (M) or low (L) (see Box 2.1)		
Frequency of loss of containment May be high (H), moderate (M) or low (L)		
Possible combination of ratings: Suggested consequent overall site hazard rating:		
HH or HM or MH	нідн	
MM or HL or LH	MODERATE	
LL or ML or LM	LOW	

Therefore, an overall site risk rating has been considered and concluded as MODERATE.



# 9.6 <u>Classification Conclusion</u>

The CIRIA guidance sets out that there is no direct quantifiable link between the site hazard or site risk and the design of the containment system. The following simple relationship is considered appropriate in most circumstances:

- low overall site risk containment type class 1, ie base level of integrity
- moderate overall site risk containment type class 2, ie intermediate degree of integrity
- high overall site risk containment type class 3, ie highest degree of integrity.

Therefore, an overall site classification has been considered and found to be moderate, with an overall site risk containment type requirement of class 2, i.e. providing an intermediate degree of integrity.

#### 9.7 Key Performance Recommendation by Class

The site risk assessment has concluded an overall site hazard rating as being MODERATE. Class 2 containment would be required.

Therefore, the following Table 6.5, will be used to assess the as-built containment.

Recommendation		Containment class		
		Class 2	Class 2	Class 3
а	Provide not less than 750 mm clearance between primary tank and bund walls for maintenance access.	Desirable	Recommended	Recommended
ь	System to detect leakage from primary tank in situations where not practicable to provide clearance between base of tank and bund.	Desirable	Desirable	Recommended
с	No structure within bund to be closer than its own height to the bund wall.	Not necessary	Desirable	Recommended
d	Pumps*, valves, couplings, delivery nozzles and other items associated with the operation of a primary container to be located inside the bund or within a separately bunded area.	Desirable	Recommended	Recommended
e	Penetrations of the bund wall to be avoided.	Desirable	Recommended	Recommended
f	No provision for rainwater draw-off via a valved outlet in bund wall.	Desirable	Recommended	Recommended
g	Take account of possible jetting failure.	Desirable	Recommended	Recommended
h	Take account of surge effects.	Desirable	Desirable	Recommended



- a. A minimum 750mm clearance has been provided between all tanks and the bund wall for maintenance. Achieved
- b. The main tanks do not have any leak detection system where the tank bases are below the bund. All tank are above the containment system or a HDPE membrane has been placed below the tank.
- Not all the tanks are beyond their own height to the bund wall. One of the three digester tanks is located 1.5m away from the bund wall, with the tank heights been 9.0m. This requirement is a desirable recommendation which has been complied with in three directions. Bund wall heights have achieved the required surge effects. Therefore, the design has considered this requirement.
   Achieved
- d. Below ground transfer pipes between the primary container are located below the bund slab. These are construction in MDPE. Achieved, all pipework shall be placed above ground
- e. There are no penetrations of the bund walls. Achieved
- f. No rainwater draw-off point has been provided. Achieved
- g. Jetting has been considered, with the tank insulation and cladding system offering a line of defence against jetting affect. The maintenance and operation team will be able to monitor loss of volume via the SCADA system. It is also recommended that visual site walkovers are undertaken to look out for wall pooling at the bottom of the tank cladding. **Achieved**
- h. Surge effects have been considered and applied in line with the recommendation set out in the CIRIA guidance in absence of detailed analysis.  **Achieved**

#### 10.0 Bund Construction Design

The following section shall provide a descriptive description of the proposed construction containment system, covering the perimeter, secondary, leak detection and any form of additional containment.

#### **Primary Containment**

The bund shall contain 5 main tanks which are to be constructed by Wolf with insitu concrete wall and a cast insitu slab.

The tanks shall sit slightly below the main containment slab due to the floor falls to aid in drainage to the south / collection pit. Given the tank is located below the bund slab a leak detection system with has been incorporated by Wolf to allow for leak detection of each tank. This system shall be sealed to prevent leaks escaping into the lower HDPE membrane and or liquid flowing into the system from above (rainfall)

See Appendix IV for Wolf details.

#### **Secondary Containment**

#### Perimeter Walls

The containment bund walls have all been designed in accordance with CIRIA C736 at the Environment Agency's Best Available Technic (BAT).

The wall height has been determined based on the provided tank numbers and volumes as outlined within section 4.0 - 8.0.

All vertical & horizontal joints within the bund wall shall have a waterbar cast to the middle of the wall at and both faces to have sealant applied to the full height.

Expansion joints shall be placed at maximum spacing of 18m. A waterbar shall be placed vertically in the wall joint and base.



The Contractor shall construct in accordance with the supplier construction drawing and GGP Consult shall perform a CQA role during the construction phase to ensure compliance.

See Appendix V for GGP Consult details.

#### Bund Floor Slab

The floor slab shall be constructed from a 175mm fibre reinforced concrete slab with a layer of A252 mesh. A specialist fibre contractor has provided a design mix for the fibres which can be see within Appendix V.

The final mix design shall be submitted for review and approval by GGP Consult before accepting any concrete on site.

The bund slab shall form a fully sealed water retaining structure, with all joints between the bund slab, walls & tank bases sealed with a Fosroc or similar approved by GGP Consult.

All joints within the bund slab and intersection with the perimeter retaining wall shall have a waterbar at the bottom and sealant to the top surface.

#### Additional Containment

A 1.0mm HDPE membrane shall be placed below the full bund slab area, with all joints lapped, welded and certified to form a fully sealed liner. This shall provide an enhanced composite secondary containment slab and the ability to perform leak detection on the secondary containment with any failures of the bund slab been trapped between the slab and HDPE membrane allowing for sampling.

See Appendix V for GGP Consult details.

#### Drainage

All drainage within the containment system shall be located above the 1.0mm HDPE membrane, with pipes, channels & chambers to have minimum 175mm concrete surround.

Where the intersection between pours and the bund slab, a Adcor waterstop shall be provided to the liner perimeter.

Drainage channel shall be BSI certified with loading rate of E600, installation shall be strictly in accordance with the manufactures details. All joints shall be sealed through the system.

All manholes shall be BSI kitemarked, D400 lids and double sealed.

Precast concrete chambers shall have a minimum internal diameter of 1200mm and be constructed in accordance with the standard details provided.

Where Precast concrete chambers are used within the defined dirty water system, all chambers are to be internally sealed / lined to ensure sealed rings and prevent deterioration of the concrete.

Plastic chambers shall hold a BSI kitemark certification and shall have a minimum internal diameter of 450mm.

All pipes shall be PVC-U or similar material approved by GGP Consult and all drainage pipes should be sealed, and pressure tested (water & air) prior to completion.

All below ground tanks shall have up & downstream penstock valves fitting to allow isolation of the tank.

The below ground effluent tank shall have a secondary liner under the full extent of the tank, carried up to the surface and sealed. A leak detection point shall be provided between the tank and the liner.

See Appendix VI for GGP Consult details.



### 11.0 Summary and Compliance Statement

It has been demonstrated within the report that the sites containment system has been designed in compliance with the recommendation and guidance set out within CIRIA C736.

The site hazard rating has been concluded as moderate with a minimum requirement of Class 2 containment system required.

The constructed containment system is in compliance with a class 2.

The proposed design bund wall level of 121.800m AOD (Concrete Walls) & 122.800m AOD (Earth Bunds) will contain the 110% volume.

The containment system shall be inspection via a CQA role performed by GGP Consult with a written compliance report confirming the As-Built containment has complied with the design.

The operator shall conform to the proposed maintenance schedule and undertake work immediately.

From GGP CONSULT

Report Checked by:-

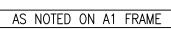
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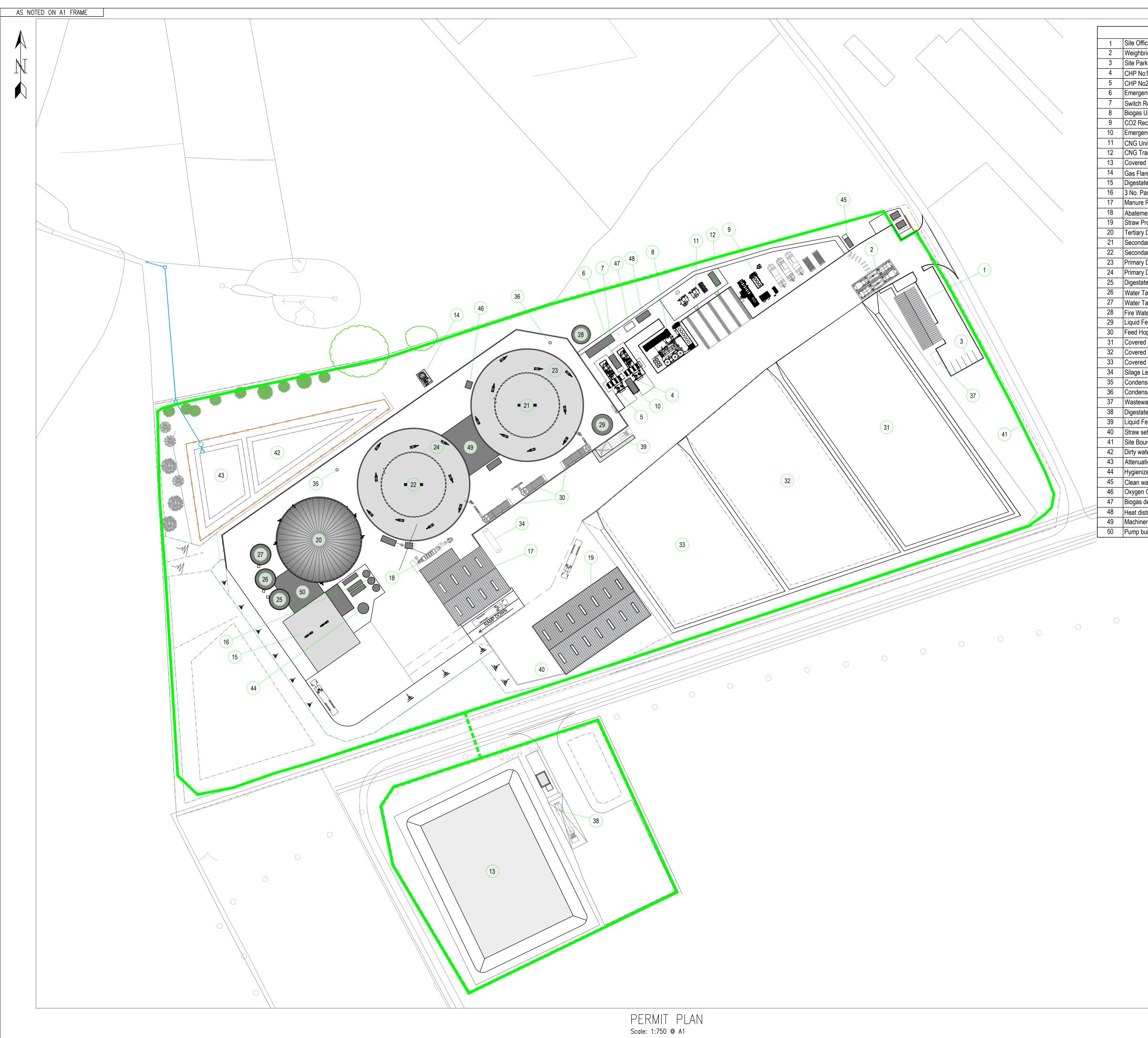
J. H. Collins BSc. (Hons), MCIWEM Director - Drainage & Infrastructure



