



**MYTILINEOS**

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Project:  <b>CORBY ENERGY-FROM-WASTE (EFW)</b>
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Title:  <b>Geotechnical Ground Investigation and Interpretive Report</b>
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Document No:	<b>112101-00-YC-CDO-DS-001</b>	Revision: <b>01</b>
Issuer Document No:		
Purpose of issue: For Information		Date: 18-03-2022

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Approved: Simon Steele  
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# Geotechnical Ground Investigation and Interpretive Report

Corby EfW

Presented to: **Mytilineos**

Issued: March 2022

Delta-Simons Project No: 15-0645.05




**Protecting people  
and planet**



## Report Details

<b>Client</b>	Mytilineos
<b>Report Title</b>	Geotechnical Ground Investigation and Interpretative Report
<b>Site Address</b>	Corby EfW, Shelton Road, Willowbrook East Industrial Estate, Corby NN17 5XH
<b>Report No.</b>	15-0645.05_REP_Corby_GGI_20220314
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## Quality Assurance

Issue No.	Status	Issue Date	Comments	Author	Technical Review	Authorised
01	Draft for Comment	14/03/2022				
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## About Us

Delta-Simons is a trusted, multidisciplinary environmental consultancy, focused on delivering the best possible project outcomes for customers. Specialising in Environment, Health & Safety and Sustainability, Delta-Simons provide support and advice within the property development, asset management, corporate and industrial markets. Operating from across the UK we employ over 180 environmental professionals, bringing experience from across the private consultancy and public sector markets.

As part of Lucion Services, our combined team of 500 in the UK has a range of specialist skill sets in over 50 environmental consultancy specialisms including asbestos, hazardous materials, ecology, air and water services, geo-environmental and sustainability amongst others.



Delta-Simons is proud to be a founder member of the Inogen Environmental Alliance, enabling us to efficiently deliver customer projects worldwide by calling upon over 5000 resources in our global network of consultants, each committed to providing superior EH&S and sustainability consulting expertise to our customers. Through Inogen we can offer our Clients more consultants, with more expertise in more countries than traditional multinational consultancy.

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## Executive Summary

<p><b>Brief</b></p>	<p>Delta-Simons Limited (“Delta-Simons”) was instructed by Mytilineos (the “Client”) to undertake a Geotechnical Ground Investigation for Corby EfW, Shelton Road, Willowbrook East Industrial Estate, Corby, NN17 5XH (the “Site”).</p> <p>The Site is to be redeveloped for a single-line energy from waste (EfW) plant.</p> <p>Mytilineos request that the aim of the geotechnical investigation is:</p> <ul style="list-style-type: none"> <li>• “To obtain an accurate picture of the geometry of the geological and tectonic elements of the background</li> <li>• To identify the stratigraphy of the ground, the geotechnical design parameters of each layer and provide guidelines for the development of the New EfW facility.”</li> </ul>
<p><b>Site Setting</b></p>	<p>The Site is 2.53Ha of a previously restored quarry and is currently a flat area covered by roadways and gravel surfaced parking bays, used for open storage of cars. A landscaped strip was noted to run along the northern and eastern edges of the Site. The Site was part of a wider area used for storage of cars. It is understood that the Site is to be developed for a new single line Energy from Waste (EfW) Facility.</p>
<p><b>Ground Conditions</b></p>	<p>The geological ground model can be summarised as Made Ground of varying thickness underlain by the Northampton Sand Formation. The Northampton Sand Formation being of variable thickness.</p> <p>Underlying the Northampton Sand Formation or the Made Ground where the Northampton Sand Formation isn’t present is the Whitby Mudstone Formation. The Whitby Mudstone Formation had a Limestone band on its upper boundary of varying thickness.</p> <p>Groundwater levels during monitoring are highly variable and indicate perched water within the Made Ground across the site.</p>
<p><b>Geotechnical Assessment</b></p>	<p>The Made Ground is considered to be too variable, weak and compressible in its existing condition for conventional shallow foundations at the Site.</p> <p>As such alternative foundation solutions, including Ground Improvement Techniques or Piling should be explored in consultation with appropriately experienced contractors.</p> <p>Ground bearing floor slabs are not considered appropriate for the site given the Made Ground present at founding depth.</p> <p>It is recommended that a conservative CBR value of 5% should be adopted for the shallow Made Ground, for preliminary pavement design for external areas.</p> <p>Geotechnical and Geochemical testing is still on going for this project. The above conclusions are subject to change upon receipt of final laboratory testing results.</p>
<p><b>Data Gaps and Uncertainty</b></p>	<ul style="list-style-type: none"> <li>• The investigation scope and geotechnical assessment provided are specific to the Energy from Waste development anticipated, and may not be relevant for other development schemes should these be considered in the future.</li> <li>• The scope of investigation was specified by the Client.</li> <li>• Schedule of geotechnical testing was specified by the Client.</li> <li>• No proposed loadings provided by the Client/engineer.</li> </ul>
<p><b>This is intended as a summary only. Further detail and the limitations of the assessment are provided within the main body of the Report.</b></p>	

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Appendix B - Borehole Logs & SPT Calibrations Certificate

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Appendix E - Geotechnical Analysis Results

Appendix F - Field Monitoring Data/Gas Monitoring Data/Soakaway Testing

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# 1.0 Introduction

## 1.1 Appointment

Delta-Simons Environmental Consultants Limited ("Delta-Simons") was instructed by Mytilineos (the "Client") to undertake a Geotechnical Ground Investigation at Corby EfW, Shelton Road, Willowbrook East Industrial Estate, Corby, NN17 5XH (the "Site").

## 1.2 Context & Purpose

The Site is to be redeveloped for a single-line energy from waste (EfW) plant.

Mytilineos request that the aim of the geotechnical investigation is:

- "To obtain an accurate picture of the geometry of the geological and tectonic elements of the background
- To identify the stratigraphy of the ground, the geotechnical design parameters of each layer and provide guidelines for the development of the New EfW facility."

## 1.3 Scope of Works

The project was undertaken to an agreed brief as set out in Delta-Simons' proposal (reference 15-0645.05, dated 18<sup>th</sup> January 2022).

The detailed scope of works is outlined in Section 3.

Specific sections of this Report may generally follow guidance set out in Eurocode 7 for a Ground Investigation Report (GIR), as defined in BS EN 1997-1:2004 and BS EN 1997-2:2007. Eurocode 7 includes specific guidance on the number and spacing of investigation positions, methods of investigation and sample quality to be achieved which may not have been met by this investigation. The Report also includes information which may support a Geotechnical Design Report (GDR) as defined in BS EN 1997-1:2004; however, unless otherwise explicitly stated, the investigation has not been undertaken in accordance with Eurocode 7 and the preliminary geotechnical interpretation, assessments, risk register (if included) and recommendations presented within this Report may not meet the full requirements of a GDR.

## 1.4 Proposed Development

The Site is 2.53Ha of a previously restored quarry and is currently a flat area covered by roadways and gravel surfaced parking bays, used for open storage of cars. A landscaped strip was noted to run along the northern and eastern edges of the Site. The Site was part of a wider area used for storage of cars. It is understood that the Site is to be developed for a new single line Energy from Waste (EfW) Facility.

The proposed site layout plan is included as Drawing 1 (ref: 112101-00-YF-GDA-SNL-001-REV0C).

## 1.5 Existing Information

This Report must be considered in the context of the previous Reports undertaken by Delta-Simons for which the Client has reliance:

- Environmental and Geotechnical Site Assessment, Proposed Site for Gasification Plant, Shelton, Road, Willowbrook East Industrial Estate, Corby, NN17 5XH, Clean Power Properties Ltd., Delta-Simons Project No. 15-0645.02, Issued: December 2015.

## 1.6 Limitations

The assessment is limited to the issues agreed within the proposal for the works. General notes on limitations associated with this assessment are provided in Appendix A.

## 1.7 Data Gaps and Uncertainty

In addition, the following specific data gaps and uncertainty apply to this assessment:

- The investigation scope and geotechnical assessment provided are specific to the Energy from Waste development anticipated, and may not be relevant for other development schemes should these be considered in the future.
- The scope of investigation was specified by the Client.
- Schedule of geotechnical testing was specified by the Client.
- No proposed loadings were provided by the Client/engineer.

## 2.0 Site Details

### 2.1 Site Setting

A summary of the current Site status, environmental setting and key historical features is presented below. This has been summarised from the existing Report(s) listed in Section 1.5 which should be consulted for further detail.

<b>Co-ordinates</b>	Centred approximately at National Grid Reference 490989, 290880.	Elevation	105 m AOD
		Area	2.53 Ha
<b>Site Address and Location</b>	<p>Shelton Road, Willowbrook East Industrial Estate, Corby, NN17 5XH.</p> <p>The Site is located to the west of Shelton Road in the Willowbrook East Industrial Estate, 3 km north-east of Corby town centre, with an area of approximately 2.53 Ha. A Site location map is provided as Figure 1.</p> <p><a href="#">Google Maps Link</a></p>		
<b>Current Site Description</b>	<p>The Site currently comprises a flat area covered by roadways and gravel surfaced parking bays, used for open storage of cars. A landscaped strip was noted to run along the northern and eastern edges of the Site.</p>		
<b>Physical Setting</b>	<p>The site is relatively flat with a slight downward slope from north to south. The site was formerly an opencast ironstone mine, as such, the site is underlain by approximately 16 to 21m of Made Ground over the bedrock geology of the Northampton Sand Formation overlying the Whitby Mudstone Formation. Given the mining on site the majority of the Northampton Sand Formation is understood to have been removed.</p> <p>The Northampton Sand Formation is classified as a Secondary A Aquifer and the site is not within a groundwater Source Protection Zone (SPZ).</p> <p>The environmental sensitivity of the Site setting is considered to be low to moderate given the proximity of the Willow Brook North Arm watercourse to the northern Site boundary, the significant thickness of low permeability reworked soils, the designation of the bedrock as a Secondary A aquifer, and the lack of proximate ground and surface water abstractions.</p>		
<b>Key Historical Features</b>	<p>Historically the Site has been associated with opencast ironstone mining and backfilling with steelworks wastes and reworked overburden materials, prior to surface remediation works carried out in 2001-2002 for construction of the current vehicle storage area.</p>		
<b>Summary of Previous /Third Party Reports</b>	<p>Delta Simons undertook an Environmental and Geotechnical Assessment of the site in December 2015. The findings of this are summarised below.</p> <p>A ground investigation comprising the following:</p> <ul style="list-style-type: none"> <li>• 20No. dynamic sampler boreholes (DS101 to 119) to a maximum depth of 3.0 m bgl;</li> <li>• 10No. cable percussion boreholes (BH101 to BH110) to a maximum depth of 20.45 m bgl;</li> <li>• Four rotary boreholes (BHR1 to BHR4) to a maximum depth of 30.0 m bgl;</li> </ul>		

- Installation of 19 boreholes with 50 mm internal diameter gas and groundwater monitoring wells;
- Standard penetration tests (SPTs) were undertaken throughout the boreholes, along with environmental and geotechnical sampling;
- Ten Cone Penetrometer Tests (CPTs) to a maximum depth of 25.15 m bgl;
- Collection of groundwater samples and undertaking four rounds of gas and groundwater level monitoring.

Encountered ground conditions comprised a thin layer of granite aggregate and topsoil, topsoil or asphalt hardstanding at each intrusive location. Made Ground (Fill) was encountered in each borehole location advanced and generally comprised greyish black/brown and greenish brown, slightly silty/sandy/gravelly clays with variable layers of pseudo-fibrous and fibrous peat. Gravels generally consisted of fine to coarse sandstone and chalk. Fill material with encountered to a maximum depth of 20.5 m bgl.

The underlying Northampton Sand Formation, consisting of strong, massive orangey brown sandstone was encountered in boreholes R1, R3 and R4 and BH109. The Northampton Sand Formation was not present in all locations drilled indicating this had been potentially extracted to its full depth in parts of the Site. Underlying the fill, or Northampton Sand Formation, were deposits of the Whitby Mudstone Formation comprising, weak, dark grey, slightly weathered, laminated mudstone and was proven to a maximum depth of 29.8 m bgl.

Resting groundwater levels recorded during the return monitoring visits were between 0.10 m bgl and 20.33 m bgl.

The chemical analysis undertaken on selected soil samples did not identify widespread significantly elevated concentrations of contamination in the tested locations.

Groundwater chemical analysis results indicate only slightly elevated concentrations of boron and selenium, limited to the rotary borehole R4. Slightly elevated concentrations of Mercury were identified in six of the locations sampled. These exceedances were not considered significant as the Site is not located within a Source Protection Zone.

Ground gas monitoring indicated low level gas flow rates and slightly elevated concentrations of methane and carbon dioxide giving the Site a Characterisation Situation 2 (CS2 - Low Risk). Basic ground gas protection measures was recommended for the development.

From a geotechnical standpoint the following conclusions were given:

- Made Ground Fill material was considered to be too soft, variable, compressible and unpredictable in its existing condition for conventional shallow foundations at the Site given the expected large design loads.
- A piled foundation solution using bored piles transferring loads to competent bedrock geology encountered at depth was likely to be suitable for the expected design loads.
- It was considered that ground improvement techniques may not be appropriate for the expected design loads given the depth of Made Ground Fill encountered beneath the Site;
- Due to significant thickness of Made Ground, soils are considered too variable and unpredictable in its existing state for ground bearing floor slabs;



	<ul style="list-style-type: none"><li>• The use of soakaways as a form of drainage was not recommended for the Site given the depth of Made Ground encountered; and</li><li>• The conditions of the soils at the Site would be classified as Design Sulphate Class DS-4 and ACEC Class AC-4 for soils and groundwater.</li></ul>
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## 3.0 Ground Investigation

### 3.1 Intrusive Investigation

Delta-Simons carried out intrusive investigation work from 3<sup>rd</sup> February to 1<sup>st</sup> March 2022 to provide additional geotechnical information.

### 3.2 Ground Investigation and Rationale

#### 3.2.1 Intrusive Works

The ground investigation comprised the following items:

- Service avoidance exercise and topographic survey of exploratory holes to x,y,z co-ordinates;
- Supervision of all works by a Delta-Simons Geo-Environmental engineer. All intrusive locations were logged to BS 5930:2015+A1:2020 Code of Practice for Ground Investigations;
- Drilling of thirteen cable percussive boreholes with rotary drilled follow on (BH1 to BH13) to a maximum depth of 30 m bgl;
- Excavation of five trial pits (TR-1 to TR-5) to a maximum depth of 3.00 m bgl. The trial pits were installed with a gravel pack and monitoring pipes to facilitate soakaway testing in accordance with BRE365;
- Undertaking of 12 Static Piezocone Penetration Tests (CPT01 to CPT12A) to a maximum depth of 23.29m bgl;
- Undertaking of one Seismic Dilatometer Marchetti Test (SCPT) to a maximum depth of 29.02m bgl;
- Undertaking of five soil resistivity tests (R1 to R5).

An intrusive exploratory hole location plan is presented as Figure 2.

Specific limitations affecting the proposed scope of works are summarised in Section 1.7.

Delta-Simons exploratory hole engineer verified borehole logs are presented as Appendix B together with the SPT Calibration Certificates, in accordance with BS EN ISO 22476-3:2005+A1:2011 (incorporating corrigendum No. 1 2007), Geotechnical investigation and testing - Field testing - Part 3: Standard penetration test for SPT trip hammers.

#### 3.2.2 Rationale

The exploratory hole positions were spread across the Site to provide site wide coverage with the exact location specified by the Client, to meet their requirements.

### 3.3 Geotechnical Sampling and In-Situ Testing

#### 3.3.1 Sampling

Sampling comprised disturbed jar/tab and bulk samples as well as undisturbed U100/ UT100 samples collected where possible in cohesive soil and core sampling and sub-sampling, details on the samples collected are available on the borehole logs (Appendix B).

#### 3.3.2 In-Situ Tests

SPT tests were undertaken in all boreholes at 1.00 m intervals until 5.00 m bgl, then every 1.5 m bgl thereafter until bedrock was encountered. The results of these tests are presented on the borehole logs included as Appendix B. A plot of Corrected SPT N values versus Depth is included as Figure 3.

Hand Shear Vanes (HSV) were undertaken at regular intervals in cohesive soils within the trial pits. The tests were undertaken in accordance with the procedure detailed in Delta-Simons' Standard Operating Procedure on disturbed samples of clay which had been excavated from the trial pits.

In-situ Cone Penetrometer Tests (CPT) were undertaken using a wheeled 14 tonne rig to hydraulically ram a cone penetrometer into the ground continuously using a series of steel rods. A piezocone was used to collect data from which soil parameters have been derived. The CPT Report is included in Appendix C.

Soil resistivity testing was undertaken in five locations across the site using vertical electrical sounding (4-pin testing) in accordance with the specification IEEE std 81-2012. The Geophysical Survey Report is included in Appendix D.

### 3.3.3 Soakaway Tests

Soakage testing was undertaken in 5 locations (TR1 to TR5) in accordance with BRE Digest 365 Soakaway Design (2016) to derive soil infiltration rates for use in soakaway design. The results from these tests are presented in Appendix F.

## 3.4 Geotechnical Laboratory Testing

A selection of soil and rock samples were submitted to the UKAS accredited laboratory for a range of geotechnical testing, the results of which are included in Appendix E. The number and type of testing was schedule by the Client. At the time of writing, laboratory testing is still on going and the final number of samples tested is subject to their completion.

Laboratory Test	Test Standard	Number of Samples Tested
<b>Classification</b>		
Water Content	BS1377-2:3 or BS EN ISO 17892-1	37
Liquid and Plastic Limits	BS1377-2:4 - 5 or BS EN ISO 17892-12	37
Particle Size Analysis and sedimentation	BS1377-2:9.2 & 9.3 or BS EN ISO 17892-4	24
Particle Density	BS1377-2:8 or BS EN ISO 17892-3	5
<b>Compaction</b>		
Water Content / Dry Density Relationship Testing (2.5 kg, 4.5 kg or vibrating hammer)	BS1377-4:3	5
<b>Pavement Design</b>		
Remoulded California Bearing Ratio (CBR) at Optimum Moisture Content	BS1377-4:7	5
<b>Soil Strength</b>		
Quick Undrained Triaxial (multi-stage)	BS1377-7:8 or BS EN ISO 17892-8	46
<b>Deformation</b>		
Oedometer Consolidation	BS1377-5:3 or BS EN ISO 17892-5	14
<b>Rock Testing</b>		
Point Load Test	ISRM 2007	40
Uniaxial Compressive Strength	ISRM 2007	42
<b>Geo-Chemical - Soil Samples</b>		
pH	BRE Special Digest 1 or other	25
Water-Soluble Sulphate (2:1 water/soil extract)	BRE Special Digest 1 or other	25
Acid Soluble Sulphate	BRE Special Digest 1 or other	25
Total Sulphur	BRE Special Digest 1 or other	25
Magnesium (2:1 water/soil extract)	BRE Special Digest 1 or other	25

Laboratory Test	Test Standard	Number of Samples Tested
Nitrate (2:1 water/soil extract)	BRE Special Digest 1 or other	25
Chloride (2:1 water/soil extract)	BRE Special Digest 1 or other	25
Organic Matter	BRE Special Digest 1 or other	23
<b>Geo-Chemical - Water Samples</b>		
pH	BRE Special Digest 1 or other	2
Soluble Sulphate	BRE Special Digest 1 or other	2
Soluble Magnesium	BRE Special Digest 1 or other	2
Nitrate Ion	BRE Special Digest 1 or other	2
Chloride Ion	BRE Special Digest 1 or other	2
Aggressive Carbon Dioxide	BRE Special Digest 1 or other	2

### 3.5 Monitoring Programme

One round of groundwater level and ground gas monitoring was undertaken on serviceable historical wells (BH103, BH106, DS104, DS107, DS107a, DS109, DS113 and DS116 to DS118) on the 23<sup>rd</sup> February 2022.

Two rounds of groundwater level and ground gas monitoring were undertaken on newly installed wells (BH1, BH2, BH7, BH10, BH12 and BH13) between 3<sup>rd</sup> and 9<sup>th</sup> March 2022.

Measurements of the depth to groundwater within the monitoring wells were taken using an electronic dip meter.

To characterise the ground gas regime at the Site, an infrared gas meter was used to measure gas flow, concentrations of carbon dioxide (CO<sub>2</sub>), methane (CH<sub>4</sub>) and oxygen (O<sub>2</sub>) in percentage by volume. Initial and steady state concentrations were recorded. The atmospheric pressure before and during monitoring, together with the weather conditions, was recorded.

All monitoring results obtained to date are contained within Appendix F.

## 4.0 Ground Summary

### 4.1 Introduction

The sections below summarise the ground and groundwater conditions encountered during the Site investigation in December 2015 and February 2022.

### 4.2 Ground Summary

A summary of the observed ground conditions at the Site is provided below and should be read in conjunction with the exploratory hole logs. A contour plot showing the base of the Made Ground is provided as Figure 4a and Figure 4b which shows indicative depths based on the investigation undertaken and existing Site elevations.

Strata	Typical Strata Description	Depth Range of Strata Top (m)	Depth Range of Strata Base (m)	Thickness Range (m)	Comments
Made Ground	Dark grey sandy gravelly clay with organic material. Gravel is generally angular to rounded of sandstone, brick, concrete, chalk and flint. Sand is fine to coarse.	<i>Ground Level</i>	<i>15.50 to 19.50</i>	<i>15.50 to 19.50</i>	
Northampton Sand Formation	Reddish brown sandstone, generally recovered as angular to subangular fine to coarse gravel.	<i>15.50 to 20.50</i>	<i>18.00 to 22.75</i>	<i>0.10 to 3.50</i>	<i>Only encountered in BH3, BH6, BH8, BH11, BH109, BHR1, BHR3 &amp; BHR4</i>
Whitby Mudstone Formation	Very weak to weak thinly laminated Mudstone with an upper layer of weak to medium strength grey Limestone.	<i>15.70 to 22.75</i>	<i>Proven to a maximum depth of 30.00m bgl</i>	<i>Not Proven</i>	

The geological ground model can be summarised as Made Ground of varying thickness (15.50 to 19.50m) underlain by the Northampton Sand Formation in 8 locations. The Northampton Sand Formation being of variable thickness between 0.10 and 3.50.

Underlying Northampton Sand Formation or the Made Ground where the Northampton Sand Formation isn't present is the Whitby Mudstone Formation, to a proven depth of 30.00m bgl. The Whitby Mudstone Formation had a Limestone band on its upper boundary of varying thickness.

### 4.3 Groundwater

#### 4.3.1 Strikes During Investigations

No groundwater strikes were encountered during the ground investigation.

### 4.3.2 Levels During Monitoring Programme

Groundwater levels were monitored on a total of four occasions between 7<sup>th</sup> September and 29<sup>th</sup> September 2015 as part of the initial ground investigation and are summarised in the table below.

Exploratory Hole	Water level during monitoring Max to Min Range		Stratum
	m bgl	m AOD.	
BHR1	14.80 to 15.96	91.034 to 89.874	Whitby Mudstone Formation
BHR2	18.48 to 20.33	87.023 to 85.173	Whitby Mudstone Formation
BHR3	18.39 to 16.66	86.173 to 85.908	Northampton Sand Formation and Whitby Mudstone Formation
BHR4	16.57 to 18.71	87.216 to 87.547	Northampton Sand Formation and Whitby Mudstone Formation
BH101	14.35 to 16.63	92.848 to 91.568	Made Ground
BH102	14.37 to 14.68	92.174 to 91.864	Made Ground
BH104	18.44 to 18.91	87.216 to 86.746	Made Ground
DS101	0.46 to 1.14	103.2772 to 103.092	Made Ground
DS104	0.40 to 0.44	104.555 to 104.515	Made Ground
DS105	0.13 to 0.31	104.359 to 104.179	Made Ground
DS107	0.16 to 0.71	105.620 to 105.070	Made Ground
DS107a	0.33 to 0.80	105.221 to 104.751	Made Ground
DS109	0.91 to 2.25	104.411 to 103.071	Made Ground
DS113	0.12 to 0.36	106.430 to 106.190	Made Ground
DS114	0.13 to 0.72	105.628 to 105.038	Made Ground
DS116	0.12 to 0.73	105.425 to 104.815	Made Ground
DS117	0.10 to 1.82	106.297 to 104.577	Made Ground
DS118	0.29 to 0.96	106.898 to 106.608	Made Ground

Groundwater levels within historical wells were monitored on one occasion on the 23<sup>rd</sup> February 2022 and within the new boreholes on a total of two occasions between 3<sup>rd</sup> and 9<sup>th</sup> March 2022 as part of the recent ground investigation. Monitoring data measurements are provided in Appendix F and summarised in the table below.

Exploratory Hole	Water level during monitoring Max to Min Range		Stratum
	m bgl	m AOD.	
BH103	17.60	88.18	Made Ground
BH106	16.96	88.74	Made Ground
DS104	0.20	104.24	Made Ground
DS107	0.22	105.56	Made Ground
DS107a	0.00	105.55	Made Ground
DS109	0.97	104.35	Made Ground
DS113	0.90	105.62	Made Ground

Exploratory Hole	Water level during monitoring Max to Min Range		Stratum
	m bgl	m AOD.	
DS116	0.00	105.54	Made Ground
DS117	0.62	105.78	Made Ground
DS118	0.00	106.90	Made Ground
BH1	14.97	90.29	Made Ground
BH2	17.69 to 17.87	87.61 to 87.79	Made Ground
BH7	14.99 to 15.02	91.22 to 91.25	Made Ground
BH10	0.75 to 5.72	99.92 to 104.89	Made Ground
BH12	13.23 to 13.95	90.52 to 91.24	Made Ground
BH13	12.63 to 13.04	93.64 to 94.05	Made Ground

Groundwater levels during monitoring are highly variable and indicate perched water within the Made Ground across the site.

#### 4.4 Visual and Olfactory Evidence of Contamination

No visual or olfactory evidence of potential gross contamination was observed during the investigation.

#### 4.5 Material Properties

The table below summarises the factual material properties based upon the results of in-situ and laboratory test data and where appropriate provides derived geotechnical parameters.

At the time of reporting not all laboratory data has been received.

Parameter	Unit	Range	Justification
<b>Made Ground</b>			
w (Water Content)	%	13 to 64	Laboratory Testing
IP (Plasticity Index)	-	13 to 54	Laboratory Testing
PL (Plastic Limit)	%	14 to 46	Laboratory Testing
LL (Liquid Limit)	%	27 to 89	Laboratory Testing
Volume Change Potential	-	Low to High	NHBC
CU (Uniformity coefficient)	-	>7.4 to >79	Laboratory Testing
Corrected SPT 'N60'	-	5 to 54	SPT N values corrected for energy ration (Er) after BS EN ISO 22476-3:2005. Er stated on borehole logs.
$\gamma$ (Bulk Density)	Mg/m <sup>3</sup>	1.98 to 2.14	Laboratory Testing
$\gamma_d$ (Dry Density)	Mg/m <sup>3</sup>	1.60 to 1.86	Laboratory Testing
cu (Undrained Shear Strength)	kPa	5 to 285	Laboratory Testing and Inferred from PI and N-Value after Stroud (1975)
mv (Coefficient of Volume of Compressibility)	m <sup>2</sup> /MN	0.087 to 0.171	Laboratory Testing
E' (Drained Elastic Modulus)	MPa	0.6 to 37	Laboratory Testing

Parameter	Unit	Range	Justification
$\gamma_{max}$ (Maximum Dry Density) 2.5kg	Mg/m <sup>3</sup>	1.78 to 1.83	Laboratory Testing
OMC (Optimum Moisture Content)	%	13 to 15	Laboratory Testing
NMC (Natural Moisture Content)	%	19 to 21	Laboratory Testing
Hand Shear Vane at OMC	kPa	42 to 100	In-Situ Testing
CBR at OMC	%	17 to 23	Laboratory Testing
<b>Northampton Sand Formation</b>			
Point Load Testing Is(50)	MPa	0.2	Laboratory Testing
<b>Whitby Mudstone Formation</b>			
w (Water Content)	%	9 to 20	Laboratory Testing
IP (Plasticity Index)	-	25 to 32	Laboratory Testing
PL (Plastic Limit)	%	23 to 28	Laboratory Testing
LL (Liquid Limit)	%	48 to 60	Laboratory Testing
Volume Change Potential	-	Medium	NHBC
Corrected SPT 'N60'	-	22 to 62	SPT N values corrected for energy ration (Er) after BS EN ISO 22476-3:2005. Er stated on borehole logs.
$\gamma$ (Bulk Density)	Mg/m <sup>3</sup>	2.10 to 2.41	Laboratory Testing
$\gamma_d$ (Dry Density)	Mg/m <sup>3</sup>	1.70 to 2.32	Laboratory Testing
Point Load Testing Is(50)	MPa	0.28 to 1.35	Laboratory Testing
Unconfined Compressive Strength Testing (UCS)	kPa	162 to 14400	Laboratory Testing

A plot of corrected SPT N value versus depth per strata is presented as Figure 3. A plot of undrained shear strength versus depth per strata is presented as Figure 5. A plasticity chart is presented as Figure 6.

#### 4.6 Geochemical Testing

Geochemical analysis was scheduled on soil samples from the Made Ground tested for selective contaminants (BRE Special Digest 1:2005 (3rd Edition), Concrete in Aggressive Ground and organic content. At the time of this report, these tests are still in process and this section will be updated upon their receipt.



## 5.0 Geotechnical Assessment

### 5.1 Introduction

#### 5.1.1 Summary of Development Proposals

The Site is 2.53Ha of a previously restored quarry and is currently a flat area covered by roadways and gravel surfaced parking bays, used for open storage of cars. A landscaped strip was noted to run along the northern and eastern edges of the Site. The Site was part of a wider area used for storage of cars. It is understood that the Site is to be developed for a new single line Energy from Waste (EfW) Facility.

At the time of writing, structural and floor loadings and final levels were unknown. Consequently, the information provided below should be treated as preliminary and will be subject to review once a scheme and levels have been finalised, and further detailed assessment and design may be required.

#### 5.1.2 Preliminary Geotechnical Hazards

The geohazards listed below have been identified to follow guidance presented in the HE document CD622 'Managing Geotechnical Risk' (2020) which aims to identify and manage the geotechnical risks associated with a scheme throughout its lifespan, from planning to construction to maintenance.

The following geohazards are considered to be substantial ground related risks associated with the proposed development. A substantial risk is defined by Delta-Simons in Appendix G.

- Made Ground: - The investigation at the Site has demonstrated the Made Ground to be of significant thickness and variable in nature. SPT results have suggested potentially low bearing capacity and, therefore, unacceptable levels of total/differential settlement may occur;
- Compressible / soft ground in the shallow soils (>5m bgl): - Low SPT results have been encountered in the Made Ground. Organic material was also encountered;
- Variable depths to bedrock - given the nature of the site being an infilled quarry, the depth to the top of bedrock varies across the site; and
- Perched groundwater: - Whilst groundwater was not encountered during intrusive investigations monitoring has indicated variable depths to groundwater. Excavations may require groundwater control measures.

#### 5.1.3 Ground Model and Characteristic Ground Parameters

At the time of this report, geotechnical testing was still on going. The ground model and characteristic ground parameters will be prepared once testing is complete.

### 5.2 Earthworks

At the time of writing, details on finished levels are unavailable, although it is anticipated to be at similar level to the current site. Whilst no significant cut and full operation is anticipated some degree of earthworks will be required as part of the proposed development.

Shallow earthworks on the Site will predominantly encounter Made Ground. The suitability of these materials for re-use has been preliminary assessed on the basis of the compaction testing carried out as part of this investigation.

Compaction test results indicate that the natural moisture content may typically be wet of the optimum moisture content (OMC) - therefore modification to these materials maybe required. Also based on their description the material may not be suitable for re-use as engineered fill without modification or consideration of significant organic content encountered in places.

Any Materials used as fill will need to be placed to a suitable engineering specification with the degree of compaction required will be dependent on end usage and serviceability criteria. Uplift in areas where vibro replacement is to be used should comprise granular fill placed loosely, or with nominal compaction.

Unprotected stockpiled materials often deteriorate due to water infiltration and they may become unsuitable for incorporation in the works. In particular, cohesive soils are very susceptible to 'wet

weathering working' and we strongly recommend that consideration should be given to lime and/or cement stabilisation of these materials if the earthworks are undertaken during inclement weather or the winter period.

A suitably detailed earthworks specification for the works should be produced prior to undertaking any earthworks.

## 5.3 Foundations

### 5.3.1 Spread Foundations

The Made Ground is considered to be highly variable, weak and compressible in its existing condition for conventional shallow foundations at the Site.

As such, it is considered that the adoption of traditional shallow foundations will not be feasible on the site unless ground improvement is undertaken.

### 5.3.2 Ground Improvement Techniques

A piled foundation solution will be suitable for the main proposed structures on site. However, for small lightly loaded ancillary buildings and external areas, ground improvement could be employed to densify soils to achieve suitable allowable bearing pressures and reduce the potential for differential settlement beneath traditional foundations and ground bearing floor slabs. Any ground improvement would need to encapsulate the pressure bulb of the proposed foundation.

Suggested ground improvement options include Vibro Concrete Columns (VCCs), rigid inclusions and soil mixing. Vibro Stone Columns are not considered appropriate due to the potential issues with hole stability due to low strength soils, and also the possible creation of a gas migration pathway.

VCCs or Rigid Inclusions improve the near surface ground conditions by creating a concrete column to laterally displace or replace the near surface soils to thereby stiffening the soil mass and reducing post construction settlements. These columns would need to be installed on a closely spaced grid, within and partially beyond the footprint of the proposed structures.

It is considered that ground improvement via soil mixing in conjunction with a load transfer platform may be feasible to improve the strength characteristics of the loose / low strength shallow soils to allow the adoption of traditional foundations bearing within these strata for more lightly loaded structures. This would also reduce the potential for excessive total and/or differential settlement.

Soil mixing improves the strength characteristics of strata using a hollow stem auger, which penetrates the ground to the required depth. A cement mix is then introduced into the ground via the hollow stem and mixed with the surrounding ground to form a column of stiff soil. Soil mixing should extend to a depth sufficient to encapsulate the pressure bulb of footings from the proposed development. Should soil mixing prove suitable at the site, an appropriate grid of columns should be designed to extend just beyond the footprint of settlement sensitive structures along with the incorporation of a suitable load transfer platform. However, the presence of organic material, variable soil types and groundwater within the Made Ground may preclude this form of ground improvement.

Due to variations in installation technique, it is recommended that a ground improvement contractor be consulted to determine suitability of the ground conditions, the nature of the most suitable improvement technique, and the likely improvement which may be achieved and costs for the differing techniques. It should be noted that both soil mixing and VCC/rigid inclusions have difficulty in overcoming soils which have significant obstructions within them. Such obstructions can affect the depth of treatment and the performance of the improved soil/concrete column.

In this scenario each position may have to be pre-drilled/probed to ensure it is free from obstruction. Similarly, both techniques rely on some inherent strength within the host soil to prevent the finished soil/concrete column from "barrelling" which may result in lower column performance and onerous long-term settlements. Such issues would need to be discussed in advance of any detailed design work to ensure the proposed improvement technique is feasible given the depth of Made Ground encountered.

The precise ground improvement technique/proprietary methods, suitability of the ground, suitability of fill materials and allowable bearing capacity that can be achieved would need to be confirmed by discussions with a suitably experienced contractor; whose design should be warranted.

### 5.3.3 Piling

A piled foundation solution using traditional bored or continuous flight auger (CFA) piles transferring loads to competent geology would be suitable for the anticipated design loads, utilising both skin friction and end bearing capacity.

The precise method of pile installation and applicability of proprietary systems, diameters and depths required would need to be informed based on the results of this investigation, by discussions with a piling contractor with suitable experience, whose design should be warranted.

Normal static and dynamic load testing (including uplift tests) should be considered to achieve satisfactory quality control/assurance in accordance with good practice.

There will be a requirement for the placement of a suitably engineered piling mat, which should be designed and validated by a suitably qualified and experienced engineer.

### 5.3.4 Floor Slabs

It is considered the significant thickness of Made Ground soils are too variable and compressible in their existing state for ground bearing floor slabs. Ground bearing floor slabs are therefore not anticipated to be suitable for the proposed development unless suitable ground improvement is undertaken.

If ground improvement is not feasible to support a ground bearing floor slab solution, then suspended floor slabs would be required to prevent excessive total and differential settlement, whereby settlement beneath the slab would be controlled by the foundations of the building. Additional loads from suspended floor slabs should be taken into account when designing foundations for the proposed development.

## 5.4 Roads and Pavements

It is understood areas of hardstanding car parking and access roads will be present across the Site. Exact levels have not been decided but it is understood these are likely to be constructed similar to existing levels within the Made Ground.

Five samples of the Made Ground from depths between 0.40 and 1.30m bgl where subject to remoulded California Bearing Ratio (CBR) test within the lab. The results are presented in the table below.

Location ID	Depth (m bgl)	Optimum Moisture Content (%)	Average CBR Values
TR-1	1.30	15	23
TR-2	0.40	13	19
TR-3	1.00	14	19.5
TR-4A	0.60	15	17
TR-5	0.50	14	17

It is recommended that a conservative CBR value of 5% should be adopted for the shallow Made Ground, for preliminary pavement design for external areas. It is recommended that plate CBR tests are undertaken at formation level after site levels are determined to finalising pavement design.

## 5.5 Drainage and Soakage Tests

Soil infiltration tests were carried out in five soakage test pits in general accordance with BRE 365. The soakage test pits were targeted at the Made Ground Formation. All pits were prepared with a gravel pack and monitoring standpipe.

All soakaways failed to complete a single test within 24hrs and furthermore, Made Ground is not considered to be an acceptable soakaway stratum; as such soakaways are not considered practical for the Site.

The full results are presented in Appendix F.

## 5.6 Excavations & Obstructions

It is expected that conventional mechanical excavators will readily remove the Made Ground likely to be encountered in shallow excavations although a breaker may be required to remove any existing concrete hardstanding.

Instability of excavations in granular material should be expected, especially during periods of adverse weather. Suitable shoring measures or battering back of slopes may be required for any excavations greater than 1.20m bgl. All temporary excavations should be undertaken in accordance with CIRIA Report 97 - Trenching Practice.

## 5.7 Groundwater

Groundwater was encountered as perched water within the Made Ground at depths between ground level and 17.87 m bgl.