# **APPENDIX I**

Layout Showing Tank Sizes



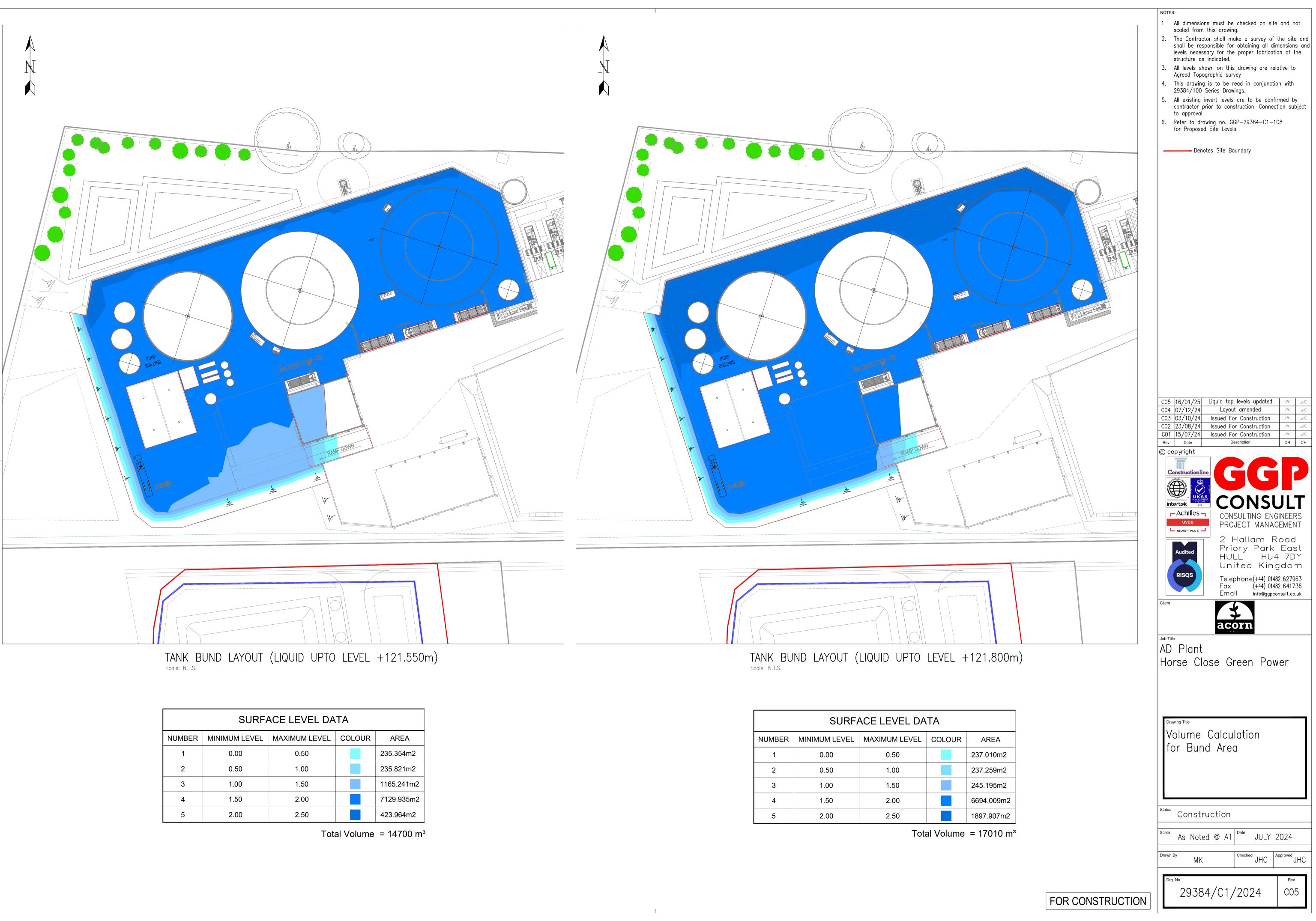


	NOTES:-
Reference Table	
Office / Staff Welfare and Workshop	Dermitted Area Deumdern (5 90hz)
hbridges (in and out)	Permitted Area Boundary (5.89ha)
Parking No1	Underground pipe conduit with leakage detection
No2	
gency Generator	
ch Room	
as Upgrade Unit Recovery Unit and CO2 tanks	
gency Boiler	
Unit	
Trailer Bays - 4 Nos.	
red lagoon - Volume 12,163m³ plus 750m freeboard Flare	
state Separator Building	
Pasteurisation tanks (25m <sup>3</sup> each)	
Ire Reception Building	
ement Plant v Process Building	
ary Digester - Volume 7444m <sup>3</sup>	
ndary Digester 1 - Volume 4512m³	
ndary Digester 2 - Volume 4512m <sup>3</sup>	
ary Digester 1 - Volume 9000m <sup>3</sup> ary Digester 2 - Volume 9000m <sup>3</sup>	
state Buffer Tank - Volume 402m <sup>3</sup>	
r Tank 1- Volume 402m <sup>3</sup>	
rr Tank 2 - Volume 402m <sup>3</sup>	
Vater Tank - Volume 250m <sup>3</sup> d Feedstock Tank - Volume 402m <sup>3</sup>	
Hoppers - Volume 2No 120m <sup>3</sup> & 1No 65m <sup>3</sup>	
red Storage Clamp 1 - Volume 19900m <sup>3</sup>	
red Storage Clamp 2 - Volume 17000m <sup>3</sup> red Storage Clamp 3 - Volume 11760m <sup>3</sup>	
e Leachate Tank - Volume 54m <sup>3</sup>	
lensate sump 1	
lensate sump 2	
state offtake bay with sump (5.1m <sup>3</sup> )	
d Feedstock loading point	
v set down bay	
Boundary Fence	
water lagoon 510m³ uation lagoon (clean) 800m³	
enized tank 80m <sup>3</sup>	
n water break tank 10m <sup>3</sup>	
en Generator as desulpherisation	A21/11/24Issued For ApprovalSUCRevDateDescriptionDRCH
distribution container	
inery Hall	
o building	
0	
	2 COKD
	BTOENERGT
	Job Title
	AD Plant.
	Horse Close
	Drawing Title
	Site Layout & Permit Plan
	Site Layout & Fernit Flan
	Status
	Approval
	Scale Date Nov '24
	As Shown Nov '24
	Drawn By
	SJC Checked - Approved -
	Drg. No. Rev
	HRCL-LAY-ABE-011 A
	TINUL LATADLOUT A



# **APPENDIX II**

2D Volume Visualisation



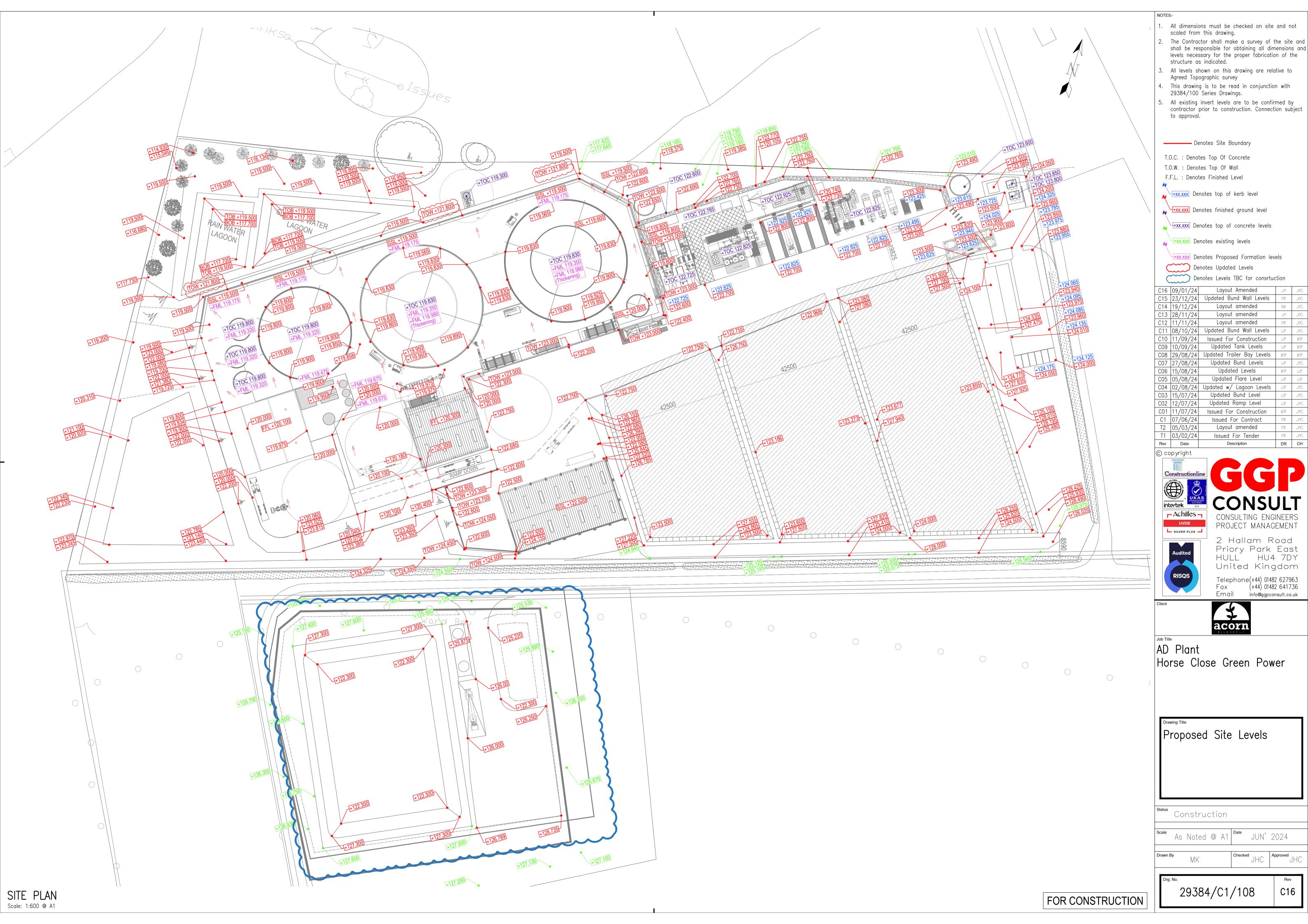
SURFACE LEVEL DATA						
NUMBER	MINIMUM LEVEL	MAXIMUM LEVEL	COLOUR	AREA		
1	0.00	0.50		235.354m2		
2	0.50	1.00		235.821m2		
3	1.00	1.50		1165.241m2		
4	1.50	2.00		7129.935m2		
5	2.00	2.50		423.964m2		

	SURFACE LEVEL DATA					
NUMBER	MINIMUM LEVEL	MAXIMUM LEVEL	COLOUR	AREA		
1	0.00	0.50		237.010m2		
2	0.50	1.00		237.259m2		
3	1.00	1.50		245.195m		
4	1.50	2.00		6694.009n		
5	2.00	2.50		1897.907n		



# **APPENDIX III**

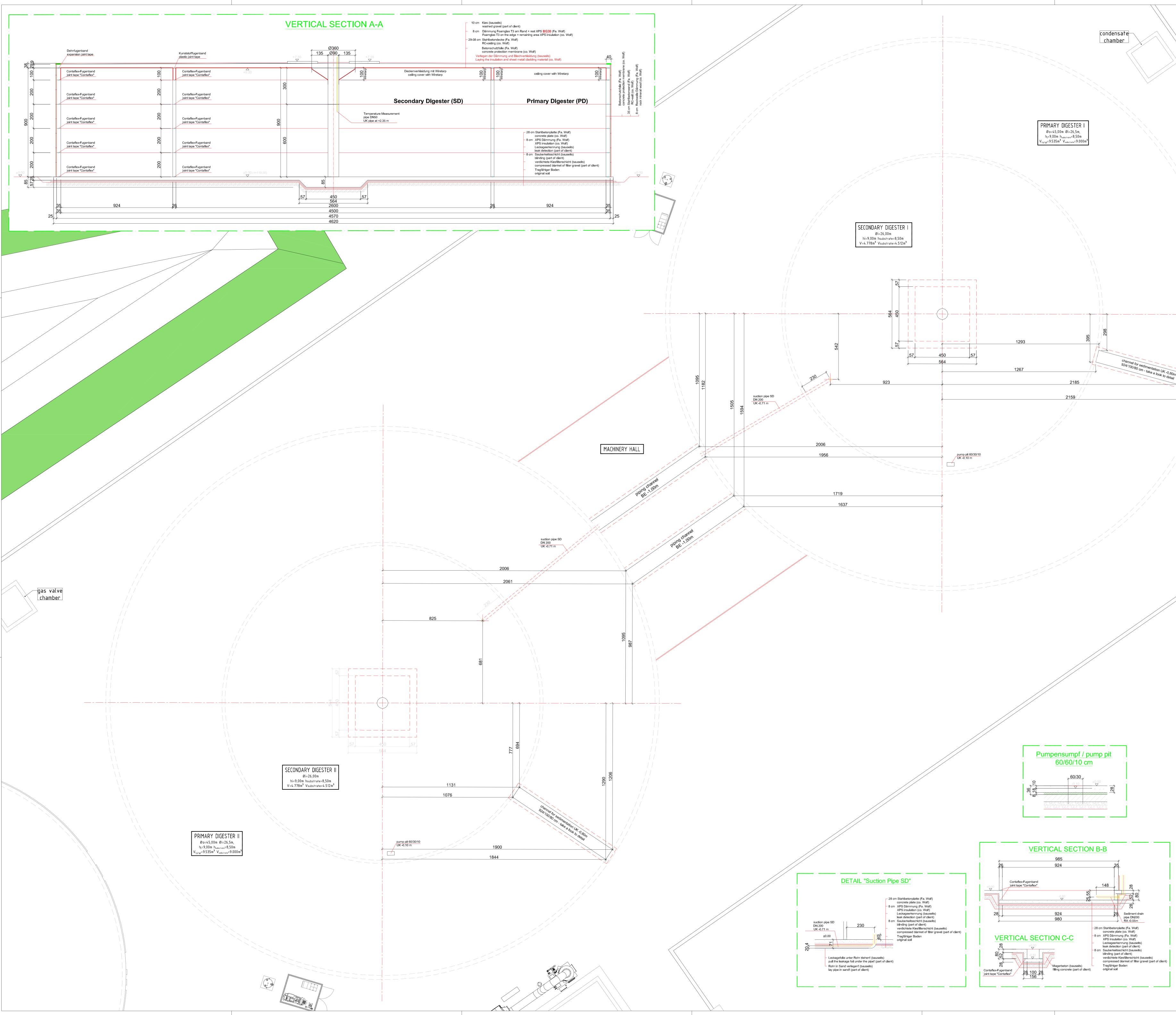
Proposed Site Levels





# **APPENDIX IV**

Primary Containment - Wolf Tanks



	R
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6	
636 539	
el for sedimentation UK -0,80m 0/80 cm - take a look to detail	
a look to detail	

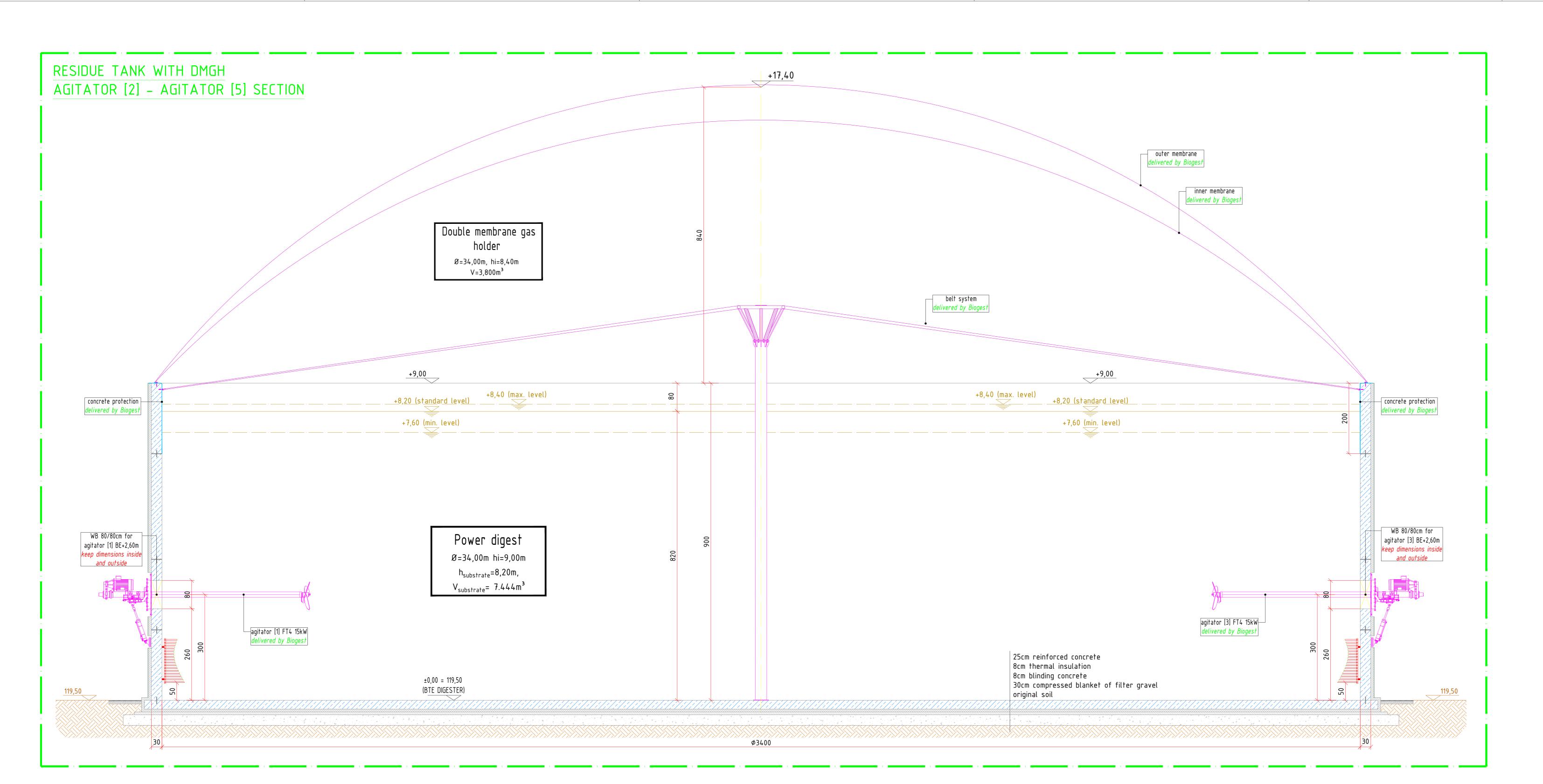
(1) <u>Earth Digging:</u> Digging and slope angles have to be made per spoil mechanics and local regulations!