Shallow excavations are therefore likely to encounter groundwater. Local dewatering by sump and pump may be appropriate, however, other forms of groundwater control may need to be considered if excavations become quickly inundated. Treatment prior to disposal to sewer may also be required.

## 5.8 Chemical Attack on Buried Concrete

The previous investigation indicated a Design Sulphate Class DS-4 and ACEC Class of AC-4 for soils and groundwater.

Geochemical testing is still on going on the samples taken from the site during the latest intrusive investigation. An updated concrete classification will be provided once these test results are received.

## 6.0 Conclusions & Recommendations

### 6.1 Ground Model Summary

The geological ground model can be summarised as Made Ground of varying thickness (15.50 to 19.50m) underlain by the Northampton Sand Formation in 8 locations. The Northampton Sand Formation being of variable thickness between 0.10 and 3.50 m.

Underlying Northampton Sand Formation or the Made Ground where the Northampton Sand Formation isn't present is the Whitby Mudstone Formation, to a proven depth of 30.00m bgl. The Whitby Mudstone Formation had a Limestone band on its upper boundary of varying thickness.

Groundwater levels during monitoring are highly variable and indicate perched water within the Made Ground across the site.

### 6.2 Geotechnical Summary

The Made Ground is considered to be too variable, weak and compressible in its existing condition for conventional shallow foundations at the Site.

As such alternative foundation solutions, including Ground Improvement Techniques or Piling should be explored in consultation with appropriately experienced contractors.

Ground bearing floor slabs are not considered appropriate for the site given the Made Ground present at founding depth.

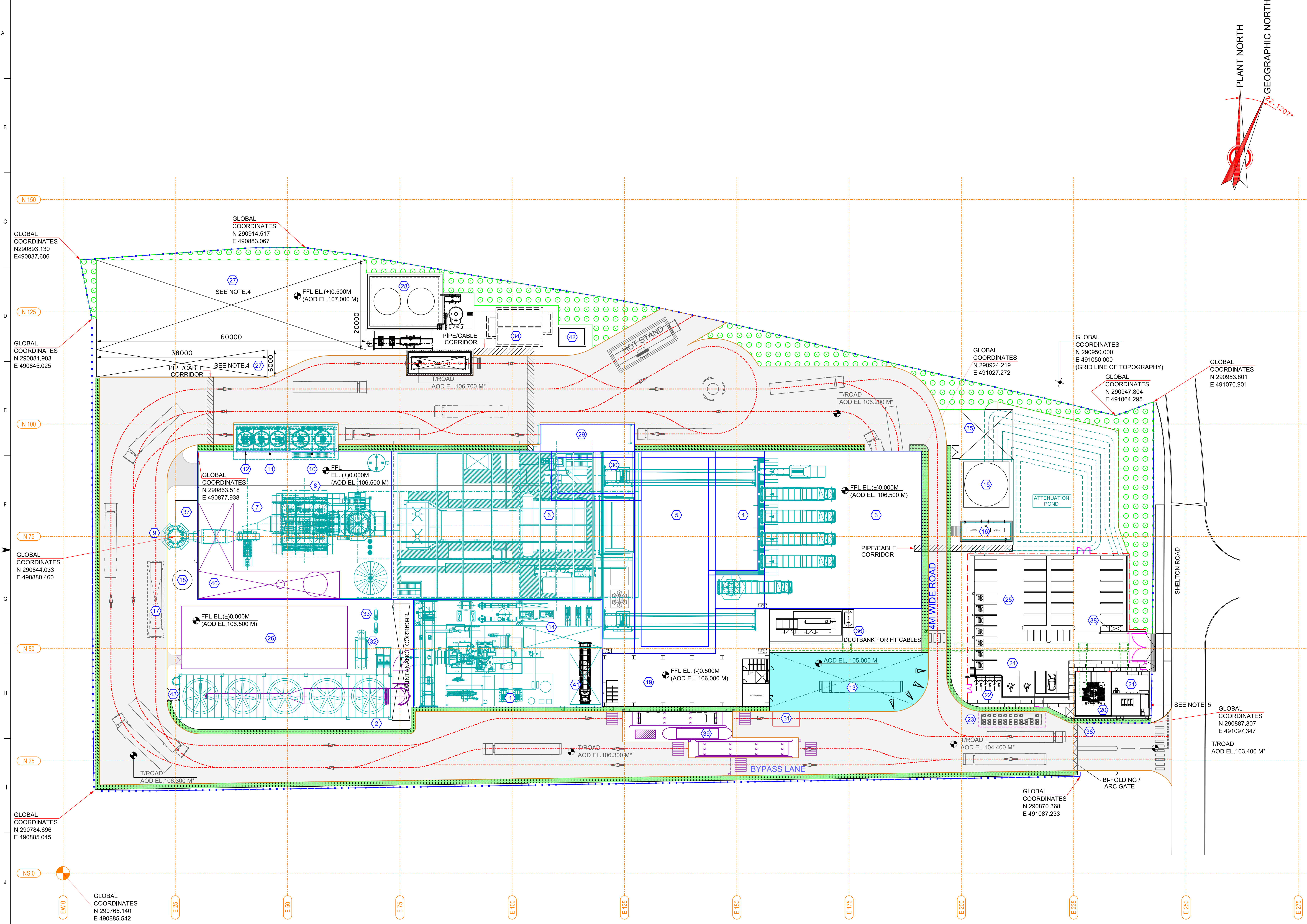
It is recommended that a conservative CBR value of 5% should be adopted for the shallow Made Ground, for preliminary pavement design for external areas.

Geotechnical and Geochemical testing is still on going for this project. The above conclusions are subject to change upon receipt of final laboratory testing results.

## Drawings

## Drawing 1 - Proposed Development Plan





EQUIPMENT LIST			
1	STEAM TURBINE HALL	28	FUEL OIL AREA
2	AIR COOLED CONDENSER	29	IBA LOADING
3	TIPPING HALL	30	IBA BUNKER
4	TIPPING BUNKER	31	TRUCK WHEEL WASHING AREA
5	MAIN WASTE BUNKER	32	ACC CONDENSATE COLLECTION TANK
6	BOILER HOUSE	33	CONDENSATE EXTRACTION PUMPS
7	FLUE GAS TREATMENT AREA	34	SETTLING BASIN
8	BAG HOUSE FILTER	35	SPACE FOR FUTURE INSTALLATION FOR DH EQUIPMENT
9	STACK	36	EMERGENCY DIESEL GENERATOR (EDG)
10	FGT RESIDUE SILOS	37	CEMS SHELTER
11	HYDRATED LIME/Ca(OH)2 SILO	38	SECURITY CABIN (2 NOS.)
12	ACTIVATED CARBON SILO	39	GATE HOUSE & WEIGHBRIDGE
13	QUARANTINE/ LAYDOWN AREA	40	WATER TREATMENT PLANT & MISCELLANEOUS TANKS
14	AUXILIARY COOLING FIN FAN COOLERS (ON THE ROOF OF STEAM TURBINE HALL)	41	AIR COMPRESSOR ROOM
15	FIRE WATER TANK	42	OILY WATER SEPARATOR
16	FIRE WATER PUMPHOUSE CONTAINER	43	ACC MOTOR DROP ZONE
17	UREA UNLOADING TRUCK AREA		
18	UREA STORAGE TANK		
19	ELECTRICAL, ADMINISTRATION & CONTROL BUILDING		
20	33 / 11KV STEP-UP TRANSFORMER		
21	ONSITE SUBSTATION		
22	CYCLE PARKING		
23	COACH DROPOFF		
24	DISABLED PARKING		
25	STAFF / VISITOR PARKING		
26	MECHANICAL MAINTENANCE WORKSHOP & STORE		
27	FUTURE ENVIRONMENTAL IMPROVEMENT AREA (2 AREAS)		

- NOTES**
- ALL DIMENSIONS ARE IN MILLIMETERS. LEVELS AND COORDINATES ARE IN METERS, UNLESS NOTED OTHERWISE.
  - ALL ELEVATIONS REFER TO EL. (+)0.000M EQUIVALENT TO (+)106.500 M ABOVE ORDNANCE DATUM (AOD).
  - LOCATION AND TYPE OF TANK SHALL BE UPDATED WITH DESIGN PROGRESS.
  - INDICATED AREA IS FOR FUTURE INSTALLATION OF THE CCS FACILITY.
  - EXTERNAL PLANT CABLES (POWER AND COMMUNICATION) CABLE SHALL INTERFACE UNDERGROUND AT SUBSTATION BUILDING.
  - EMISSION/VENT SOURCES CO-ORDINATE SHOWN IN TABLE IS TENTATIVE. SAME SHALL BE VERIFIED AFTER RECEIPT OF VENDOR INPUT.
  - \*\*\* MARKED ELEVATION WILL BE FINALIZED DURING DETAIL ENGINEERING AND SAME WILL COVERED IN SEPERATE ROAD LAYOUT.

**LEGENDS**

	SITE BOUNDARY		FFL FINISHED FLOOR LEVEL
	ROAD		FGL FINISHED GRADE LEVEL
	FIRE BARRIER WALL		T/ROAD TOP OF ROAD
	BIODIVERSITY AREA		VEHICLE TRAVEL DIRECTION
	UNDERGROUND CABLE CORRIDOR		SLOPE DIRECTION FOR ROAD
	FENCE		GRATING
	WALK WAY		
	PIPE/CABLE CORRIDOR		

**REFERENCE DRAWINGS**

NO.	DESCRIPTION
220049-001 REV.P7	SITE PLAN
112101-00-YTC-CDA-MET-201	TOPO SURVEY DRAWING
1275.1.20.36.952.I02.130.01	BOILER LAYOUT PLAN - TOP VIEW

REV.	DESCRIPTION	DATE	PREP.	CHECK.	APPROV.	ISSUED FOR
01	WORK IN PROGRESS	04/03/22	PND	SVP	SUB	WORK IN PROGRESS
02	FOR REVIEW	08/02/22	PND	SVP	SUB	FOR REVIEW
03	FOR REVIEW	03/02/22	PND	SVP	SUB	FOR REVIEW

**Corby Energy from Waste (EfW)**

**PLOT PLAN**

Drawing No. Purchaser: 112101-00-YF-GDA-SNL-001 | Drawing No. Supplier: 00-YF-GDA-SNL-001 | Rev: 01

Drawing No. Subcontractor: 00-YF-GDA-SNL-001 | Rev: 01

Contains information for the design of structures, systems and components. YES  NO

VERIFICATION: N/A  HOUSEKEEPING:  VERIFICATION: L/D  NO

DOCUMENT PREPARED WITH CAD DO NOT MODIFY MANUALLY

Scale: 1:300 | SHEET 1 OF 1

**EMISSION/VENT SOURCES TABLE**

SR.NO.	FACILITIES NAME	CO-ORDINATES (IN METERS)		
		NORTH	EAST	ELEVATION
1	CHIMNEY	N 75.000	E 25.000	75.000
2	EDG (VENT)	N 56.023	E 170.876	LATER
3	FIRE WATER DIESEL PUMP	N 76.417	E 209.629	LATER
4	FGT RESIDUE SILOS (VENT)-1	E 57.303	N 97.746	26.570
5	FGT RESIDUE SILOS (VENT)-2	E 52.303	N 97.746	26.570
6	Ca(OH)2 SILO (VENT)-1	E 47.188	N 97.746	28.695
7	Ca(OH)2 SILO (VENT)-2	E 43.588	N 97.746	28.695
8	AC SILO (VENT)	E 40.035	N 97.746	19.885
9	FUEL OIL TANK VENT-1	E 81.797	N 121.306	LATER
10	FUEL OIL TANK VENT-2	E 81.797	N 126.106	LATER

**TERMINAL POINT**

SR.NO.	FACILITIES NAME	CO-ORDINATES (IN METERS)		
		NORTH	EAST	ELEVATION
1	TOWN WATER	LATER	LATER	LATER
2	POWER EVACUATION	LATER	LATER	LATER
3	STORM WATER DISCHARGE	LATER	LATER	LATER

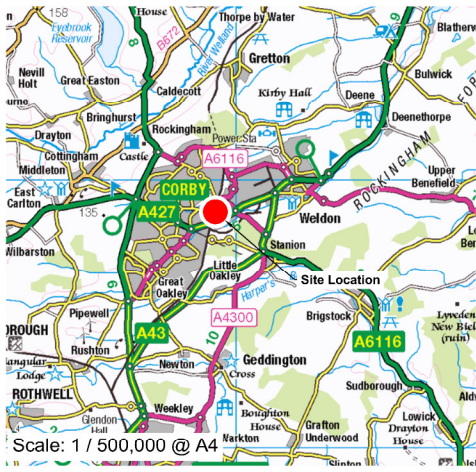
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This document contains proprietary information of MYTILINEOS and is to be used solely for the Project and the purpose for which it is furnished. It may not be disclosed to others for a different use without the written permission of MYTILINEOS.



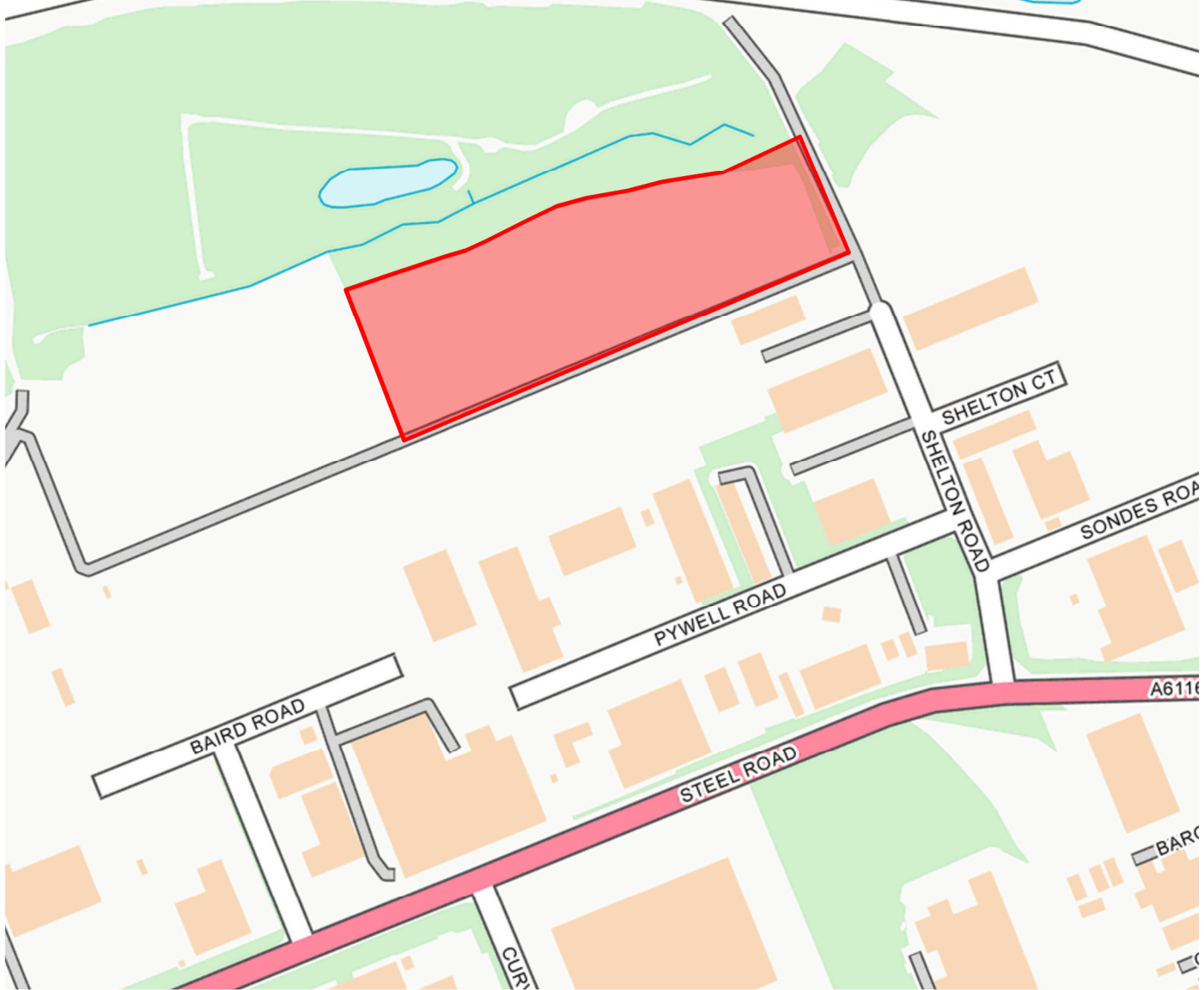
## Figures

## Figure 1 - Site Location Map



**LEGEND**

Site Boundary



Scale: 1 / 20,000 @ A4

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**TITLE:**  
Site Location Map  
Sheldon Road  
Corby

DRAWN BY:	YA	SCALE:	To Scale@A4
CHECKED BY:	MH	REVISION:	1
DATE:	12 March 2022		






<b>PROJECT NO:</b>	15-0645.05
<b>FIGURE NO:</b>	1

## Figure 2 - Exploratory Hole Location Plan





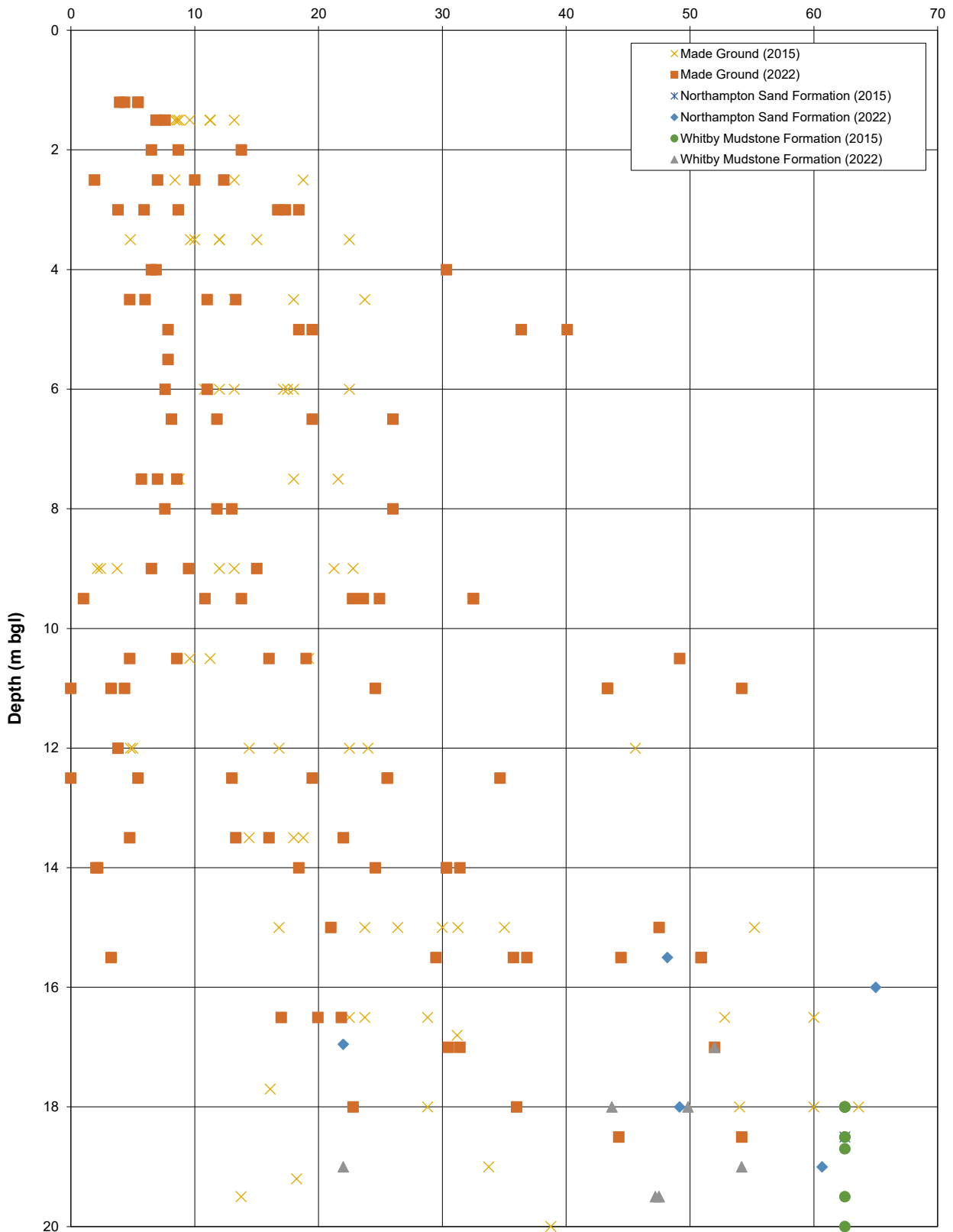
**LEGEND**

-  Site Boundary
-  Borehole location
-  Cone Penetration test
-  Trial Pit Location
-  Rotary Hole Location

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## Figure 3 - Corrected SPT vs Depth Graph

Corrected\* SPT 'N'



\* Corrected for Energy Ratio only



TITLE:

Corrected\* SPT, Depth and Strata Type  
Corby EFW

DWN:

MH

PROJECT NO:

15-0645.05

DATE:

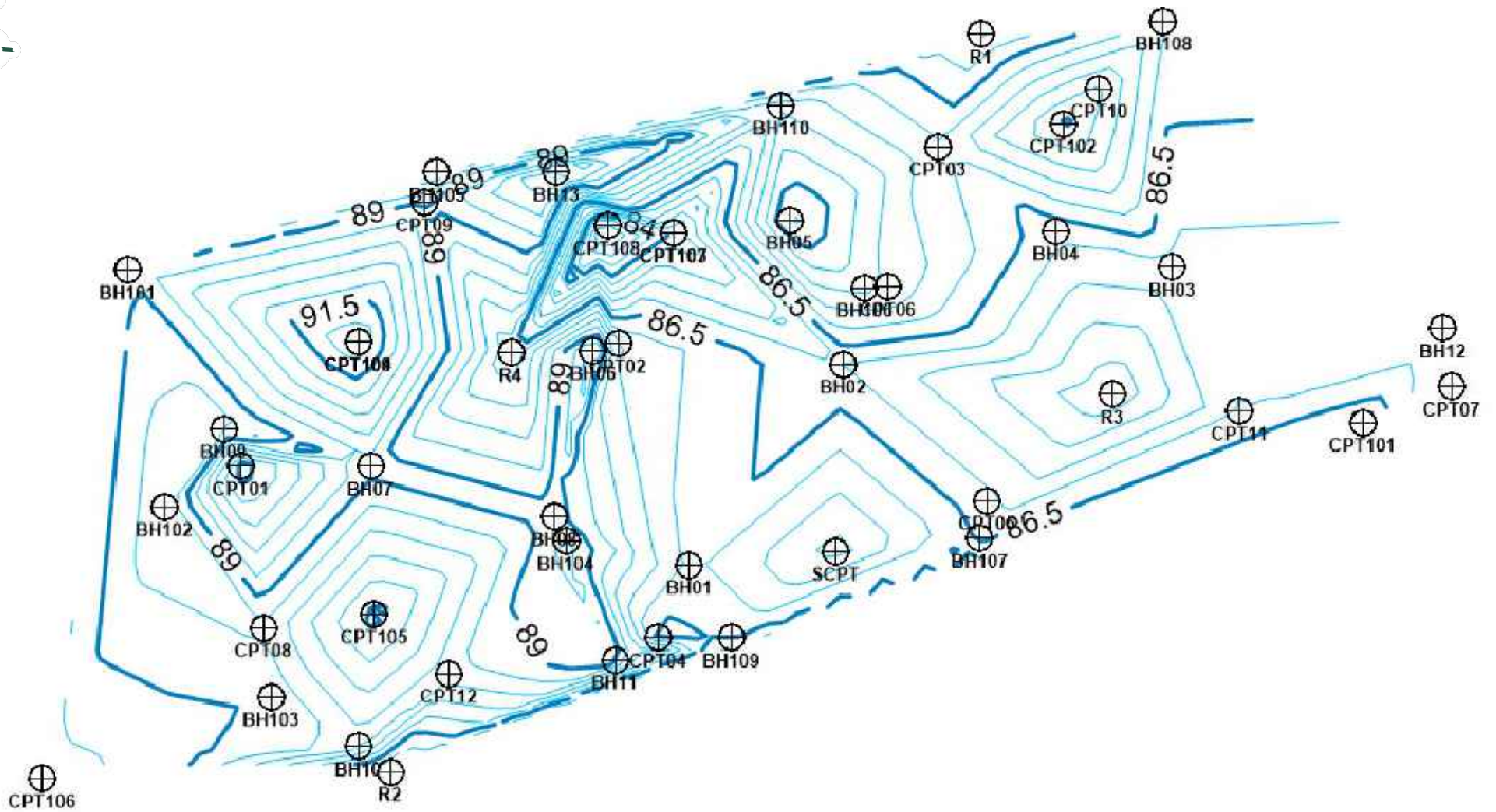
14/03/2022

FIGURE NO:

3

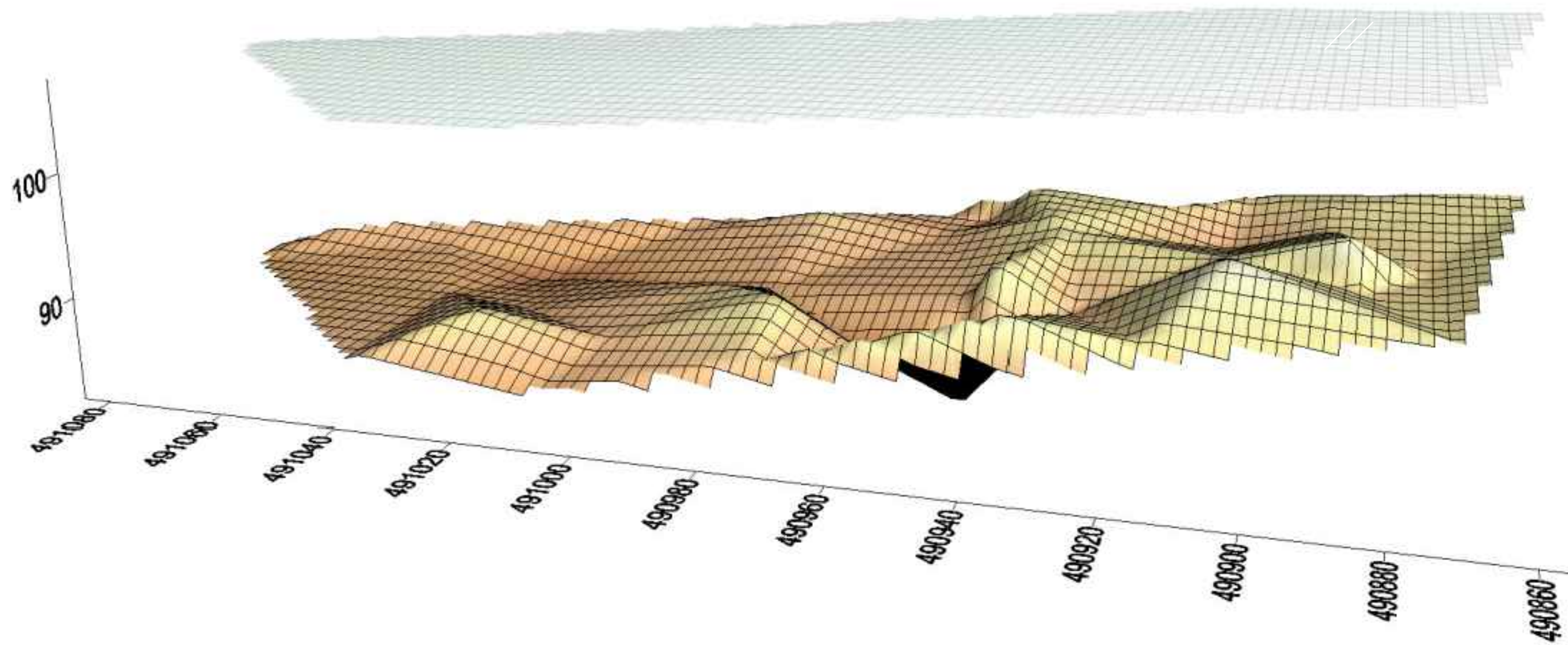
## Figure 4a - Depth to base of Made Ground (2D)





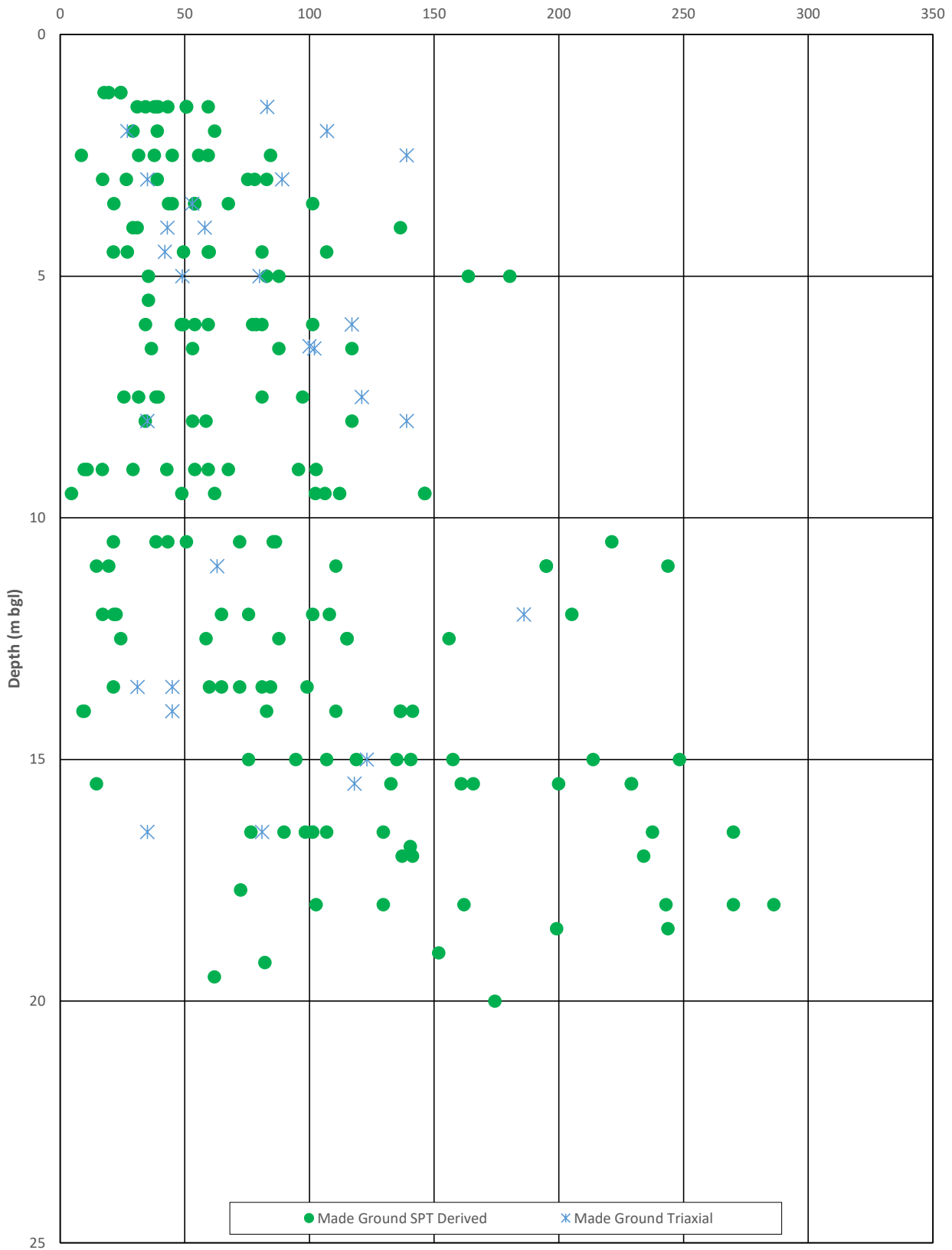
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## Figure 4b - Depth to base of Made Ground (3D)



## Figure 5 - Undrained Shear Strength vs Depth

Undrained Shear Strength (Cu)



TITLE:

Undrained Shear Strength vs Depth  
Corby EfW

DWN:

MH

PROJECT NO:

15-0645.05

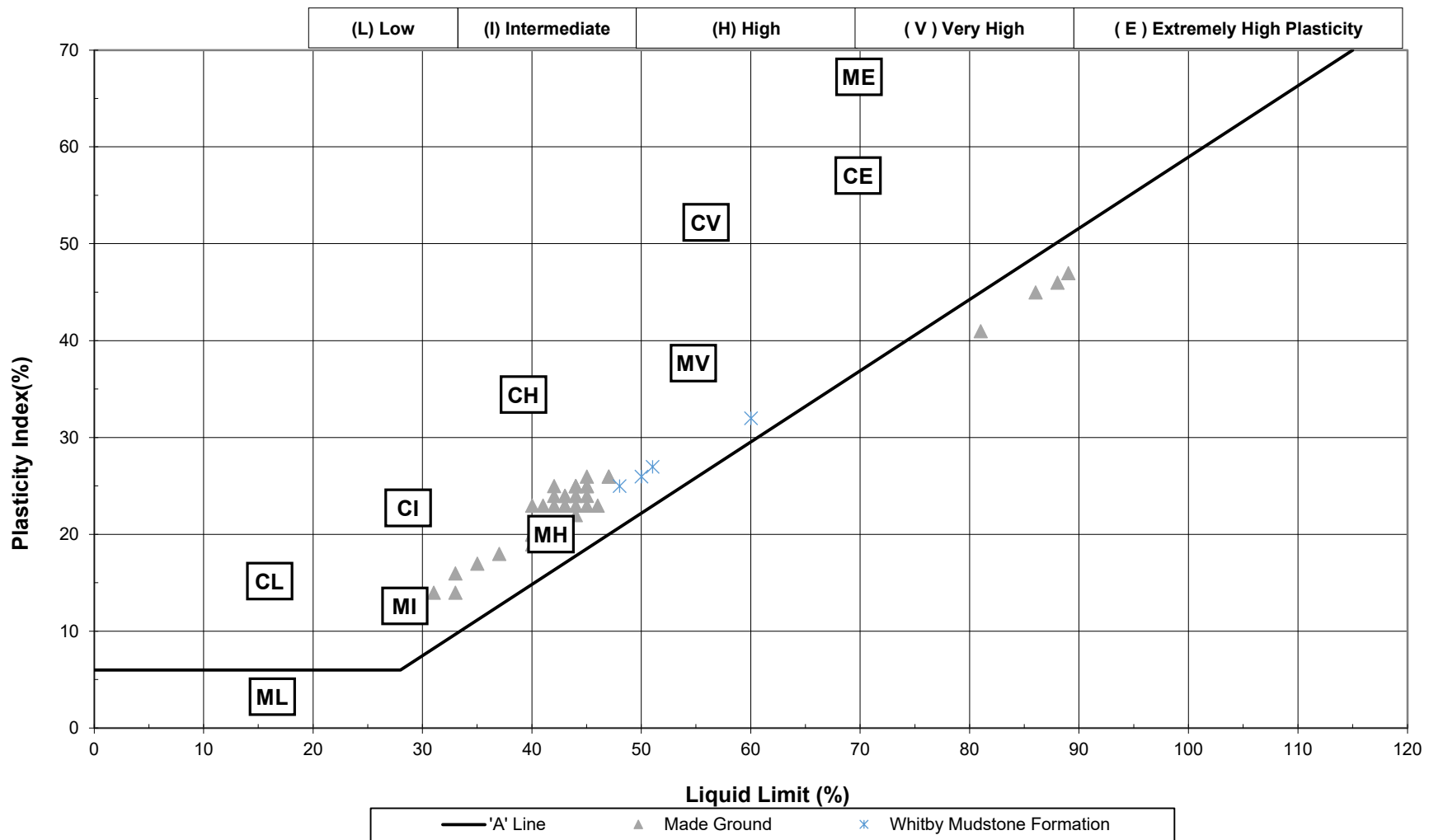
DATE:

14/03/2022

FIGURE NO:

5

## Figure 6 - A-line Plot



TITLE:

Plasticity Chart - All Soils  
Corby EfW

DWN:

MH

PROJECT NO:

15-0645.05

DATE:

14 March 2022

FIGURE NO:

6

## Appendices



## Appendix A - Limitations

## Limitations

This Report was prepared by Delta-Simons Ltd (Delta-Simons) for the sole and exclusive use of the Client and for the specific purpose for which Delta-Simons was instructed. Nothing contained in this Report shall be construed to give any rights or benefits to anyone other than the Client and Delta-Simons, and all duties and responsibilities undertaken are for the sole and exclusive benefit of the Client and not for the benefit of any other party. Delta-Simons does not intend, without its written consent through a formal letter of reliance or warranty, for this Report to be disseminated to any party other than the named Client or to be used or relied upon by any party other than the named Client. Use of the Report by any other party is unauthorised and such use is at the sole risk of the user. Any party using or relying upon this Report, other than the Client, agrees by virtue of its use to indemnify and hold harmless Delta-Simons from and against all claims, losses and damages (of whatsoever nature and howsoever or whensoever arising), arising out of or resulting from the performance of the work by Delta-Simons. Unless explicitly agreed otherwise, in writing, this Report has been prepared under Delta-Simons' Standard Terms and Conditions as included within our proposal to the Client.

The recommendations contained within this Report represent Delta-Simons professional opinions, based upon the information detailed within the Report, exercising the reasonable skill and care to be expected of a professional consultant holding itself out as having the competence, experience and resources necessary for the purpose of carrying out similar work in scope and character to the services performed. The Report needs to be considered in the light of the proposal and associated limitations of scope. The Report needs to be read and considered in full and isolated sections cannot be used without full reference to other elements of the Report and any previous works referenced within the Report.

Where Delta-Simons has obtained, reviewed and evaluated information in preparing this Report from the Client and others and Delta-Simons conclusions, opinions and recommendations has been reasonably determined using this information, Delta-Simons does not warrant the accuracy of the third-party information provided to it and cannot be responsible for any opinions which Delta-Simons has expressed, or conclusions which it has reached in reliance upon information which is subsequently proven to be inaccurate.

Site surveys document the conditions encountered at the time of survey only and conditions may change due to natural processes or human intervention. As such, surveys represent an assessment at a specific point in time and Delta-Simons cannot be responsible for adverse conditions which arise or become apparent after the time of the survey or for conditions which sit outside the scope for which the survey or Report was commissioned.