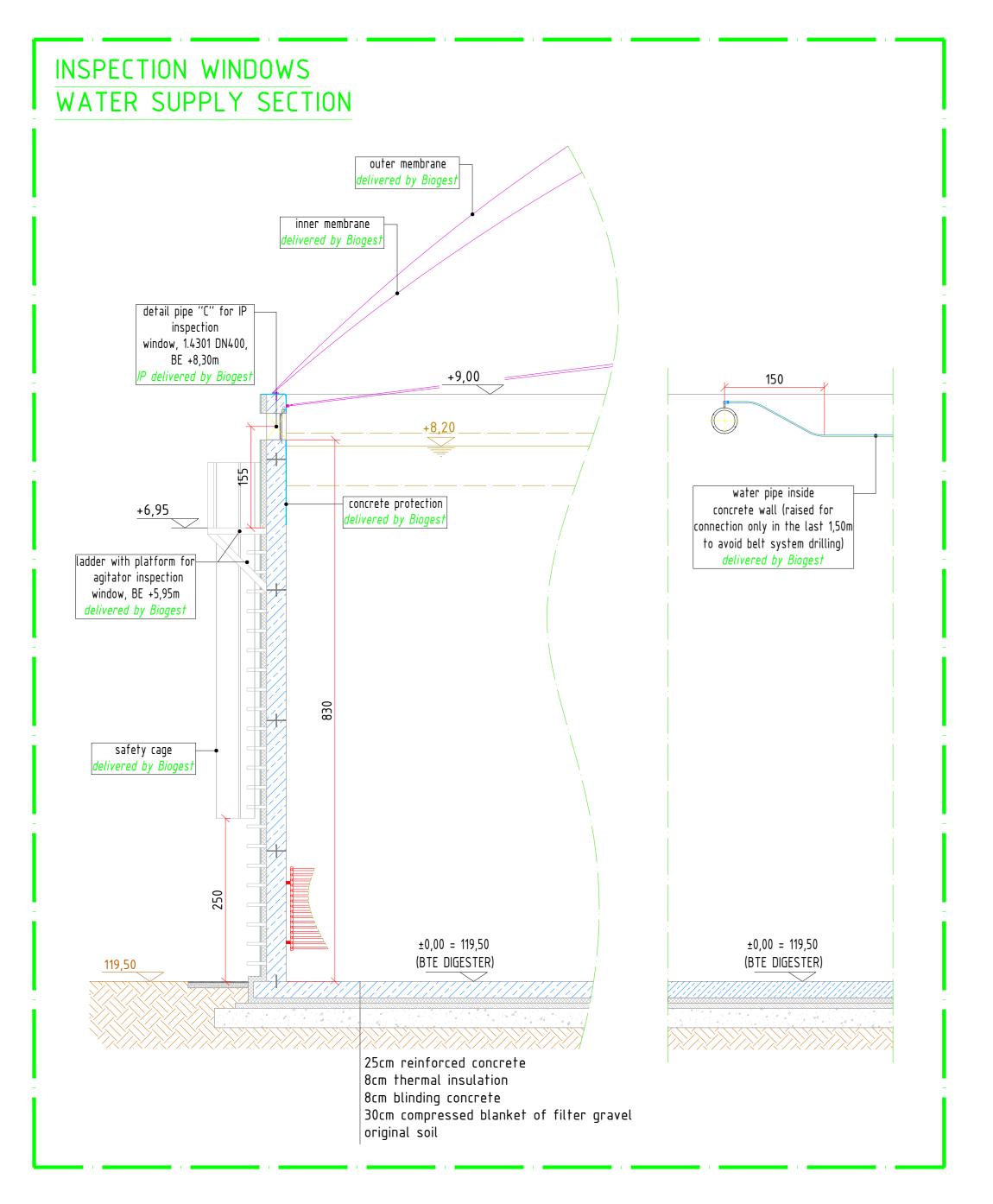
(2) <u>Electrical Grounding:</u> Grounding together with jumper flags will be provided by the customer and installed together with the construction company.

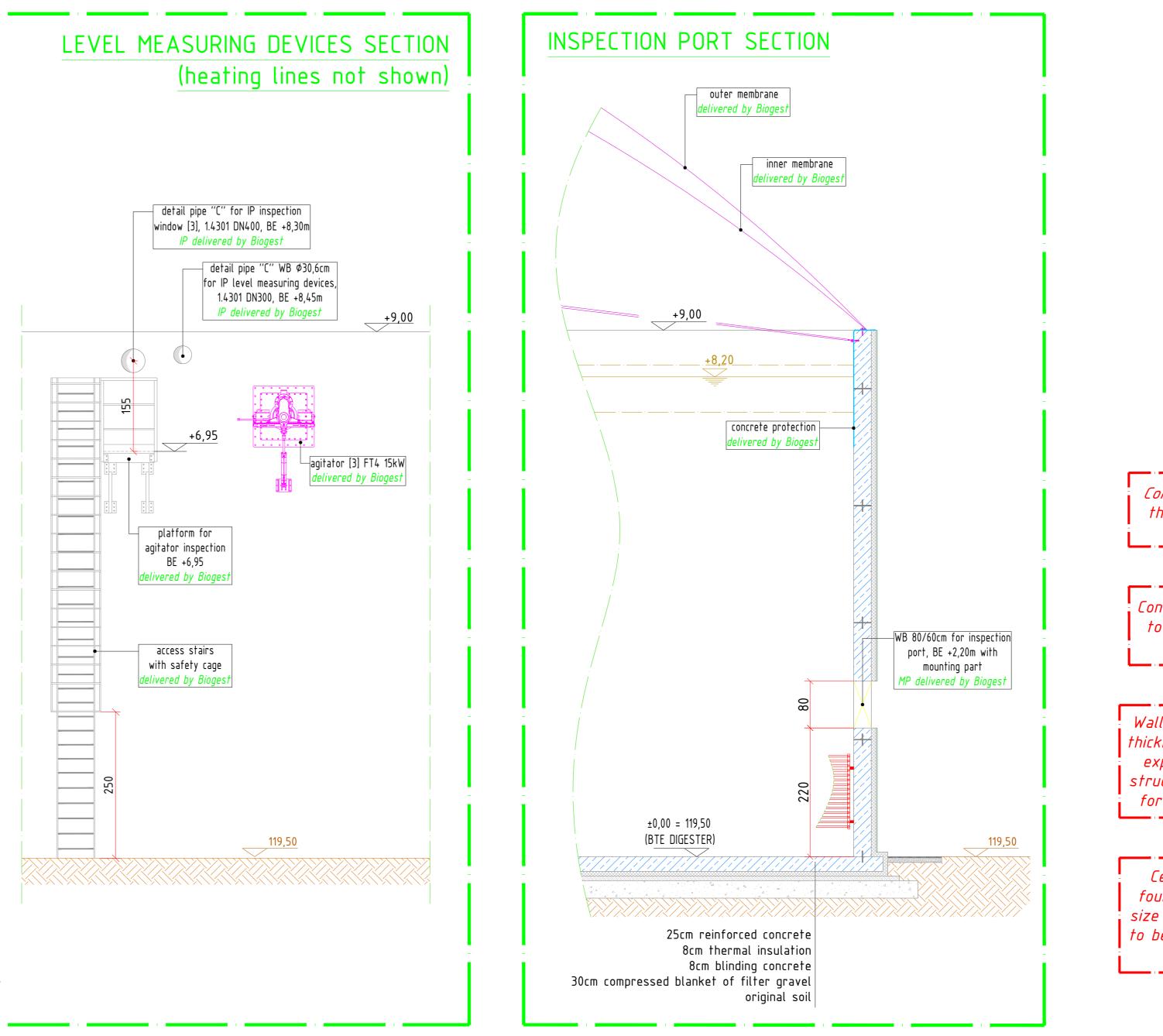
(3) <u>Block-Outs</u>: All levels refer to the top edge base plate of the digester. Mounting parts and immure pipes will be provided by Biogest. Wall breakthroughs, ceiling breaks and grounding of these has to be done by the building contractor!

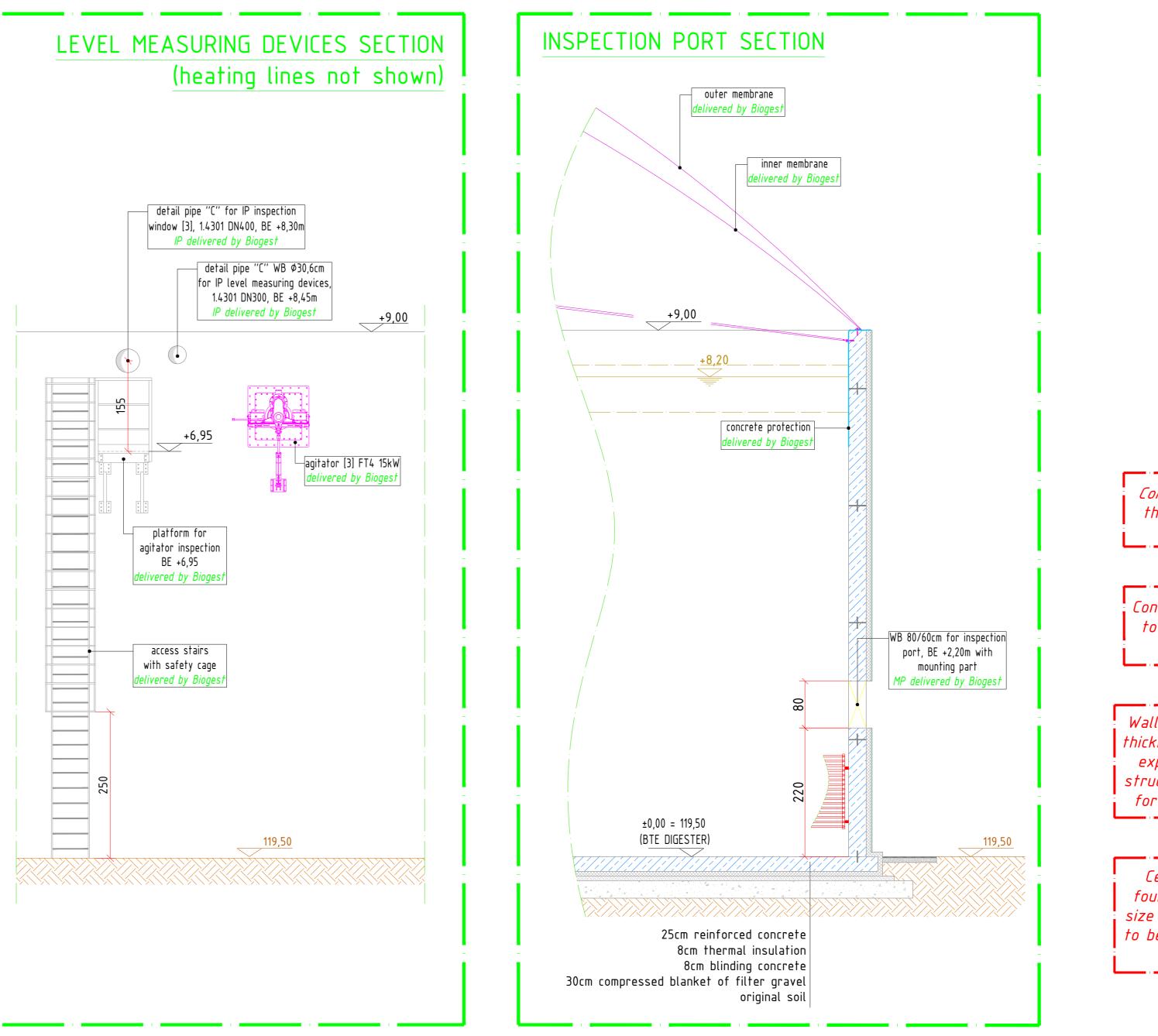
±0,00 = +xx,xx (BTE DIGESTER)