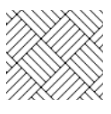
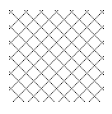
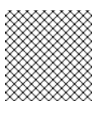

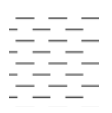




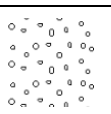
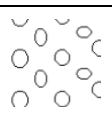
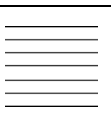
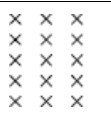
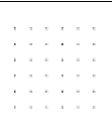
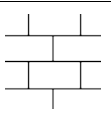
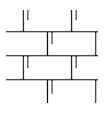



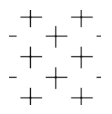




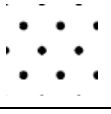

Where intrusive investigations have been completed, information, comments and opinions given in this Report are based on the ground conditions encountered during the site work period and on the results of laboratory and field tests performed during the investigation. Ground conditions are inherently variable such that no investigation can be exhaustive to the extent that all adverse conditions are revealed. Conditions may therefore be present beneath the site that were not apparent in the data reviewed or obtained as part of this assessment. It should be noted that groundwater levels vary due to seasonal and other effects and may at times differ to those measured during the investigation. Delta-Simons does not warrant or guarantee that the Site is free of hazardous or potentially hazardous materials or conditions. Where risk assessment is undertaken, this is based upon the standards, guidance and common practice at the time of the assessment and Delta-Simons cannot be responsible for conditions which become apparent following changes in guidance or practice or advancements in scientific knowledge which change the position in relation to assessment of risk.

No aspect of this Report constitutes a design. Where this information is used in design, the designer should verify the information has been used appropriately.




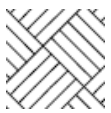

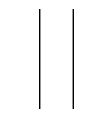

Where budgets are prepared and presented within the Report, these are for information only to indicate the likely magnitude of a cost and do not represent an invitation to treat for the works. All budgets and programmes presented should be reviewed and verified by appropriately qualified and experienced independent Project Managers and Cost Consultants.

## Appendix B - Borehole Logs & SPT Calibrations Certificate

**KEY TO BOREHOLE AND TRIAL PIT LOGS**  
**MATERIAL LEGENDS**

	Topsoil		Made Ground		Bituminous Material
	Concrete		Clay		Silt
	Sand		Gravel		Peat
	Cobbles		Boulders		Mudstone
	Siltstone		Sandstone		Limestone
	Chalk		Coal		Breccia
	Conglomerate		Igneous		Metamorphic
	Pyroclastic (volcanic ash)		Gypsum		Shale
	Ironstone		Bedrock (Unidentified)		Void

**INSTALLATION/BACKFILL LEGENDS**

	Sand		Gravel		Bentonite/Grout
	Arisings		Concrete		Plain Pipe
	Slotted Pipe				

Legend symbols in general accordance with BS 5930:2015+A1:2020 and standard industry practice.

### SAMPLE TYPES

<b>ACM</b>	Asbestos Containing Material Sample
<b>B</b>	Bulk Disturbed Sample
<b>BLK</b>	Block Sample
<b>C</b>	Core Sample
<b>CBR</b>	Undisturbed Sample for California Bearing Ratio Test – 154mm diameter
<b>D</b>	Disturbed Sample - Tub
<b>ES</b>	Soil Sample for Environmental Testing
<b>EW</b>	Water Sample for Environmental Testing
<b>G</b>	Gas Sample
<b>U</b>	Undisturbed Driven Tube Sample – 70/102mm diameter, 450mm long
<b>W</b>	Water Sample



### TEST TYPES

<b>CPT</b>	Cone Penetrometer Test (kN/m <sup>2</sup> )
<b>FID</b>	Flame Ionisation Detector Test (ppm)
<b>HV</b>	In-Situ Hand Shear Vane Test (kN/m <sup>2</sup> )
<b>PID</b>	Photoionisation Detector Test (ppm)
<b>SPT (S)</b>	Standard Penetration Test – Split Spoon Sampler
<b>SPT (C)</b>	Standard Penetration Test – Solid 60 Degree Cone





### CORE DETAILS

<b>If</b>	Fracture Spacing (mm) – Minimum, Average, Maximum
<b>NI</b>	Non-Intact where >25 fracture spacings per metre
<b>TCR</b>	Total Core Recovery (%)
<b>SCR</b>	Solid Core Recovery (%)
<b>RQD</b>	Rock Quality Designation (%)
<b>AF</b>	Air Flush Return (%)
<b>WF</b>	Water Flush Return (%)
<b>NIDD</b>	Non-Intact - Drilling Disturbed
<b>AZCL</b>	Assessed Zone of Core Loss

### WATER COLUMN DETAILS

	Water Strike
	Water Level

**Rotary Core Borehole Log**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill	
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results		
MADE GROUND: Pinkish grey angular to subangular medium to coarse GRAVEL of granite. MADE GROUND: Yellow sandy subrounded fine to coarse GRAVEL of limestone. Black fabric geotextile at 0.30m bgl. MADE GROUND: Soft becoming firm dark grey gravelly CLAY. Gravel is subangular to subrounded fine to coarse limestone and quartzite.		0.05	(0.25)	105.21													
		0.30		104.96													
MADE GROUND: Soft brownish grey slightly gravelly CLAY. Gravel is subangular to subrounded fine to medium mixed lithologies.		4.00	(3.70)	101.26													
		6.20		99.06													
MADE GROUND: Firm becoming stiff orangish brown and grey mottled sandy gravelly CLAY. Gravel is subangular to subrounded fine to medium quartzite and flint. Sand is fine to medium.		6.20	(3.80)	99.06													
		10.00		95.26													
MADE GROUND: Orangish brown very clayey fine to medium SAND.		10.00	(1.30)	95.26													
		10.50		92.96													

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. Hole installed with 50mm HDPE pipe and flush cover. 8. SPT Hammer ID: AR3828. Energy Ratio 60%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

**Rotary Core Borehole Log**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill	
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results		
MADE GROUND: Orangish brown very clayey fine to medium SAND.		11.30		93.96													
MADE GROUND: Firm dark grey fine to medium sandy CLAY. Sand is fine to medium.			(1.70)														
		13.00		92.26													
MADE GROUND: Stiff orangish brown and dark grey mottled slightly sandy CLAY with low cobble content of concrete and quartzite. Sand is fine to medium.			(2.70)														
		15.70		89.56													
MADE GROUND: Firm slightly gravelly sandy dark grey CLAY. Gravel is subangular to subrounded fine to medium flint and mixed lithologies. Sand is fine to medium.			(2.70)														
		18.40		86.86													
Stiff dark grey CLAY. (WHITBY MUDSTONE FORMATION)		18.82	(0.42)	86.44													
Moderately weak grey LIMESTONE with interbedded orangish brown (oxidised fractures). (WHITBY MUDSTONE FORMATION)			(2.28)														
		21.10		84.16													
Weak dark grey thinly bedded MUDSTONE. (WHITBY MUDSTONE FORMATION)																	

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. Hole installed with 50mm HDPE pipe and flush cover. 8. SPT Hammer ID: AR3828. Energy Ratio 60%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %



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Project No: **15-0645.05**      Hole ID: **BH1**      Page: **3 of 3**

Project: **Corby EfW**

**Rotary Core Borehole Log**      Date: **15/02/2022 - 22/02/2022**      Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results	
Weak dark grey thinly bedded MUDSTONE. (WHITBY MUDSTONE FORMATION)							1.5	100	81	69		22.22 - 22.38	U8	22.22		
												22.56 - 22.91	U9	22.56		
												22.91 - 23.11	U10	22.91		
							1.5	100	100	100	20 90 210					
							1.5	97	97	97	40 32 1100					
							1.5	87	83	83	90 150 290					
							1.5				10 350 700					
		30.00		75.26												
Borehole complete at 30.00 m bgl.																

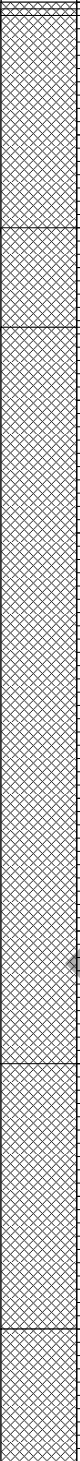
**Remarks:**  
 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. Hole installed with 50mm HDPE pipe and flush cover. 8. SPT Hammer ID: AR3828. Energy Ratio 60%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

Coordinates: **E490961.10 N290847.52**      Elevation (mAOD): **105.26**      Drilled By: **SDA Site Investigations/ Delta Drilling**      Plant Used: **Dando 2000**      Logged: **BK**      Checked:      Approved:      Scale (m): **1:57**



**Rotary Core Borehole Log** Date: **09/02/2022 - 15/02/2022** Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery					Sample Details		Test Details		Backfill		
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results			
<p>MADE GROUND: Pink angular to subangular medium to coarse GRAVEL of granite.</p> <p>MADE GROUND: Yellowish brown gravelly fine to coarse SAND. Gravel is angular to subrounded fine to coarse of sandstone and granite.</p> <p>MADE GROUND: Soft to firm dark grey gravelly CLAY with low cobble content. Gravel is angular to rounded fine to coarse of chalk and sandstone.</p> <p>MADE GROUND: Firm dark grey gravelly CLAY. Gravel is angular to rounded fine to coarse of sandstone and chalk.</p> <p>MADE GROUND: Soft dark grey slightly gravelly very sandy CLAY. Gravel is angular to rounded fine to coarse of sandstone. Sand is fine to coarse.</p>		0.05		105.43								0.10	B1					
		0.10		105.38														
			(1.60)											1.00	B2			
				1.70		103.78								1.65 - 1.70	D1			
			(0.75)											2.00	B3	2.00	SPT(S) N=14 (4,4/10,1,1,2)	
				2.45		103.03								2.00 - 2.45	D2			
														3.00	B4			
														4.00	B5	4.00	SPT(S) N=7 (1,1/2,1,2,2)	
														4.00 - 4.45	D3			
														5.00	B6			
												5.50 - 5.95	D4	5.50	SPT(S) N=8 (1,1/1,3,2,2)			
														6.50	SPT(S) N=12 (1,2/2,3,3,4)			
		8.00		97.48								8.00 - 8.45	U1	8.00	U=30 Blows for 100%			
												8.45 - 8.95	D6					
												9.00	B7					
												9.50 - 9.95	D7	9.50	SPT(S) N=24 (4,6/6,4,7,7)			
		10.00		95.48										10.50	SPT(S) N=50 (4,5/5,5,10,30)			
												11.00	B8	11.00	SPT(S) N=25 (2,4/6,6,7,6)			
												11.00 - 11.45	D8					

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. Hole installed with 50mm HDPE pipe and flush cover. 8. SPT Hammer ID: CABLE01. Energy Ratio 59%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

**Rotary Core Borehole Log** Date: **09/02/2022 - 15/02/2022** Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results	
MADE GROUND: Soft dark grey slightly gravelly clayey fine to coarse SAND. Gravel is angular to subrounded fine to medium of sandstone.		12.50	(2.50)	92.98							12.50 - 12.95	D9	12.50	SPT(S) N=26 (2,6/6,6,6,8)		
MADE GROUND: Stiff dark grey mottled brownish orange slightly gravelly sandy CLAY. Gravel is angular to subrounded fine to coarse of sandstone. Sand is fine to coarse.		15.00	(2.50)	90.48							13.00	B9				
MADE GROUND: Dark yellowish grey slightly gravelly very sandy CLAY. Gravel is subangular to subrounded fine to medium of flint. Sand is fine to medium.		18.00	(3.00)	87.48							14.00 - 14.45	D10	14.00	SPT(S) N=25 (2,4/4,6,7,8)		
MADE GROUND: Dark orangish brown slightly gravelly very sandy CLAY. Gravel is subangular to subrounded fine to coarse of sandstone. Sand is fine to medium.		19.50	(1.50)	85.98							15.00	B10				
											15.50 - 15.95	U2	15.50	U=71 Blows for 100%		
											15.95 - 16.00	D11				
Weak to moderate weathered grey thinly bedded LIMESTONE with interbedded brown staining. (WHITBY MUDSTONE FORMATION)		21.00		84.48			1.5			20 100 220	17.00	B11	17.00	SPT(S) N=31 (2,6/6,8,8,9)		
											17.00 - 17.45	D12				
Weak homogeneous MUDSTONE with weathered clay content with Limestone bedding. (WHITBY MUDSTONE FORMATION)											18.50 - 18.95	D13	18.50	SPT(S) N=45 (18,14/18,10,9,8)		
											19.00	B12				
											19.50 - 19.95	D14	19.50	SPT(S) N=48 (7,9/9,10,14,15)		
											20.10 - 20.31	U1	20.10			
											20.50 - 20.95	D15				
											21.06 - 21.20	U2	21.06			
											21.72 - 21.84	U3	21.72			
											21.93 - 22.24	U5	21.93			
											21.93 - 22.84	U4	21.93			

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. Hole installed with 50mm HDPE pipe and flush cover. 8. SPT Hammer ID: CABLE01. Energy Ratio 59%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %



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Project No: **15-0645.05**

Hole ID: **BH2**

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Project: **Corby EfW**

**Rotary Core Borehole Log**

Date: **09/02/2022 - 15/02/2022**

Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill	
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results		
Weak homogeneous MUDSTONE with weathered clay content with Limestone bedding. (WHITBY MUDSTONE FORMATION)		24.00	(3.00)	81.48				100	100	91		22.23 - 22.45	U6	22.23			
							1.5					22.95 - 23.26	U7	22.95			
												23.26 - 23.58	U8	23.26			
												23.84 - 23.99	U9	23.84			
Weak to moderate thinly laminated MUDSTONE. (WHITBY MUDSTONE FORMATION)		25.50	(1.50)	79.98								24.50 - 24.70	U10	24.50			
							1.5					24.83 - 25.09	U11	24.83			
												25.29 - 25.50	U12	25.29			
												25.50 - 25.79	U13	25.50			
Light grey weak to moderate laminated MUDSTONE. (WHITBY MUDSTONE FORMATION)			(4.50)									26.26 - 26.65	U15	26.26			
							1.5					26.65 - 26.96	U16	26.65			
												26.93	U14	26.93			
												27.14 - 27.49	U17	27.14			
							1.5						27.65 - 28.02	U18	27.65		
													28.22 - 28.49	U19	28.22		
													29.06 - 29.37	U20	29.06		
1.5						29.37 - 29.77	U21	29.37									
Borehole complete at 30.00 m bgl.		30.00		75.48													

**Remarks:**  
 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation.3. Hand dug service inspection pit advanced to 1.20 m bgl.4. Elevation and location data from GPS survey.5. Borehole commenced as cable percussive with rotary core follow-on.6. Borehole complete at 30.0 m bgl.7. Hole installed with 50mm HDPE pipe and flush cover.8. SPT Hammer ID: CABLE01. Energy Ratio 59%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

Coordinates: <b>E490986.03 N290880.03</b>	Elevation (mAOD): <b>105.48</b>	Drilled By: <b>Borehole Surveys/ CC Ground Investigations</b>	Plant Used: <b>Dando 2000</b>	Logged: <b>RS</b>	Checked:	Approved:	Scale (m): <b>1:57</b>
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**Rotary Core Borehole Log** Date: **07/02/2022 - 21/02/2022** Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery					Sample Details		Test Details		Backfill	
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results		
<p>MADE GROUND: Reddish brown angular to subangular medium to coarse GRAVEL of granite.</p> <p>MADE GROUND: Brown slightly sandy clayey angular to subangular fine to coarse GRAVEL of granite. Sand is fine to coarse. Black fabric geotextile at 0.30m bgl.</p> <p>MADE GROUND: Soft grey sandy gravelly CLAY. Gravel is angular to subrounded find to coarse granite, chalk and mudstone. Sand is fine to coarse.</p> <p>MADE GROUND: Firm dark grey gravelly CLAY. Gravel is angular to subrounded fine to coarse chalk and mudstone.</p> <p>MADE GROUND: Firm to stiff brown mottled grey slightly sandy gravelly CLAY. Gravel is angular to subrounded fine to coarse sandstone and flint. Sand is fine to coarse.</p> <p>MADE GROUND: Soft firm blackish brown organic CLAY with rootlets.</p> <p>MADE GROUND: Yellowish brown slightly clayey fine to coarse SAND.</p>		0.05		104.78													
		0.30	(0.25)	104.52													
			(0.70)								0.50	D1					
		1.00		103.82							0.50 - 1.20	B1					
											1.00	D2					
											1.20 - 1.65	B2	1.20	SPT(S) N=4 (1,1/1,1,1,1)			
											1.65 - 2.00	D3					
											2.00 - 2.45	U1	2.00				
											2.45 - 2.65	D4					
			(3.00)								2.65 - 3.00	D5					
											3.00 - 3.45	B3	3.00	SPT(S) N=17 (2,2/4,4,4,5)			
											3.45 - 4.00	D6					
			4.00		100.82						4.00 - 4.45	U2	4.00				
										4.45 - 4.65	D7						
										4.65 - 5.00	D8						
										5.00 - 5.45	B4	5.00	SPT(S) N=37 (4,6/8,8,10,11)				
										5.45 - 6.00	D9						
										6.50 - 6.95	U3	6.50					
		6.80		98.02						6.95 - 7.15	D10						
										7.15 - 8.00	D11						
										8.00 - 8.45	B5	8.00	SPT(S) N=12 (2,3/3,3,3,3)				
										8.45 - 9.50	D12						
		9.00		95.82						9.50	B6	9.50	SPT(S) N=23 (3,3/4,5,7,7)				
										9.95 - 11.00	D13						
										11.00 - 11.45	B7	11.00	SPT(S) 50 (9,15/50 for 95mm)				

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. SPT Hammer ID: AR2417. Energy Ratio 65%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

**Rotary Core Borehole Log** Date: **07/02/2022 - 21/02/2022** Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill	
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results		
MADE GROUND: Yellowish brown slightly clayey fine to coarse SAND.		12.50		92.32							11.45 - 12.50	D14					
MADE GROUND: Firm grey slightly gravelly very sandy CLAY. Gravel is angular to subrounded fine to coarse of sandstone. Sand is fine to coarse.			(4.50)								12.50 - 12.95	D8	12.50	SPT(S) N=32 (5,7/7,9,9,7)			
											12.95 - 14.00	D15					
											14.00 - 14.45	B9	14.00				SPT(S) N=29 (3,3/4,9,8,8)
											14.45 - 15.50	D16					
MADE GROUND: Firm locally stiff grey slightly gravelly CLAY. Gravel is subangular to subrounded fine to coarse of sandstone.		17.00		87.82							15.50 - 15.95	B10	15.50	SPT(S) N=34 (3,3/6,9,7,12)			
											15.95 - 17.00	D17					
MADE GROUND: Yellowish brown fine to coarse SAND. (REWORKED NATURAL).		17.50		87.32							17.00 - 17.45	B18	17.00	SPT(S) N=48 (7,9/11,11,13,13)			
Blueish grey SANDSTONE recovered as angular to subangular fine to coarse gravel of sandstone. (NORTHAMPTON SAND FORMATION) Moderately weak bluish grey shelly carbonaceous MUDSTONE. Fractures are horizontal bedding, close to medium spacing, rough to planar, undulating rough in places, partly open to moderately wide. Orangish brown iron staining on fracture surfaces. (WHITBY MUDSTONE FORMATION)		19.00	(0.20)	85.62							18.50 - 18.95	B19	18.50	SPT(S) 50 (25 for 95mm/50 for 180mm) SPT(S) 56 (35 for 110mm/56 for 45mm)			
											19.00 - 19.20						
											19.65 - 19.84	U1	19.65				
											19.84 - 19.99	U2	19.84				
											20.23 - 20.50	U3	20.23				
											20.50 - 20.66	U4	20.50				
		22.00		82.82							20.72 - 20.85	U5	20.72				
											21.03 - 21.25	U6	21.03				

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. SPT Hammer ID: AR2417. Energy Ratio 65%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

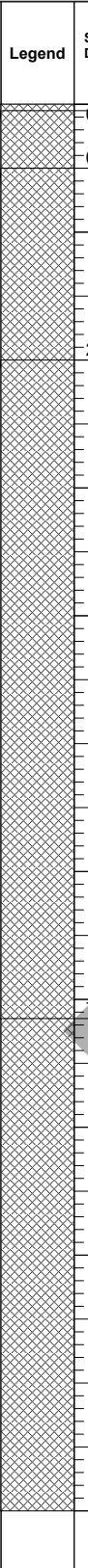
Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill	
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results		
Thinly laminated dark grey MUDSTONE. (WHITBY MUDSTONE FORMATION)							1.0										
Thinly laminated dark grey MUDSTONE.								100	100	100		23.13 - 23.44	U7	23.13			
							1.5					23.88 - 24.20	U8	23.88			
								100	100	100		24.70 - 25.00	U9	24.70			
							1.5					25.30 - 25.60	U10	25.30			
				(8.04)				100	100	90		26.20 - 26.40	U11	26.20			
				(7.04)			1.5				20 305 1240	26.60 - 26.85	U12	26.60			
								97	97	93		26.85 - 27.05	U13	26.85			
							1.5					27.60 - 27.80	U14	27.60			
												27.90 - 28.20	U15	27.90			
							1.5					28.68 - 28.90	U16	28.68			
								100	100	100		29.00 - 29.24	U17	29.00			
							1.0					29.24 - 29.50	U18	29.24			
												29.85 - 30.04	U19	29.85			
Borehole complete at 30.04 m bgl.		30.04		74.78													

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. SPT Hammer ID: AR2417. Energy Ratio 65%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %



<b>Rotary Core Borehole Log</b>	Date: <b>10/02/2022 - 21/02/2022</b>	Client: <b>Mytilineos</b>
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Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill				
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results					
MADE GROUND: Reddish brown subrounded to subangular medium to coarse GRAVEL of granite. MADE GROUND: Yellowish brown slightly gravelly fine to coarse SAND. Gravel is angular to subrounded fine to coarse of granite and red brick. MADE GROUND: Soft dark brown sandy gravelly CLAY. Gravel is angular to subrounded fine to coarse of mudstone, redbrick and chalk. Sand is fine to coarse. <u>Black geotextile membrane.</u> MADE GROUND: Soft becoming firm dark grey slightly sandy gravelly CLAY. Gravel is angular to subrounded fine to coarse mudstone, chalk and sandstone. Sand is fine to coarse.		0.05	0.45	105.11																
		0.50		104.66													0.00 - 1.20	B1	SPT(S) N=5 (1,1/1,2,1,1)	
		1.00	1.50	1.20 - 1.65													B2			
		1.65 - 2.00		D3																
		2.00	103.16	2.00 - 2.45													U1			
		2.45 - 2.65	D4																	
		2.65 - 3.00	D5																	
		3.00 - 3.45	B3	3.00													SPT(S) N=8 (1,1/2,2,2,2)			
		3.45 - 4.00	D6																	
		4.00 - 4.45	U2	4.00																
		4.45 - 4.65	D7																	
		4.65 - 5.00	D8																	
		5.00 - 5.45	B4	5.00													SPT(S) N=17 (2,2/3,4,4,6)			
		5.45 - 6.50	D9																	
6.45 - 6.95	U3	6.45																		
6.95 - 7.15	D10																			
7.15	98.01	7.15 - 8.00	D11																	
MADE GROUND: Soft black organic CLAY with some rootlets.			4.30																	
																	8.00 - 8.45	B5	8.00	SPT(S) N=7 (1,2/2,2,2,1)
																	8.45 - 9.50	D12		
																	9.50 - 9.95	B6	9.50	SPT(S) N=10 (2,3/2,2,3,3)
																	9.50 - 9.95	D13		
9.95 - 11.00	D14																			

**Remarks:**  
 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole terminated at 23.5 m bgl due to casing becoming detached within the borehole. 7. Recovery attempts failed to recover metal casing which has been backfilled. 8. SPT Hammer ID: AR2417. Energy Ratio 65%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %



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Project No: **15-0645.05** Hole ID: **BH4** Page: **2 of 3**

Project: **Corby EfW**

**Rotary Core Borehole Log** Date: **10/02/2022 - 21/02/2022** Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details		Test Details		Backfill
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	
MADE GROUND: Soft black organic CLAY with some rootlets.		11.45		93.71											
MADE GROUND: Yellowish brown mottled grey sandy gravelly CLAY. Gravel is angular to subrounded fine to coarse sandstone, mudstone and chalk. Sand is fine to coarse.			(4.05)												
		15.50		89.66											
MADE GROUND: Firm to stiff grey slightly sandy gravelly CLAY. Sand is fine to coarse. Gravel is fine to coarse subangular to subrounded of sandstone and mudstone.			(1.50)												
MADE GROUND: Firm to stiff grey slightly sandy gravelly CLAY. Gravel is subangular to subrounded fine to coarse of sandstone and mudstone. Sand is fine to coarse.		17.00		88.16											
			(3.50)												
		19.00		86.16											
Weak weathered grey thinly bedded LIMESTONE. (WHITBY MUDSTONE FORMATION)		19.82	(0.82)	85.34						60 132 250	19.54 - 19.74 UC1	19.54			
Weak grey thinly bedded LIMESTONE. (WHITBY MUDSTONE FORMATION)			(1.48)								20.21 - 20.33 UC3	20.21			
										60 262 690	20.50 - 20.69 UC4	20.50			
		21.30		83.86							20.95 - 21.36 UC5	20.95			
Very weak becoming weak dark grey thinly laminated MUDSTONE (WHITBY MUDSTONE)											21.67 - 22.00 UC6	21.67			


**Remarks:**  
 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole terminated at 23.5 m bgl due to casing becoming detached within the borehole. 7. Recovery attempts failed to recover metal casing which has been backfilled. 8. SPT Hammer ID: AR2417. Energy Ratio 65%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

Coordinates: **E491020.56 N290901.58** Elevation (mAOD): **105.16** Drilled By: **VC Drilling/ CC Ground Investigation** Plant Used: **Dando 2000** Logged: **EC/BK** Checked: Approved: Scale (m): **1:57**



**Rotary Core Borehole Log**      Date: **10/02/2022 - 21/02/2022**      Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details		Test Details		Backfill
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	
Very weak becoming weak dark grey thinly laminated MUDSTONE (WHITBY MUDSTONE FORMATION)		23.50	(2.20)	81.66			0.9	100							
							0.6								
Borehole complete at 23.50 m bgl.															

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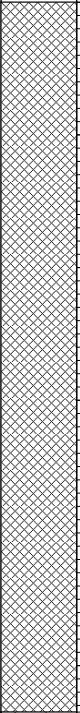
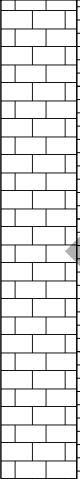

<b>Remarks:</b> 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation.3. Hand dug service inspection pit advanced to 1.20 m bgl.4. Elevation and location data from GPS survey.5. Borehole commenced as cable percussive with rotary core follow-on.6. Borehole terminated at 23.5 m bgl due to casing becoming detached within the borehole.7. Recovery attempts failed to recover metal casing which has been backfilled.8. SPT Hammer ID: AR2417. Energy Ratio 65%.	<b>Water Level Observations</b>				<b>Flush</b>		
	Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %	
Coordinates: <b>E491020.56 N290901.58</b>	Elevation (mAOD): <b>105.16</b>	Drilled By: VC Drilling/ CC Ground Investigation	Plant Used: <b>Dando 2000</b>	Logged: <b>EC/BK</b>	Checked:	Approved:	Scale (m): <b>1:57</b>

**Rotary Core Borehole Log** Date: **08/02/2022 - 24/02/2022** Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details		Test Details		Backfill	
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)		Results
MADE GROUND: Pink subrounded to subangular medium to coarse GRAVEL of granite.		0.05	(0.25)	105.98												
MADE GROUND: Yellow sandy subrounded fine to coarse GRAVEL of limestone. Sand is fine to coarse.		0.30		105.73							0.30	B1				
MADE GROUND: Brown and grey very gravelly CLAY with high cobble content of concrete and brick. Gravel is rounded to subangular fine to medium chalk, brick and concrete.		1.50	(1.20)	104.53							1.50 1.50 - 1.95	B2 D1	1.50	SPT(S) N=7 (2,2/1,1,2,3)		
MADE GROUND: Soft grey slightly sandy CLAY. Sand is fine to medium. (REWORKED NATURAL)		2.50	(1.00)	103.53							2.00 2.00 - 2.45	B3 U1	2.00	U=29 Blows for 89%		
MADE GROUND: Firm grey slightly gravelly CLAY. Gravel is rounded to subrounded fine to medium chalk. (REWORKED NATURAL).		5.00	(2.50)	101.03							3.00 3.00 - 3.45	B4 D2	3.00	SPT(S) N=6 (0,1/1,2,1,2)		
											4.00 4.00 - 4.45	B5 U2	4.00	U=30 Blows for 100%		
											4.45 - 4.50	D3				
MADE GROUND: Soft dark grey gravelly CLAY. Gravel is angular to subrounded fine to coarse granite and limestone. <i>Limestone recovered as 20cm core.</i>		6.90	(1.90)	99.13							5.00 5.00 - 5.45	B6 D4	5.00	SPT(S) N=8 (1,1/1,2,2,3)		
											6.40 - 6.50 6.50 - 6.95	D5 D6	6.50	SPT(S) N=8 (1,0/1,2,2,3)		
MADE GROUND: Firm dark grey gravelly CLAY. Gravel is subangular to subrounded fine to medium chalk.		8.00	(1.10)	98.03							7.00 - 7.50	B7				
MADE GROUND: Soft greenish brown slightly gravelly CLAY. Gravel is angular to subrounded fine to medium chalk and flint.		9.20	(1.20)	96.83							8.00 - 8.45	U3	8.00			
											8.45 - 8.55 8.50 - 9.00	D7 B8				
MADE GROUND: Very soft black organic rich slightly gravelly CLAY. Gravel is subangular fine granite and chalk. No recovery from 14.00 m bgl to 15.50 m bgl.											9.50 - 10.00 9.50 - 9.95	B9 D9	9.50	SPT(S) N=1 (1,0/1,0,0,0)		
											10.50	D10				
											11.00 - 11.25	D8	11.00	SPT(S) N=0 (1,0/0,0,0,0)		

<b>Remarks:</b> 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. SPT Hammer ID: CC03. Energy Ratio 61%.	<b>Water Level Observations</b>				<b>Flush</b>		
	Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %	
Coordinates: <b>E490977.30 N290903.34</b>	Elevation (mAOD): <b>106.03</b>	Drilled By: <b>Borehole Surveys/ CC Ground Investigations</b>	Plant Used: <b>Dando 2000</b>	Logged: <b>RS/BK</b>	Checked:	Approved:	Scale (m): <b>1:57</b>

**Rotary Core Borehole Log** Date: **08/02/2022 - 24/02/2022** Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details		Test Details		Backfill			
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)		Results		
MADE GROUND: Very soft black organic rich slightly gravelly CLAY. Gravel is subangular fine granite and chalk. No recovery from 14.00 m bgl to 15.50 m bgl.			(7.15)	89.68								11.50 - 12.00	B10					
													12.50 - 13.90	D11	12.50	SPT(S) N=0 (0,0/0,0,0,0)		
													14.00 - 14.43	D12	14.00	SPT(S) N=2 (1,0/0,2,0,0)		
													15.50 - 15.95	D13	15.50	SPT(S) N=29 (3,4/5,7,8,9)		
Weak weathered brown thinly bedded LIMESTONE. Grey unweathered limestone band between 18.85 m bgl and 19.36 m bgl. (WHITBY MUDSTONE FORMATION)			(3.65)	86.03				87	78	70								
							1.5				115 40 460							
								86	79	54								
Weak dark grey thinly laminated MUDSTONE. (WHITBY MUDSTONE FORMATION)												20.00 - 20.30	U2	20.00				
													18.87 - 19.36	U1	18.87			
							1.5											
								100	100	100			20.00 - 20.30	U2	20.00			
													20.48 - 20.80	U3	20.48			
											21.19 - 21.50	U4	21.19					
											21.84 - 22.18	U5	21.84					

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. SPT Hammer ID: CC03. Energy Ratio 61%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

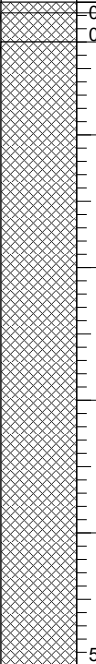
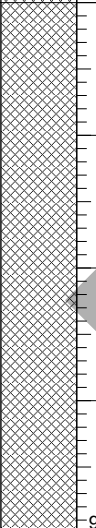
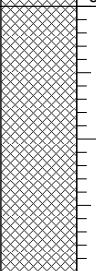

**Rotary Core Borehole Log**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill						
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results							
Weak dark grey thinly laminated MUDSTONE. (WHITBY MUDSTONE FORMATION)				(10.00)			1.5					22.48 - 22.74	U6	22.48								
								92	92	92		23.00 - 23.30	U7	23.00								
												23.30 - 23.60	U8	23.30								
							1.5					23.94 - 24.20	U9	23.94								
								13	13	13												
							1.5															
								90	79	79		26.17 - 26.33	U10	26.17								
												26.50 - 26.68	U11	26.50								
							1.5					26.92 - 27.09	U12	26.92								
								100	100	94												
												27.75 - 28.00	U13	27.75								
							1.5					28.26 - 28.51	U14	28.26								
								100	100	95		28.78 - 28.93	U15	28.78								
												29.05 - 29.29	U16	29.05								
							1.0					29.29 - 29.49	U17	29.29								
												29.64 - 30.00	U18	29.64								
							Borehole complete at 30.00 m bgl.		30.00		76.03											

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. SPT Hammer ID: CC03. Energy Ratio 61%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

**Rotary Core Borehole Log** Date: **16/02/2022 - 21/02/2022** Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details		Test Details		Backfill															
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)		Results														
MADE GROUND: Reddish brown subrounded to subangular medium to coarse GRAVEL of granite. MADE GROUND: Yellow sandy subrounded fine to coarse GRAVEL of limestone. MADE GROUND: Soft grey slightly gravelly CLAY. Gravel is subangular to subrounded fine to medium chalk. (REWORKED NATURAL)		0.08	(0.22)	106.06																										
		0.30		105.84																										
																(4.70)														
MADE GROUND: Firm grey gravelly CLAY. Gravel is rounded to subrounded fine to medium chalk. (REWORKED NATURAL)		5.00	(4.00)	101.14																										
MADE GROUND: Soft black very organic CLAY.		9.00	(4.00)	97.14																										
			(4.00)																											

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation.3. Hand dug service inspection pit advanced to 1.20 m bgl.4. Elevation and location data from GPS survey.5. Borehole commenced as cable percussive with rotary core follow-on.6. Borehole complete at 30.0 m bgl.7. SPT Hammer ID: AR2417. Energy Ratio 65%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %



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Project No: **15-0645.05** Hole ID: **BH6** Page: **2 of 3**

Project: **Corby EfW**

**Rotary Core Borehole Log** Date: **16/02/2022 - 21/02/2022** Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details		Test Details		Backfill
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	
MADE GROUND: Soft black very organic CLAY.	[Cross-hatch pattern]										11.45 - 12.50	D18			
			(6.70)								12.50 12.50 - 12.95 12.95 - 14.00	B18 D18 D18	12.50	SPT(S) N=5 (1,1/1,2,1,1)	
		15.70		90.44							14.00 14.45 - 15.00	B18 D18	14.00	SPT(S) N=2 (0,1/0,0,1,1)	
Very weak weathered orange LIMESTONE.	[Brick pattern]	16.00	(0.30)	90.14							15.50 15.80 16.00	B18 D18 D18	15.50 16.00	SPT(S) N=3 (1,0/1,1,0,1) SPT(S) 60 (25 for 70mm/60 for 140mm)	
Very weak weathered orange LIMESTONE. (NORTHAMPTON SAND FORMATION)	[Brick pattern]	17.00	(1.30)												
Orange brown coarse grained weak SANDSTONE. (NORTHAMPTON SAND FORMATION) <i>Recovered as medium to coarse angular gravel.</i>	[Dotted pattern]		(2.50)	89.14						1.0 1.5					
		19.50		86.64											
Moderately weak grey thinly bedded LIMESTONE with orange stained fractures. (WHITBY MUDSTONE FORMATION)	[Brick pattern]		(1.50)												
		21.00		85.14											
Weak dark grey thinly laminated MUDSTONE. (WHITBY MUDSTONE FORMATION)	[Horizontal lines pattern]														

**Remarks:**  
 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. SPT Hammer ID: AR2417. Energy Ratio 65%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

Coordinates: **E490945.48 N290882.18** Elevation (mAOD): **106.14** Drilled By: **VC Drilling/ Delta Drilling** Plant Used: **Dando 2000** Logged: **RS/ TR** Checked: Approved: Scale (m): **1:57**



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Project No: **15-0645.05** Hole ID: **BH6** Page: **3 of 3**

Project: **Corby EfW**

**Rotary Core Borehole Log** Date: **16/02/2022 - 21/02/2022** Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill	
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results		
Weak dark grey thinly laminated MUDSTONE. (WHITBY MUDSTONE FORMATION)				(9.00)								22.10 - 22.30	U5	22.10			
								89	89	84			22.67 - 22.96	U6	22.67		
							1.5						23.13 - 23.47	U7	23.13		
								91	90	75							
							1.5										
								100	100	100			25.18 - 25.27	U8	25.18		
													25.37 - 25.46	U9	25.37		
													25.50 - 25.80	U10	25.50		
							1.5						26.17 - 26.40	U11	26.17		
								95	95	78							
							1.5						27.25 - 27.50	U12	27.25		
													27.90 - 28.20	U14	27.90		
								96	96	83			28.14 - 28.30	U13	28.14		
													28.50 - 28.61	U15	28.50		
							1.5						29.12 - 29.30	U16	29.12		
													29.67 - 29.94	U17	29.67		
							Borehole complete at 30.00 m bgl.		30.00		76.14						

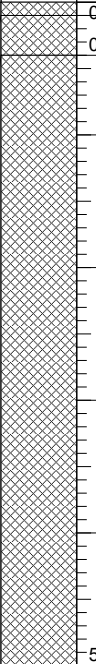
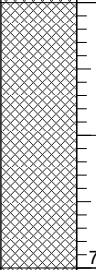
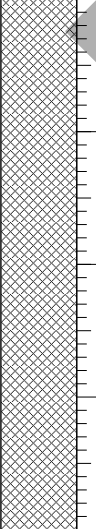
**Remarks:**  
 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. SPT Hammer ID: AR2417. Energy Ratio 65%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

Coordinates: <b>E490945.48 N290882.18</b>	Elevation (mAOD): <b>106.14</b>	Drilled By: <b>VC Drilling/ Delta Drilling</b>	Plant Used: <b>Dando 2000</b>	Logged: <b>RS/ TR</b>	Checked:	Approved:	Scale (m): <b>1:57</b>
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**Rotary Core Borehole Log**

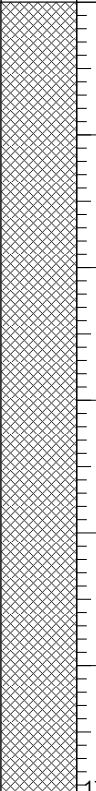
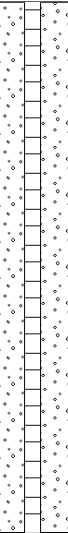
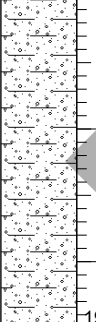



Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery					Sample Details			Test Details		Backfill																		
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results																				
<p>MADE GROUND: Pinkish grey angular to subangular medium to coarse GRAVEL of granite.</p> <p>MADE GROUND: Yellow sandy subrounded fine to coarse GRAVEL of limestone.</p> <p>MADE GROUND: Firm dark grey slightly sandy gravelly CLAY. Gravel is angular to subrounded fine to medium granite and limestone. Sand is fine to coarse.</p>		0.10	(0.30)	106.14																															
		0.40		105.84																															
				(4.60)																															
				5.00																101.24															
<p>MADE GROUND: Stiff blackish brown slightly gravelly CLAY. Gravel is subangular to subrounded fine to medium of flint and limestone.</p>			(2.00)																																
<p>MADE GROUND: Soft greenish black slightly gravelly organic CLAY. Gravel is fine to coarse angular to subrounded of limestone.</p>		7.00		99.24																															

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. SPT Hammer ID: AR2102. Energy Ratio 57%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %



**Rotary Core Borehole Log**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill						
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results							
MADE GROUND: Soft greenish black slightly gravelly organic CLAY. Gravel is fine to coarse angular to subrounded of limestone.			(10.00)	89.24																		
																		11.80	D8	12.00	U=11 Blows for 100%	
																		12.00 - 12.45	U3			
																		12.50	D9			
																		13.00	D10			
																		13.50 - 13.95	D11	13.50	SPT(S) N=5 (1,2/2,1,1,1)	
																		14.80	D12	15.00	U=9 Blows for 100%	
																		15.00 - 15.45	U4			
																		15.50	D13			
																		16.00	D14			
16.50 - 16.95	D15	16.50	SPT(S) N=21 (11,8/4,5,5,7)																			
Orange slightly clayey sandy angular to subrounded fine to medium GRAVEL of limestone. (WHITBY MUDSTONE FORMATION)			(2.50)																			
																		17.80	D16	18.00	SPT(S) N=46 (2,2/2,4,13,27)	
18.00 - 18.45	D17																					
Moderately weak dark grey LIMESTONE. (WHITBY MUDSTONE FORMATION)			(0.53)	86.74																		
																			19.20	D18	19.50	SPT(S) N=50 (25 for 115mm/50 for 265mm)
																			19.45 - 19.95	D19		
																			19.78 - 19.98	U1	19.78	
Recovered as gravel. Weak dark grey thinly laminated MUDSTONE.								1.5														
Weak dark grey thinly laminated MUDSTONE. (WHITBY MUDSTONE FORMATION)																			20.16 - 20.52	U2	20.16	
																						
																			21.42 - 21.79	U3	21.42	

**Remarks:**  
 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. SPT Hammer ID: AR2102. Energy Ratio 57%.

**Water Level Observations**

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %



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Project No: **15-0645.05**

Hole ID: **BH7**

Page: **3 of 3**

Project: **Corby EfW**

**Rotary Core Borehole Log**

Date: **17/02/2022 - 25/02/2022**

Client: **Mytilineos**


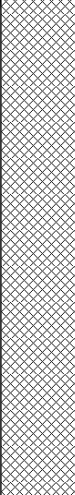
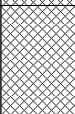
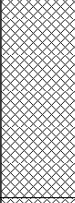
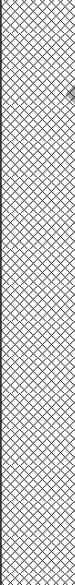
Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details		Test Details		Backfill	
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)		Results
Weak dark grey thinly laminated MUDSTONE. (WHITBY MUDSTONE FORMATION)											22.22 - 22.34	U4	22.22			
											22.70 - 22.90	U5	22.70			
		1.5						20 240 670			23.33 - 23.76	U6	23.33			
									94	94	86	23.83 - 24.00	U7	23.83		
											24.20 - 24.50	U8	24.20			
		1.5						30 320 840			24.70 - 25.00	U9	24.70			
									96	96	80	25.24 - 25.41	U10	25.24		
											25.62 - 25.95	U11	25.62			
		1.5						50 200 380			26.51 - 26.70	U12	26.51			
									92	1	81	27.00 - 27.25	U13	27.00		
		1.5						20 120 360			27.55 - 27.86	U14	27.55			
									97	97	97	28.23 - 28.37	U15	28.23		
											28.57 - 28.81	U16	28.57			
											29.72 - 29.95	U17	29.72			
				29.95		76.29										
		Borehole complete at 30.00 m bgl.		30.00		76.24										

**Remarks:**  
 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. SPT Hammer ID: AR2102. Energy Ratio 57%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

Coordinates: <b>E490909.36 N290863.44</b>	Elevation (mAOD): <b>106.24</b>	Drilled By: <b>SDA Site Investigations/ Delta Drilling</b>	Plant Used: <b>Dando 115</b>	Logged: <b>BK/ TR/ EC</b>	Checked:	Approved:	Scale (m): <b>1:57</b>
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**Rotary Core Borehole Log**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details		Test Details		Backfill
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	
MADE GROUND: Pinkish grey angular to subangular medium to coarse GRAVEL of granite.		0.05	(0.35)	105.70											
		0.40		105.36											
MADE GROUND: Yellow sandy subrounded fine to coarse GRAVEL of limestone and quartzite.			(3.80)												
MADE GROUND: Firm black and dark grey mottled gravelly CLAY. Gravel is angular to subrounded fine to medium flint and quartzite.		4.20		101.56											
MADE GROUND: Stiff blackish brown slightly gravelly CLAY. Gravel is angular to subrounded fine flint and mixed lithologies.			(2.30)												
MADE GROUND: Soft black slightly gravelly organic rich CLAY. Gravel is angular to subrounded fine to medium flint and mixed lithologies.		6.50		99.26											
		11.00		94.76											

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.2 m bgl. 7. SPT Hammer ID: AR3828. Energy Ratio 60%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

**Rotary Core Borehole Log**

 Date: **16/02/2022 - 23/02/2022**

 Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results	
MADE GROUND: Firm dark grey and orange mottled slightly gravelly sandy CLAY. Gravel is angular to subrounded fine to medium flint, sandstone and mudstone. Sand is fine to medium.	[Cross-hatched pattern]										11.50	D5				
											12.00 - 12.45	U5	12.00	U=42 Blows for 90%		
											12.50	D6				
			(5.50)										13.50	SPT(S) N=16 (2,3/4,4,4,4)		
											14.50 - 15.00	B6				
											15.00 - 15.45	U6	15.00	U=42 Blows for 90%		
											15.50	D7				
											16.00 - 16.50	B7				
		16.50		89.26												
Orange brown weak SANDSTONE. (NORTHAMPTON SAND FORMATION)	[Dotted pattern]															
<i>Recovered as medium to coarse angular gravel.</i>																
<i>Recovered as medium to coarse angular gravel.</i>																
<i>Recovered as medium to coarse angular gravel.</i>																
<i>Pocket of gravel.</i>																
<i>Pocket of gravel.</i>																
<i>Pocket of gravel.</i>																
			(3.50)													
													16.95	SPT(S) N=22 (4,8/7,7,4,4)		
							1.5				60					
											130					
											170					
								75	69	53						
							1.5				70		18.75 - 18.84	U1	18.75	
											110		19.00 - 19.10	U2	19.00	
											190					
								67	44	22						
		20.00		85.76			1.5						20.00 - 20.21	U3	20.00	
Moderately weak weathered blue grey thinly bedded LIMESTONE with orange stained fractures. (WHITBY MUDSTONE FORMATION)	[Horizontal line pattern]		(0.40)	85.36							30					
		20.40									70					
											220					
Weak dark grey thinly laminated MUDSTONE. (WHITBY MUDSTONE FORMATION)	[Horizontal line pattern]							100	100	100			21.00 - 21.30	U4	21.00	
							1.6						21.55 - 21.85	U5	21.55	

**Remarks:**  
 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.2 m bgl. 7. SPT Hammer ID: AR3828. Energy Ratio 60%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

Coordinates: <b>E490939.16 N290855.38</b>	Elevation (mAOD): <b>105.76</b>	Drilled By: <b>SDA Site Investigations/ Delta Drilling</b>	Plant Used: <b>Dando 115</b>	Logged: <b>BK/TR</b>	Checked:	Approved:	Scale (m): <b>1:57</b>
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Project No: **15-0645.05**

Hole ID: **BH8**

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Project: **Corby EfW**

**Rotary Core Borehole Log**

Date: **16/02/2022 - 23/02/2022**

Client: **Mytilineos**





Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details		Test Details		Backfill							
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)		Results						
Weak dark grey thinly laminated MUDSTONE. (WHITBY MUDSTONE FORMATION)		30.20	(9.80)	75.56								22.20 - 22.50	U6	22.20								
								77	77	73		22.60 - 22.95	U7	22.60								
							1.5					23.15 - 23.30	U8	23.15								
												23.75 - 23.81	U9	23.75								
								100	100	100		24.10 - 24.40	U11	24.10								
							1.6					25.08 - 25.33	U10	25.08								
								83	75	75	20 170 480	25.60 - 25.75	U12	25.60								
												26.00 - 26.38	U13	26.00								
							1.5					26.52 - 26.80	U14	26.52								
								100	33	93	120 250 370	27.28 - 27.52	U15	27.28								
												27.52 - 27.80	U16	27.52								
							1.5					28.14 - 28.73	U17	28.14								
								100	100	97	50 210 400	28.75 - 29.02	U18	28.75								
												29.08	U19	29.08								
							1.5					29.55 - 29.85	U20	29.55								
												29.85 - 30.20	U21	29.85								
							Borehole complete at 30.20 m bgl.															

**Remarks:**  
 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.2 m bgl. 7. SPT Hammer ID: AR3828. Energy Ratio 60%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

Coordinates: <b>E490939.16 N290855.38</b>	Elevation (mAOD): <b>105.76</b>	Drilled By: <b>SDA Site Investigations/ Delta Drilling</b>	Plant Used: <b>Dando 115</b>	Logged: <b>BK/TR</b>	Checked:	Approved:	Scale (m): <b>1:57</b>
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**Rotary Core Borehole Log** Date: **21/02/2022 - 24/02/2022** Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill		
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results			
MADE GROUND: Pink subrounded to subangular medium to coarse GRAVEL of granite.		-0.20	(0.20)	106.51														
		-0.50	(0.30)	106.21														
MADE GROUND: Yellow sandy subrounded fine to coarse GRAVEL of limestone. MADE GROUND: Soft grey slightly gravelly CLAY. Gravel is subangular to subrounded fine to medium chalk. (REWORKED NATURAL)			(2.50)								1.50 - 1.95	D3	1.50	SPT(S) N=8 (1,0/2,2,2,2)				
												2.00 - 2.50	B1					
												2.50 - 2.95	U1	2.50	U=13 Blows for 100%			
												3.00	D1	3.00	SPT(S) N=4 (1,0/1,1,1,1)			
												3.50 3.50 - 3.95	D4 D5					
MADE GROUND: Soft grey gravelly CLAY. Gravel is subangular to subrounded fine to medium chalk. (REWORKED NATURAL)			(4.10)								4.20	D6						
											4.50 - 4.95	U2	4.50	U=27 Blows for 50%				
												5.00 5.00 - 5.50	D7 B2					
												6.00 6.00 - 6.45	D2 D8	6.00	SPT(S) N=8 (1,2/2,2,2,2)			
												7.10 - 7.50	B3					
MADE GROUND: Soft black organic rich CLAY.			(7.10)								7.50 - 7.95	U3	7.50	U=14 Blows for 100%				
											8.00	B4						
												8.50	D9					
												9.00 - 9.45	D10	9.00	SPT(S) N=10 (6,2/3,2,2,3)			
												9.50 - 10.00	B5					
										10.50 10.50 - 10.95	D11 U4	10.50	U=33 Blows for 100%					
										11.00	D12							

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. SPT Hammer ID: AR2102. Energy Ratio 57%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %



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Project No: **15-0645.05**

Hole ID: **BH9**

Page: **2 of 3**

Project: **Corby EfW**

**Rotary Core Borehole Log**

Date: **21/02/2022 - 24/02/2022**

Client: **Mytilineos**

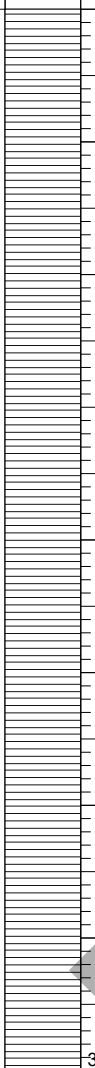
Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results	
MADE GROUND: Soft black organic rich CLAY.											11.50	D13				
											12.00 - 12.35	D14	12.00	SPT(S) N=4 (1,0/1,1,1,1)		
												12.50 - 13.00	B6			
												13.50	D15	13.50	U=12 Blows for 100%	
												13.50 - 13.95	U5			
				14.20		92.51						14.00	D16			
MADE GROUND: Orange slightly clayey sandy angular to subrounded fine to medium GRAVEL of weathered limestone.											14.40 - 14.70	B7				
											15.00 - 15.45	D17	15.00	SPT(S) 50 (9,15/50 for 97mm)		
												16.20	D18			
					(4.30)							16.50 - 16.95	D19	16.50	SPT(S) N=23 (3,5/5,7,5,6)	
												17.20	D20			
				18.50		88.21						18.00 - 18.45	D21	18.00	SPT(S) N=24 (3,4/3,7,7,7)	
Extremely weak grey LIMESTONE. (WHITBY MUDSTONE FORMATION)											18.50 - 19.00	B8				
					(1.50)						19.20	D22				
Weak dark grey thinly laminated MUDSTONE. (WHITBY MUDSTONE FORMATION)											19.50 - 19.95	D23	19.50	SPT(S) 50 (7,12/50 for 173mm)		
				20.00		86.71						20.00 - 20.15	U1	20.00		
												20.00 - 27.33	U13	20.00		
								1.5				20.63 - 20.70	U2	20.63		
												20.80 - 28.00	U14	20.80		
										21.07 - 21.25	U3	21.07				
										21.50 - 21.60	U4	21.50				
										21.80 - 22.10	U5	21.80				

**Remarks:**  
 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation.3. Hand dug service inspection pit advanced to 1.20 m bgl.4. Elevation and location data from GPS survey.5. Borehole commenced as cable percussive with rotary core follow-on.6. Borehole complete at 30.0 m bgl.7. SPT Hammer ID: AR2102. Energy Ratio 57%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

Coordinates: <b>E490885.59 N290869.55</b>	Elevation (mAOD): <b>106.71</b>	Drilled By: <b>SDA Site Investigations/ Delta Drilling</b>	Plant Used: <b>Dando 115</b>	Logged: <b>RS/EC</b>	Checked:	Approved:	Scale (m): <b>1:57</b>
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Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill										
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results											
Weak dark grey thinly laminated MUDSTONE. (WHITBY MUDSTONE FORMATION)				(10.00)																						
																		1.5					22.64 - 22.90	U6	22.64	
																			95	95	95		23.00 - 23.22	U7	23.00	
																		1.5					24.00 - 24.17	U8	24.00	
																			100	100	100		24.50 - 24.95	U11	24.50	
																		1.5					25.20 - 25.44	U10	25.20	
																							25.45 - 25.70	U9	25.45	
																			100	100	93		26.07 - 26.43	U12	26.07	
																		1.5					28.06 - 28.20	U15	28.06	
																							28.41 - 28.73	U16	28.41	
					29.20 - 29.47	U17	29.20																			
		30.00		76.71																						
Borehole complete at 30.00 m bgl.																										

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. SPT Hammer ID: AR2102. Energy Ratio 57%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %









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Project No: **15-0645.05**

Hole ID: **BH10**

Page: **3 of 3**

Project: **Corby EfW**

**Rotary Core Borehole Log**

Date: **22/02/2022 - 23/02/2022**

Client: **Mytilineos**

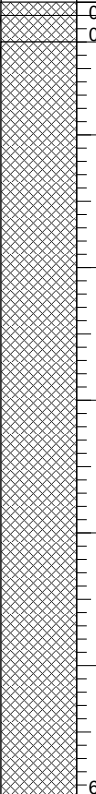
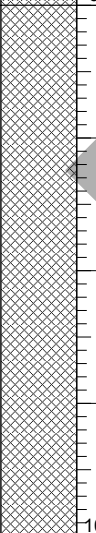
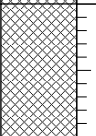
Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill				
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results					
Weak grey laminated MUDSTONE. (WHITBY MUDSTONE FORMATION)				(10.00)			1.5					22.60 - 22.90	U10	22.60						
								100	100	100		23.00 - 23.40	U11	23.00						
												23.44 - 23.73	U12	23.44						
							1.5													
								100	100	96										
							1.5						290 420 540	25.10 - 25.50	U13	25.10				
														25.50 - 25.93	U14	25.50				
								100	100	100				26.00 - 26.30	U15	26.00				
							1.5							27.20 - 27.50	U16	27.20				
								99	99	92				27.68 - 28.02	U17	27.68				
														28.02 - 28.28	U18	28.02				
							1.5							28.37 - 28.57	U19	28.37				
														28.74 - 28.96	U20	28.74				
	100	100	100			90 320 960	29.00 - 29.30	U21	29.00											
							29.30 - 29.60	U22	29.30											
	1.0						29.60 - 29.96	U23	29.60											
Borehole complete at 30.00 m bgl.		30.00		75.64																

**Remarks:**  
 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. Hole installed with 50mm HDPE pipe and flush cover. 8. SPT Hammer ID: AR2102. Energy Ratio 57%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

Coordinates: <b>E490907.41 N290818.12</b>	Elevation (mAOD): <b>105.64</b>	Drilled By: <b>SDA Site Investigations/ CC Ground Investigation</b>	Plant Used: <b>Dando 115</b>	Logged: <b>RS</b>	Checked:	Approved:	Scale (m): <b>1:57</b>
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**Rotary Core Borehole Log**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery					Sample Details			Test Details		Backfill	
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results			
<p>MADE GROUND: Reddish brown subrounded to subangular medium to coarse GRAVEL of granite.</p> <p>MADE GROUND: Reddish brown sandy rounded to subangular fine to coarse GRAVEL of sandstone and limestone. Sand is fine to medium.</p> <p>MADE GROUND: Soft becoming firm grey mottled brown slightly gravelly silty CLAY. Gravel is rounded to subrounded fine to medium of limestone.</p>		0.10		105.05														
		0.30	(0.20)	104.85								0.30	B1					
													1.00	B2				
													1.20 - 1.65	D1	1.20	SPT(S) N=4 (1,1/1,1,1,1)		
													2.00	B3	2.00			
													2.00 - 2.45	U1				
													2.45 - 2.50	D2				
					(5.70)								3.00	B4	3.00	SPT(S) N=17 (2,2/4,4,4,5)		
													3.00 - 3.45	D3				
													4.00	B5	4.00			
<p>MADE GROUND: Firm to stiff grey mottled orange slightly gravelly sandy CLAY with lenses of dark grey silt. Gravel is subangular to rounded fine to medium sandstone.</p>		6.00		99.15														
												6.00	B7					
													6.50 - 6.95	D6				
					(4.00)								8.00	B8	8.00	SPT(S) N=12 (2,3/3,3,3,3)		
													8.00 - 8.45	D7				
<p>MADE GROUND: Stiff grey mottled orange and red slightly gravelly silty CLAY. Gravel is subangular to rounded fine to medium sandstone.</p>		10.00		95.15														
												9.50 - 9.95	D8	9.50	SPT(S) N=14 (9,1/2,3,2,7)			
												10.00	B9					
											11.00 - 11.45	U3	11.00					

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. Hole installed with 50mm HDPE pipe and flush cover. 8. SPT Hammer ID: CABLE01. Energy Ratio 59%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

**Rotary Core Borehole Log**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results	
MADE GROUND: Stiff grey mottled orange and red slightly gravelly silty CLAY. Gravel is subangular to rounded fine to medium sandstone.		12.00	(2.00)	93.15							12.00	B10				
MADE GROUND: Stiff grey slightly sandy gravelly CLAY. Gravel is subangular to rounded fine to coarse of sandstone. Sand is fine to coarse.		15.50	(3.50)	89.65							12.50 - 12.95	D9	12.50	SPT(S) N=26 (4,5/6,7,8)		
Reddish brown SANDSTONE, recovered as very gravelly fine to coarse SAND with small clay lenses. Gravel is subrounded to subangular fine to medium of sandstone. (NORTHAMPTON SAND FORMATION)		18.00	(2.50)	87.15							14.00	B11	14.00	SPT(S) N=49 (2,5/9,15,12,13)		
											14.00 - 14.45	U4				
											14.45 - 14.50	D10				
											15.50 - 15.95	D11	15.50			
Grey mottled brown slightly gravelly sandy CLAY. Gravel is subrounded coarse of sandstone. Sand is fine to coarse. (NORTHAMPTON SAND FORMATION)		18.30	(0.30)	86.85							16.00	B12		SPT(S) 50 (44 for 75mm/50 for 0mm)		
											17.00 - 17.45	U5	17.00			
											17.45 - 17.50	D12				
Weak fractured shelly grey MUDSTONE. Fractures are horizontal to inclination of 45 degrees, close to medium spacing, rough plane, partly open. (WHITBY MUDSTONE FORMATION)		21.12	(2.82)	84.03							18.00 - 18.15	D18	18.00	SPT(S) 50 (44 for 75mm/50 for 0mm)		
											18.30 - 18.46	U1	18.30			
Very weak red thinly laminated MUDSTONE. Fractures are horizontal, wide spacing, smooth planes, very tight. (WHITBY MUDSTONE)											18.88 - 19.04	U2	18.88	SPT(S) 50 (44 for 75mm/50 for 0mm)		
											19.85 - 20.34	U3	19.85			
											19.85 - 20.34	U3	19.85			
											21.26 - 21.33	U4	21.26			
											21.94 - 22.34	U6	21.94			

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. Hole installed with 50mm HDPE pipe and flush cover. 8. SPT Hammer ID: CABLE01. Energy Ratio 59%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %



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Project No: **15-0645.05**

Hole ID: **BH11**

Page: **3 of 3**

Project: **Corby EfW**

**Rotary Core Borehole Log**

Date: **07/02/2022 - 09/02/2022**

Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill				
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results					
Very weak red thinly laminated MUDSTONE. Fractures are horizontal, wide spacing, smooth planes, very tight. (WHITBY MUDSTONE FORMATION) Calcite nodule with clay infill at 21.79m bgl. Calcite nodule with clay infill at 21.92m bgl.  Calcite nodule with clay infill at 25.5m bgl.				(8.93)				100	48	34		22.40 - 22.56	U5	22.40						
							1.6					30 150 230	22.94 - 23.11	U7	22.94					
								65	56	37			23.27 - 23.57	U8	23.27					
							1.5					50 130 200	24.17 - 24.30	U9	24.17					
								65	61	41										
							1.5					60 70 420	25.89 - 26.30	U10	25.89					
								100	99	84										
							1.5					30 340 340	27.45 - 27.77	U11	27.45					
								100	97	100			28.07 - 28.34	U12	28.07					
							1.6					140 220 490	28.64 - 28.84	U13	28.64					
													29.66 - 30.05	U14	29.66					
							Borehole complete at 30.05 m bgl.		30.05		75.10									

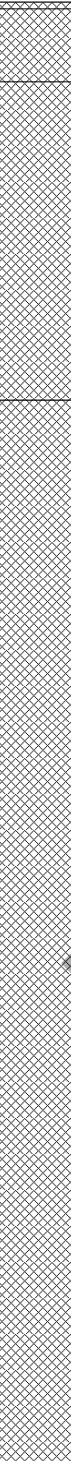
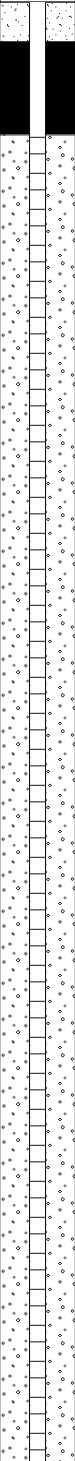
**Remarks:**  
 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. Hole installed with 50mm HDPE pipe and flush cover. 8. SPT Hammer ID: CABLE01. Energy Ratio 59%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

Coordinates: <b>E490949.02 N290832.20</b>	Elevation (mAOD): <b>105.15</b>	Drilled By: <b>Borehole Surveys/ VC Drilling</b>	Plant Used: <b>Dando 2000</b>	Logged: <b>LB</b>	Checked:	Approved:	Scale (m): <b>1:57</b>
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**Rotary Core Borehole Log**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill							
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results								
MADE GROUND: Reddish brown subrounded to subangular medium to coarse GRAVEL of granite.		0.05	(0.55)	104.42																			
		0.60		103.87														0.50	D1	SPT(S) N=8 (1,2/2,2,2,2)			
MADE GROUND: Brown slightly clayey gravelly fine to medium SAND. Gravel is angular to subangular fine to coarse granite, sandstone and brick.			(2.40)															0.60 - 1.20	B1				
		1.00																1.00	1.20 - 1.65		D2 D3 U1		
<u>Cobble of brick.</u> <u>Black geotextile membrane.</u>																		1.65 - 1.80	D4				
MADE GROUND: Soft dark greyish brown sandy gravelly CLAY. Gravel is angular to subrounded fine to coarse chalk, sandstone and mudstone. Sand is fine to coarse.																		2.00 - 2.45	B2		2.00		
																		2.45 - 3.00	D5				
																		3.00 - 3.45	U2		3.00		
MADE GROUND: Soft dark grey slightly sandy gravelly CLAY. Gravel is angular to subrounded fine to coarse chalk and sandstone. Sand is fine to coarse.																		3.45 - 3.65	D6		SPT(S) N=6 (1,1/1,2,2,1)		
																		3.65 - 4.00	D7				
																		4.00 - 4.45	B3			4.00	
																		4.45 - 5.00	D8				
																		5.00 - 5.45	U3			5.00	
																		5.45 - 5.65	D9				
																		5.65 - 6.50	D10				
				6.50 - 6.95	B4	6.50	SPT(S) N=24 (2,4/4,6,6,8)																
				6.95 - 8.00	D12																		
				8.00 - 8.45	U4	8.00																	
				9.50 - 9.95	D13	9.50	SPT(S) N=21 (4,4/5,5,5,6)																
				9.50 - 9.95	D14																		
				9.95 - 11.00	D15																		
				11.00 - 11.45	U5	11.00																	

**Remarks:**

1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. Hole installed with 50mm HDPE pipe and flush cover. 8. SPT Hammer ID: AR2417. Energy Ratio 65%.

**Water Level Observations**

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

 Coordinates:  
**E491083.29 N290885.81**

 Elevation (mAOD):  
**104.47**

 Drilled By:  
 VC Drilling/ CC Ground Investigation

 Plant Used:  
**Dando 2000**

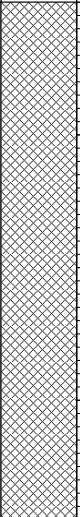
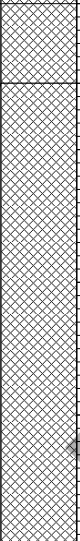
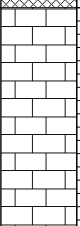


 Logged:  
**BK**

Checked:

Approved:

 Scale (m):  
**1:57**

**Rotary Core Borehole Log**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery					Sample Details			Test Details		Backfill
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results		
MADE GROUND: Soft dark grey slightly sandy gravelly CLAY. Gravel is angular to subrounded fine to coarse chalk and sandstone. Sand is fine to coarse.												11.45 - 11.63	D16				
												12.50 - 12.95	B5	12.50	SPT(S) N=18 (1,2/4,4,4,6)		
													12.95 - 14.00	D17			
													14.00 - 14.45	U6	14.00		
													14.45 - 14.63	D18			
		14.90		89.57													
MADE GROUND: Yellowish brown slightly clayey gravelly fine to medium SAND. Gravel is angular to subrounded fine to coarse mudstone and chalk. MADE GROUND: Firm dark grey slightly gravelly CLAY. Gravel is subangular to subrounded fine to coarse mudstone and limestone.			(0.60)	88.97								15.50 - 15.95	B6	15.50	SPT(S) 41 (5,7/41 for 225mm)		
													15.95 - 17.00	D19			
													17.00 - 17.45	B7	17.00	SPT(S) N=29 (3,6/9,9,6,5)	
													17.45 - 17.95	D20			
													17.80	D21			
		19.00	(3.50)	85.47													
Weak weathered grey thinly bedded LIMESTONE. Weathered brown staining at 19.35 m to 19.50 m. Interbedded weathered brown staining from 19.66 m to 20.39 m. (WHITBY MUDSTONE FORMATION)			(1.68)									19.53 - 19.69	U1	19.53	SPT(S) 50 (10,14/50 for 145mm)		
													20.37 - 20.50	U2	20.37		
													20.50 - 20.63	U3	20.50		
		20.68		83.79													
Weak grey thinly bedded LIMESTONE. (WHITBY MUDSTONE FORMATION)			(0.70)	83.09													
		21.38															
Very weak becoming weak dark grey thinly laminated MUDSTONE												21.50	U4	21.50			

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. Hole installed with 50mm HDPE pipe and flush cover. 8. SPT Hammer ID: AR2417. Energy Ratio 65%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %





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Project No: **15-0645.05**      Hole ID: **BH12**      Page: **3 of 3**

Project: **Corby EfW**

**Rotary Core Borehole Log**      Date: **11/02/2022 - 16/02/2022**      Client: **Mytilineos**

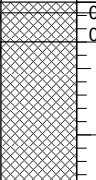
Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill							
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results								
Very weak becoming weak dark grey thinly laminated MUDSTONE (WHITBY MUDSTONE FORMATION)				(8.62)				61	60	60		22.50 - 22.67	U5	22.50									
							1.5					22.96 - 23.42	U6	22.96									
							100	100	94		24.13 - 24.34	U7	24.13										
							1.5				24.78 - 25.20	U8	24.78										
											25.05 - 25.87	U9	25.05										
							100	100	100		26.20 - 26.47	U10	26.20										
							1.5							26.60 - 27.00	U11	26.60							
							100	100	100		27.30 - 27.64	U12	27.30										
							1.5				27.95 - 28.18	U13	27.95										
											28.18 - 28.50	U14	28.18										
							97	97	94		28.50 - 28.94	U15	28.50										
							1.5				28.94 - 29.37	U16	28.94										
											29.70 - 29.93	U17	29.70										
									30.00		74.47												
							Borehole complete at 30.00 m bgl.																

**Remarks:**  
 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 30.0 m bgl. 7. Hole installed with 50mm HDPE pipe and flush cover. 8. SPT Hammer ID: AR2417. Energy Ratio 65%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

Coordinates: **E491083.29 N290885.81**      Elevation (mAOD): **104.47**      Drilled By: **VC Drilling/ CC Ground Investigation**      Plant Used: **Dando 2000**      Logged: **BK**      Checked:      Approved:      Scale (m): **1:57**

**Rotary Core Borehole Log** Date: **17/02/2022** Client: **Mytilineos**

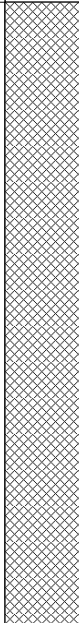
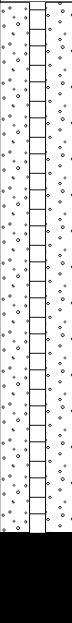
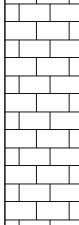





Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery					Sample Details			Test Details		Backfill																	
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results																			
<p>MADE GROUND: Pink subrounded to subangular medium to coarse GRAVEL of granite.</p> <p>MADE GROUND: Yellow sandy subrounded fine to coarse GRAVEL of limestone. Sand is medium to coarse.</p> <p>MADE GROUND: Stiff grey gravelly CLAY. Gravel is rounded to subrounded fine to medium chalk. (REWORKED NATURAL)</p>		0.08	(0.22)	106.60																														
		0.30		106.38															0.00 - 1.20	B1														
																				0.50	D1													
																				1.00	D2													
																				1.20 - 1.65	U1	1.20												
																				1.65 - 1.85	D3													
																				1.85 - 2.00	D4													
																				2.00	B2	2.00	SPT() N=6 (1,1/1,1,1,3)											
																				2.00 - 2.45	D5													
																				2.45 - 3.00	D6													
																				3.00	U2	3.00												
																				3.45 - 3.65	D7													
				3.65 - 4.00	D8																													
				4.00	B3	4.00	SPT() N=28 (2,4/6,6,8,8)																											
				4.00 - 4.45	D9																													
				4.45 - 5.00	D10																													
				5.00	U3	5.00																												
				5.45 - 5.65	D11																													
				5.65 - 6.50	D12																													
				6.50	B4	6.50	SPT() N=18 (2,4/4,4,4,6)																											
				6.50 - 6.95	D13																													
				6.95 - 8.00	D14																													
				8.00	U4	8.00																												
				8.45 - 8.65	D15																													
				8.65 - 9.50	D16																													
				9.50	B5	9.50	SPT() N=30 (4,4/6,6,8,10)																											
				9.50 - 11.00	D17																													
				11.00	B6	11.00	SPT() N=40 (5,9/9,10,10,11)																											
				11.00 - 11.45	D18																													

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 27 m bgl. 7. Hole installed with 50mm HDPE pipe and flush cover. 8. SPT Hammer ID: AR2417. Energy Ratio 65%.

**Water Level Observations** **Flush**

Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

**Rotary Core Borehole Log**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill	
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results		
MADE GROUND: Soft grey slightly sandy CLAY. Sand is fine to medium. (REWORKED NATURAL)												11.45 - 12.50	D19				
													12.00	U5	12.00		
													12.95 - 13.15	D20			
													13.15 - 14.00	D21			
													14.00	B7	14.00		SPT() N=28 (2,5/6,7,7,8)
													14.45 - 15.30	D22			
													15.50	B8	15.50		SPT() N=33 (3,5/7,8,9,9)
													15.50 - 15.95	D23			
													15.95 - 17.00	D24			
													17.00	B9	17.00		SPT() 48 (8,4/48 for 180mm)
Extremely weak weathered orange LIMESTONE. (WHITBY MUDSTONE FORMATION)			(1.75)									17.00 - 17.45	D25				
		17.45		89.23								17.45 - 18.00	D26				
Very weak grey MUDSTONE. (WHITBY MUDSTONE FORMATION)			(0.55)									18.00	D27	18.00	SPT() N=46 (3,5/9,9,14,14)		
		18.00		88.68													
Very weak grey MUDSTONE recovered as soft grey clay. (WHITBY MUDSTONE FORMATION)			(1.76)														
		19.76		86.92													
Very weak grey laminated MUDSTONE. Bedding 0°. (WHITBY MUDSTONE FORMATION)			(1.18)									20.00 - 20.30	U6	20.00			
		20.94		85.74								20.30 - 20.54	U7	20.30			
		21.00		85.68								20.54 - 20.87	U8	20.54			
No recovery - MUDSTONE. (WHITBY MUDSTONE FORMATION)			(1.50)									21.00 - 21.74	U9	21.00			
		21.00		85.68								21.00					
Weak dark grey finely laminated thinly bedded MUDSTONE.												21.46 - 21.87	U10	21.46			
												21.87 - 22.26	U11	21.87			

**Remarks:**  
 1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 27 m bgl. 7. Hole installed with 50mm HDPE pipe and flush cover. 8. SPT Hammer ID: AR2417. Energy Ratio 65%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

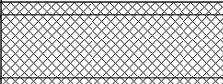
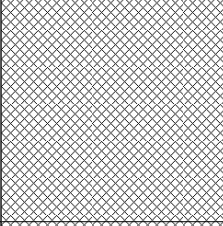
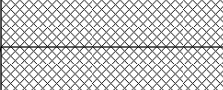
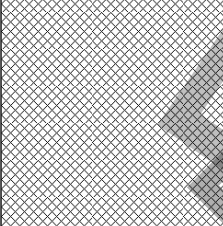
**Rotary Core Borehole Log** Date: **17/02/2022** Client: **Mytilineos**

Description of Strata	Legend	Strata Depth (m)	Strata Thickness (m)	Reduced Level (mAOD)	Casing Diameter (mm)	Water	Core Recovery				Sample Details			Test Details		Backfill
							Run (m)	TCR %	SCR %	RQD %	Min. Fl Av. Fl Max. Fl	Depth (m)	Type & Ref	Depth (m)	Results	
Weak dark grey finely laminated thinly bedded MUDSTONE. (WHITBY MUDSTONE FORMATION)		22.50		84.18				100	97	96						
<i>Sideritic</i> Weak grey laminated medium bedded MUDSTONE.			(1.20)				1.5				22.90 - 23.39	U12	22.90			
Weak grey laminated medium bedded MUDSTONE. (WHITBY MUDSTONE FORMATION)		23.70		82.98				100	60	14	23.39 - 23.64	U13	23.39			
<i>Sideritic</i> Weak grey laminated medium bedded MUDSTONE.			(4.50)								23.64 - 23.84	U14	23.64			
<i>Sideritic</i> Weak grey laminated medium bedded MUDSTONE.			(3.30)								24.58 - 24.68	U15	24.58			
							1.5	89	87	81						
		27.00		79.68												
Borehole complete at 27.00 m bgl.		27.00		79.68												

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020. 2. Borehole location cleared for underground utilities prior to excavation. 3. Hand dug service inspection pit advanced to 1.20 m bgl. 4. Elevation and location data from GPS survey. 5. Borehole commenced as cable percussive with rotary core follow-on. 6. Borehole complete at 27 m bgl. 7. Hole installed with 50mm HDPE pipe and flush cover. 8. SPT Hammer ID: AR2417. Energy Ratio 65%.