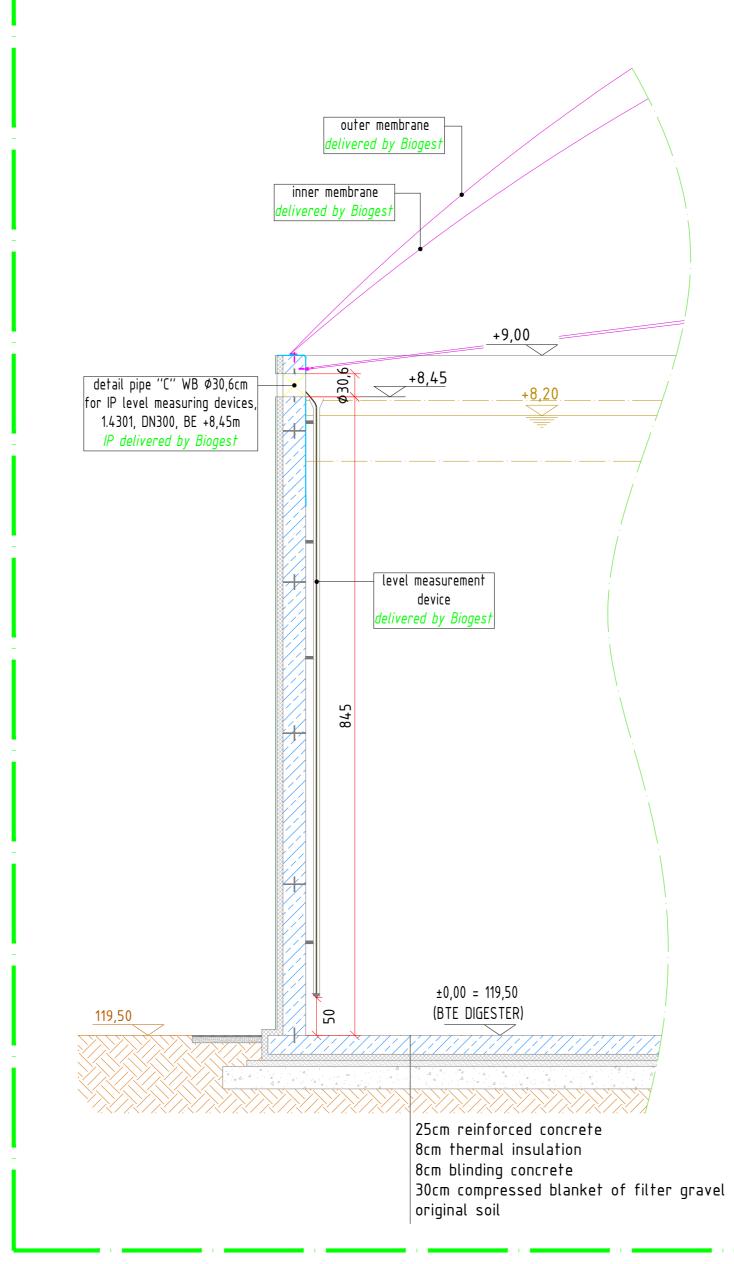
	ATIONS						
NO.	DATE	MODIFICATION(S)				DONE BY	CHECKED BY
$\rightarrow$							
This draw	ving is our intel	lectual property and is n	ot allowed to b	e reproduced or r	nade available to th	ird parties witho	ut our consent
DESIGNER:					BIOQUADRAT ENERGIE		
JESIUNEK:		BIOGEST	R		Ge Tov	The Icon Vien trude-Froehlich-Sar ver 9, Floor 9, A-11 43 20840 00 fax: +	na Central Statior ndner Strasse 2-4 00 Vienna, Austria
	TION:	<b>BIOGEST</b> Kingdom	. ®		Ge Tov	The Icon Vien trude-Froehlich-Sar ver 9, Floor 9, A-11 43 20840 00 fax: +	na Central Statior ndner Strasse 2–4 00 Vienna, Austria 43 2243 20840 40
PROJECT-LOCAT PROJECT-NAME:	united		. (R)		Ge Tov	The Icon Vien trude-Froehlich-Sar ver 9, Floor 9, A-11 43 20840 00 fax: +	na Central Statior ndner Strasse 2–4 00 Vienna, Austria 43 2243 20840 40
PROJECT-LOCAT	United UK-202	Kingdom	. (R)	CONTENT:	Ge Tov	The Icon Vien trude-Froehlich-Sar ver 9, Floor 9, A-11 43 20840 00 fax: +	na Central Statior ndner Strasse 2–4 00 Vienna, Austria 43 2243 20840 40
PROJECT-LOCAT PROJECT-NAME: PLANNED CONST	United UK-202 TRUCTION: WANAER(	Kingdom			Ge Tov	The Icon Vien trude-Froehlich-Sar ver 9, Floor 9, A-110 43 20840 00 fax: + office@biogest.a	na Central Statior ndner Strasse 2-4 00 Vienna, Austria 43 2243 20840 4( at www.biogest.at
PROJECT-LOCAT PROJECT-NAME: PLANNED CONST	United UK-202 TRUCTION: WANAERO IN H	Kingdom 22-01-259-Horse Close DBIC DIGESTION F HORSE CLOSE		CHANN DRAWING-NO.	Ge Tov tel: +43 22	The Icon Vien trude-Froehlich-Sar ver 9, Floor 9, A-110 43 20840 00 fax: + office@biogest.a	na Central Statior ndner Strasse 2-4 00 Vienna, Austria 43 2243 20840 4( at www.biogest.at
PROJECT-LOCAT PROJECT-NAME: PLANNED CONST NE	ION: United UK-202 TRUCTION: WANAERC IN H EER: DI Gerald	Kingdom 22-01-259-Horse Close DBIC DIGESTION F HORSE CLOSE	PLANT	( CHANN	Ge Tov tel: +43 22	The Icon Vien trude-Froehlich-Sar ver 9, Floor 9, A-110 43 20840 00 fax: + office@biogest.a	na Central Station ndner Strasse 2-4 00 Vienna, Austria 43 2243 20840 4( at www.biogest.at at www.biogest.at

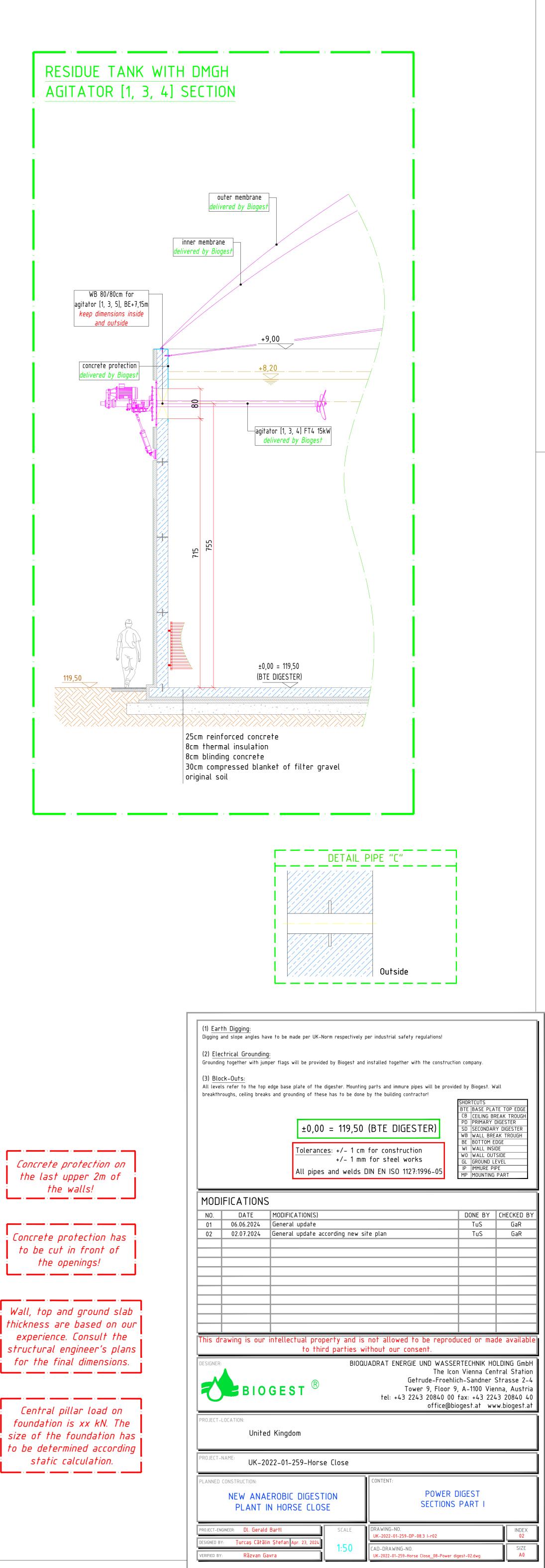








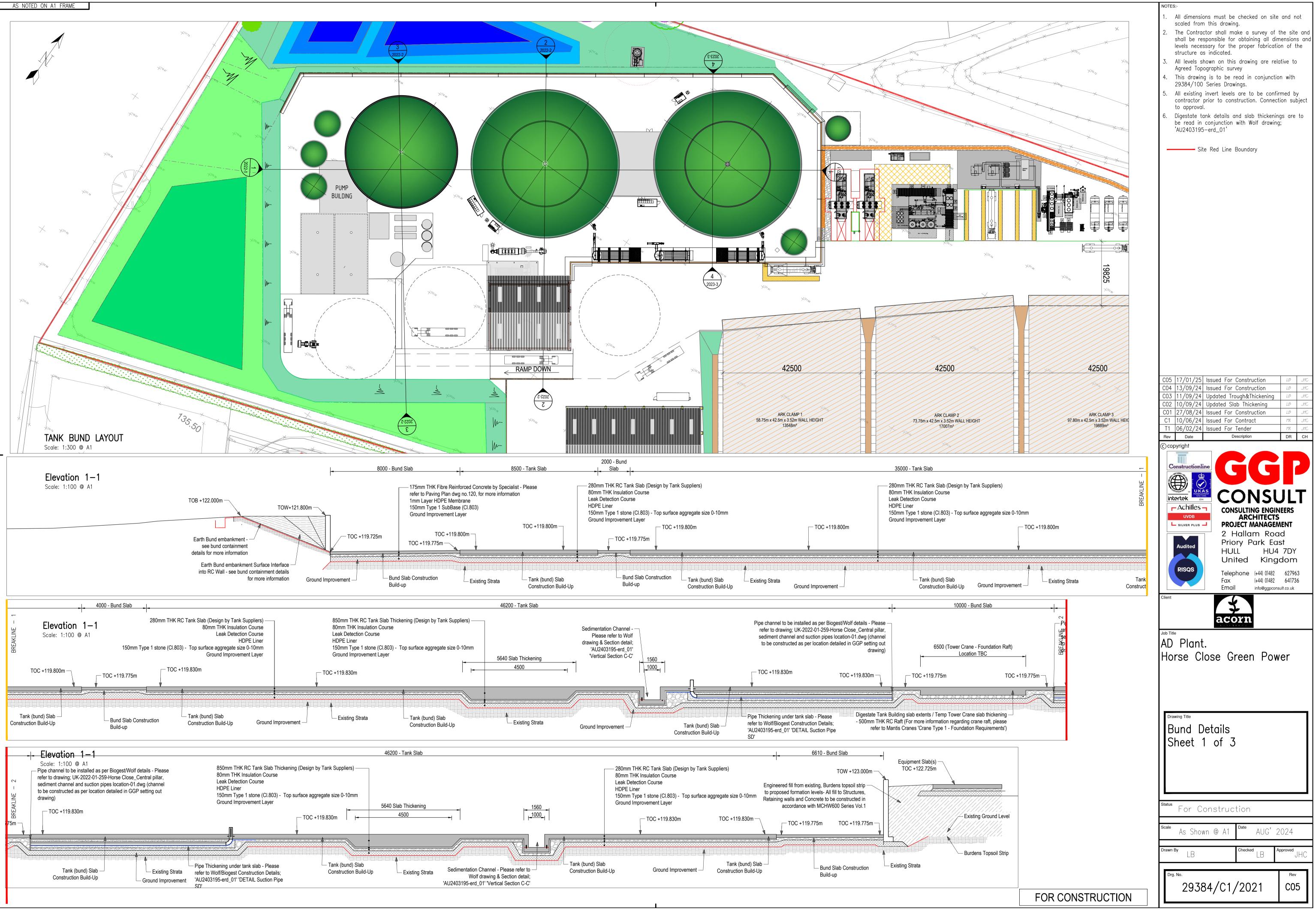


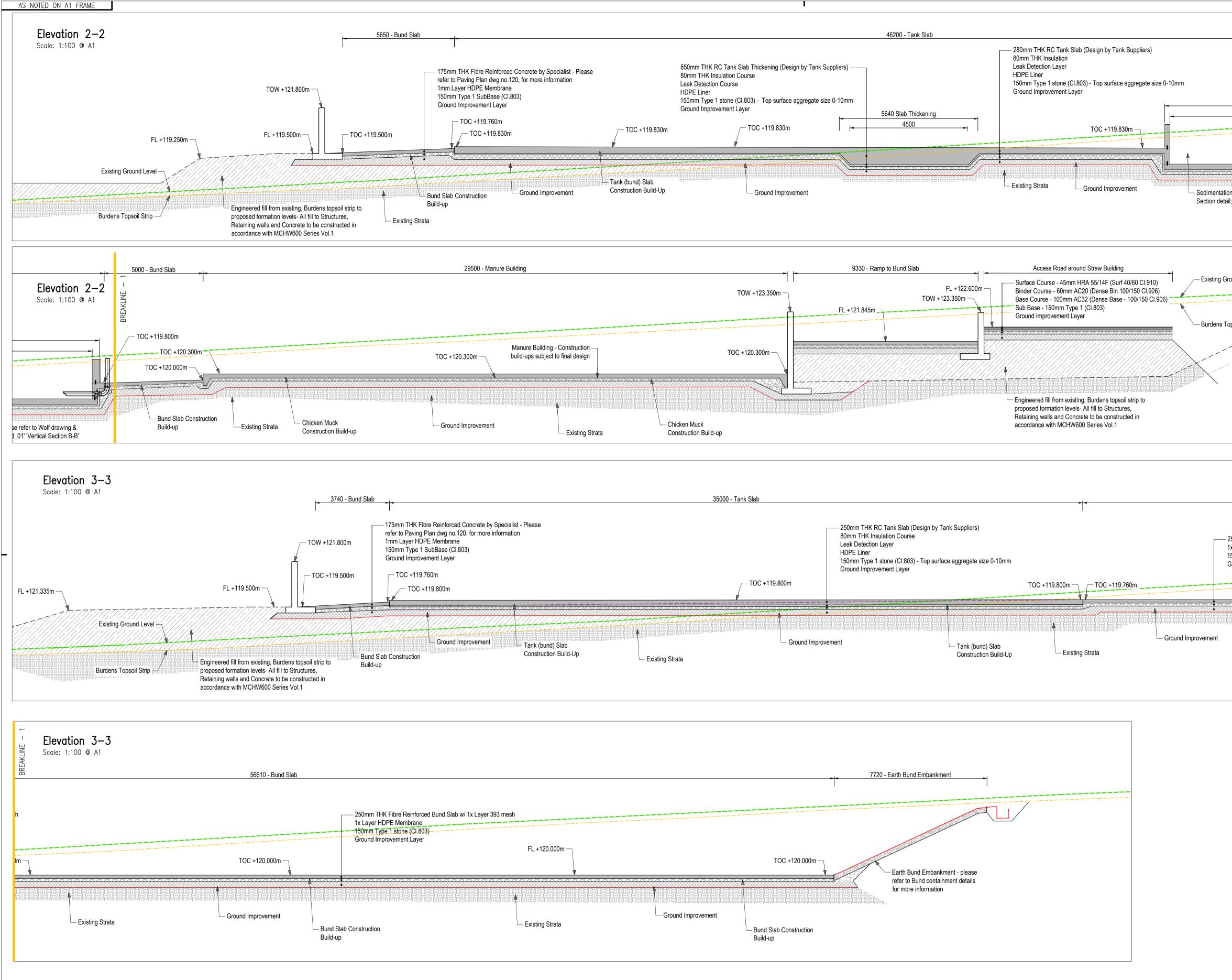




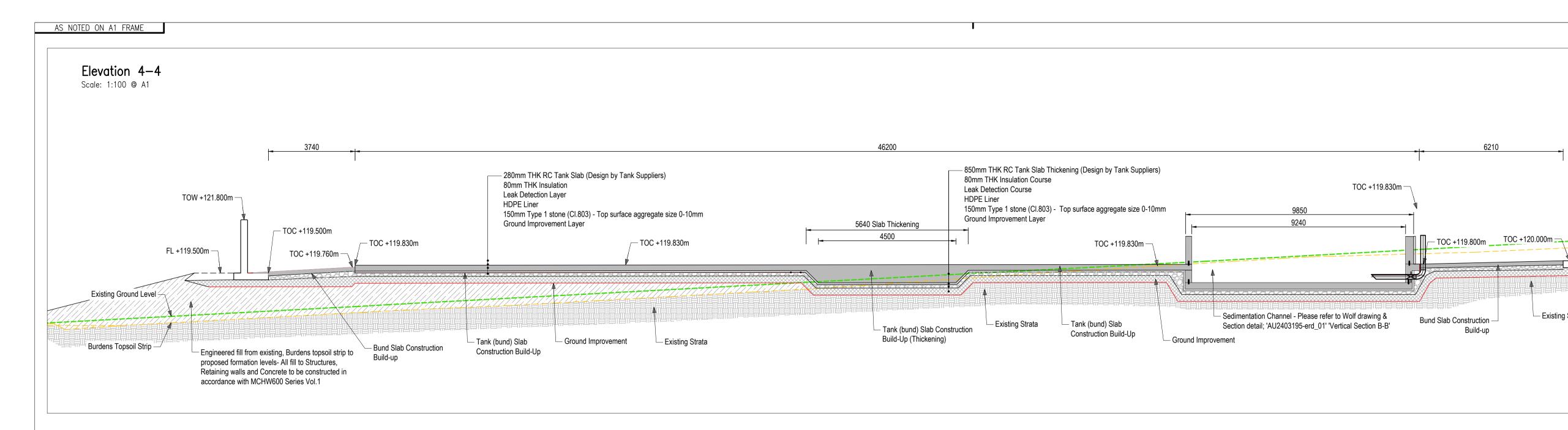
# **APPENDIX V**

Secondary Containment Details

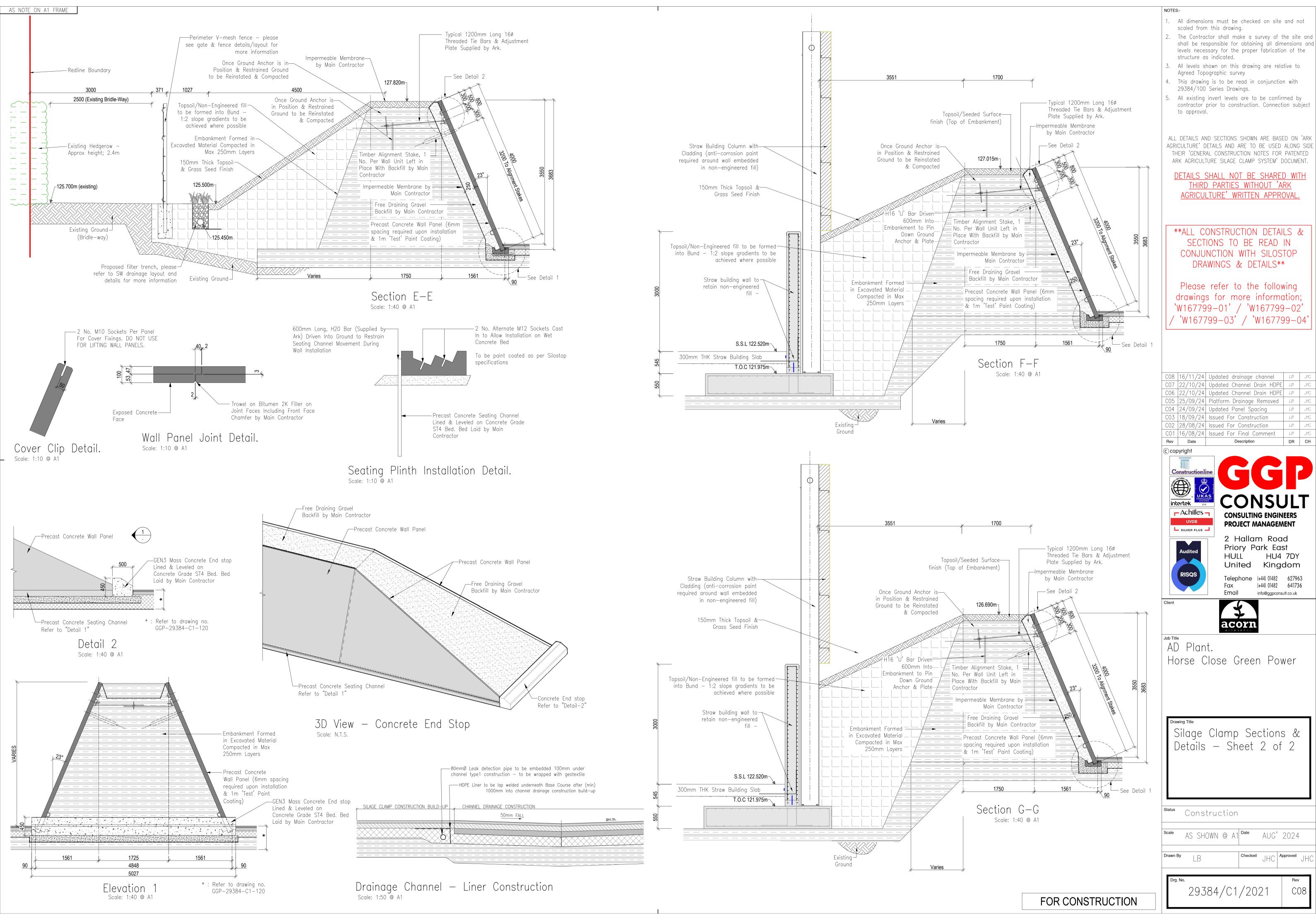


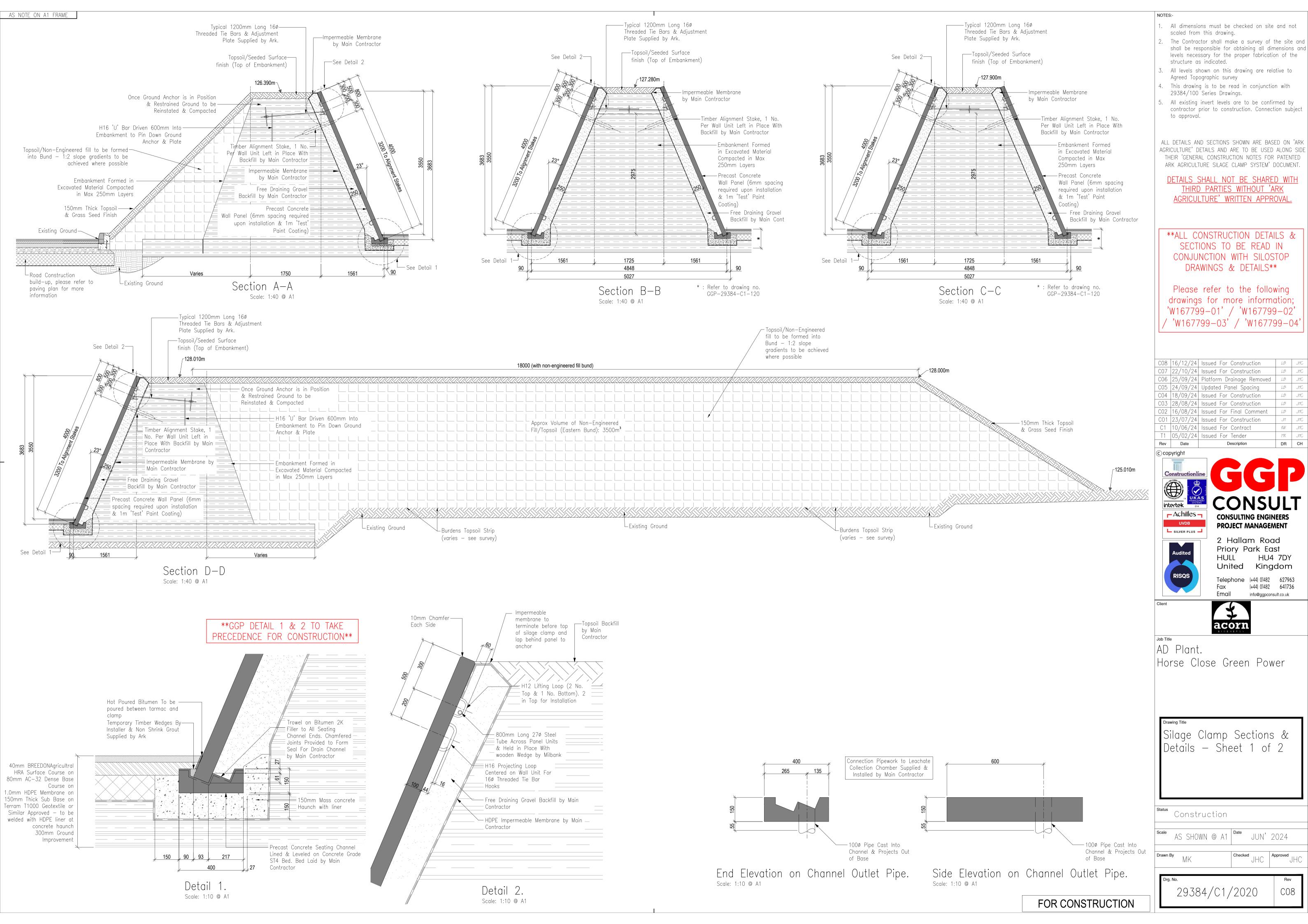


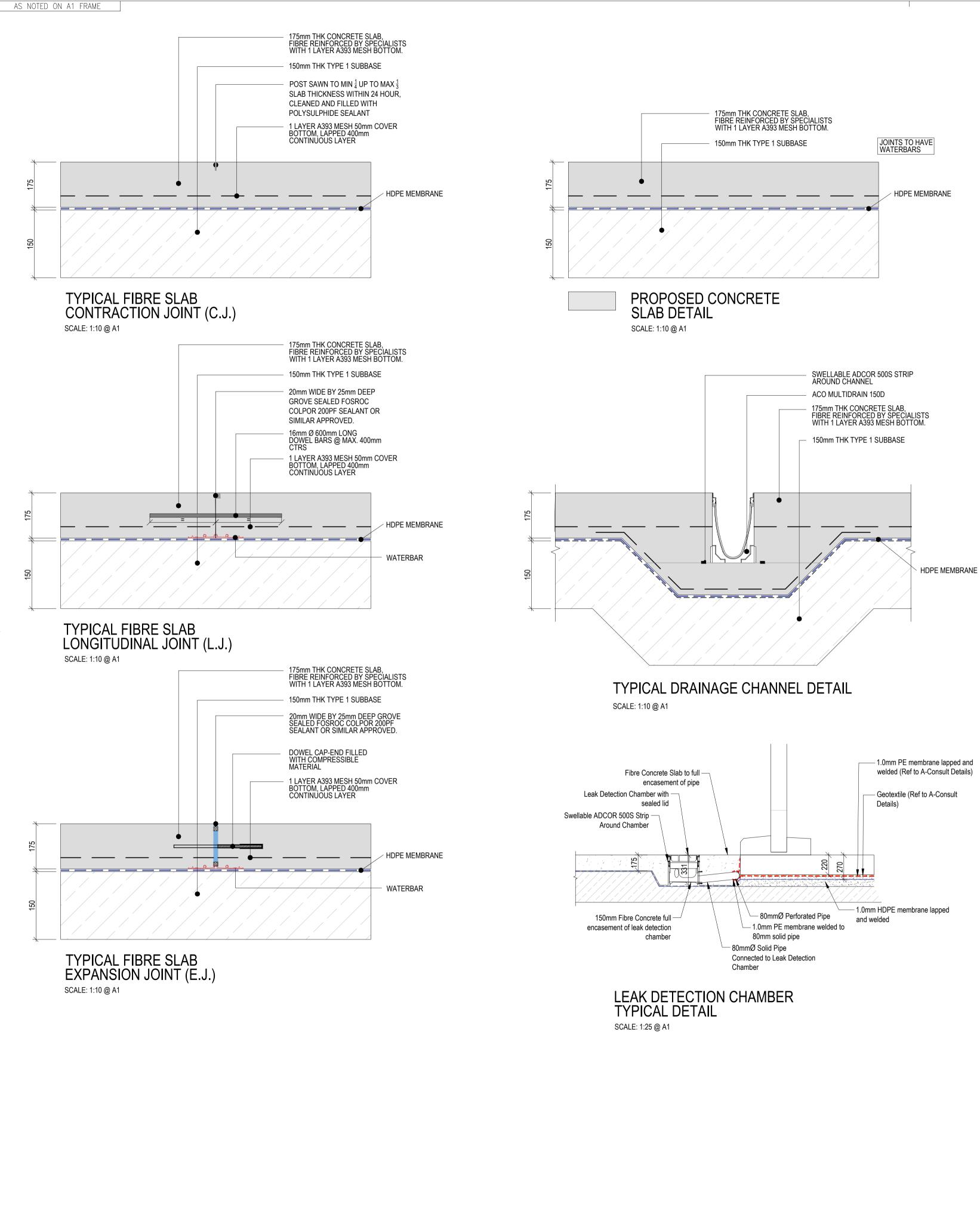
9850 9240 9240 or Channel - Please refer to Wolf drawing & al; 'AU2403195-erd_01' 'Vertical Section B-B'	<ol> <li>NOTES:-</li> <li>All dimensions must be checked on site and not scaled from this drawing.</li> <li>The Contractor shall make a survey of the site and shall be responsible for obtaining all dimensions and levels necessary for the proper fabrication of the structure as indicated.</li> <li>All levels shown on this drawing are relative to Agreed Topographic survey</li> <li>This drawing is to be read in conjunction with 29384/100 Series Drawings.</li> <li>All existing invert levels are to be confirmed by contractor prior to construction. Connection subject to approval.</li> <li>Digestate tank details and slab thickenings are to be read in conjunction with Wolf drawing; 'AU2403195-erd_01'</li> </ol>
iround Level	
Topsoil Strip	
	C0517/01/25Issued For ConstructionLØJHCC0413/09/24Issued For ConstructionLØJHCC0311/09/24Updated Trough&ThickeningLØJHC
BREAKLINE	C0210/09/24Updated Slab ThickeningLPJHCC0127/08/24Issued For ConstructionLPJHCC110/06/24Issued For ContractKNJHCT106/02/24Issued For TenderMKJHC
250mm THK Fibre Reinforced Bund Slab w/ 1x Layer 393 mesh 1x Layer HDPE Membrane 150mm Type 1 stone (CI.803) Ground Improvement Layer TOC +120.000m Bund Slab Construction Build-up	Rev       Date       Description       DR       CH         C copyright       Image: Construction line       Image: Construle       Image: Construction line
	AuditedPriory Park East HULLRISQSPriory Park East HULLRISQSTelephoneTelephone(+44)01482627963 641736
	Email info@ggpconsult.co.uk Client
	AD Plant. Horse Close Green Power
	Drawing Title Bund Details Sheet 2 of 3
	Status For Construction
	Scale     AS     SHOWN     Date     AUG'     2024       Drawn By     LB     Checked     Approved     JHC
FOR CONSTRUCTION	Drg. No. Rev 29384/C1/2022 C05