Water Level Observations				Flush	
Date	Depth Strike (m)	Duration (min)	Standing (m)	Depth (m)	Return %

**Trial Pit Log**

Description of Strata	Legend	Strata Depth (m)	Reduced Level (mAOD)	Water Strike (m)	Sample Details		Test Details		
					Depth (m)	Type & Ref	Depth (m)	Results	
MADE GROUND: Reddish brown subrounded to subangular medium to coarse GRAVEL of granite. MADE GROUND: Light yellowish brown sandy subrounded fine to coarse GRAVEL of limestone.		0.05	104.46						
		0.30	104.21						
MADE GROUND: Stiff grey gravelly CLAY. Gravel is rounded to subrounded fine to medium chalk. (REWORKED NATURAL)					0.50	D1	0.50	HV=49 kPa	
							1.00	HV=56 kPa	
			1.20	103.31					
MADE GROUND: Stiff grey mottled brown slightly sandy gravelly CLAY. Gravel is rounded to subrounded fine to medium chalk. Sand is medium to coarse. (REWORKED NATURAL)					1.30	B1			
							1.50	HV=83 kPa	
			1.40	103.11					
MADE GROUND: Stiff grey slightly gravelly CLAY. Gravel is rounded to subrounded fine to medium chalk.					2.00	D2	2.00	HV=90 kPa	
					2.40	B2			
							2.60	HV=54 kPa	
		3.00	101.51						
Trial pit complete at 3.00 m bgl.									

Dimensions and Orientation:



Orientation:

Inclination:

**Remarks:**

1. Logged in general accordance with BS5930:2015+A1:2020.2. Location cleared for services by specialist utilities avoidance contractor prior to excavation. Elevation and location data from GPS survey.3. Installed for infiltration testing.

Coordinates:  
**E491034.03 N290872.00**

Elevation (mAOD):  
**104.51**

Excavated By:  
**F.W. Pammenter & Son**


Plant Used:  
**JCB 3CX**

Logged:  
**RS**


Checked:

Approved:

Scale:  
**1:30**

Description of Strata	Legend	Strata Depth (m)	Reduced Level (mAOD)	Water Strike (m)	Sample Details		Test Details	
					Depth (m)	Type & Ref	Depth (m)	Results
MADE GROUND: Reddish brown subrounded to subangular medium to coarse GRAVEL of granite.		0.10	104.11		0.40	B1	0.50	HV=42 kPa
MADE GROUND: Light yellowish brown sandy subrounded fine to coarse GRAVEL of limestone.		0.30	103.91					
MADE GROUND: Firm grey gravelly CLAY. Gravel is rounded to subrounded fine to medium chalk. (REWORKED NATURAL)		0.60	103.61					
MADE GROUND: Stiff brown sandy gravelly CLAY. Gravel is rounded to subangular fine to medium chalk. Sand is medium to coarse. (REWORKED NATURAL)		1.00	103.21					
MADE GROUND: Stiff grey slightly gravelly CLAY. Gravel is rounded to subrounded fine to medium chalk.		2.90	101.31					
Trial pit complete at 2.90 m bgl.								

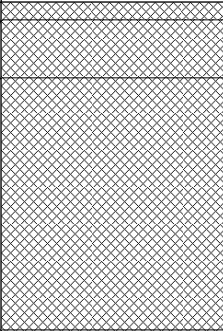

Dimensions and Orientation:




Orientation: \_\_\_\_\_

Inclination: \_\_\_\_\_

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020.2. Location cleared for services by specialist utilities avoidance contractor prior to excavation. Elevation and location data from GPS survey.3. Installed for infiltration testing.

Description of Strata	Legend	Strata Depth (m)	Reduced Level (mAOD)	Water Strike (m)	Sample Details		Test Details	
					Depth (m)	Type & Ref	Depth (m)	Results
MADE GROUND: Reddish brown subrounded to subangular medium to coarse GRAVEL of granite.		0.07	104.41					
MADE GROUND: Light yellowish brown sandy subrounded fine to coarse GRAVEL of limestone.		0.30	104.18					
MADE GROUND: Firm grey gravelly CLAY with moderate concrete cobble content. Gravel is rounded to subrounded fine to medium chalk. (REWORKED NATURAL)					0.50	D1		
					1.00	B1	1.00	HV=45 kPa
		1.30	103.18					
MADE GROUND: Stiff grey slightly gravelly CLAY. Gravel is rounded to subrounded fine to medium chalk. (REWORKED NATURAL)					1.50	D2		
					2.00	B2	2.00	HV=63 kPa
					2.50	D3		
			2.80	101.68				
Trial pit complete at 2.80 m bgl.						3.00	HV=69 kPa	

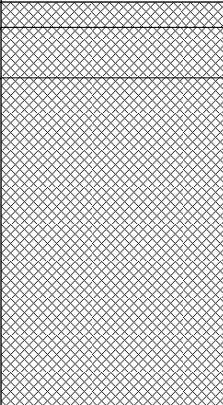
Dimensions and Orientation:



Orientation: \_\_\_\_\_

Inclination: \_\_\_\_\_

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020.2. Location cleared for services by specialist utilities avoidance contractor prior to excavation. Elevation and location data from GPS survey.3. Installed for infiltration testing.

Description of Strata	Legend	Strata Depth (m)	Reduced Level (mAOD)	Water Strike (m)	Sample Details		Test Details	
					Depth (m)	Type & Ref	Depth (m)	Results
MADE GROUND: Reddish brown subrounded to subangular medium to coarse GRAVEL of granite.		0.10	104.85					
MADE GROUND: Light yellowish brown sandy subrounded fine to coarse GRAVEL of limestone.		0.30	104.65					
MADE GROUND: Stiff grey slightly gravelly CLAY. Gravel is rounded to subrounded fine to medium chalk. (REWORKED NATURAL)							1.00	HV=90 kPa
		1.60	103.35				1.50	HV=50 kPa
Trial pit complete at 1.60 m bgl.								

Dimensions and Orientation:




Orientation: \_\_\_\_\_


Inclination: \_\_\_\_\_

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020.2. Location cleared for services by specialist utilities avoidance contractor prior to excavation. Elevation and location data from GPS survey.3. Installed for infiltration testing.



Description of Strata	Legend	Strata Depth (m)	Reduced Level (mAOD)	Water Strike (m)	Sample Details		Test Details	
					Depth (m)	Type & Ref	Depth (m)	Results
MADE GROUND: Reddish brown subrounded to subangular medium to coarse GRAVEL of granite.		0.10	104.85					
MADE GROUND: Light yellowish brown sandy subrounded fine to coarse GRAVEL of limestone. Sand is fine to coarse.		0.35	104.60					
MADE GROUND: Stiff grey slightly gravelly CLAY. Gravel is rounded to subrounded fine to medium chalk and brick.					0.60	B1	0.60	HV=66 kPa
					1.00	D1	1.20	HV=83 kPa
					1.50	B2	1.60	HV=66 kPa
				2.00	D2			
				2.30		2.30	HV=73 kPa	
		2.50	102.45					
MADE GROUND: Stiff light yellowish brown and grey mottled sandy gravelly CLAY. Gravel is rounded to subangular fine to medium chalk. Sand is medium to coarse. (REWORKED NATURAL)				2.50	B3			
		3.00	101.95					
Trial pit complete at 3.00 m bgl.								

Dimensions and Orientation:




Orientation: \_\_\_\_\_

Inclination: \_\_\_\_\_

**Remarks:**  
1. Logged in general accordance with BS5930:2015+A1:2020.2. Location cleared for services by specialist utilities avoidance contractor prior to excavation. Elevation and location data from GPS survey.3. Installed for infiltration testing.

**Trial Pit Log**

Description of Strata	Legend	Strata Depth (m)	Reduced Level (mAOD)	Water Strike (m)	Sample Details		Test Details	
					Depth (m)	Type & Ref	Depth (m)	Results
MADE GROUND: Reddish brown subrounded to subangular medium to coarse GRAVEL of granite.		0.10	104.53					
MADE GROUND: Light yellowish brown sandy subrounded fine to coarse GRAVEL of limestone.		0.35	104.28		0.30	B1		
MADE GROUND: Stiff reddish brown and grey mottled slightly gravelly CLAY. Gravel is rounded to subrounded fine to medium chalk.					0.50	B2		
					1.00	D1		
MADE GROUND: Stiff brown and grey mottled slightly gravelly CLAY. Gravel is rounded to subrounded fine to medium chalk.		1.40	103.23		1.50	B3	1.50	HV=100 kPa
					2.00	D2		
							2.50	HV=90 kPa
Trial pit complete at 2.90 m bgl.		2.90	101.73					

Dimensions and Orientation:



Orientation:

Inclination:

**Remarks:**

1. Logged in general accordance with BS5930:2015+A1:2020.2. Location cleared for services by specialist utilities avoidance contractor prior to excavation. Elevation and location data from GPS survey.3. Installed for infiltration testing.



# SPT Hammer Energy Test Report

in accordance with BSEN ISO 22476-3:2005 + A1:2011

SPT Hammer Ref: CABLE 01  
Test Date: 10/02/2022  
Report Date: 14/02/2022  
File Name: CABLE 01.spt  
Test Operator: RW

## Instrumented Rod Data

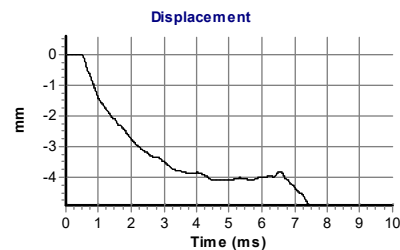
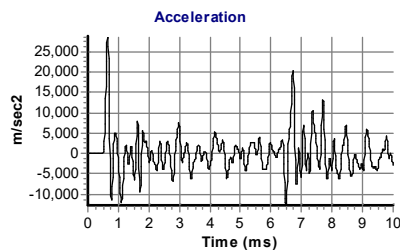
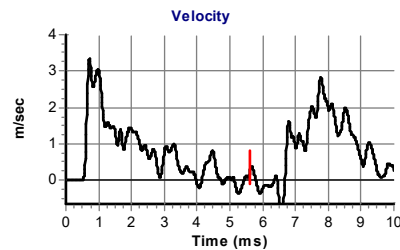
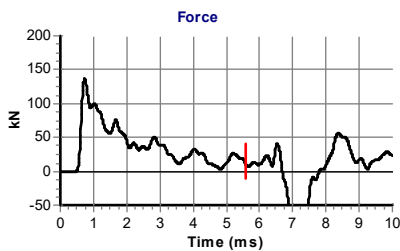
Diameter  $d_r$  (mm): 54  
Wall Thickness  $t_r$  (mm): 6.6  
Assumed Modulus  $E_a$  (GPa): 208  
Accelerometer No.1: 63177  
Accelerometer No.2: 63178

## SPT Hammer Information

Hammer Mass  $m$  (kg): 63.5  
Falling Height  $h$  (mm): 760  
SPT String Length  $L$  (m): 13.6

## Comments / Location

Test performed at J&M yard.



## Calculations

Area of Rod  $A$  (mm<sup>2</sup>): 983  
Theoretical Energy  $E_{\text{theor}}$  (J): 473  
Measured Energy  $E_{\text{meas}}$  (J): 281

**Energy Ratio  $E_r$  (%):** 59

Signed: Richard Walter BEng (Hons)  
Title: Drilling Manager (J&M Drilling Ltd)

# SPT Hammer Energy Test Report

in accordance with BSEN ISO 22476-3:2005

**ARCHWAY ENGINEERING (UK) LTD**  
**AINLEYS INDUSTRIAL ESTATE**  
**ELLAND**  
**WEST YORKSHIRE**  
**HX5 9JP**

SPT Hammer Ref: AR2417  
Test Date: 21/12/2021  
Report Date: 21/12/2021  
File Name: AR2417.spt  
Test Operator: JL

## Instrumented Rod Data

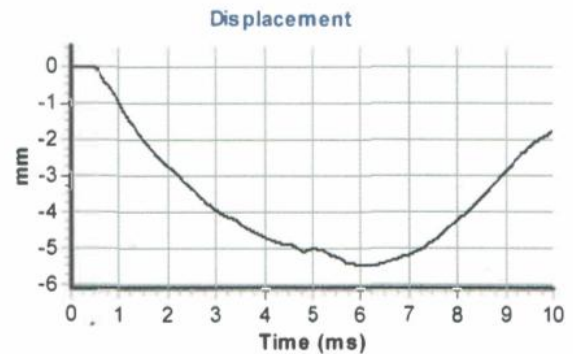
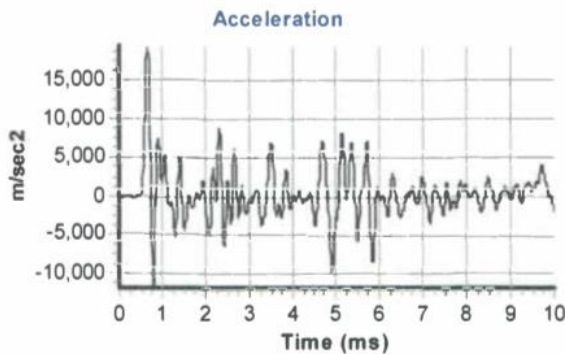
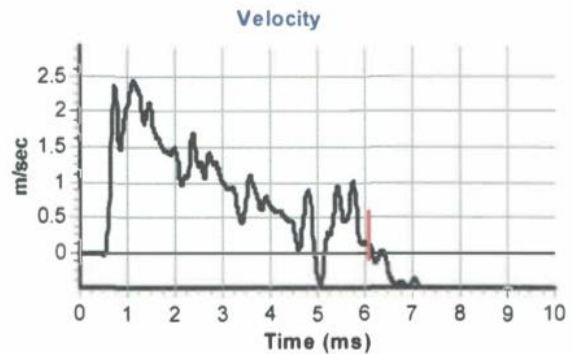
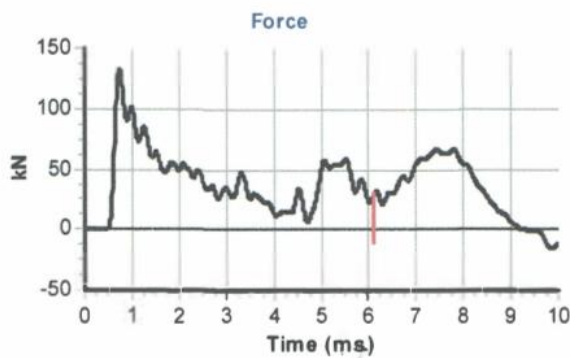
Diameter  $d_r$  (mm): 54  
Wall Thickness  $t_r$  (mm): 6.3  
Assumed Modulus  $E_a$  (GPa): 208  
Accelerometer No.1: 7080  
Accelerometer No.2: 11609

## SPT Hammer Information

Hammer Mass  $m$  (kg): 63.5  
Falling Height  $h$  (mm): 760  
SPT String Length  $L$  (m): 10.0

## Comments / Location

VC DRILLING - 73802



## Calculations

Area of Rod A ( $\text{mm}^2$ ): 944  
Theoretical Energy  $E_{\text{theor}}$  (J): 473  
Measured Energy  $E_{\text{meas}}$  (J): 307

**Energy Ratio  $E_r$  (%):** **65**

Signed: J.LOCK

Title: FITTER

The recommended calibration interval is 12 months

# SPT Hammer Energy Test Report

in accordance with BSEN ISO 22476-3:2005

**Southern Testing**  
**Unit 11**  
**Charlwood Road**  
**East Grinstead**  
**West Sussex**  
**RH19 2HU**

SPT Hammer Ref: AR2102  
Test Date: 15/05/2021  
Report Date: 15/05/2021  
File Name: AR2102.spt  
Test Operator: NPB

## Instrumented Rod Data

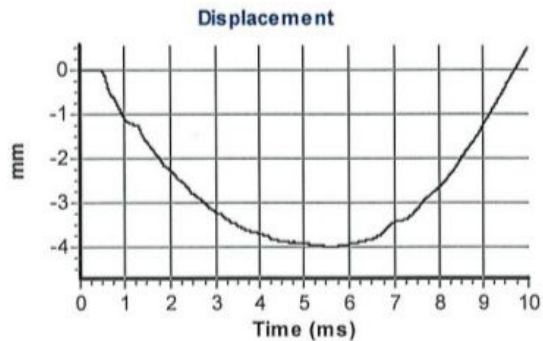
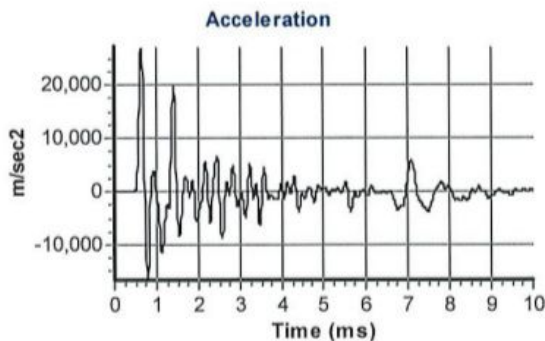
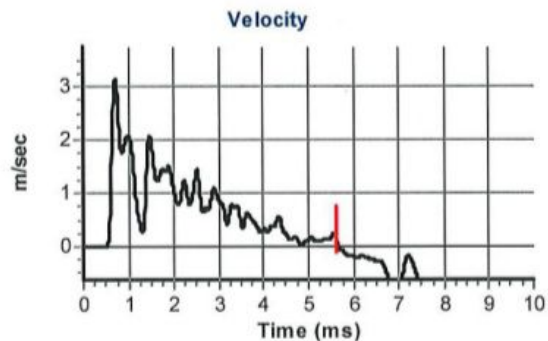
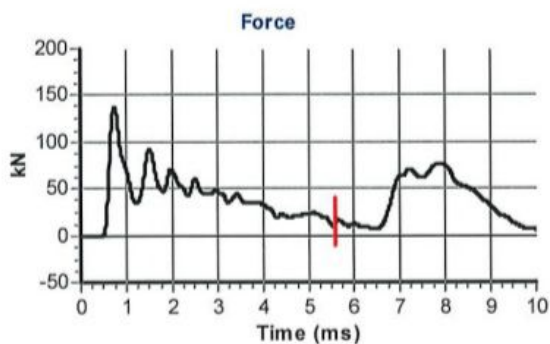
Diameter  $d_r$  (mm): 54  
Wall Thickness  $t_r$  (mm): 6.6  
Assumed Modulus  $E_a$  (GPa): 208  
Accelerometer No.1: 64786  
Accelerometer No.2: 64789

## SPT Hammer Information

Hammer Mass  $m$  (kg): 63.5  
Falling Height  $h$  (mm): 760  
SPT String Length  $L$  (m): 14.5

## Comments / Location

CHARLWOODS



## Calculations

Area of Rod A ( $\text{mm}^2$ ): 983  
Theoretical Energy  $E_{\text{theor}}$  (J): 473  
Measured Energy  $E_{\text{meas}}$  (J): 269

**Energy Ratio  $E_r$  (%)**:

**57**

Signed: N P Burrows

Title: Field Operations Manager

The recommended calibration interval is 12 months



# SPT Hammer Energy Test Report

in accordance with BSEN ISO 22476-3:2005

**ARCHWAY ENGINEERING (UK) LTD**  
**AINLEYS INDUSTRIAL ESTATE**  
**ELLAND**  
**WEST YORKSHIRE**  
**HX5 9JP**

SPT Hammer Ref: AR3828  
Test Date: 16/12/2021  
Report Date: 16/12/2021  
File Name: AR3828.spt  
Test Operator: JL

## Instrumented Rod Data

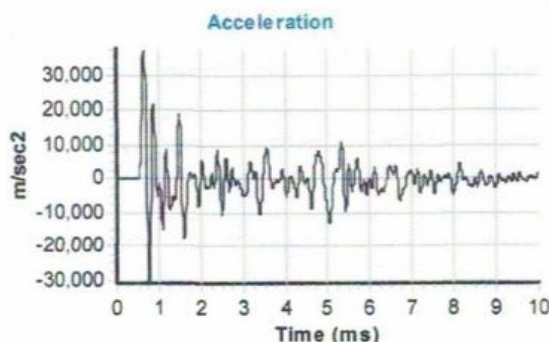
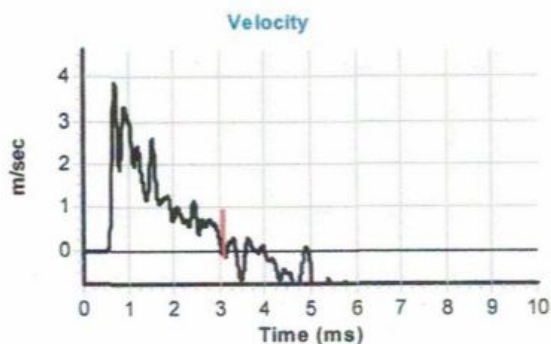
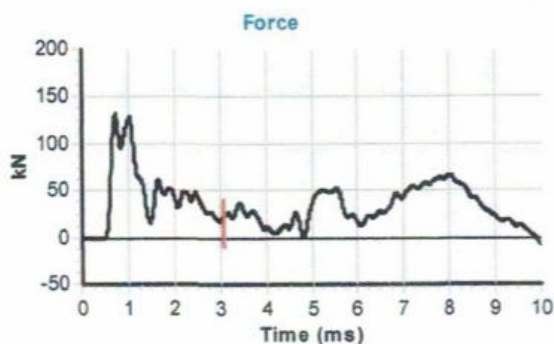
Diameter  $d_r$  (mm): 54  
Wall Thickness  $t_r$  (mm): 6.0  
Assumed Modulus  $E_a$  (GPa): 200  
Accelerometer No.1: 7080  
Accelerometer No.2: 11609

## SPT Hammer Information

Hammer Mass  $m$  (kg): 63.5  
Falling Height  $h$  (mm): 760  
SPT String Length  $L$  (m): 10.0

## Comments / Location

SDA SITE INVESTIGATION LTD - 78525



## Calculations

Area of Rod A ( $\text{mm}^2$ ): 905  
Theoretical Energy  $E_{\text{theor}}$  (J): 473  
Measured Energy  $E_{\text{meas}}$  (J): 284

**Energy Ratio  $E_r$  (%):** 60

Signed: J.LOCK  
Title: FITTER

The recommended calibration interval is 12 months



# SPT Hammer Energy Test Report

in accordance with BSEN ISO 22476-3:2005 +A1:2011

**James and Milton Drilling Ltd**  
**63 Fakenham Road**  
**Great Ryburgh**  
**NR21 7AW**

SPT Hammer Ref: CC03..  
Test Date: 26/02/2022  
Report Date: 01/03/2022  
File Name: CC03.spt  
Test Operator: RW

## Instrumented Rod Data

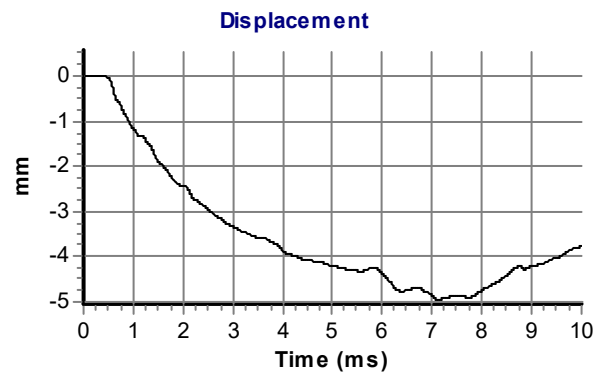
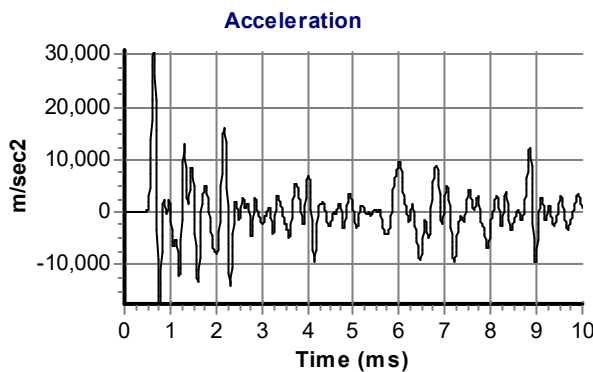
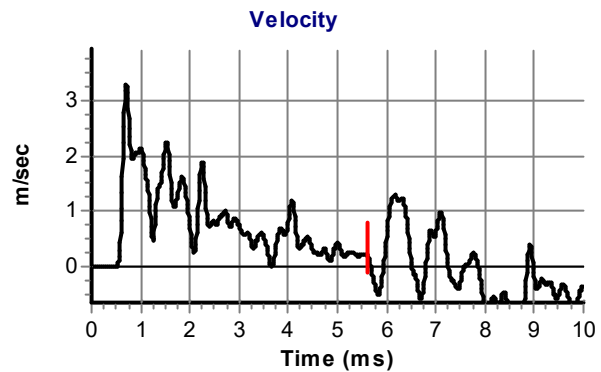
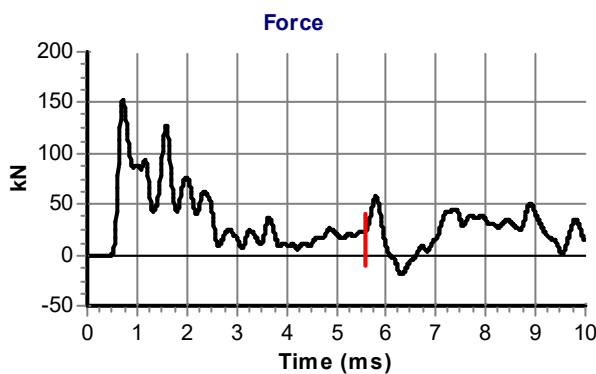
Diameter  $d_r$  (mm): 54  
Wall Thickness  $t_r$  (mm): 6.6  
Assumed Modulus  $E_a$  (GPa): 208  
Accelerometer No.1: 63177  
Accelerometer No.2: 63178

## SPT Hammer Information

Hammer Mass  $m$  (kg): 63.5  
Falling Height  $h$  (mm): 760  
SPT String Length  $L$  (m): 13.7

## Comments / Location

CC YARD



## Calculations

Area of Rod A (mm<sup>2</sup>): 983  
Theoretical Energy  $E_{theor}$  (J): 473  
Measured Energy  $E_{meas}$  (J): 289

**Energy Ratio  $E_r$  (%):** **61**

Signed: Richard Walter BEng (Hons)  
Title: Drilling Manager (J&M Drilling Ltd)

## Appendix C - Cone Penetration Testing (CPT) Report



# IN SITU

SITE INVESTIGATION

## STATIC CONE PENETRATION TEST FACTUAL REPORT

**CLIENT:** Delta Simons  
**PROJECT:** Corby EFW



<b>Project</b>	<b>Corby EFW</b>
<b>Project No.</b>	<b>1220144</b>
<b>Client</b>	<b>Delta Simons</b>
<b>Address</b>	<b>3 Henley Office Park, Doddington Road, Lincoln, LN6 3QR</b>

**Attention:** Mr Harry Whittle

Dear Mr Whittle,

We have pleasure in providing a digital copy of our report and data in AGS format for the above project.

We hope that you are satisfied with the performance of our staff, equipment and reporting on this project. If you should have any queries about any aspect of the works carried out, please do not hesitate to contact us. We look forward to being of service to you in the future.

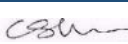


Yours faithfully,

**In Situ Site Investigation Limited**



Darren Ward  
Director

**Report Issue**

Issue	Date	Prepared	Sign	Checked	Sign	Approved	Sign
01	21/02/2022	Chloe Donovan		Luisa Dhimitri		Darren Ward	

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## 1.0 INTRODUCTION

In Situ Site Investigation Limited (In Situ) was engaged in a geotechnical site investigation at Corby EFW at the request of Delta Simons. The site investigation consisted of completing 20 Static Piezocone Penetration Tests (CPTU) and 1 Seismic Dilatometer Marchetti Tests (SDMT) to provide information on the soil conditions and derived geotechnical parameters at:

Shelton Road,  
Willowbrook East Industrial Estate,  
Corby  
NN17 5XH

All test locations were provided by the client. A site map is included in the end of Appendix A of this report (if provided by the client). The tests were stopped when they reached the target depth as per the client's technical specifications or for other technical reasons, as detailed in the *Project Summary Table* in *Appendix A.1* and on each CPTU log included in Appendix B of this report.

The fieldwork was carried out from 9<sup>th</sup> February 2022 to 11<sup>th</sup> February 2022 as per the client's request.

The work on site and the final factual reporting have been undertaken in accordance with the international technical standard *BS EN ISO 22476-1:2012*.

## 2.0 FIELDWORK

### 2.1 CONE PENETRATION TESTS

The fieldwork activity is summarised in Table 2.1.

Table 2.1 Fieldwork Summary	
CPT Operator/s	Tom Rademaker
Date Started	9 <sup>th</sup> February 2022
Date Finished	11 <sup>th</sup> February 2022
In Situ S.I. Project Manager	Darren Ward
Main Contractor's Site Manager	Robert Stafford

#### 2.1.1 Rig Information

Details of CPTU rig used in this project are shown in Table 2.2. Full data sheet for the rig is presented in *Appendix A.2*.

Table 2.2 Rig Summary	
Rig Name	Rig Description
CPT016	20 Tonne Wheel Mounted CPT Rig

#### 2.1.2 CPTU Cone

Details of electric CPTU cones (Type TE2) used in this project conforming to the requirements of Application Class 2 of *ISO 22476-1:2012*, are shown in Table 2.3.

Table 2.3 Cone Summary		
Number	Cross-section area	Filter position
S15-CFIP.1867	15cm <sup>2</sup>	u <sub>2</sub>
DP10-CFPTxy.60154	10cm <sup>2</sup>	

A full datasheet of the cones used are shown in *Appendix A.3*.

The cone's measured parameters are shown in Table 2.4.

Table 2.4 Completed Fieldwork Summary
20 CPTU to a maximum depth of 29.02m. Each test measured Cone Resistance, $q_c$ , Sleeve Friction, $f_s$ , Porewater Pressure in the shoulder position, $u_2$ , Inclination in X and Y axes.
<i>Provision of factual report with estimated soil type, derived geotechnical parameters &amp; AGS data file.</i>

### 2.1.3 CPTU Cone Calibration

The cone resistance and sleeve friction are recorded by calibrated load cells in the cone. The CPTU load cells and pressure transducers are regularly calibrated in line with *ISO 22476-1:2012* standard by the cone manufacturer. The cone calibration certificate for the cone used at this site are presented in *Appendix A.4*.

### 2.1.4 CPTU Cone Saturation

The pore water pressure is recorded using a calibrated pressure transducer located in the piezocone. To ensure pore water pressure measurements are not affected by the presence of air in the measuring transducer, a de-airing procedure is carried out prior to each test. The cone and filter are saturated using a glycerine fluid with a viscosity of 10,000 CST.

### 2.1.5 Test Procedure

The tests are carried out in accordance with the *International Standard for Electrical Cone and Piezocone Penetration Test (ISO 22476-1:2012)*.

The final depths of the tests were determined by either completion to the specified test depth or when the maximal safe capacity of the equipment was reached. A schedule of the tests performed is shown in *Appendix A.1*, which has been compiled from the operators' daily progress reports.

The data is transmitted from the digital CPTU through an umbilical cable that runs through the push rods to the data acquisition system. Results are displayed instantaneously on the computer logging screen. The results are recorded on the computer hard disc.

The rate of penetration is kept constant at 20 mm/s  $\pm$  5 mm/s except when penetrating very dense or hard strata. Before each test is carried out zero values are taken of the cone to check if it is within calibration. At the end of each test, zero values are taken again to see if there has been any drift during the test. These values are inspected during the post processing stage. This is a quality check on the data and the testing procedure. Individual test zero values are shown on their corresponding test results in *Appendix B*.

### 2.1.6 In Situ Pore Pressure ( $u_0$ )

The in situ or hydrostatic pore pressure is required for the calculation of several derived parameters included in this report. For this report, the groundwater level is assumed at 2.00 m below ground surface, for calculation purposes. The in situ pore pressure ( $u_0$ ) values are presented on the pore pressure plot, on *CPT Log 01*, which is included in *Appendix B*.



## 2.2 POSITIONING

Positioning and surveying of all investigated locations was the responsibility of the client.

## 2.4 SEISMIC TESTS

The shear wave velocity,  $V_s$  data was measured every 50 cm, by using Seismic Dilatometer Marchetti, *SDMT* probe. Results of the tests are shown in *CPT Log 06, Appendix B* also in Appendix C, where a SDMT report generated from SDMT software is included.

### 2.3.1 S Wave Test Procedure

SDMT tests are carried out in accordance with *ASTM D7400-14* standard and ISSMGE TC10 guideline (*Butcher et al., 2015*). The seismic module is a tubular element equipped with two S wave receivers, at a distance of 0.5 m and two P wave receivers at a distance of 0.604 m apart. The test interval varies from 0.5m to 1m depending on the client’s requirements.

The S wave is generated at the ground surface by hitting a steel beam that sits under the tracks of the CPT rig with a hammer. The S wave reaches the upper and then the lower receivers and  $V_s$  is obtained by the following formula and Figure 2.1:

$$V_s = \frac{S_2 - S_1}{\Delta t}$$

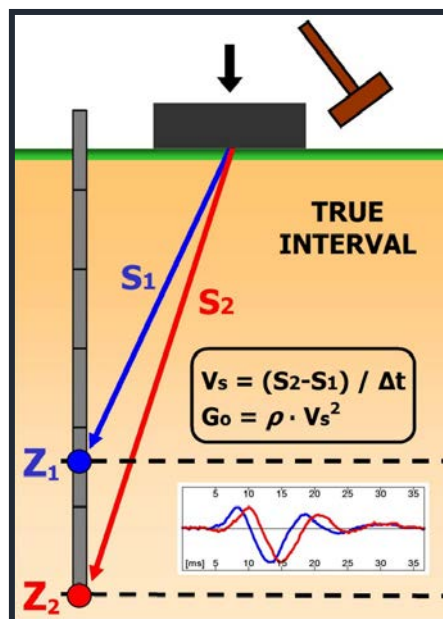
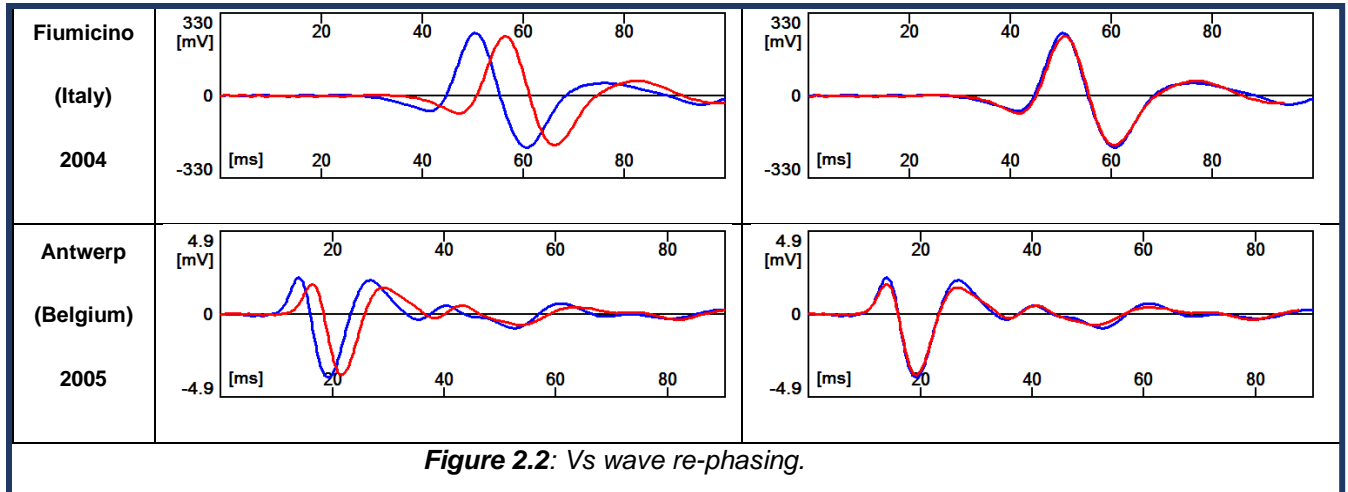


Figure 2.1: Test procedure to obtain  $V_s$ .

This process is carried out 3 times and if the coefficient of variation is less than 10% then the test is accepted. If it is more than 10% further hits are taken until the variation is less than 10%.

Once collected the Vs is calculated by re-phasing the S2 wave over the S1 wave as shown in Figure 2.2. All Vs results are presented alongside the CPT results in *Appendix B*. All seismogram data and tabular data are presented in *Appendix C*.



## 3.0 CONE PENETRATION MEASURED PARAMETERS

All measured parameters of tests carried with the CPTU cone are shown in *Appendix B* and all the information about data processing and results are given in sections 3.1, 3.2 and 3.3.

### 3.1 DATA PROCESSING

The measured parameters, cone end resistance,  $q_c$ , sleeve friction,  $f_s$ , porewater pressure measurements with filter in shoulder position,  $u_2$  and inclination for  $x$  and  $y$  axis,  $l_x$ ,  $l_y$ , were recorded for every 10 mm of penetration keeping a constant speed of 20 mm/s  $\pm$  5 mm/s, which may slightly change when the cone is penetrating hard strata.

The measured data from the site works is processed and presented using specialised CPT software. The interpretations on the CPTU results were carried out following the recommendations of *Lunne et al. (1997)*, *Robertson (2015)* and *BS EN ISO 22476-1:2012*. Measured parameters, mentioned in *Sections 3.2* and *3.3*, were used to derive all the geotechnical parameters, which are presented in *Chapter 4.0*. The soil behaviour type method used on this report is *Robertson et al. (1986)*, shown in *Figure 3.2*.

#### 3.1.1 Zero Measurements

Before and after each CPTU test, zero measurements are recorded for each channel of the cone. The zero measurements are presented on the logs in *Appendix B*. This is a routine quality check carried out on site.