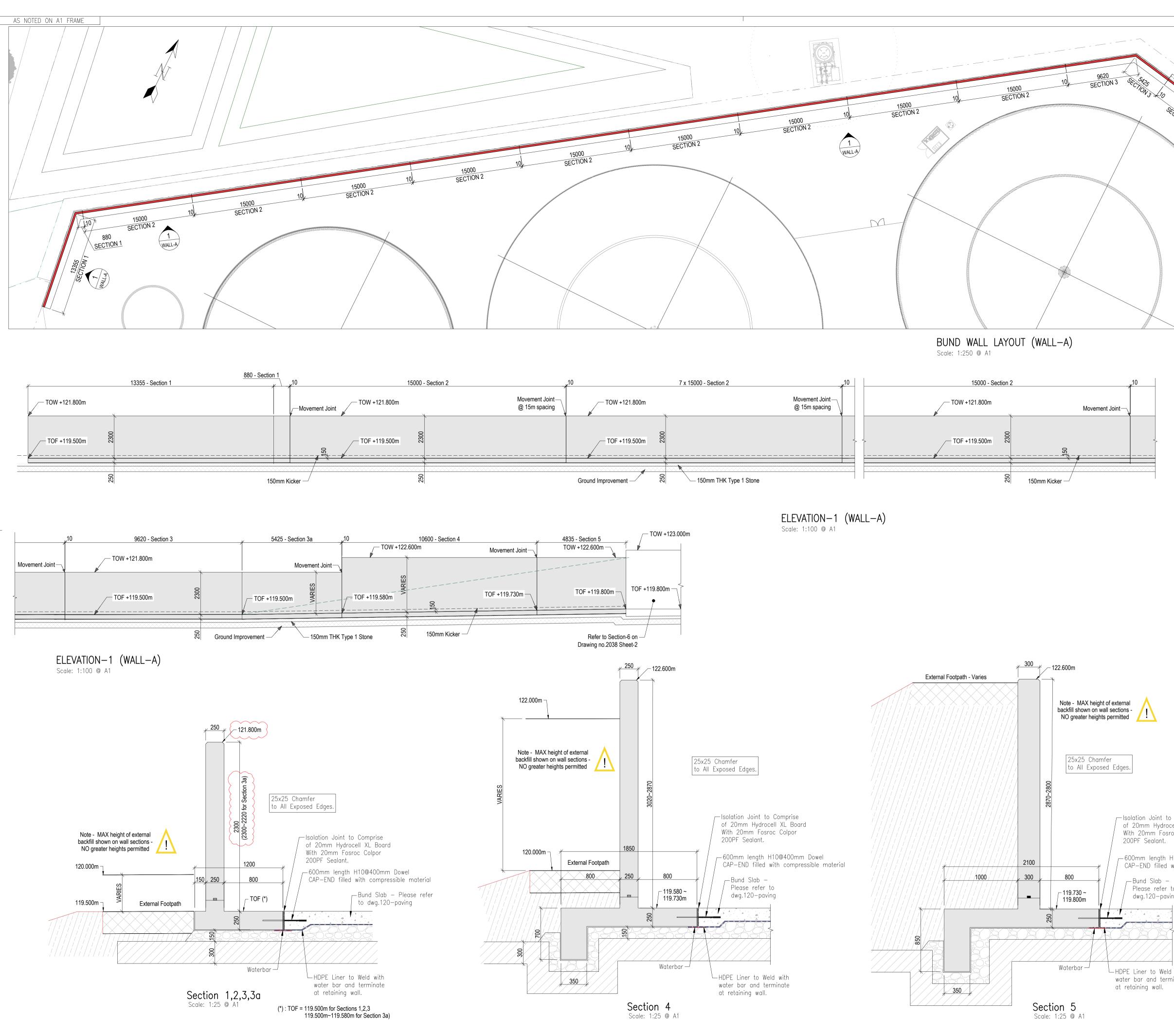












HDPE Liner to Weld with water bar and terminate at retaining wall.

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-Bund Slab -Please refer to dwg.120-paving

-600mm length H10@400mm Dowel CAP-END filled with compressible material

200PF Sealant.

Isolation Joint to Comprise of 20mm Hydrocell XL Board With 20mm Fosroc Colpor



SECTION A

MALL A

SECTION 5 ¥

- NOTES:-
- . All dimensions must be checked on site and not scaled from this drawing.
- The Contractor shall make a survey of the site and shall be responsible for obtaining all dimensions and levels necessary for the proper fabrication of the structure as indicated.
- All levels shown on this drawing are relative to Agreed Topographic survey
- 4. All existing invert levels are to be confirmed by contractor prior to construction. Connection subject to approval.
- When The Distance Between The Top Of Bund Wall & External Concrete/Ground Levels is Less Than 1.1m Provide Medium Duty Galvanised Steel Handrailing
- Fixed to The Top of the Wall. Height of Handrailing Varies to Suit Change in Concrete/Ground Levels.
- Provide Movement Joints at 18m Centres Along Length of Wall in Accordance With Typical
- Contraction Joint Detail. 25x25 Chamfer to all Exposed Edges 8. Concrete cover to reinforcement = 50mm U.N.O

Site Red Line Boundary

T.O.W. :	Denotes	Top Of Wall
T.O.F. :	Denotes	Top Of Foundation
T.O.C. :	Denotes	Top Of Concrete
F.F.L. :	Denotes	Finished Level
G.L. :	Denotes	Ground Level
I.F. :	Denotes	Inner Face
0.F. :	Denotes	Outer Face
т :	Denotes	Тор
В :	Denotes	Bottom
`		
	5	
∽+xx.	xxx Der	notes finished ground level

----- Denotes Proposed Backfill Profile

Date	Description	DR	СН
0/ 10/ 2 1			
)8/10/24	ISSUED FOR CONSTRUCTION	LB	JHC
5/11/24	ISSUED FOR CONSTRUCTION	MK	JHC
21/11/24	Dowels notes added	MK	JHC
8/12/24	Top of wall levels updated	MK	JHC
	1/11/24 5/11/24	5/11/24 ISSUED FOR CONSTRUCTION	1/11/24Dowels notes addedMK5/11/24ISSUED FOR CONSTRUCTIONMK



Telephone(+44) 01482 627963 Fax (+44) 01482 641736 Fax Email info@ggpconsult.co.uk