### 3.2 MEASURED PARAMETERS

#### 3.2.1 Cone Resistance ( $q_c$ )

Cone resistance,  $q_c$ , is measured as the total force acting on the cone, divided by the projected area of the cone. The results are presented in MPa, on *CPT Log 01*, in *Appendix B*, scale 0-20 MPa with a minor scale printing on the same graph at 0-4 MPa.

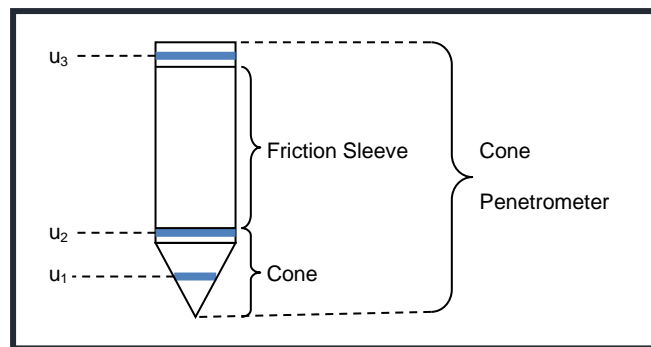
#### 3.2.2 Sleeve Friction ( $f_s$ )

Sleeve friction,  $f_s$ , is measured as the total frictional force acting on the friction sleeve divided by its surface area. The results are presented in kPa, on *CPT Log 01*, in *Appendix B*, using a scale of 0-500 kPa.

### 3.2.3 Porewater pressure ( $u_2$ )

The pore pressure,  $u_2$ , is measured during the test. If the material is free draining and saturation is maintained it will normally measure hydrostatic pore pressure. In materials that are not free draining, it will record the total pore pressure (hydrostatic plus any excess pore pressures generated) created by the cone penetration through this material.

The filter element can be mounted in one of three positions. For all tests carried out in this project the filter was mounted in the  $u_2$  position (see *Figure 3.1*).



**Figure 3.1:** Diagram showing pore pressure filter locations (after Lunne et al., 1997)

### 3.2.4 Inclination ( $I_x, I_y$ )

The CPT rig was set up to obtain a thrust direction as near as possible to vertical. The CPTU cones have inclinometers incorporated to measure the non-verticality of the test. For test depths less than 15 m, significant non-verticality is unusual, provided the initial thrust direction is vertical.

## 3.3 ESTIMATED SOIL BEHAVIOUR TYPE

### 3.3.1 Friction Ratio ( $R_f$ )

The friction ratio,  $R_f$  is the ratio between the sleeve friction and the cone resistance (Lunne et al., 1997).

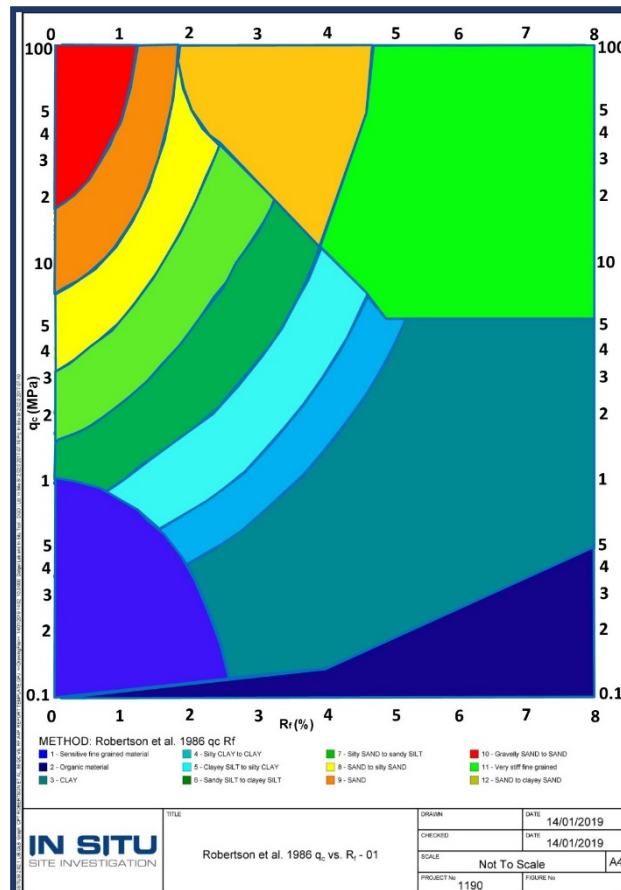
$$\text{Friction Ratio } (R_f) = \left( \frac{\text{Sleeve Friction } (f_s)}{\text{Cone Resistance } (q_c)} \right) \times 100$$

### 3.3.2 Estimated Soil Behaviour Type (SBT)

The estimation of soil behaviour type, *SBT*, using measurements of cone resistance and sleeve friction is based upon the variations of the friction ratio and cone resistance. The friction

ratio varies depending upon whether the soil is cohesive or granular. The cone resistance varies depending on the strength and densities of the soil.

The interpretation used in this report is *Robertson et al. (1986)*, which is shown in Figure 3.2. The results are presented on *CPT Log 01*, in *Appendix B*.



**Figure 3.2:** *Robertson et al., 1986 soil behaviour type chart.*

### 3.3.3 Pore Pressure Ratio ( $B_q$ )

Pore pressure ratio,  $B_q$  is the ratio between the measured pore pressure generated during penetration and the corrected cone resistance minus the total overburden stress.

Pore pressure ratio as defined by *Senneset and Janbu (1985)* is defined as:

$$B_q = \frac{u_2 - u_0}{q_t - \sigma_{vo}}$$

where

- $u_2$  is pore pressure measured between the cone and the friction sleeve
- $u_0$  is equilibrium pore pressure
- $\sigma_{vo}$  is total overburden stress
- $q_t$  is cone resistance corrected for unequal end area effects

### 3.4 APPLIED CORRECTIONS

#### 3.4.1 Corrected Cone Resistance ( $q_t$ )

For each penetration test, the measured cone resistance,  $q_c$ , can be corrected for the “unequal area effect” due to the influence of the ambient pore water pressure acting on the cone.

The correction has been applied using the following equation by Lunne et al., 1997:

$$q_t = q_c + [u_2 \cdot (1 - \alpha)]$$

where

$\alpha$  is the cone area ratio

The cone used on this project has a cone area ratio of 0.79. This value is geometrically measured.

#### 3.4.2 Depth Correction

All tests in the report have been corrected for depth difference caused by inclination. This has been calculated using the method described in ISO 22476-1:2012.

To calculate the corrected depth the following formula is used:

$$z = \int_0^l C_{inc} \cdot dl$$

where

$z$  is penetration depth, in  $m$

$l$  is penetration length, in  $m$

$C_{inc}$  is correction factor for the effect of the inclination of the CPTU relative to the vertical axis.

The equation for calculating the correction factor for the influence of the inclination for a bi-axial inclinometer is:

$$C_{inc} = \frac{1}{\sqrt{(1 + \tan^2 \beta_1 + \tan^2 \beta_2)}}$$

where

$\beta_1$  is the angle between the vertical axis and the projection of the axis of the CPTU on a vertical plane, in degrees

$\beta_2$  is the angle between the vertical axis and the projection of the axis of the CPTU on a vertical plane that is perpendicular to the plane of angle  $\beta_1$ , in degrees

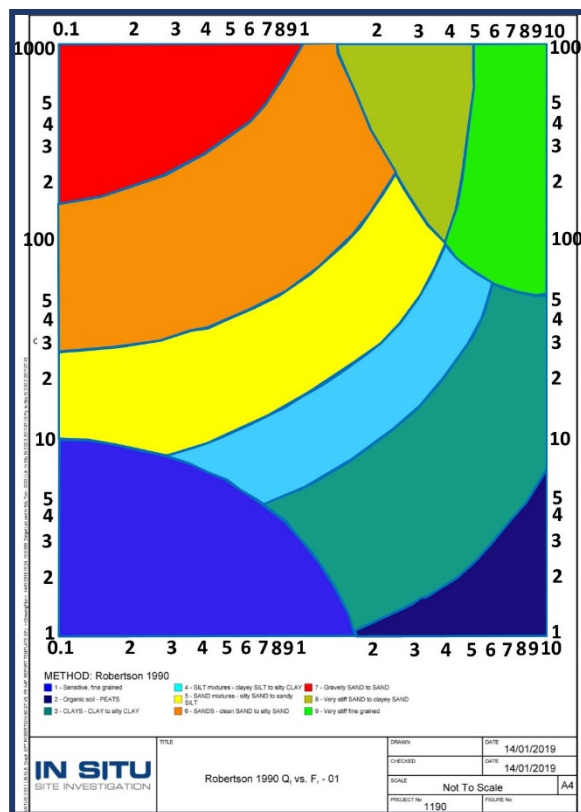
## 4.0 GEOTECHNICAL DERIVED PARAMETERS

A number of empirical correlations can be used to derive geotechnical parameters from CPTU data. This report includes only the parameters which are described in this chapter. The results of all correlations used to obtain the geotechnical derived parameters are presented on *CPT Log 02* and *CPT Log 03* in *Appendix B*.

**Please, note that each empirical correlation is derived for a certain type of soil, and may not be appropriate for all the soil types encountered on this project.**

### 4.1 SOIL BEHAVIOUR TYPE INDEX ( $I_c$ )

The soil behaviour type index,  $I_c$ , was derived by *Jefferies and Davies (1991)*, and was created to simplify the application of CPTU SBT chart shown in *Chapter 3, Figure 3.2*. This approach has been modified for use with the *Robertson (1990)* normalised CPT soil classification chart, *Figure 4.1*. The normalised cone parameters  $Q_t$  and  $F_r$  (for definitions see *Appendix A5 Symbol List*) can be combined into one Soil Behaviour Type Index,  $I_c$ , (*Lunne et al., 1997*).



**Figure 4.1:** Robertson 1990 soil behaviour type chart.



The soil behaviour type index,  $I_c$ , can then be defined using *Robertson (2010)* formula, given below:

$$I_c = ((3.47 - \log Q_t)^2 + (\log F_r + 1.22)^2)^{0.5}$$

where

$Q_t$  is the normalized cone resistance which represents the simple normalization with a stress exponent ( $n$ ) of 1.0, which applies well to clay-like soils

$F_R$  is the normalized friction ratio, in %

The boundaries of soil behaviour type are then given in terms of the index,  $I_c$ , presented in *Table 4.1* below.

The soils behaviour type index does not apply to zones 1, 8 and 9. The profiles of  $I_c$  provide a simple guide to the continuous variation of soil behaviour type in a given soil profile based on CPTU results, with a reliability greater than 80% compared with soil samples (*Robertson, 2015*).

Zone	Soil Behaviour Type	$I_c$
1	Sensitive fine grained	N/A
2	Organic Soils – clay	>3.6
3	Clays – silty clay to clay	2.95 – 3.6
4	Silt mixtures – clayey silt to silty clay	2.60 – 2.95
5	Sand mixtures – silty sand to sandy silt	2.05 – 2.6
6	Sands – clean sand to silty sand	1.31 – 2.05
7	Gravelly sand to dense sand	<1.31
8	Very stiff sand to clayey sand*	N/A
9	Very stiff fine grained *	N/A

\* Heavily over consolidated or cemented

**Table 4.1:** Normalized CPTU Soil Behaviour Type ( $SBT_n$ ) Index values,  $I_c$ . (*Robertson, 2010*)

## 4.2 N VALUE OF STANDARD PENETRATION TEST (SPT) ( $N_{60}$ )

The derived  $N$  value of  $SPT$ ,  $N_{60}$ , is strongly and directly related to the cone resistance,  $q_c$ .

In this report the  $N_{60}$  value is derived using the following correlations, developed by *Robertson and Wride (1998)* and *Jefferies and Davies (1998)*

- 1) *Robertson & Wride (1998)*

$$N_{60} = \frac{q_c}{8.5 \cdot p_a \left(1 - \frac{I_c}{4.6}\right)}$$

- 2) *Jefferies and Davies (1993)*

$$N_{60} = \frac{q_c}{0.85 \cdot \left(1 - \frac{I_c}{4.75}\right)}$$

where

- $q_c$  is the cone resistance
- $p_a$  is the atmospheric pressure equal to  $100 \text{ kPa}$
- $I_c$  is the soil behaviour type index calculated as given in *section 4.1*

It is suggested that this method provides a better estimation of the  $N$  value than the actual  $SPT$  test, due to its poor repeatability. But in fine grained soil with high sensitivity these methods of estimating  $N_{60}$  may overestimate it (*Jefferies and Davies, 1991*).

## 4.3 RELATIVE DENSITY ( $D_r$ )

Relative density,  $D_r$ , is an intermediate parameter for coarse grained soils, widely used to describe sand deposits. All the research on deriving the relative density from CPTU tests results are carried out for **clean predominantly quartz sands**. The studies have shown that CPTU resistance in granular soils is controlled by sand relative density, in situ effective stresses and compressibility. The more compressible sands tend to give lower penetration resistance for a given relative density than less compressible sands.

In this report relative density is calculated using the methods suggested by *Baldi et al., (1986)*, *Jamiolkowski et al., (2001)* and *Kulhawy and Mayne (1990)* as shown in the equations below:

- 1) *Baldi et al., (1986)*

$$D_r = \frac{1}{C_2} \cdot \ln \left( \frac{q_c \cdot Wehr}{C_1 \cdot (\sigma'_{v0})^{0.55}} \right) \cdot 100$$

where

$C_1$  is a consolidation coefficient which is 157 for normally consolidated soils and 181 for over consolidated soils

$C_2$  is a consolidation coefficient which is 2.41 for normally consolidated soils and 2.46 for over consolidated soils

Wehr is a correction coefficient for calcareous soils

2) Jamiolkowski et al., (2001)

$$D_r = 100 \cdot \left[ 0.268 \cdot \ln \left( \frac{q_t / \sigma_{atm}}{\sqrt{\sigma'_{v0} / \sigma_{atm}}} \right) + C_1 \right]$$

where

$C_1$  is a compressibility coefficient which is -0.675 for average compressible soils,  $\leq 1.0$  for high compressible soils and carbonate or calcareous sands and  $\geq -2.0$  for low compressible soils

$q_t$  is corrected cone resistance

$\sigma_{atm}$  is the atmospheric pressure

3) Kulhawy and Mayne, (1990)

$$D_r = \left[ \frac{q_{c1}}{305 \cdot C_1 \cdot OCR^{0.18} \cdot (1.2 + 0.05 \cdot \log(t/100))} \right]^{0.5} \cdot 100$$

where

$q_{c1}$  is the cone resistance corrected for initial vertical effective stress and atmospheric pressure, calculated by the following formula

$$q_{c1} = \frac{q_c}{\sqrt{\sigma'_{v0} \cdot \sigma_{atm}}}$$

where

$q_c$  is the cone resistance in *kPa*

$\sigma'_{v0}$  is the initial vertical effective stress in *kPa*

$C_1$  is a compressibility coefficient which is -0.91 for low compressible sands, 1.0 for medium compressible sands and 1.09 for high compressible sands

$t$  is time in years

#### 4.4 FRICTION ANGLE ( $\phi'$ )

Friction angle,  $\phi'$ , is used to express the shear strength of uncemented, coarse grained soils. In this report friction angle is derived by the correlations of *Mayne and Campanella (2005)*, *Robertson and Campanella (1983)* and *Kulhawy and Mayne (1990)*.

1) Mayne and Campanella, (2005)

$$\varphi' = 29.5^0 \cdot B_q^{0.121} \cdot [0.256 + 0.336 \cdot B_q + \log Q_t]$$

where

- $B_q$  is the pore pressure ratio, calculated as in Session 3.3
- $Q_t$  is the normalized cone resistance

2) Robertson and Campanella, (1983)

$$\varphi' = \tan^{-1} \left( 0.1 + 0.38 \cdot \log \left( \frac{q_t}{\sigma'_{v0}} \right) \right)$$

where

- $q_c$  is the cone resistance in *kPa*
- $\sigma'_{v0}$  is the initial vertical effective stress in *kPa*

3) Kulhawy and Mayne, (1990)

$$\varphi' = 17.6^0 + 11.0^0 \cdot \log(q_{t1})$$

where

- $q_{t1}$  is the corrected cone resistance corrected for initial vertical effective stress and atmospheric pressure, calculated by the following formula

$$q_{t1} = \frac{q_t}{\sqrt{\sigma'_{v0} \cdot \sigma_{atm}}}$$

The method suggested by *Mayne and Campanella (2005)* will not provide reliable results for heavily over consolidated soils, fissured geomaterials and highly cemented or structures clays. This approach gives reliable results when pore pressure is positive and varies  $0.1 < B_q < 1.0$ . The correlation suggested by *Robertson and Campanella (1983)* estimates the peak friction angle for uncemented, unaged, moderately compressible, predominately quartz sands. For sands of higher compressibility, the method will tend to predict low friction angles. The method suggested by *Kulhawy and Mayne (1990)* is an alternate relationship for clean, rounded, uncemented, quartz sands.

## 4.5 FINES CONTENT (FC)

The fines content, *FC*, in this report is estimated using two different methods, one from *Robertson and Wride (1998)* and the other, *Suzuki et al. (1998)* as presented below:

1) Robertson and Wride (1998)

$$I_c < 1.26: FC = 0$$

$$1.26 \leq I_c \leq 3.5: FC(\%) = 1.75I_c^{3.25} - 3.7$$

$$3.5 < I_c: FC = 100\%$$

2) Suzuki et al. (1998)

$$FC(\%) = 2.8I_c^{2.6}$$

where

$I_c$  is the soil behaviour type index, calculated as in section 4.1

#### 4.6 UNDRAINED SHEAR STRENGTH ( $s_u$ )

Estimation of undrained shear strength,  $s_u$ , from CPTU tests using corrected cone resistance is carried out using the following correlation from *Lunne et al. (1981)*:

$$s_u = \frac{(q_t - \sigma_{v0})}{N_{kt}}$$

where

$N_{kt}$  is the empirical cone factor, which varies from 10 (6 for very soft sensitive fine grained soils) to 20. In this report 3 values are considered: 15, 17.5 and 20.  $N_{kt}$  tends to increase with increasing plasticity and decrease with increasing soil sensitivity. It decreases as  $B_q$  increases. (*Lunne et al., 1997*)

$\sigma_{v0}$  = total overburden stress.

This report only presents the undrained shear strength data on soils with soil behaviour type index,  $I_c$  values greater than 2.60.

The value of undrained shear strength,  $s_u$  to be used in analysis depends on the design problem. In general, the simple shear in the direction of loading often represents the average undrained strength. For larger, moderate to high risk projects, where high quality field and laboratory data may be available, site specific correlations should be developed based on appropriate and reliable values of  $s_u$ .

#### 4.7 SENSITIVITY ( $S_t$ )

The sensitivity,  $S_t$  of clays is defined as the ratio of undisturbed peak undrained shear strength to totally remoulded undrained shear strength.

In this report  $S_t$  is calculated using two correlations developed by *Schmertmann (1978)* and *Mayne (2007)*.

1) Schmertmann (1978)

$$S_t = \frac{s_u}{s_{u(rem)}} = \frac{q_t - \sigma_v}{N_{kt}} \left( \frac{1}{f_s} \right)$$

where

$s_{u(rem)}$  is the remoulded undrained shear strength. It can be assumed equal to the sleeve resistance,  $f_s$ .

2) Mayne (2007)

$$S_t = \frac{0.073 \cdot (q_t - \sigma_{v0})}{f_s}$$

For relatively sensitive clays,  $S_t > 10$ , the value of  $f_s$  can be very low and not very accurate, hence the estimate of sensitivity should be used as a guide only.

#### 4.8 SOIL UNIT WEIGHT ( $\gamma$ )

Soil unit weight,  $\gamma$  in this report is calculated by using one method for sands, considered under dry conditions and two methods for clays, considered under saturated conditions. These relationships are developed by *Mayne (2007)* and the equations are presented below:

1) Mayne (2007)

Dry unit weight for sands:

$$\gamma_{dry} = 1.89 \cdot \log(q_{t1}) + 11.82$$

Saturated unit weight for clays method 1

$$\gamma_{sat} = 8.32 \cdot \log(V_s) - 1.61 \cdot \log(z)$$

Saturated unit for clays method 2

$$\gamma_{sat} = 2.60 \cdot \log(f_s) + 15 \cdot G_s - 26.5$$

where

$q_{t1}$  is the corrected cone resistance corrected for initial vertical effective stress and atmospheric pressure, calculated by the following formula:

$$q_{t1} = \frac{q_t}{\sqrt{\sigma'_{v0} \cdot \sigma_{atm}}}$$

$z$  is the depth

$V_s$  is the shear wave velocity, calculated as  $V_s = 118.8 \cdot \log(f_s) + 18.5$

$G_s$  is the specific gravity of solids, typically between 2.40 and 2.90

## 4.9 STATE PARAMETER ( $\psi$ )

The state parameter,  $\psi$  is defined as the difference between the current void ratio,  $e$  and the void ratio at critical state  $e_{cs}$ , at the same mean effective stress for granular soils.

The problem of evaluating the state parameter from CPTU response is complex and depends on several soil parameters, including shear stiffness, shear strength, compressibility and plastic hardening. (*Jefferies and Been, 2006*)

In this report, the state parameter is calculated based on five methods as follows:

- 1) Been et al. (1987)

$$\psi = -\frac{\ln\left(\frac{Q_p}{k}\right)}{m}$$

and

$$Q_p = \left(\frac{3Q_t}{1 + 2K_0}\right)$$

where

$Q_t$  is the normalized cone resistance  
 $K_0$  is the coefficient of lateral earth pressure

- 2) Shuttle and Jefferies (1998)

$$\psi = -\frac{\ln\left(\frac{Q_p}{k}\right)}{m}$$

where

$$k = \left((3.79 + 1.12\ln(I_r))(1 + 1.06(M - 1.25))(1 - 0.30(N - 0.2))(H/1000)^{0.326}(-1.55(\lambda - 0.01))\right)^{1.45}$$

$$m = 1.45(1.04 + 0.46\ln(I_r))(1 - 0.4(M - 1.25))(1 - 0.30(N - 0.2))(H/100)^{0.15}(1 - 2.21(\lambda - 0.01))$$

where

$Q_t$  is the normalised cone resistance  
 $I_r$  is rigidity index  
 $K_0$  is the coefficient of lateral earth pressure  
 $M$  is critical state ratio  
 $N$  is dilation parameter  
 $H$  is plastic hardening modulus;  
 $\lambda$  is slope CSL line

- 3) Shuttle and Jefferies (1998)



The state parameter calculated according this third method is similar to state parameter calculated as presented in the second method, except for the rigidity index that is calculated as follows:

$$I_r = I_{r100} \left( \frac{P_a}{\sigma'_{v0}} \right)^{0.5}$$

where

- $I_{r100}$  is rigidity index in reference pressure
- $P_a$  is the reference pressure equal to 100 kPa
- $\sigma'_{v0}$  is effective vertical overburden stress

4) Plewes (1992)

$$\psi = - \frac{\ln \left( \frac{Q_p / (1 - B_q)}{k'} \right)}{m'}$$

where

$$k' = M \left( 3 + \frac{0.85}{\lambda} \right)$$

$$m' = 11.9 - 13.3\lambda$$

$$\lambda = \frac{F_r}{10}$$

where

- $Q_t$  is the normalised cone resistance
- $B_q$  is pore pressure ratio
- $K_0$  is the coefficient of lateral earth pressure
- $F_R$  is normalised friction ratio
- $M$  is critical state ration

5) Been and Jefferies (1992)

$$\psi = - \frac{\ln \left( \frac{Q_p / (1 - B_q)}{k'} \right)}{m'}$$

where

$$k' = M \left( 3 + \frac{0.85}{\lambda} \right)$$

$$m' = 11.9 - 13.3\lambda$$

$$\lambda = \frac{1}{34 - 10I_c}$$

For high-risk projects a detailed interpretation of CPTU results using laboratory results and numerical modelling can be appropriate (e.g. *Shuttle and Cunning, 2007*), although soil variability can complicate the interpretation procedure. For low risk projects and in the initial screening for high-risk projects there is a need for a simple estimate of soil state.

*Plewes et al (1991)* provided a mean to estimate soil state using the normalised soil behaviour type, *SBT<sub>n</sub>* chart suggested by *Jefferies and Davies (1991)*. *Jefferies and Been (2006)* suggested that soils with a state parameter less than  $-0.05$  are dilative at large strains.

#### 4.10 IN SITU STRESS RATIO ( $K_0$ )

There are various estimations to determine in situ stress ratio,  $K_0$ , from CPTU in fine grained soils. In this report the methods suggested by *Mayne (2007)* and *Kulhawy and Mayne (1990)* are used, as given below:

- 1) Mayne (2007)

$$K_0 = (1 - \sin\phi')OCR^{\sin\phi'}$$

$$\text{Max } K_0 = K_p = \frac{(1 + \sin\phi')}{(1 - \sin\phi')}$$

$$K_0 = 0.192 \left( \frac{q_t}{\sigma_{atm}} \right)^{0.22} \left( \frac{\sigma_{atm}}{\sigma_{v0}} \right)^{0.22} OCR^{0.27}$$

where

OCR is the overconsolidation ratio, calculated as presented in session 4.12

- 2) Kulhawy and Mayne (1990)

$$K_0 = 0.1 \left( \frac{q_t - \sigma_{v0}}{\sigma_{v0}'} \right)$$

These approaches are generally limited to mechanically overconsolidated, fine grained soils. As considerable scatter exists in the database used for these correlations, in moderate to high risk projects further tests should be performed and these correlations must be considered only as a guide.

#### 4.11 OVERCONSOLIDATION RATIO (OCR)

Overconsolidation ratio, *OCR* is defined as the ratio of the maximum past effective consolidation stress and the present effective overburden stress:

$$OCR = \frac{\sigma'_p}{\sigma'_{v0}}$$

This definition is appropriate for mechanically overconsolidated soils, where the only change has been the removal of overburden stress. For cemented and aged soils, the *OCR* may represent the ratio of the yield stress and the present effective overburden stress.

In this report  $\sigma'_p$  is calculated based on six methods as presented below:

- 1) Mayne (1995)

$$\sigma'_p = 0.33(q_t - \sigma_{v0})$$

- 2) Chen and Mayne (1996)

$$\sigma'_p = 0.53\Delta u$$

- 3) Mayne (2005)

$$\sigma'_p = 0.6(q_t - u_2)$$

- 4) Robertson (2009)

$$\sigma'_p = 0.25(Q_t^{1.25} - \sigma'_{v0})$$

- 5) Mayne (2005)

$$\sigma'_p = \left[ \frac{0.192 \left( \frac{q_t}{\sigma_{atm}} \right)^{0.125}}{(1 - \sin\phi') \left( \frac{\sigma'_{v0}}{\sigma_{atm}} \right)^{0.31}} \right]^{\left( \frac{1}{\sin\phi' - 0.27} \right)} \sigma'_{v0}$$

- 6) Mayne (2007)

$$\sigma'_p = 0.101\sigma_{atm}^{0.102}(G_0)^{0.478}\sigma'_{v0}{}^{0.420}$$

For larger, moderate to high risk projects, where additional high-quality field and laboratory data may be available, site specific correlations should be developed based in consistent and relevant values of *OCR*.

#### 4.12 SMALL STRAIN YOUNG'S MODULUS ( $E_0$ )

Deriving small strain undrained Young's modulus,  $E_0$ , from CPTU is difficult. There is insufficient data available to make a direct correlation and it is recommended that  $c_u$  should be derived, then  $E_U$  estimated as a rough order of value from one of the available correlations between  $E_U$  and  $c_u$  (Meigh, 1987).

In this report the small strain Young's modulus is derived as follows:

- 1) Defined from elastic theory:

$$E_0 = 2(1 + \nu)G_0$$

where

- $\nu$  is the Poisson ratio, equal to 0.2
- $G_0$  is the small strain shear modulus calculated by the formula given below:

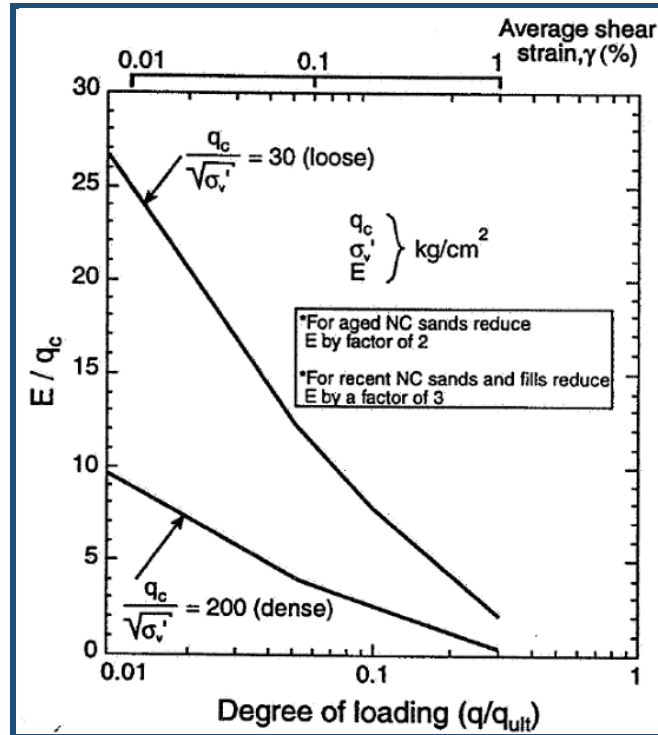
$$G_0 = 1634 \left( \frac{q_c}{\sqrt{\sigma'_{v0}}} \right)^{-0.75} q_c$$

2) Calculated based on the degree of loading,  $q_c$ , effective stress and reduction factor

$$E_0 = \alpha q_c$$

where

$\alpha$  is calculated from degree of loading,  $q_c$ , effective stress and reduction factor, given in *Figure 4.2*



**Figure 4.2:** Estimation of equivalent Young's modulus for sand based on degree of loading (Robertson, 1990)

### 4.13 CONSTRAINED MODULUS (M)

Constrained Modulus,  $M$ , can be estimated by CPTU using the following empirical relationship:

$$M = \alpha_M (q_t - \sigma_{v0})$$

where

$\alpha_M$  varies with soil plasticity and natural water content for a wide range of fine-grained soils and organic soils. *Meigh (1987)* suggested that  $\alpha_M$  lies in the range of 2 to 8, whereas *Mayne (2001)* suggested the value of 5.

*Robertson (2001)* suggested that  $\alpha_M$  varies with  $Q_t$ , such that:

When  $I_c > 2.2$  (fine grained soils) use:  $\alpha_M = Q_t$  when  $Q_t < 14$   
 $\alpha_M = 14$  when  $Q_t > 14$

When  $I_c < 2.2$  (coarse grained soils) use:  $\alpha_M = 0.0188[10^{(0.55I_c+1.68)}]$

In this report the Constrained Modulus,  $M$ , is calculated after *Kulhawy and Mayne (1990)* using the equation below:

$$M = 8.25(q_t - \sigma_{v0})$$

Also, an alternative method is included in the results, developed by *Burns and Mayne (2002)* using the following relationship:

$$M = 0.02G_0$$

#### 4.13.1 Equivalent Oedometer Coefficient of Compressibility ( $m_v$ )

Equivalent oedometer coefficient of compressibility,  $m_v$  can be calculated directly by the Constrained Modulus,  $M$ , as follows:

$$m_v = \frac{1}{M}$$

#### 4.14 SMALL STRAIN SHEAR MODULUS ( $G_0$ )

Elastic theory states that the small strain shear modulus,  $G_0$ , can be determined from the following equation:

$$G_0 = \rho v_s^2$$

where

$\rho$  is the mass density of the soil  
 $v_s$  is the shear wave velocity

In this report the small strain shear modulus,  $G_0$ , will be presented calculated by the two methods shown below, developed by *Rix and Stoke (1992)* and *BE, UB Rix and Stoke (1992)*, respectively.

$$G_0 = 1634 \left( \frac{q_c}{\sqrt{\sigma'_{v0}}} \right)^{-0.75} q_c$$

$$G_0 = \frac{\gamma_{bulk}}{g} v_s^2$$

where

$q_c$  is the net cone tip resistance in kPa  
 $\sigma'_{v0}$  is the effective initial vertical stress in kPa  
 $\gamma_{bulk}$  is the bulk density of the soil  
 $v_s$  is the shear wave velocity

This correlation of  $G_0$  is applicable to all soil types.

#### 4.14.1 Mass Density of Soil ( $\rho$ )

Mass density of soil,  $\rho$ , is defined as:

$$\rho = \frac{\gamma}{g}$$

where

$\gamma$  is the elastic stiffness of the soils at shear strain less than  $10^{-4}\%$ ,  $\gamma < 10^{-4}\%$ .

#### 4.15 HYDRAULIC CONDUCTIVITY (k)

An approximate estimate of soil hydraulic conductivity or coefficient of permeability,  $k$ , can be made from an estimate of soil behaviour type using the CPTU *SBT chart* as presented in the table below:

SBT Zone	SBT	Range of k (m/s)	SBT <sub>n</sub> I <sub>c</sub>
1	Sensitive fine grained	3x10 <sup>-10</sup> to 3x10 <sup>-8</sup>	NA
2	Organic soils-clay	1x10 <sup>-10</sup> to 1x10 <sup>-8</sup>	I <sub>c</sub> >3.60
3	Clay	1x10 <sup>-10</sup> to 1x10 <sup>-9</sup>	2.95<I <sub>c</sub> <3.60
4	Silt Mixture	3x10 <sup>-9</sup> to 1x10 <sup>-7</sup>	2.60<I <sub>c</sub> <2.95
5	Sand Mixture	1x10 <sup>-7</sup> to 1x10 <sup>-5</sup>	2.05<I <sub>c</sub> <2.60
6	Sand	1x10 <sup>-5</sup> to 1x10 <sup>-3</sup>	1.31<I <sub>c</sub> <2.05
7	Dense sand to gravelly sand	1x10 <sup>-3</sup> to 1	I <sub>c</sub> <1.31
8	*Very dense/ stiff soil	1x10 <sup>-8</sup> to 1x10 <sup>-3</sup>	NA
9	*Very stiff fine grained soil	1x10 <sup>-9</sup> to 1x10 <sup>-7</sup>	NA

\*Overconsolidated and/ or cemented

**Table 4.2:** Estimated soils' permeability ( $k$ ) based on the CPTU SBT chart by Robertson (2009)

The average relationship between soils' permeability,  $k$  and SBT<sub>n</sub> I<sub>c</sub>, shown in Table 4.2, can be represented by the following relationships:

$$\begin{aligned} \text{When } 1.0 < I_c \leq 3.27 & \quad k = 10^{(0.952-3.04I_c)} \\ \text{When } 3.27 < I_c \leq 4.0 & \quad k = 10^{(-4.52-1.37I_c)} \end{aligned}$$

In this report, the hydraulic conductivity is estimated as a function of soil types from 2 CPTU classification charts, *Robertson et al. (1986)* and *Robertson et al. (1990)*, considering both minimum and maximum values.

The hydraulic conductivity (coefficient of permeability),  $k$ , values (minimum and maximum), defined after soils' behaviour type by *Robertson et al. (1986)* are presented in *Table 4.3*, below:

SBT Zone	Soil Behaviour Type (SBT)	Range of hydraulic conductivity, $k$ (m/s)
1	Sensitive fine grained	$3 \times 10^{-9}$ to $3 \times 10^{-8}$
2	Organic soils	$1 \times 10^{-8}$ to $1 \times 10^{-6}$
3	Clay	$1 \times 10^{-10}$ to $1 \times 10^{-9}$
4	Silty CLAY to CLAY	$3 \times 10^{-9}$ to $1 \times 10^{-8}$
5	Clayey SILT to silty CLAY	$1 \times 10^{-8}$ to $1 \times 10^{-7}$
6	Sandy SILT to clayey SILT	$1 \times 10^{-7}$ to $1 \times 10^{-6}$
7	Silty SAND to sandy SILT	$1 \times 10^{-5}$ to $1 \times 10^{-6}$
8	SAND to silty SAND	$1 \times 10^{-5}$ to $1 \times 10^{-4}$
9	SAND	$1 \times 10^{-4}$ to $1 \times 10^{-3}$
10	Gravelly SAND to SAND	$1 \times 10^{-3}$ to 1
11	Very stiff fine grained	$1 \times 10^{-8}$ to $1 \times 10^{-6}$
12	SAND to clayey SAND	$3 \times 10^{-7}$ to $3 \times 10^{-4}$

**Table 4.3:** Estimated soil permeability ( $k$ ) based on SBT chart by *Robertson et al. (1986)*

The hydraulic conductivity (coefficient of permeability),  $k$  values (min and max), defined after soils' behaviour type by *Robertson et al. (1990)* are presented in *Table 4.4*, below:

SBT Zone	Soil Behaviour Type (SBT)	Range of hydraulic conductivity, $k$ (m/s)
1	Sensitive fine grained	$3 \times 10^{-9}$ to $3 \times 10^{-8}$
2	Organic soils	$1 \times 10^{-8}$ to $1 \times 10^{-6}$
3	Clay	$1 \times 10^{-10}$ to $1 \times 10^{-9}$
4	Silt Mixture	$3 \times 10^{-9}$ to $1 \times 10^{-7}$
5	Sand Mixture	$1 \times 10^{-7}$ to $1 \times 10^{-5}$
6	Sand	$1 \times 10^{-5}$ to $1 \times 10^{-3}$
7	Gravelly sands to dense sands	$1 \times 10^{-3}$ to 1
8	Very stiff sand to clayey sand	$1 \times 10^{-8}$ to $1 \times 10^{-6}$
9	Very stiff fine grained	$1 \times 10^{-8}$ to $1 \times 10^{-6}$

**Table 4.4:** Estimated soils' permeability ( $k$ ) based on SBT chart by *Robertson et al. (1990)*.



#### 4.16 RIGIDITY INDEX ( $I_R$ )

The rigidity index,  $I_R$ , for fine grained soils is defined using the following formula, developed by *Mayne (2001)*:

$$I_R = \exp \left[ \left( \frac{1.5}{M} + 2.925 \right) \left( \frac{q_t - \sigma_{v0}}{q_t - u_2} \right) \right] - 2.925$$

where

$M$  is the Cam-Clay constant, slope of the critical state line defined as:

$$M = \frac{6 \sin \phi'}{3 - \sin \phi'}$$

where

$\phi'$  is the internal friction angle.