acorn Job Title AD Plant. Horse Close

RISQS

Drawing Title Bund Details Wall A Sheet-1

Status Construction

AS NOTED @ A1 Date Scale

Drawn By LB

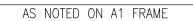
JHC Rev C04

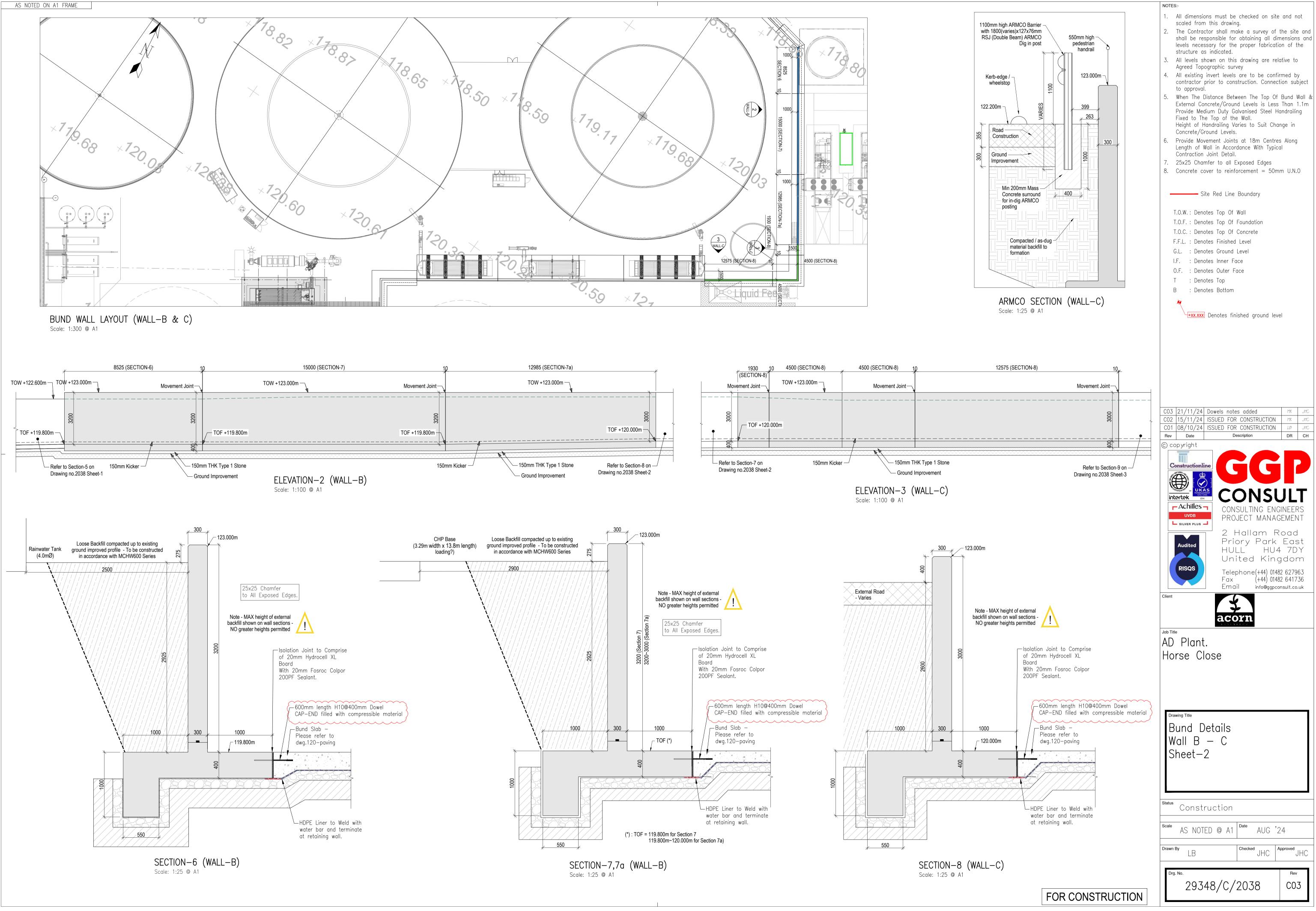
Approved

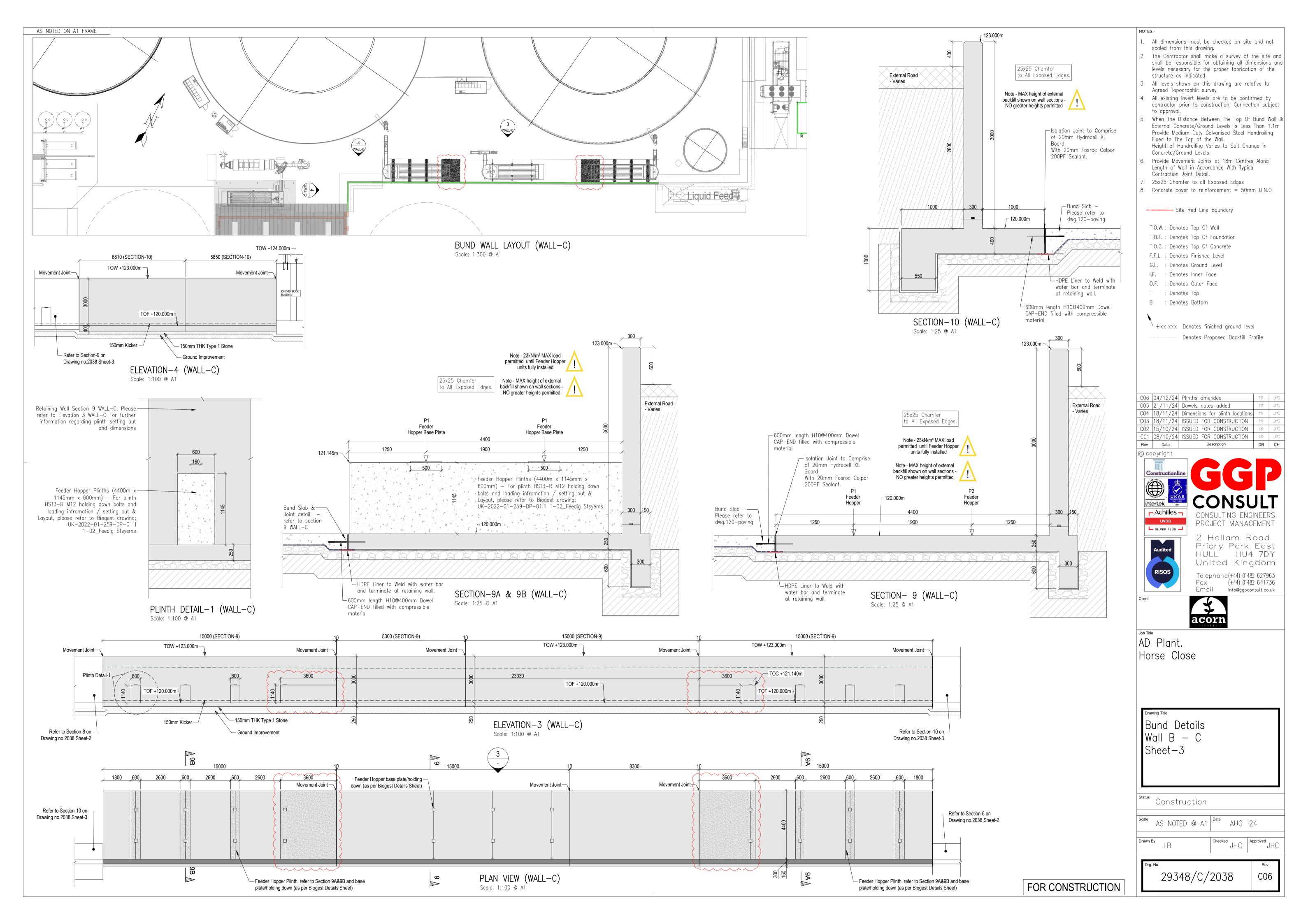
AUG '24

Checked

29348/C/2038



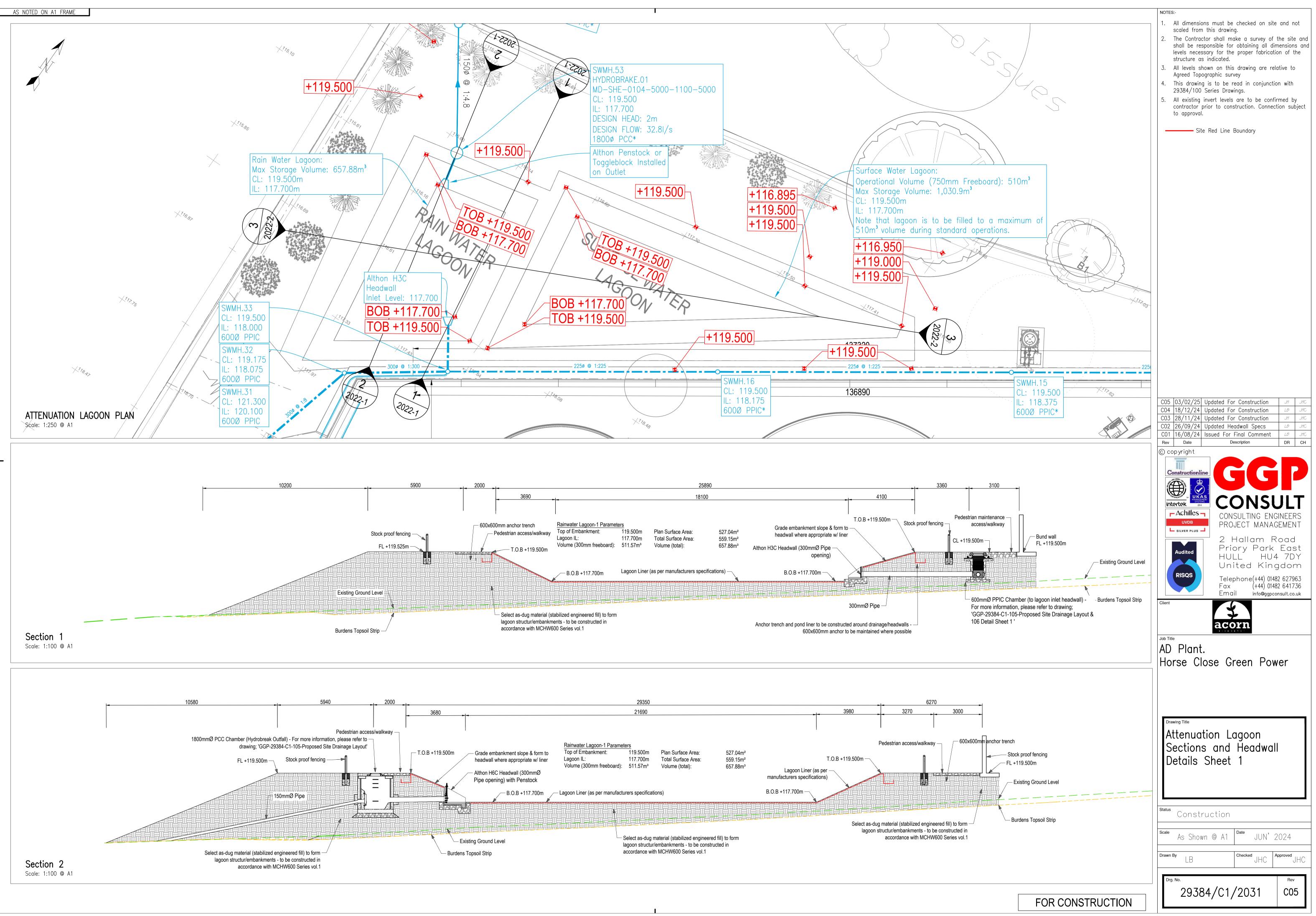


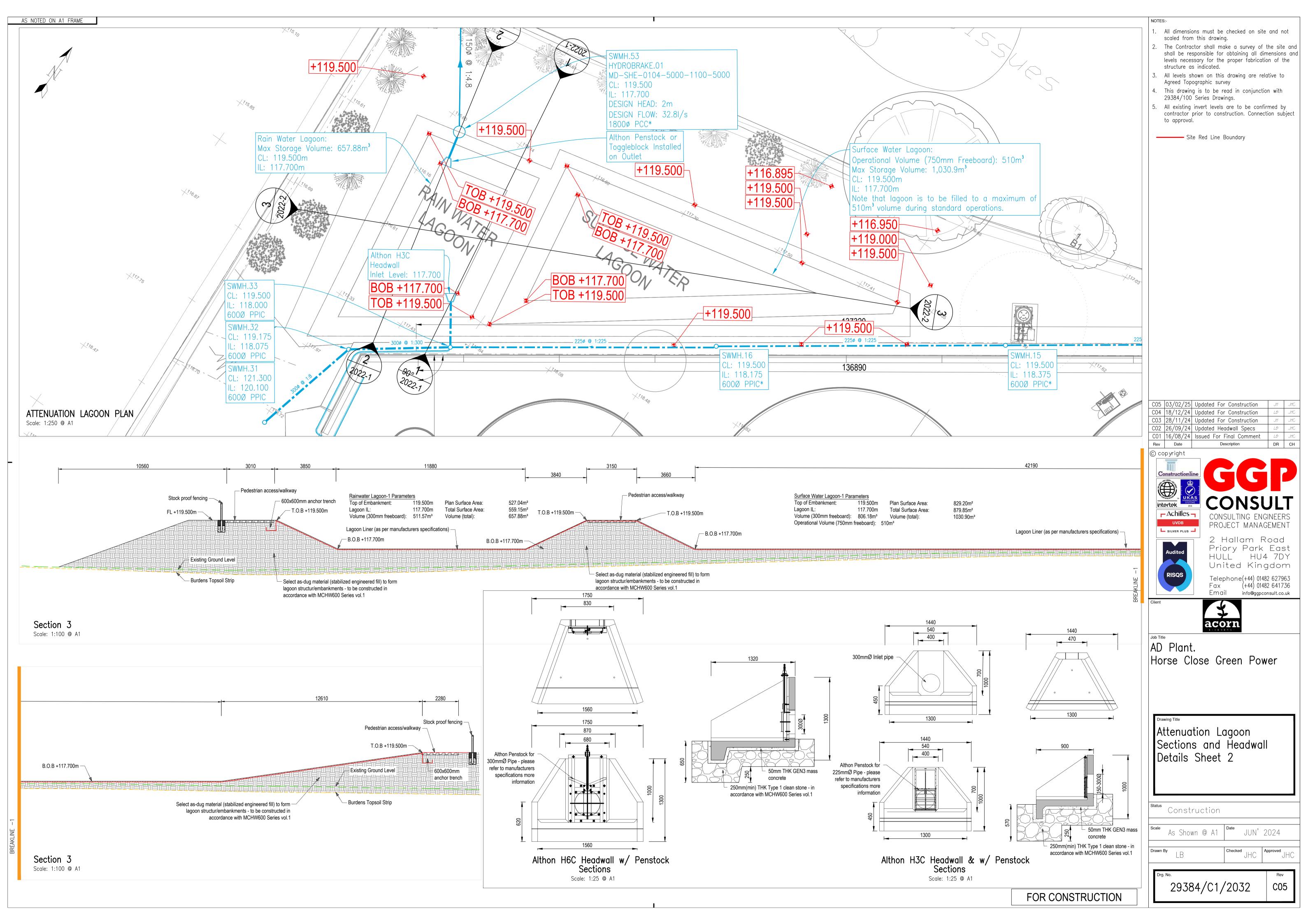


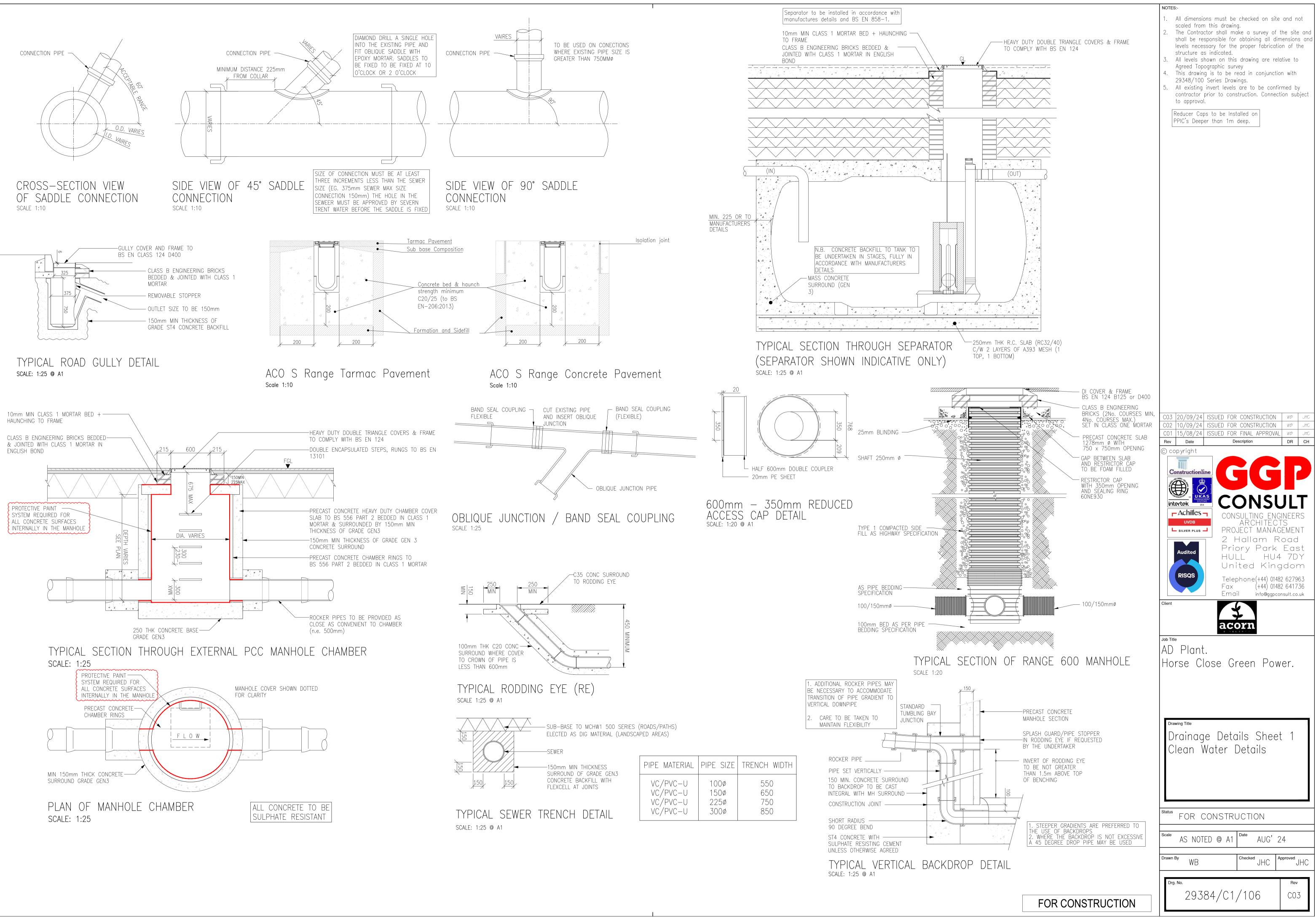


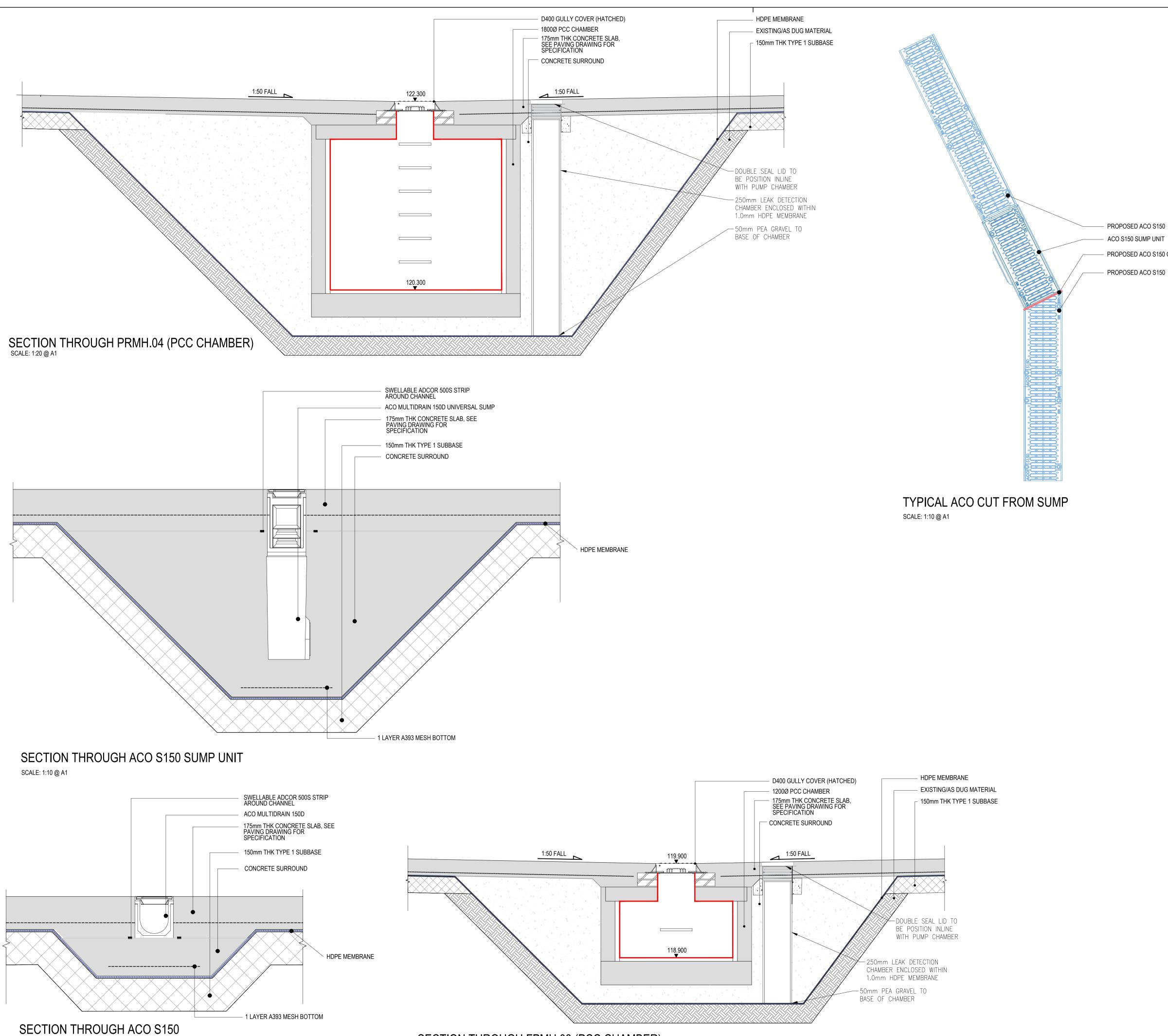
# **APPENDIX VI**

Drainage Details









SCALE: 1:10 @ A1

2. 3. 4.	scaled from th The Contractor shall be respon levels necessary structure as in All levels shown Agreed Topogra This drawing is 29348/100 Ser	shall ma nsible for y for the dicated. n on this uphic sur- to be r ries Draw	oke a s obtaini proper drawin vey ead in ings.	ng all dir fabricati g are rel conjunctir	mensions c on of the ative to on with
5.	All existing inve contractor prior to approval.				
C03 C02 C01	10/09/24 ISS	UED FOR UED FOR	CONST	RUCTION RUCTION APPROVAI	WB JI WB JI _ WB JI
С	Date opyright onstructionline		escription	G	
	Achilles     UVDB	CON	SULTIN ARC	NG ENC HITEC	JLT GINEERS TS GEMENT
	Audited RISQS	Prid HUI Un Telep	ory _L ited phone	H∪∠ Kin∢ (+44) 0148	Coad East 7 DY gdom 82 627963 82 641736
Client				info@ggpco	onsult.co.uk
	Plant. orse Clos	se Gi	reen	Pov	ver
	awing Title	Deto	ails	Shee	t 2
Status	FOR CO	NSTRI	JCTIC	DN	
Scale	AS NOTED	@ A1	Date	AUG'	24
Drawn	<sup>by</sup> WB		Checked	JHC '	Approved JH(
Drg	<sup>3. №.</sup> 29384	/_1	/11	$\mathbf{O}$	Rev

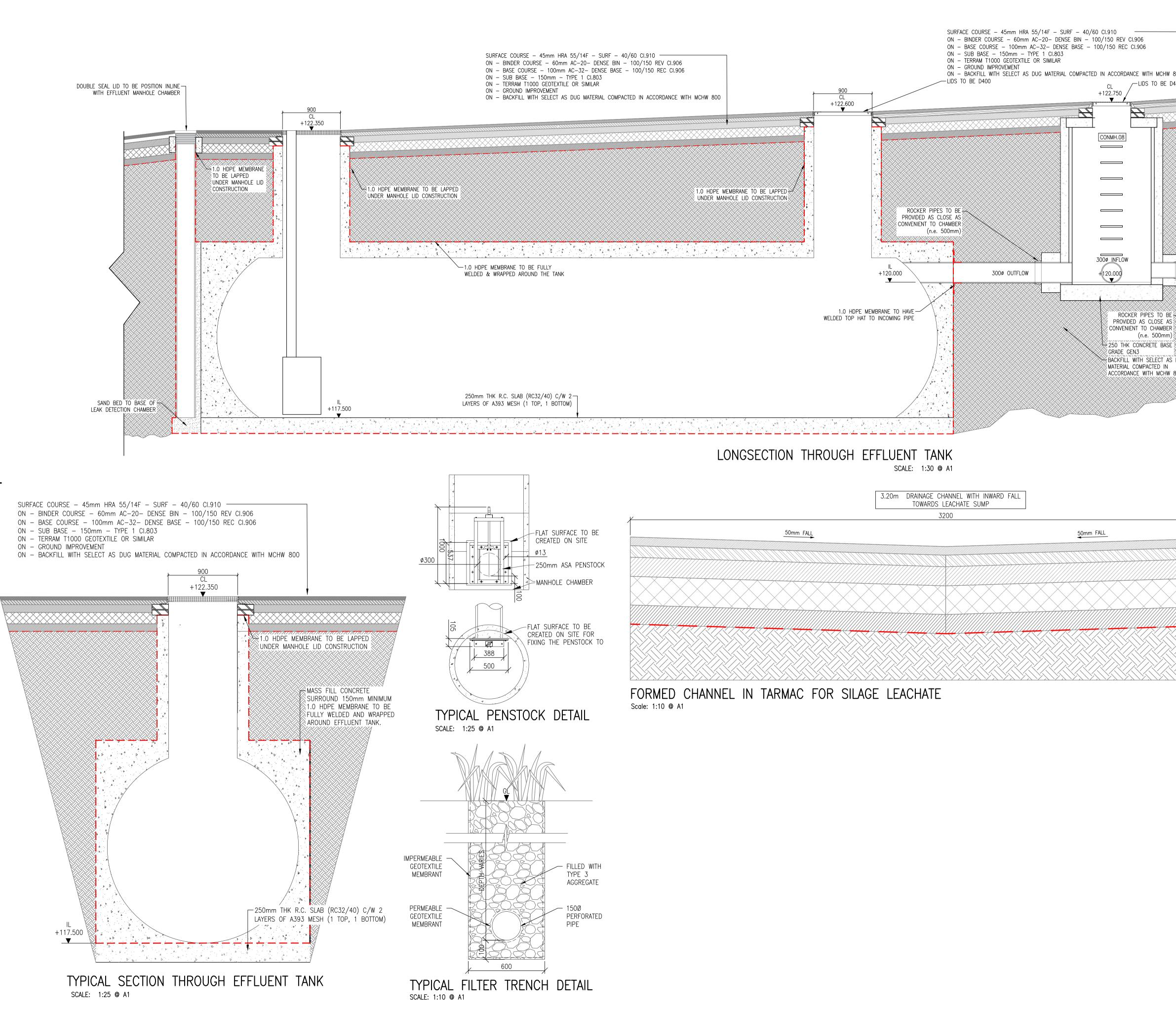
NOTES:-

. All dimensions must be checked on site and not

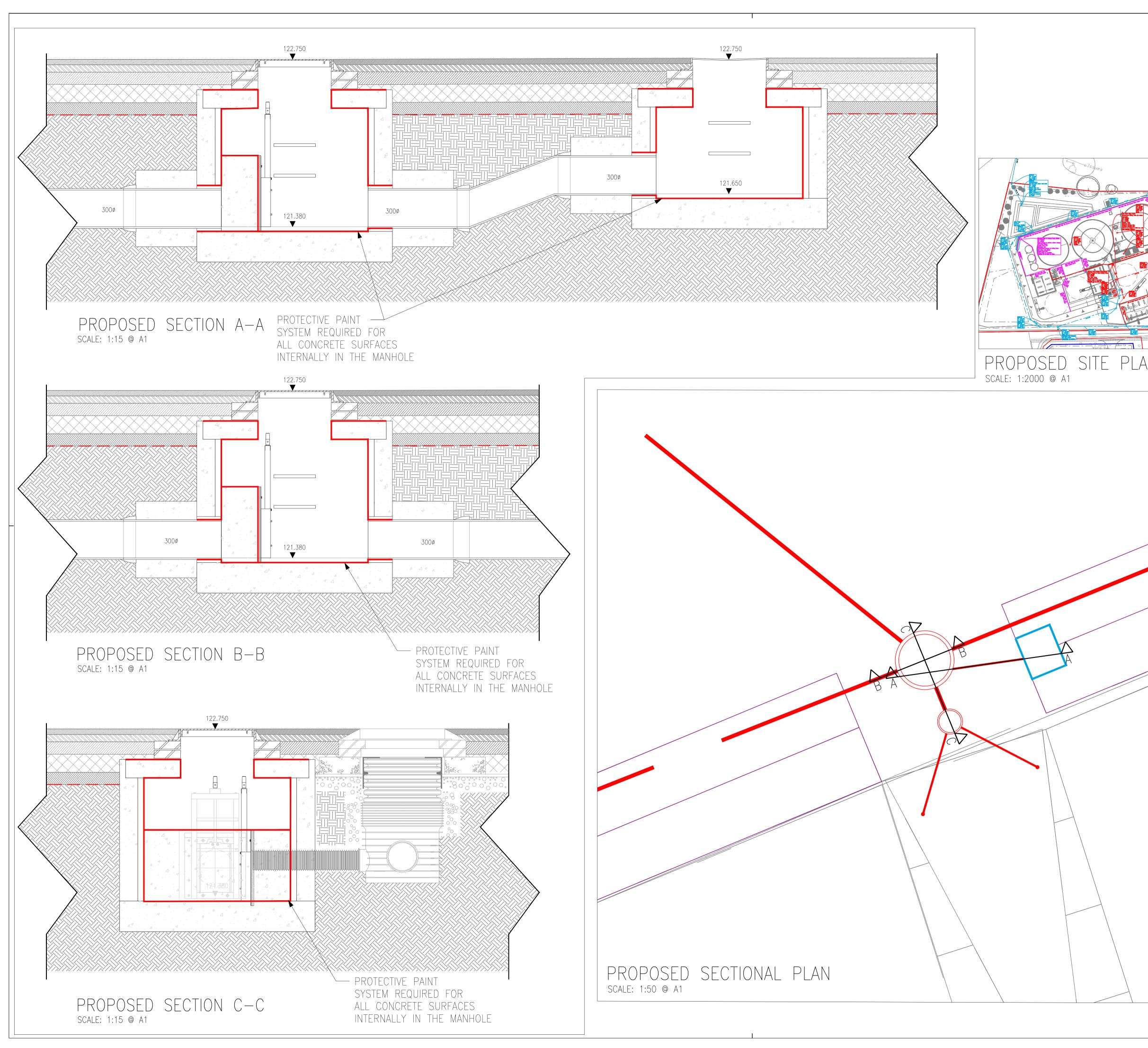
PROPOSED ACO S150 CUT TO SUIT SUMP UNIT

FOR CONSTRUCTION

SECTION THROUGH FPMH.03 (PCC CHAMBER) SCALE: 1:20 @ A1



	<ol> <li>NOTES:</li> <li>All dimensions must be checked on site and not scaled from this drawing.</li> <li>The Contractor shall make a survey of the site and shall be responsible for obtaining all dimensions and levels necessary for the proper fabrication of the structure as indicated.</li> <li>All levels shown on this drawing are relative to Agreed Topographic survey</li> <li>This drawing is to be read in conjunction with 29348/100 Series Drawings.</li> <li>All existing invert levels are to be confirmed by contractor prior to construction. Connection subject to approval.</li> </ol>