The second method used to define the rigidity index,  $I_R$ , for fine grained soils is based on plasticity index and overconsolidation ratio,  $OCR$  and calculated after the relationship developed by *Keaveny and Mitchell (1986)* as follows:

$$I_R = \frac{\exp(0.0435(137 - PI))}{[1 + \ln\{1 + 0.385(OCR - 1)^{3.2}\}]^{0.8}}$$

where

$PI$  is the plasticity index of the soil, equal to 20.

$OCR$  is the overconsolidation ratio of the soil

#### 4.17 CORRELATED SHEAR WAVE VELOCITY ( $V_s$ )

Correlated Shear wave velocity,  $V_s$  in this report is estimated after *Mayne (2006)*, *Hegazy and Mayne (1995)*, *Mayne and Rix (1995)* and *Baldi et al. (1989)* as follows:

- 1) *Mayne (2006)*

$$V_s = 118.8 \log f_s + 18.5$$

where

$f_s$  is in  $kPa$

- 2) *Hegazy and Mayne (1995)*

$$V_s = (10.1 \log q_t - 11.4)^{1.67} \left( \frac{f_s}{q_t} \cdot 100 \right)^{0.3}$$

where

$q_t, f_s$  are in  $kPa$

## 3) Mayne and Rix (1995)

$$V_s = 1.75(q_t)^{0.627}$$

where

$q_t$  is in *kPa*

## 4) Baldi et al. (1989)

$$V_s = 277(q_t)^{0.13}(\sigma'_{v0})^{0.13}$$

where

$q_t, \sigma'_{v0}$  are in *kPa*

## 5.0 CPTU RESULTS APPLICATIONS

### 5.1 SOIL PROFILING AND APPLICATIONS IN GEOTECHNICAL DESIGN

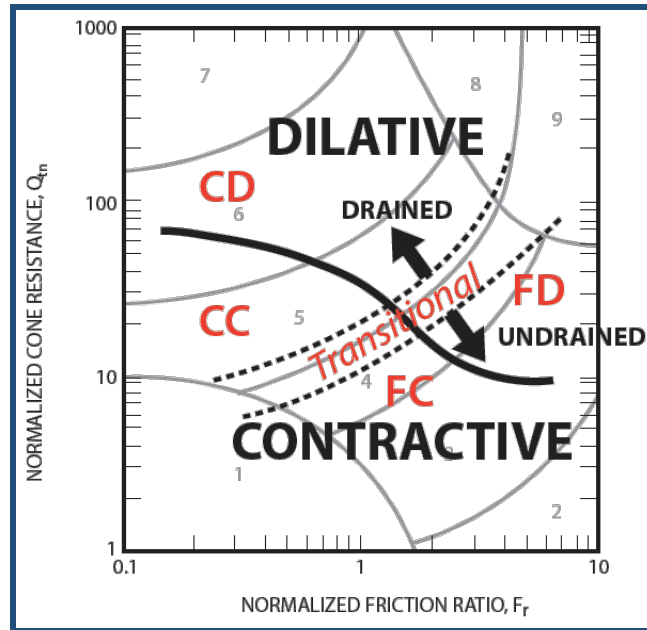
#### 5.1.1 Soil Behaviour Type

The major applications of CPTU are on *soil behaviour type and soil profiling*. Typically, the cone resistance,  $q_c$  is high in sands and low in clays, and the friction ratio,  $R_f = f_s/q_t$  is low in sands and high in clays. The CPTU cannot be expected to provide accurate predictions of soil type based on *physical characteristics*, e.g. *grain size distribution*, but provides a guide to the *mechanical characteristics*, including: *strength, stiffness, and compressibility* of the soils, or the *soil behaviour type, SBT*.

The most commonly used CPTU soil behaviour type chart, suggested by *Robertson et al. (1986)* uses the basic CPTU measured parameters of cone resistance,  $q_c$  and friction ratio,  $R_f$ . The chart is global in nature and can provide reasonable predictions of soil behaviour type for CPTU testing. The expected overlap in some zones is modified in the interpretations of this report somewhat based on previous experience or local knowledge of the site.

Since both the penetration resistance and sleeve resistance increase with depth due to the increase in effective overburden stress, the CPTU data requires normalization for overburden stress for very shallow and/or very deep tests. A popular CPTU soil behaviour chart based on normalized CPTU data is firstly proposed by *Robertson (1990)*. The chart identifies general trends in ground response, such as: *increasing soil density, OCR, age and cementation* for granular soils, and *increasing stress history, OCR and soil sensitivity* for cohesive soils.

A more general normalized CPTU SBT chart, using large strain *soil behaviour* descriptions, proposed by *Robertson (2012)* is shown in *Figure 5.1*.



**Figure 5.1:** Normalized CPTU Soil Behaviour Type ( $SBT_n$ ) chart,  $Q_{tn}$ - $F_R$  using general large strain soil behaviour description (Robertson, 2012).

\*

- CD is coarse grained dilative soil-predominately drained CPTU
- CC is coarse grained contractive soil-predominately drained CPTU
- FD is fine grained dilative soil-predominately undrained CPTU
- FC is fine grained contractive soil-predominately undrained CPTU

### 5.1.2 Soil Profiling

CPTU is an excellent test for soil profiling. The continuous monitoring of pore pressure during the cone penetration improves the soil stratigraphy descriptions. The pore pressure develops in response to the soil type being penetrated in the area where the pore pressure element is located. Soft, firm or stiff clays and contractive silts can show very high pore pressure. Very stiff overconsolidated clays and dilative silts can give very low or negative pore pressures same as very dense silty sands.

The thin layers of sand, or silt in a thick layer of clay, or thin layers of clay or silt in a thick layer of sand are easily distinguished during a CPTU test, which will give a response time sufficiently fast to observe pore pressure changes even in the very thin layers of soils (< 5mm), depending on the response of soil to the advancing of cone.

The sandy soils tend to produce high cone resistance and low friction ratio, whereas soft clayey soils tend to produce low cone resistance and high friction ratio. Organic soils such as peat tend to have very low cone resistance and very high friction ratio. Soils with high horizontal stresses (*high OCR*) tend to have higher cone resistance and friction ratio.

CPTU is an excellent tool to classify the soils based on their behaviour type, and not based on grain size distribution.

The measurement of sleeve friction,  $f_s$  is often less reliable than the measurement of cone resistance,  $q_c$  (Lunne *et al.*, 1986), but to overpass these problems pore pressure parameter ratio,  $B_q$ , and the classification charts based on it.

For more reliability in soil profiling, the soil interpretations in this report are carried out based on three parameters measured on site, cone resistance, sleeve friction and pore pressure and three derived geotechnical parameters soil behaviour type index for all soils, undrained shear strength for cohesive soils and relative density for granular soils.

Generally, soils that fall in zones 8, 9 and 10 of Robertson *et al.* (1986) chart (6 and 7 of Robertson (1990) chart) represent approximately drained penetration, whereas, soils in zones 1, 2, 3, 4, 5 and 6 of Robertson *et al.* (1986) chart (1, 2, 3 and 4 of Robertson (1990) chart) represent approximately undrained penetration. Soils in zones 7, 11 and 12 of Robertson *et al.* (1986) (5, 8 and 9 of Robertson (1990) chart) may represent partially drained penetration. The classification is often influenced by changes in *stress history, in situ stresses, sensitivity, stiffness, mineralogy, etc.* An advantage of pore pressure measurements during cone penetration is the ability to evaluate drainage conditions more directly. (Lunne *et al.*, 1997)

The information about the rate and manner of excess pore pressures during the dissipations significantly helps the accurate classification in the corresponding depths of dissipation tests. In very stiff, overconsolidated clayey soils, the pore pressure behind the cone is very low and sometimes negative of the equilibrium pore pressure,  $u_0$ , whereas the pore pressure on the face of the cone is very large due to the large increase in normal stresses created by the cone penetration. When penetration is stopped in overconsolidated clays, pore pressure recorded behind the cone may initially increase before decreasing to the equilibrium pore pressure. The rise is caused by local equalization of the high pore pressure gradient around the cone.

Cone penetration in fine grained soils, such as clays and silts, is generally undrained. Cone penetration tests under undrained conditions generate high pore pressure and this reading is extremely useful, because it affects both cone resistance and sleeve friction measurements. These parameters should be corrected using the measured pore pressure.

CPTU in coarse grained soils, such as sandy or gravelly soils is generally drained. In these conditions there is no excess pore pressure generated as a result of cone penetration. Relative density has been used as the main parameter for description of sandy deposits.

*5.1.3 Applications in geotechnical design*

CPTU measured parameters are used to derive geotechnical parameters, which are the input in several geotechnical analyses. An alternate approach is to directly apply CPTU results to the geotechnical calculations.

As a guide, *Table 7.1* shows a summary of the applicability of CPTU results for direct design applications. The ratings shown in the table have been assigned based on current experience and represent a qualitative evaluation of the confidence level assessed to each design problem and general soil type. Details of ground conditions and project requirements can influence these ratings.

Type of soil	Pile Design	Bearing Capacity	Settlement	Compaction Control	Liquefaction
Sand	A-B	A-B	B-C	A-B	A-B
Clay	A-B	A-B	B-C	C-D	A-B
Intermediate Soils	A-B	B-C	B-C	B-C	A-B

**Table 5.1:** *Perceived applicability of CPTU for various direct design problems.*

- A is high
- B is high to moderate
- C is moderate
- D is moderate to low

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## APPENDIX A

## APPENDIX A1 – Project Summary Sheet

### *Piezocene Tests Summary Sheet*

HOLE ID	Final Depth (m)	Date of Test	Cone Used	Test Remarks
CPT01	6.18	09/02/2022	S15-CFIP.1867	Test refused on tip resistance.
CPT01A	14.61	09/02/2022	S15-CFIP.1867	Test refused on tip resistance.
CPT02	18.69	09/02/2022	S15-CFIP.1867	Test refused on tip resistance.
CPT03	2.06	10/02/2022	S15-CFIP.1867	Test refused on tip resistance.
CPT03A	18.62	10/02/2022	S15-CFIP.1867	Test refused on tip resistance.
CPT04	18.82	10/02/2022	S15-CFIP.1867	Test refused on tip resistance.
CPT05	10.66	10/02/2022	S15-CFIP.1867	Test refused on tip resistance.
CPT05A	18.39	10/02/2022	S15-CFIP.1867	Test refused on tip resistance.
CPT06	1.70	09/02/2022	S15-CFIP.1867	Test refused on tip resistance.
CPT06A	1.28	09/02/2022	S15-CFIP.1867	Test refused on tip resistance.
CPT06B	2.48	10/02/2022	S15-CFIP.1867	Test refused on tip resistance.
CPT07	18.85	10/02/2022	S15-CFIP.1867	Test refused on tip resistance.
CPT08	4.27	09/02/2022	S15-CFIP.1867	Test refused on inclination.
CPT08A	17.82	09/02/2022	S15-CFIP.1867	Test refused on tip resistance.
CPT09	23.29	09/02/2022	S15-CFIP.1867	Test refused on tip resistance.
CPT10	16.86	10/02/2022	S15-CFIP.1867	Test refused on tip resistance.
CPT11	18.27	10/02/2022	S15-CFIP.1867	Test refused on tip resistance.
CPT12	9.65	09/02/2022	S15-CFIP.1867	Test refused on inclination.
CPT12A	17.18	09/02/2022	S15-CFIP.1867	Test refused on tip resistance.
SCPT	29.02	11/02/2022	DP10-CFPTxy.60154	Test refused on tip resistance.

*Piezocene Test Coordinates*

<b>HOLE ID</b>	<b>Eastings</b>	<b>Northings</b>	<b>Elevation</b>
CPT01	490888.44	290863.51	106.56
CPT01A	490888.44	290863.51	106.56
CPT02	490949.52	290883.38	106.11
CPT03	491001.39	290915.22	105.72
CPT03A	491001.39	290915.22	105.72
CPT04	490956.09	290835.72	105.14
CPT05	491009.42	290857.94	104.53
CPT05A	491009.42	290857.94	104.53
CPT06	490993.29	290892.52	105.63
CPT06A	490993.29	290892.52	105.63
CPT06B	490993.29	290892.52	105.63
CPT07	491084.70	290876.35	104.07
CPT08	490892.03	290837.38	106.23
CPT08A	490892.03	290837.38	106.23
CPT09	490918.12	290906.18	106.87
CPT10	491027.58	290924.64	105.48
CPT11	491050.41	290872.44	104.30
CPT12	490922.10	290829.93	105.49
CPT12A	490922.10	290829.93	105.49
SCPT	490984.81	290849.71	105.22

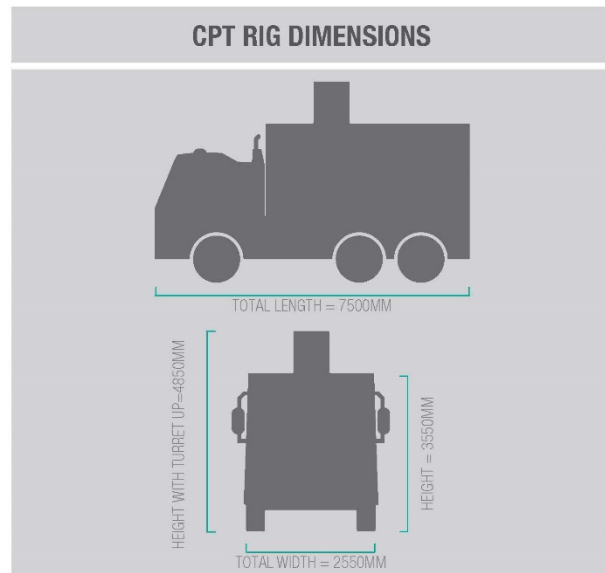
## APPENDIX A2 – CPT Rig Datasheet

### RIGS

#### 22 TONNE CPT WHEEL MOUNTED RIG (CPT 016)

This 6 x 6 wheeled drive CPT rig is ideal for geotechnical testing on hardstanding sites such as roads and car parks. It can also be used on dry non-hardstanding sites making it one of our versatile rigs as it can be deployed to many different types of site. It weighs 22 tonnes and can push up to 100-150 metres per day, depending on the ground conditions.

CPT RIG DETAILS	
<b>DRIVE SYSTEM</b>	6x6 WHEEL DRIVE
<b>TOTAL WEIGHT</b>	22 TONNES
<b>GROUND BEARING PRESSURE</b>	56kPa
<b>CPT RAM THRUST CAPACITY</b>	20 TONNES
<b>MAXIMUM PENETRATION</b>	30-40M DEPENDING ON THE GROUND CONDITIONS.
<b>PERFORMANCE RATES</b>	100-150M OF TESTING IN A DAY, DEPENDING ON ACCESS TO POSITIONS.
<b>TYPICAL SITES FOR THIS RIG</b>	HARDSTANDING SITES, E.G. ROADS INCLUDING MOTORWAYS, CAR PARKS AND DOCKS, DRY NON-HARDSTANDING SITES.

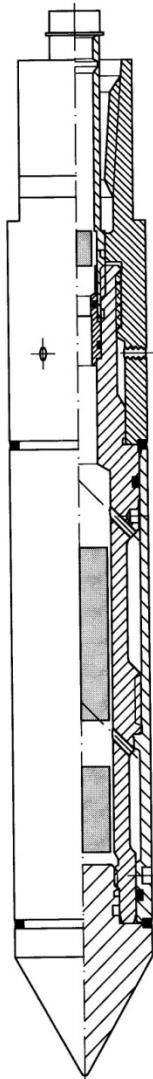




**APPENDIX A3 – Cone Datasheet**



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Postbank : 5226758  
BTW nr. : NL806331677801



# SPECIFICATIONS

## S15 SERIES

### ELECTRICAL CONES

The electronic subtraction cones have been developed to address the durability problems inherent in other cone designs. The unit consists of a single element temperature compensated strain gauge transducer for measuring both cone resistance and local sleeve friction. This design is therefore more robust than a compression type cone. The cone support electronics package is located directly behind the transducer. The precision strain gauge amplifiers and power supply eliminate the effects of cable resistance on the measurements. A standard subtraction cone is capable of measuring simultaneously the following channels: Tip, Local friction, Pore pressure, Temperature and Inclination.

**GENERAL SPECIFICATIONS**

Cone Tip Section Area	1,500 mm <sup>2</sup>
Friction Sleeve Surface	22,500 mm <sup>2</sup>
Total Length	325 mm
Weight	4200 g
Power Supply	± 15 VDC, 100 mA.
Output	0 – 10 VDC*
Working Temperature	0 - 60°C
Storage Temperature	- 40 to + 85°C
Connector	Lemo 10 pins (others on request)

**TIP RESISTANCE**

Range	100/150* kN
Accuracy	0.25 % FS
Maximum Load	150 % of range
Cone Area Ratio	0.75

**LOCAL SLEEVE FRICTION**

Range	100/150* kN
Accuracy	0.50 % FS
Maximum Load	150 %
Sleeve Area Ratio	1.0 (EA)

**PORE PRESSURE**

Range	1/2/5/10* MPa
Accuracy	0.5 % FS
Maximum Load	150 % of range

**INCLINATION**

Range	25 ° (biaxial)
Accuracy	< 2 °

All our equipment complies with the ISSMGE, ASTM, DIN and NEN Standards.

*\*Other output and voltage ranges available on request. Loadcells may be calibrated for lower ranges.*





Manual: Electric CPT Cone P10-CFPTxy and P15CFPTxy (PIEZOCONE)

All cones are temperature compensated and provided with a built-in precision strain-gauge amplifier. The cone characteristics and available measurement ranges are listed below.

<b>2</b>	<b>Technical Specifications</b>	<b>P10CFPTxy</b>	<b>P15CFPTxy</b>
	Overall length	: 254 mm	307 mm
	Section area of conical tip	: 1,000 mm <sup>2</sup>	1,500 mm <sup>2</sup>
	Apex angle of conical tip	: 60°	60°
	Surface of friction sleeve	: 15,000 mm <sup>2</sup>	22,500 mm <sup>2</sup>
	Weight	: 1,480 gr	2,250 gr
	Power supply	: 5 Vdc	5 Vdc
	Analogue signal output	: 0 – 5 Vdc	0 – 5 Vdc
	Digital signal output	: RS-485	RS-485
	Screw thread	: Female GHD-36	Female GHD-44
	Connector	: Gold-plated 10 pins	Gold-plated 10 pins
	Working temperature	: 0 till 60 °C	0 till 60 °C
	Storage temperature	: -40 till 85 °C	-40 till 85 °C
	<b>Cone Resistance (q<sub>C</sub>)</b>		
	Available measuring ranges *)	: 0 – 100 MPa	0 – 100 MPa
	Accuracy	: 0.25% of the full scale (FS)	0.25% of the full scale
	Maximum allowable load	: 150% of the measuring range	150% of the range
	Cone area factor	: 0.71	0.75
	<b>Local Sleeve Friction (f<sub>S</sub>) + Cone Resistance (q<sub>C</sub>)</b>		
	Available measuring ranges *)	: 0 – 100 kN	0 – 150 kN
	Accuracy local sleeve friction	: 0.50% of the full scale (FS)	0.50% of the full scale
	Maximum allowable load	: 150% of the measuring range	150% of the range
	Sleeve area ratio	: 1.0	1.0
	<b>Inclination</b>	<b>(biaxial)</b>	
	Available measuring range	: 0 – 25° (biaxial)	0 – 25° (biaxial)
	Accuracy	: < 0,5°	< 0,5°
	<b>Pore Pressure (p)</b>		
	Available measuring ranges *)	: 0 – 5 MPa (standard)	0 – 5 MPa
	Accuracy	: 0.5% of the full scale (FS)	0.5% of the full scale
	<b>Temperature (T)</b>		
	Available measuring ranges	: 0 – 50 °C	0 – 50 °C

**APPENDIX A4 – Cone Calibration Certificate**

Certificate Number: S15-CFIIP.1867-05.03.2021					
<b>CPT CONE CALIBRATION CERTIFICATE</b>					
Cone No.	S15-CFIIP.1867	Date of Calibration	05.03.2021		
Manufacturer	Geopoint	Reference Standards	BS 1377 : 1990 Part 9		
Compression/ Subtraction	Subtraction	Reference Equipment	Pressure meter	LTR01	
Pore Pressure Channel (Y/N)	Y		Vernier callipers	GCV4	
			Load cell	22541	
			Voltmeter	6402486	
Cone end area ratio (by dimension measurement), a	0.70	Sleeve end area ratio (by dimension measurement), b	1.0		
Expanded Combined Uncertainty (U) C1	9.93337 mV	Expanded Combined Uncertainty (U) C2	1.51553 mV	Expanded Combined Uncertainty (U) C3	296.958 mV
Note: Calibration Zero taken as no load in free air, Output taken as slope of linear regression line x maximum load.					
Temperature differential during calibration					0 °C
Cone Type (S/ C/ M/ D/ T)		S		Ch 3 (P/ C/ T/ N/ F)	
				P	
Channel 1	Output 6026 mV	Input 100 kN	Zero 311 mV	Area 15 cm <sup>2</sup>	Alarm 80 kN
Channel 2	6225 mV	100 kN	280 mV	225 cm <sup>2</sup>	80 kN
Channel 3	8517 mV	20 Bar	214 mV		12 Bar
Inclination					Alarm 12 °
	X -20° 448 mV	0° 2524 mV	20° 4629 mV		
	Y 389 mV	2437 mV	4456 mV	Extra Channels N	
CHANNEL 1 - TP			CHANNEL 2 - FRICTION SLEEVE		
CHANNEL 3 - PORE PRESSURE			CHANNEL 4 - INCLINATION		
<b>Calibration Manual</b> Calibration Sheet No. NNN-CP201 Issue Number: 2020-10 Issue Date: 26/10/2020 Calibration Procedure: CP201		<b>Cone calibrated by:</b>  db		<b>Authorised for use by:</b>   Craig Curtis (In Situ Testing Manager)	
This certificate relates to the item calibrated only		Opinions and interpretations expressed herein are outside the scope of UKAS accreditation. © Copyright 2020 SOCOTEC UK Limited			



Gouda Geo-Equipment B.V.  
Satellietbaan 8  
2181 MH Hillegom  
The Netherlands  
  
Tel. + 31 (0)715.318.475  
E-mail: info@gouda-geo.com

## Certificate of Calibration

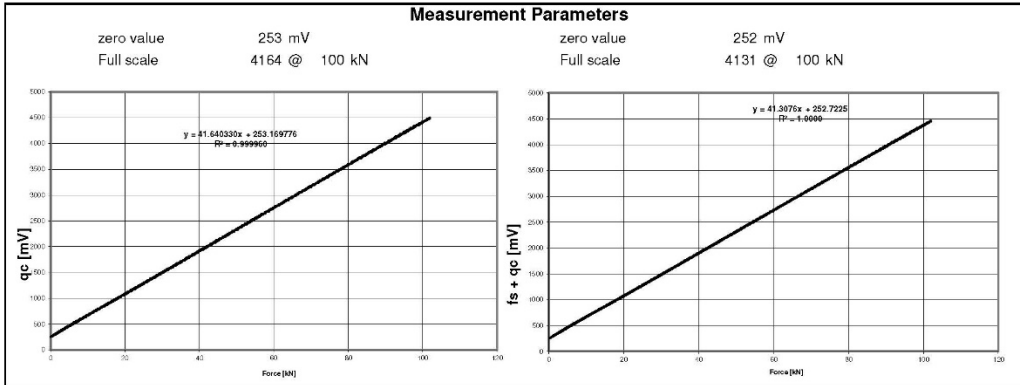
Certificate No. CMI 20.12.3547

Instrument		
Instrument Type:	Electrical Subtraction Cone	Calibration Result: Certified
Manufacturer:	Gouda Geo-Equipment B.V	
Model No.:	DP10-CFPTxy	Date Calibrated: 3-12-2020
Serial No.:	60214	Next Due Date: 3-6-2021
Cone area factor:	0,71	
Used Calibration Procedure: GGECF004, ISO22476		Location: Hillegom (The Netherlands)

Customer
In Situ Site Investigation Ltd.

Calibration Instruments		
Instrument Type: CPT Logger	Instrument Type: CPT Logger	Instrument Type: Load-cell + amplifier
Manufacturer: Gouda Geo Equipment	Manufacturer: Gouda Geo Equipment	Manufacturer: Futek
Model No.: A	Model No.: A	Model No.: LCF500 + IAA100
Serial No.: 3010	Serial No.: 3129	Serial No.: 847498 + 782865
Accuracy: 0.01% + 2 Counts	Accuracy: 0.01% + 2 Counts	Accuracy: 0.1%
Date Calibrated: 11 September, 2020	Date Calibrated: 2 July, 2020	Date Calibrated: 16 September, 2020
Next Due Date: 11 March, 2021	Next Due Date: 2 January, 2021	Next Due Date: 16 September, 2021
Calibrated By: Manufacturer	Calibrated By: Manufacturer	Calibrated By: Futek
Traceability: CMI 20.09.3375	Traceability: CMI 20.07.3208	Traceability: 2009160027

Calibration Conditions		
Environmental conditions whilst performing the calibration:	Ambient Temperature:	21.3 °C
	Relative Humidity:	35.7 %
Condition of Calibrated Apparatus when Received: Fair		



**Remarks**

Data "As Received" = "As Left" unless otherwise noted. Calibration data for this item was derived from one or more of the following sources: the Netherlands Meetinstituut (NMI) or other national laboratory, a natural physical constant, or a ratio technique. The data is on file at the NMI. This calibration is compliant with Gouda Geo-Equipment's internal quality system, internal calibration procedure and meets the requirements of standard ISO22476.

The Calibration Interval will vary from customer use and different conditions. All calibrations are verified at a moment in time; and confirmed within controlled temperature and humidity specified standards. Gouda Geo-Equipment is not responsible for future calibrations. Improper use of the apparatus (e.g. dropping) may cause loss of calibration.

Calibration performed by:	Approved by:
Vincent Vermeer (Engineer)	Rogier Tijm (Senior Engineer)

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## APPENDIX A5 – Symbol List

### English

a	is area ratio of the cone ( $= A_n/A_c$ )
A	is area
$A_c$	is projected area of the cone
$A_n$	is cross sectional area of load cell or shaft
$A_s$	is area of friction sleeve
$A_{sb}$	is bottom end area of friction sleeve
$A_{st}$	is top end area of friction sleeve
$B_q$	is pore pressure parameter ( $= (u_2 - u_0)/(q_t - \sigma_{v0})$ )
$C_h$	is horizontal coefficient of consolidation
$C_v$	is vertical coefficient of consolidation
D	is diameter
$D_r$	is relative density ( $= \frac{e_{max}-e}{e_{max}-e_{min}} \times 100\%$ )
e	is void ratio
$e_{max}$	is maximum void ratio
$e_{min}$	is minimum void ratio
E	is Young's modulus
$f_s$	is unit sleeve friction resistance
$f_t$	is sleeve friction corrected for pore pressure effects
$F_s$	is total force acting on friction sleeve
$F_R$	is normalized friction ratio ( $= f_s/(q_t - \sigma_{v0})$ )
FoS	is factor of safety
FC	is fines content
g	is acceleration due to gravity
$G_0$	is initial or maximum shear modulus, shear stiffness
$I_c$	is soil behavior type index
$I_r$	is rigidity index ( $= G/s_u$ )
$I_p$	is plasticity index
k	is coefficient of permeability
$k_h$	is coefficient of permeability in horizontal direction
$k_v$	is coefficient of permeability in vertical direction
$K_0$	is coefficient of earth pressure at rest ( $= \sigma'_{h0}/\sigma'_{v0}$ )
L	is length
$m_v$	is coefficient of volume change
M	is constrained deformation modulus
M7.5	is earthquake magnitude of 7.5 Richter scale
N	is number of blows of SPT
$N_{60}$	is SPT energy ratio
$N_k$	is cone factor
$N_{ke}$	is cone factor
$N_{kt}$	is cone factor
$N_{\Delta u}$	is cone factor
$p_a$	is reference stress ( $= 100 \text{ kPa}$ )
$q_c$	is measured cone resistance
$q_e$	is effective cone resistance ( $= q_t - u_2$ )
$q_n$	is net cone resistance ( $= q_t - \sigma_{v0}$ )
$q_t$	is corrected cone resistance ( $= q_c - (1 - a)u_2$ )
$Q_c$	is total force acting on the cone
$Q_t$	is normalized cone resistance ( $= q_t - \sigma_{v0}/\sigma'_{v0}$ )

$R_f$	is friction ratio $(= (f_t/q_t) \times 100\%$ or alternatively $= (f_t/q_t) \times 100\%$ )
$s_u$	is undrained shear strength
$s_{ur}$	is remoulded undrained shear strength
$S_t$	is sensitivity
$t$	is time
$t_{50}$	is time for 50% dissipation of excess pore water pressure
$T_{50}$	is time factor at $U = 50\%$
$u$	is pore water pressure
$u_0$	is in situ pore pressure
$u_1$	is pore pressure measured on the cone
$u_2$	is pore pressure measured behind the cone
$u_3$	is pore pressure measured behind sleeve friction
$\Delta u$	is excess pore water pressure
$U$	is normalized excess pore pressure
$V_s$	is shear wave velocity
$z$	is depth

### Greek

$\alpha$	is constant
$\alpha$	is cone roughness
$\beta$	is constant
$\beta_1$	is the angle between the vertical axis and the projection of the axis of the CPTU on a vertical plane, in degrees
$\beta_2$	is the angle between the vertical axis and the projection of the axis of the CPTU on a vertical plane that is perpendicular to the plane of angle $\beta_1$ , in degrees
$\gamma$	is unit weight of soil
$\gamma_w$	unit weight of water
$\Delta$	is change
$\Delta u$	is excess pore pressure $(= u - u_0)$
$\mu$	is Poisson's ratio
$\rho$	is density
$\psi$	is state parameter
$\sigma, \sigma'$	is normal stress (total, effective)
$\sigma_h, \sigma'_h$	is horizontal stress (total, effective)
$\sigma_v, \sigma'_v$	is horizontal stress (total, effective)
$\sigma_{v0}, \sigma'_{v0}$	is overburden stress (total, effective)
$T_{av}$	is average cyclic shear stress
$T_{cy}$	is cyclic shear stress
$\phi'$	is effective friction angle

## APPENDIX A6 – Abbreviations

ASTM	American Society for Testing and Materials
CPTU	Cone Penetration Test with Pore Pressure Measurement (Piezocone Test)
CRR	Cyclic Resistance Ratio
CSR	Cyclic Stress Ratio
GWT	Ground Water Table
NC	Normally Consolidated
OC	Over consolidated
OCR	Over consolidation Ratio
PL	Limit Pressure
SDMT	Seismic Dilatometer Marchetti
SPT	Standard Penetration Test
TC	Technical Committee

## APPENDIX A7 – Glossary

### **CPT**

Cone Penetration Test.

### **Cone**

The part of the cone penetrometer on which the end bearing is developed.

### **Cone Penetrometer**

The assembly containing the *cone*, *friction sleeve*, any other sensors and measuring systems, as well as the connections to the *push-rods*.

### **Cone resistance, $q_c$**

The total force acting on the cone,  $Q_c$ , divided by the projected area of the cone,  $A_c$ .  $q_c = Q_c/A_c$

### **Corrected cone resistance, $q_t$**

The *cone resistance*,  $q_c$  corrected for pore water pressure effects.

### **Corrected sleeve friction, $f_t$**

The *sleeve friction* corrected for pore water pressure effects on the ends of the *friction sleeve*.

### **Data acquisition system**

The system used to measure and record the measurements made by the *cone penetrometer*.

### **Dissipation Test**

A test when the decay of the pore water pressure is monitored during a pause in penetration.

### **Filter element**

The porous element inserted into the cone penetrometer to allow transmission of the pore water pressure to the pore pressure sensor, while maintaining the correct profile of the *cone penetrometer*.

### **Friction ratio, $R_f$**

The ratio, expressed as a percentage of the *sleeve friction*,  $f_s$ , to the *cone resistance*,  $q_c$ , both measured at the same depth.

### **Friction reducer**

A local enlargement on the push-rod surface, placed at a distance above the cone penetrometer, and provided to reduce the friction on the *push-rods*.

### **Friction sleeve**

The section of the *cone penetrometer* upon which the *sleeve friction* is measured.

### **Normalized cone resistance, $Q_c$ or $Q_t$**

The *cone resistance* expressed in a non-dimensional form and taking account of stress changes *in situ*,  $Q_c = (q_c - \sigma_{v0})/\sigma'_{v0}$ , or when the *corrected cone resistance* is used  $Q_t = (q_t - \sigma_{v0})/\sigma'_{v0}$ . Where  $\sigma_{v0}$  and  $\sigma'_{v0}$  are the total and effective vertical stress respectively.

### **Net cone resistance, $q_n$**

The *corrected cone resistance* minus the vertical total stress.  $q_n = q_t - \sigma_{v0}$

### **Normalized friction ratio, $F_r$**

The *sleeve friction* normalized by the *net cone resistance*.

### **Piezocone**

A *cone penetrometer* containing a pore pressure sensor.



**Pore pressure,  $u$** 

The pore pressure generated during penetration and measured by a pore pressure sensor,  $u_1$  when measured on the cone,  $u_2$  when measured just behind the cone and  $u_3$  when measured just behind the friction sleeve.

**Pore pressure ratio,  $B_q$** 

The *net pore pressure* normalized with respect to the *net cone resistance*.

**Push-rods**

The thick-walled tubes or rods used for advancing the cone penetrometer.

**Rig machine**

The equipment which pushes the cone penetrometer and rods into the ground.