225ø INFLOW 225ø INFLOW 5 DUG 800	
	C03       10/09/24       ISSUED FORCONSTRUCTION       WP       JrtC         C02       03/09/24       ISSUED FOR FINAL APPROVAL       WP       JrtC         C01       15/08/24       ISSUED FOR FINAL APPROVAL       WP       JrtC         Rev       Date       Description       DR       CH         C       copyright       Constructionline       Rev       Dread       CONSULTING ENGINEERS         Intertek       ON       ON       CONSULTING ENGINEERS       ARCHITECTS         Intertek       ON       PROJECT MANAGEMENT       2       Hallam Road         Priory Park East       HULL       HU4 7DY       United Kingdom         Telephone(+44) 01482 627963       Fax (+44) 01482 627963       Fax (+44) 01482 641736
	Client Job Title AD Plant. Horse Close Green Power
	Drainage Details Sheet 3
	Status FOR CONSTRUCTION Scale AS NOTED @ A1 Date SEP' '23
	Drawn By MK Checked JHC Approved JHC
FOR CONSTRUCTION	Drg. No. Rev 29348/C1/111 C03



	<ol> <li>NOTES:-</li> <li>All dimensions must be checked on site and not scaled from this drawing.</li> <li>The Contractor shall make a survey of the site and shall be responsible for obtaining all dimensions and levels necessary for the proper fabrication of the structure as indicated.</li> <li>All levels shown on this drawing are relative to Agreed Topographic survey</li> <li>This drawing is to be read in conjunction with 29348/100 Series Drawings.</li> <li>All existing invert levels are to be confirmed by contractor prior to construction. Connection subject to approval.</li> </ol>
	C03       20/09/24       ISSUED FOR CONSTRUCTION       WP       Jrtc         C02       10/09/24       ISSUED FOR CONSTRUCTION       WP       Jrtc         C01       03/09/24       ISSUED FOR FINAL APPROVAL       WP       Jrtc         Rev       Date       Description       DR       CH         © copyright       Constructionline       Constructionline       Constructionline       Constructionline         Image: Construction       Image: Constructionline       Constructionline       Constructionline       Constructionline
	Job Title AD Plant. Horse Close Green Power
	<sup>Drawing Title</sup> Drainage Details Sheet 4
	<sup>Status</sup> FINAL APPROVAL
	Scale AS NOTED @ A1 Date SEP' 23
	Drawn By WB Checked JHC Approved JHC
FOR CONSTRUCTION	Drg. No. Rev 29348/C1/112 C03



# **APPENDIX VII**

Drainage Schematic Plan