**Sleeve friction,  $f_s$** 

The total frictional force acting on the *friction sleeve*,  $F_s$ , divided by its *surface area*,  $A_s$ .  $f_s = F_s/A_s$

## APPENDIX A8 – Soils Description Tables

### GRANULAR SOILS (Sands and Gravels)

Description	Relative Density $D_r$ (%)	SPT N value, $N_{SPT}$
Very Loose	0 – 15	0 - 4
Loose	15 – 35	4 - 10
Medium Dense	35 – 65	10 - 30
Dense	65 – 85	30 - 50
Very Dense	>85	>50

### COHESIVE SOILS (Clays and Silts)

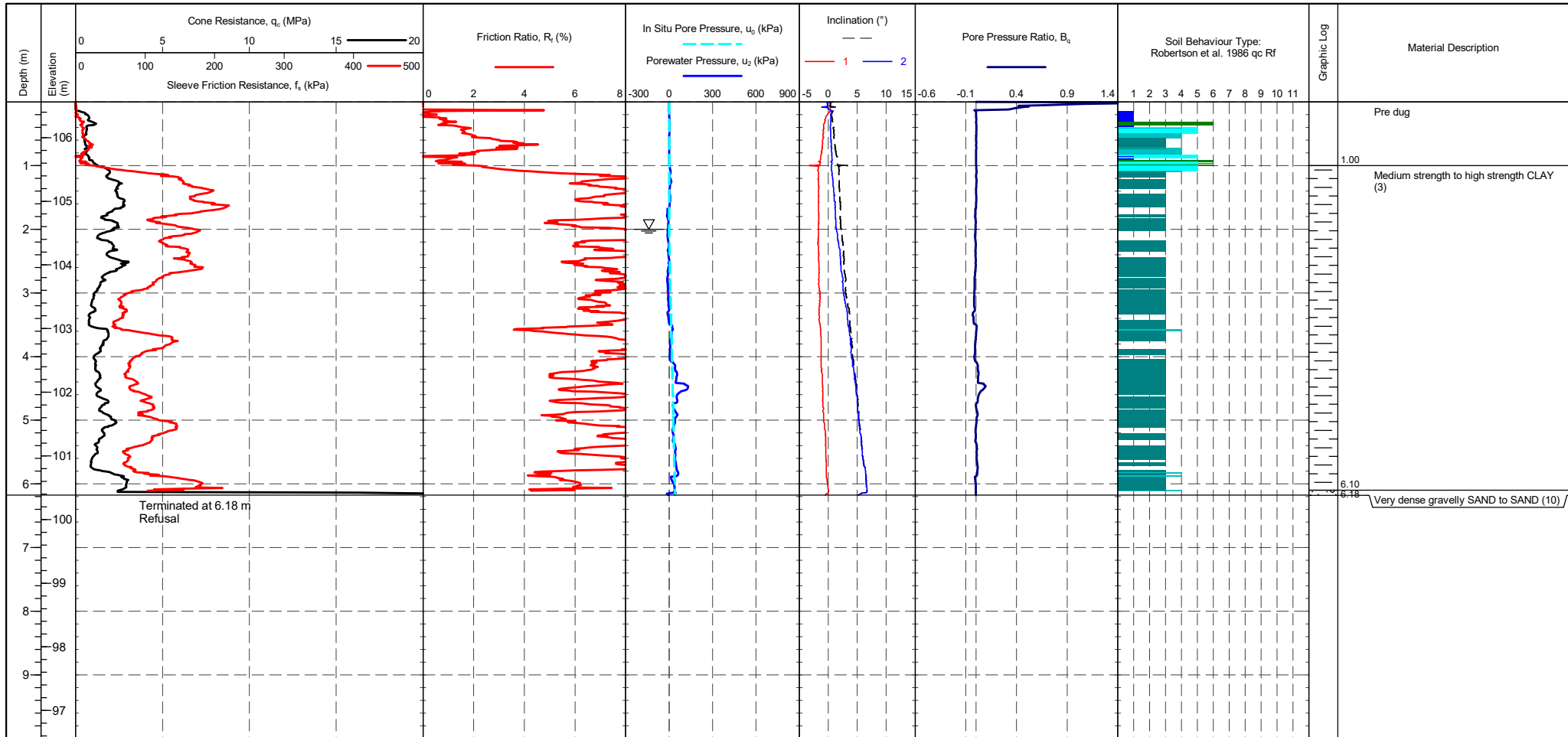
Term based on measurement	Undrained Shear Strength Classification, $s_u$ (kPa)
Extremely low	<10
Very low	10 - 20
Low	20 - 40
Medium	40 - 75
High	75 - 150
Very high	150 - 300
Extremely high	>300

## **APPENDIX B**

# **Cone Penetration Measured Parameters and Geotechnical Derived Parameters**

PointID	<b>CPT01</b>
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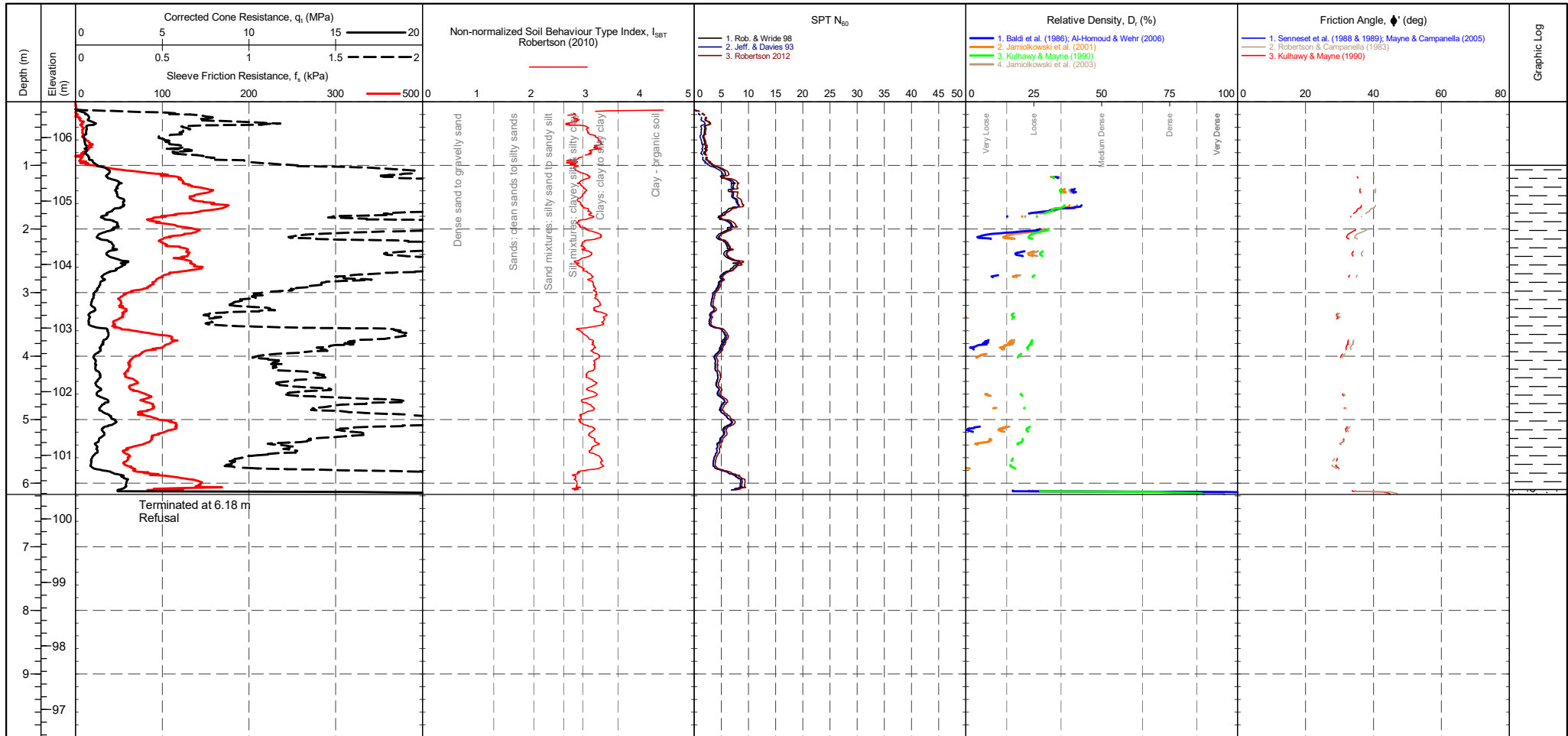
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490888.438 m <b>NORTHING</b> : 290863.511 m <b>ELEVATION</b> : 106.560 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip: Pre 365 mV, Post 364 mV, Difference -0.011 MPa Sleeve: Pre 289 mV, Post 287 mV, Difference -0.001 kPa Pore Pressure 2: Pre 220 mV, Post 251 mV, Difference 0.007 kPa X-Y Inclinator: Pre 2599 mV, Post 2501 mV	<b>METHOD:</b> Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravelly SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID  
**CPT01**

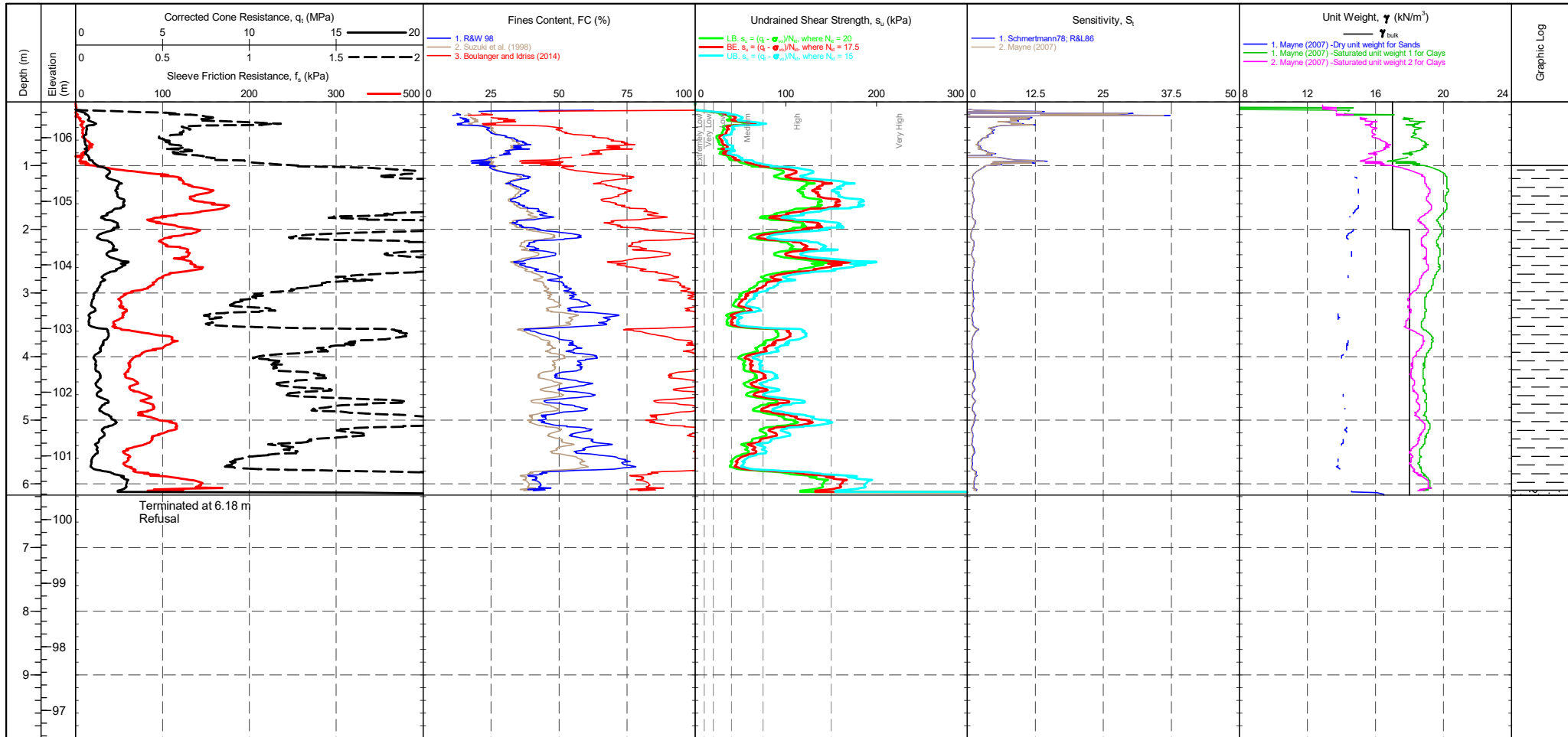
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490888.438 m <b>NORTHING</b> : 290863.511 m <b>ELEVATION</b> : 106.560 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> <b>Tip</b> : 365 mV <b>Sleeve</b> : 289 mV <b>Pore Pressure 2</b> : 220 mV <b>X-Y Inclinator</b> : 2599 mV	<b>CPTU ZERO VALUES</b> <b>Post</b> : 364 mV <b>Difference</b> : -0.011 MPa <b>Difference</b> : -0.001 kPa <b>Difference</b> : 0.007 kPa <b>Difference</b> : 2501 mV	<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, I<sub>c</sub></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density Dr (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, I <sub>c</sub>	Description	SPT N value, NSPT	Description	Relative Density Dr (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
Description	SBT Index, I <sub>c</sub>	Description	SPT N value, NSPT	Description	Relative Density Dr (%)																																				
Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15																																				
Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35																																				
Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65																																				
Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85																																				
Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85																																				

PointID	<b>CPT01</b>
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490888.438 m <b>NORTHING</b> : 290863.511 m <b>ELEVATION</b> : 106.560 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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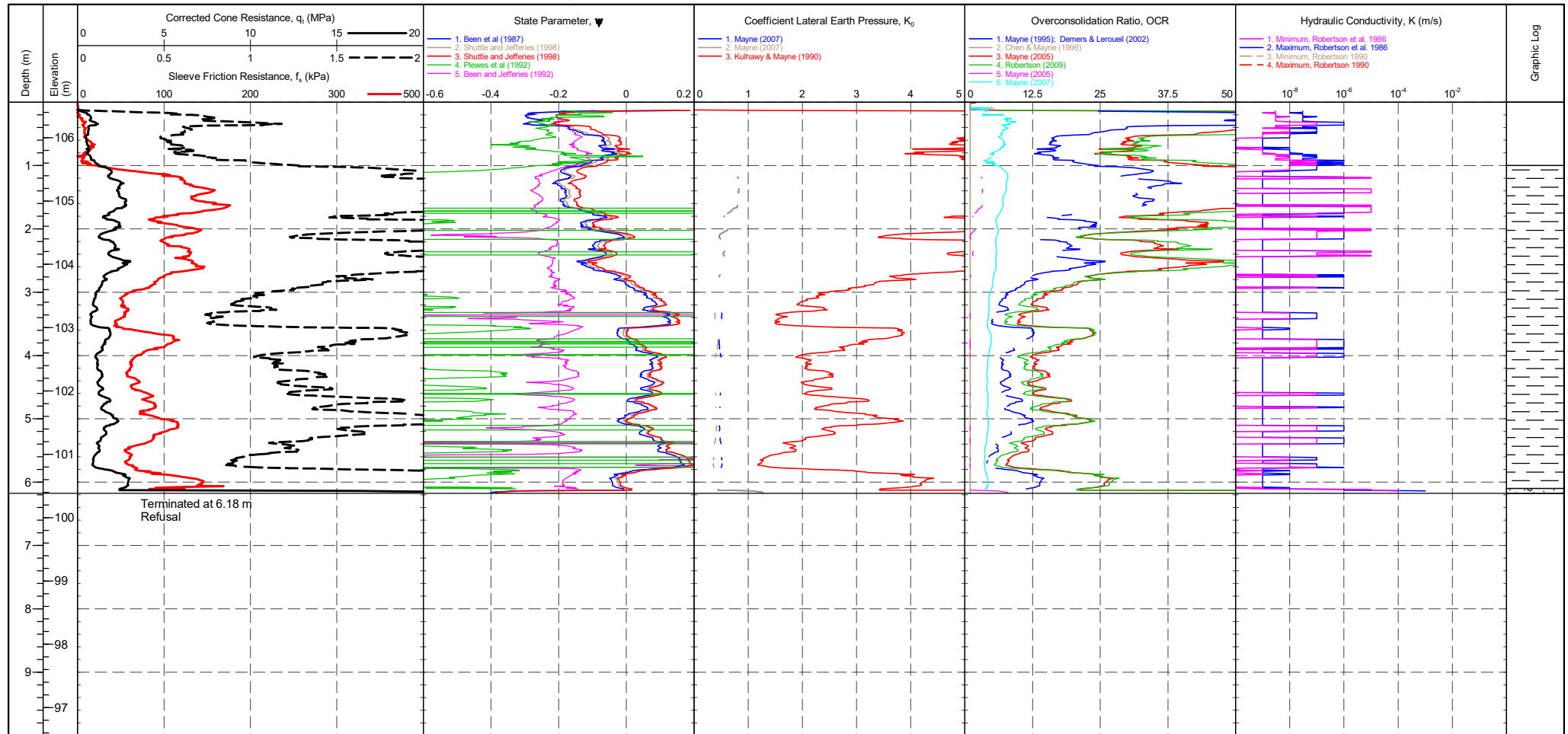


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 365 mV / 364 mV / -0.011 MPa Sleeve: 289 mV / 287 mV / -0.001 kPa Pore Pressure 2: 220 mV / 251 mV / 0.007 kPa X-Y Inclinator: 2599 mV / 2501 mV	<b>CPTU ZERO VALUES</b> Pre: 365 mV Post: 364 mV Difference: -0.011 MPa	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement su (kPa) Extremely low strength <10 Very low strength 10-20 Low strength 20-40	Term based on measurement su (kPa) Medium strength 40-75 High strength 75-150 Very high strength 150-300 Extremely high strength >300	▽ Groundwater Level ▮ Dissipation Test
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PointID

CPT01

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490888.438 m <b>NORTHING</b> : 290863.511 m <b>ELEVATION</b> : 106.560 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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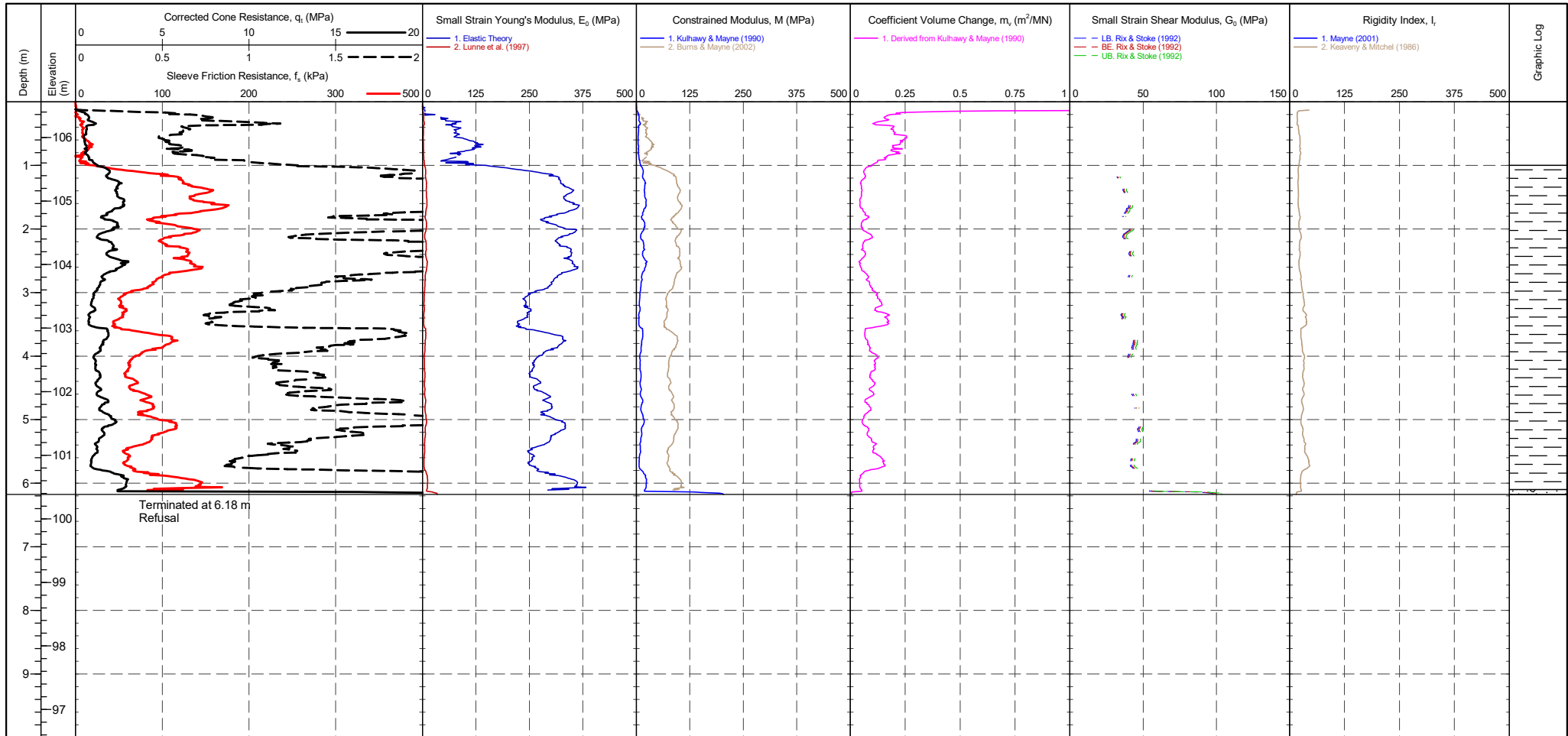


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 365 mV (Pre), 364 mV (Post), -0.011 MPa (Difference) Sleeve: 289 mV (Pre), 287 mV (Post), -0.001 kPa (Difference) Pore Pressure 2: 220 mV (Pre), 251 mV (Post), 0.007 kPa (Difference) X-Y Inclinator: 2599 mV (Pre), 2501 mV (Post)	<b>CPTU ZERO VALUES</b> Tip: 365 mV (Pre), 364 mV (Post), -0.011 MPa (Difference) Sleeve: 289 mV (Pre), 287 mV (Post), -0.001 kPa (Difference) Pore Pressure 2: 220 mV (Pre), 251 mV (Post), 0.007 kPa (Difference) X-Y Inclinator: 2599 mV (Pre), 2501 mV (Post)	Groundwater Level Dissipation Test
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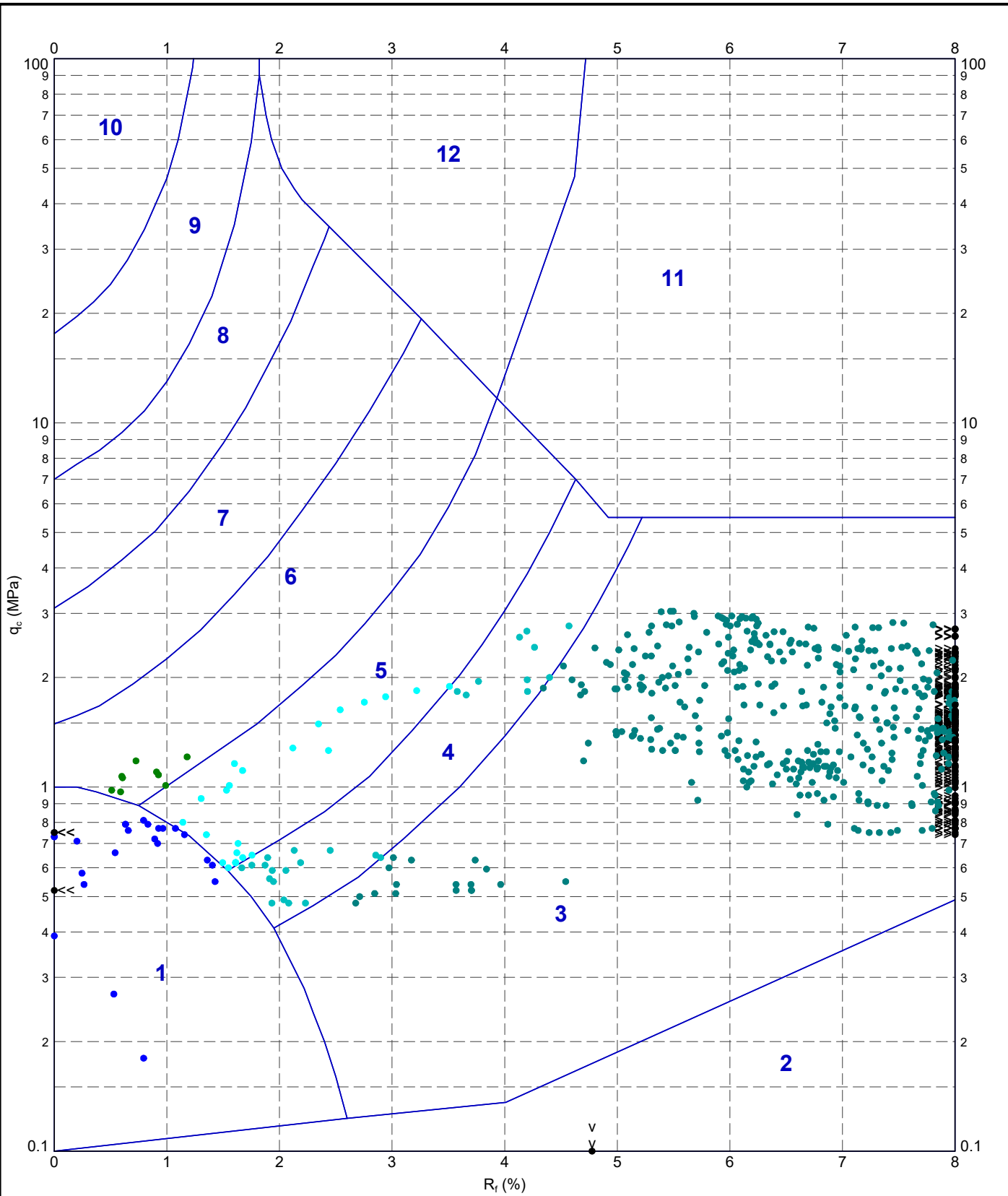
PointID  
**CPT01**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490888.438 m <b>NORTHING</b> : 290863.511 m <b>ELEVATION</b> : 106.560 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>365 mV</td> <td>364 mV</td> <td>-0.011 MPa</td> </tr> <tr> <td>Sleeve</td> <td>289 mV</td> <td>287 mV</td> <td>-0.001 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>220 mV</td> <td>251 mV</td> <td>0.007 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2599 mV</td> <td>2501 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	365 mV	364 mV	-0.011 MPa	Sleeve	289 mV	287 mV	-0.001 kPa	Pore Pressure 2	220 mV	251 mV	0.007 kPa	X-Y Inclinator	2599 mV	2501 mV		Groundwater Level Dissipation Test
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220228-ADVANCED REPORT INSTITUTE 2.02.1 LIB - CHLOE.GLB Graph CPT ROBERTSON ET AL. 8F QC VS. RF APF 1220144 CORBY DELTA SIMONS.GPJ <<DrawingFile>> 04/03/2022 15:26 10.01.00.11 Datagel Lab and In Situ Tool - DGD [Lib: In Situ SI 2.02.0/2017-07-10 Proj: In Situ SI 2.02.0 2017-07-10]



METHOD: Robertson et al. 1986 qc Rf

- 1 - Sensitive fine grained material
- 2 - Organic material
- 3 - CLAY
- 4 - Silty CLAY to CLAY
- 5 - Clayey SILT to silty CLAY
- 6 - Sandy SILT to clayey SILT
- 7 - Silty SAND to sandy SILT
- 8 - SAND to silty SAND
- 9 - SAND
- 10 - Gravelly SAND to SAND
- 11 - Very stiff fine grained
- 12 - SAND to clayey SAND

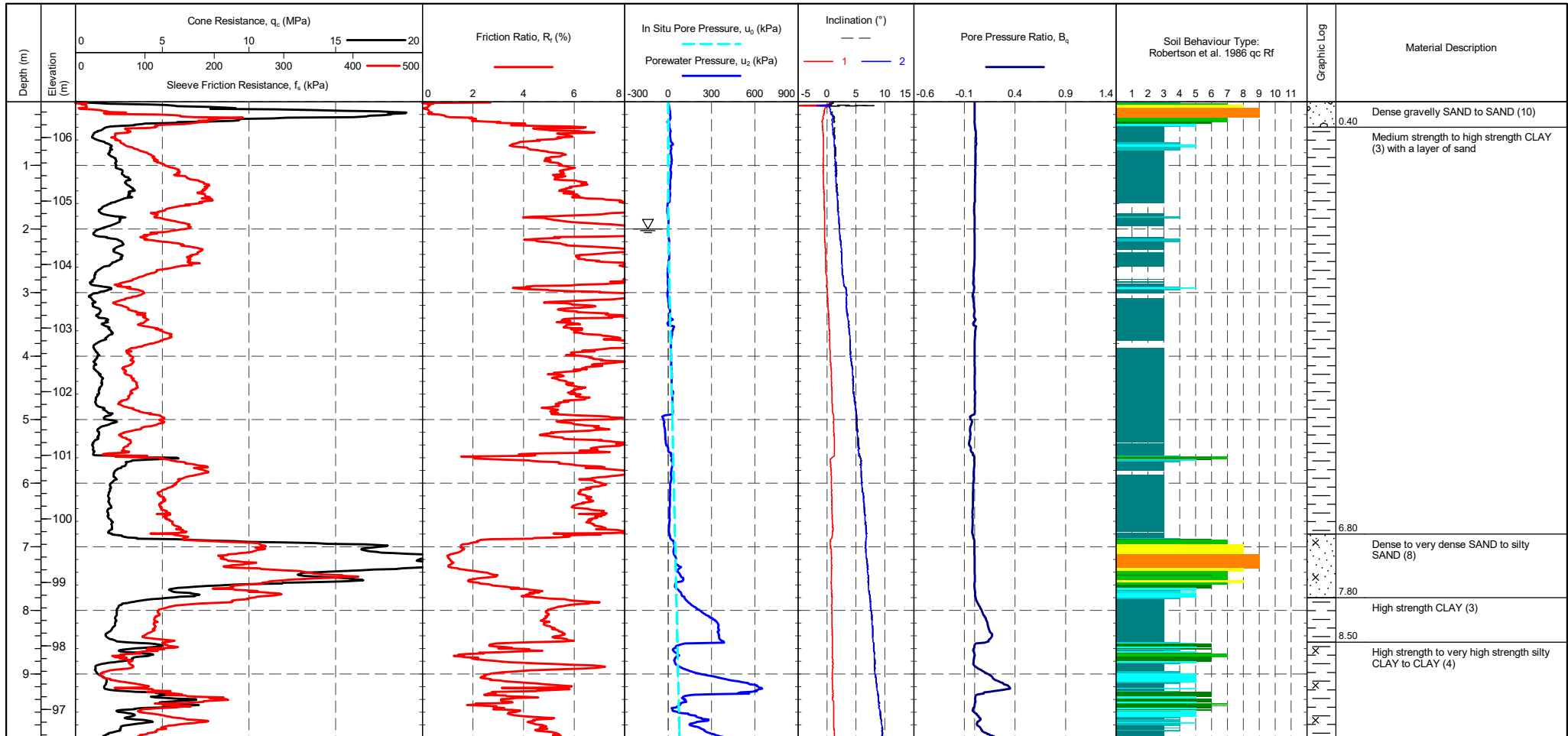


TITLE  
 Delta Simons  
 Cordby  
 Corby  
 Robertson et al. 1986 qc vs. Rf - CPT01

DRAWN	DATE	04/03/2022
CHECKED	DATE	04/03/2022
SCALE	Not To Scale	
PROJECT No	1220144	
FIGURE No	A4	

PointID	<b>CPT01A</b>
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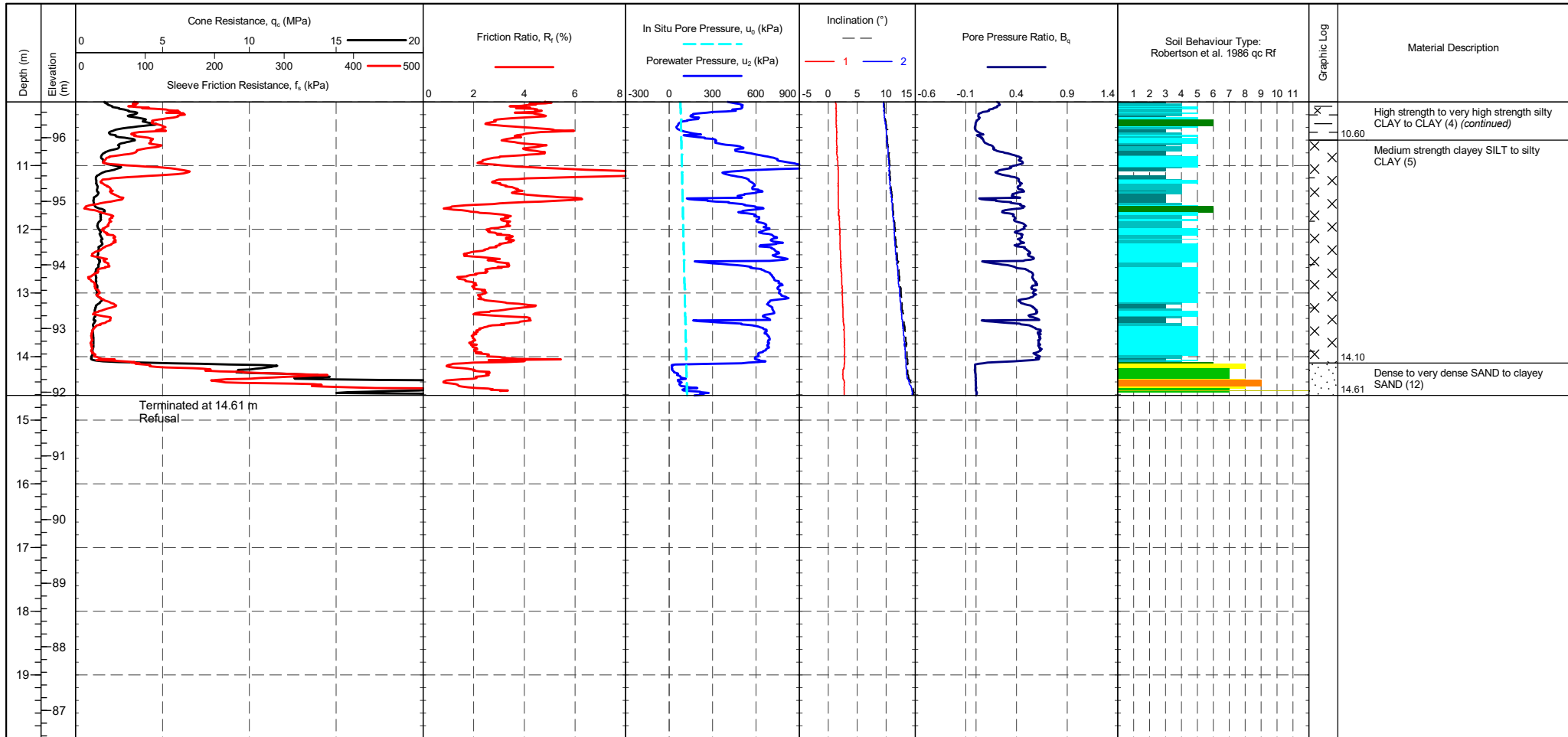
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490888.438 m <b>NORTHING</b> : 290863.511 m <b>ELEVATION</b> : 106.560 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip : 367 mV / 359 mV / -0.089 MPa Sleeve : 290 mV / 287 mV / -0.002 kPa Pore Pressure 2 : 224 mV / 296 mV / 0.017 kPa X-Y Inclinator : 2603 mV / 2576 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravelly SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID	<b>CPT01A</b>
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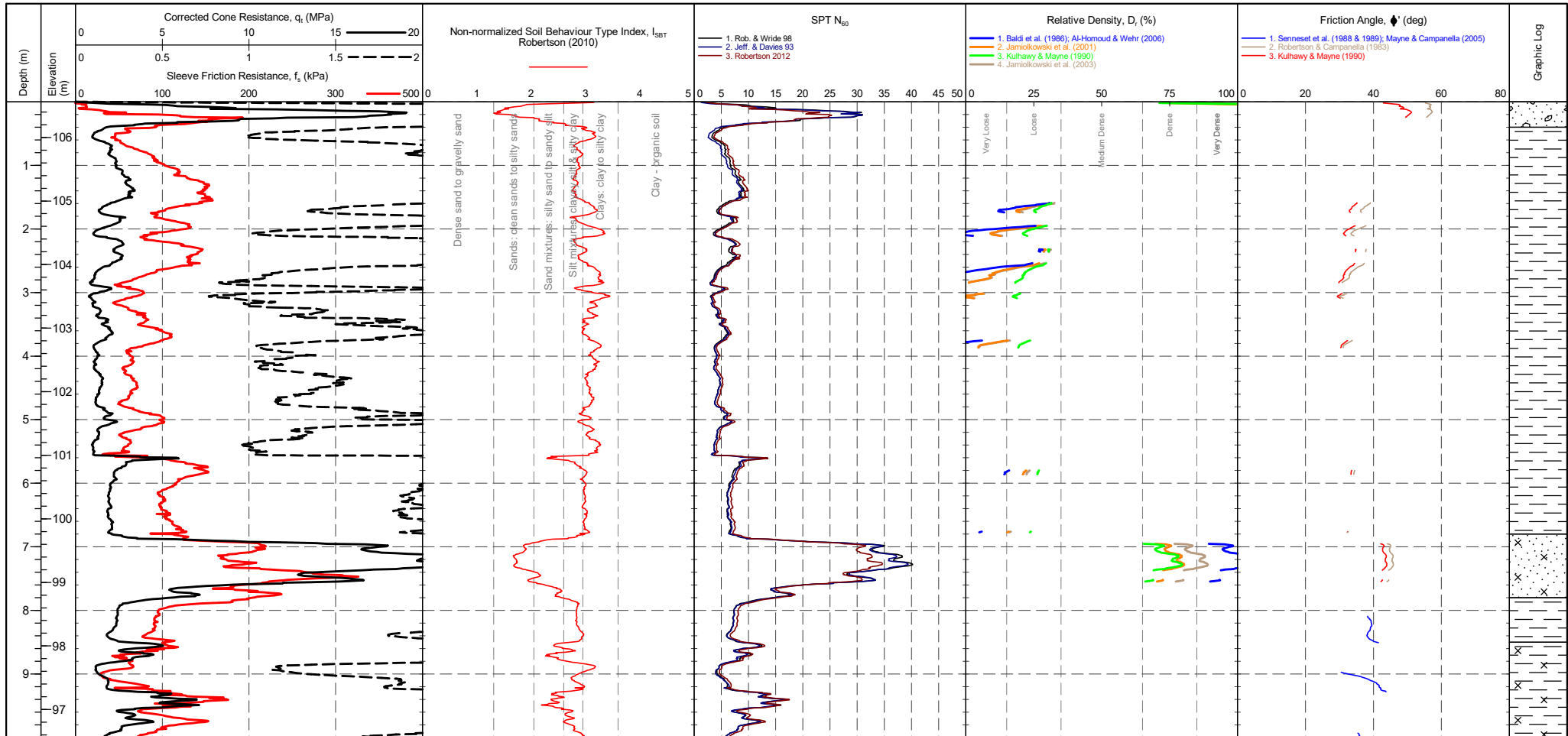
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**CPT01A**

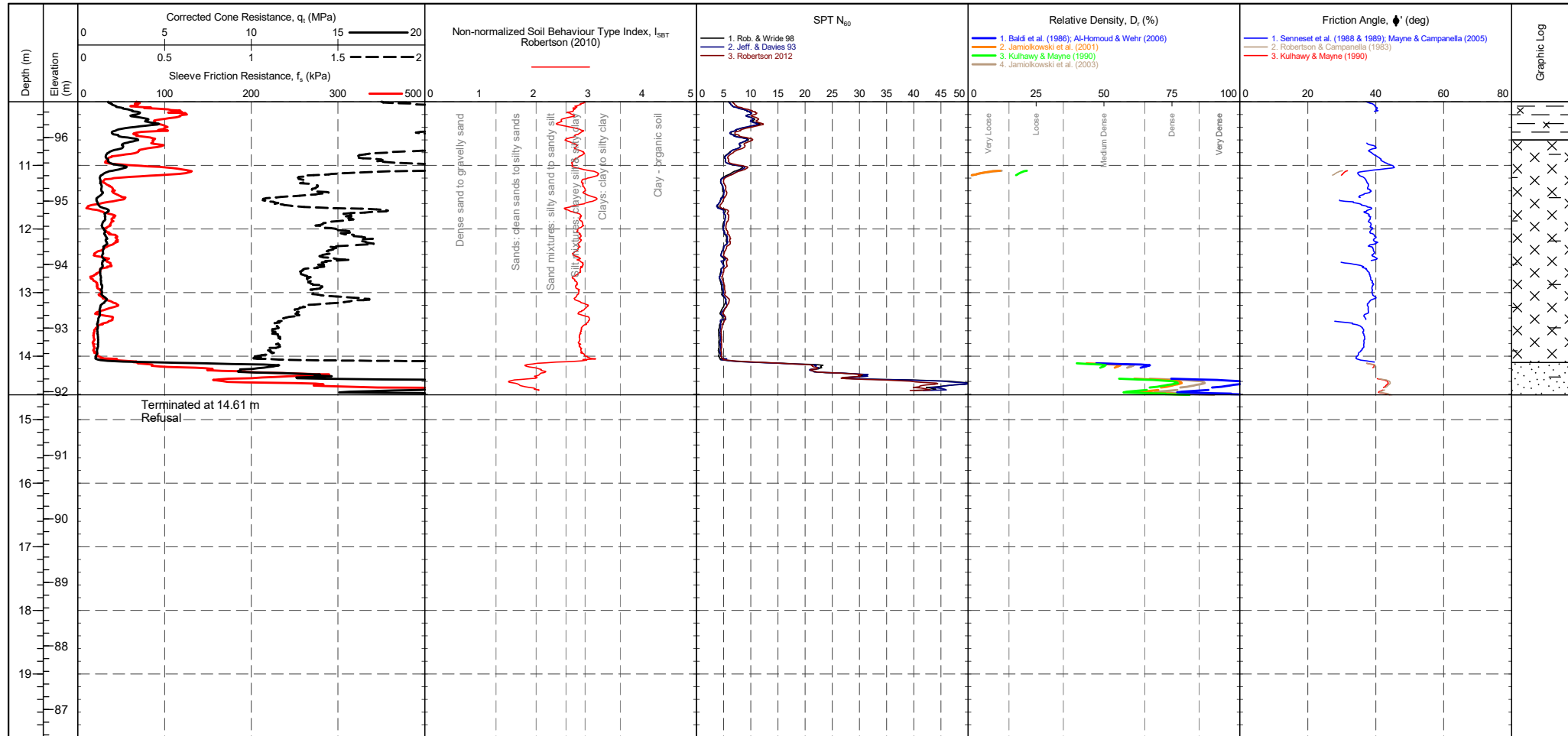
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**CPT01A**

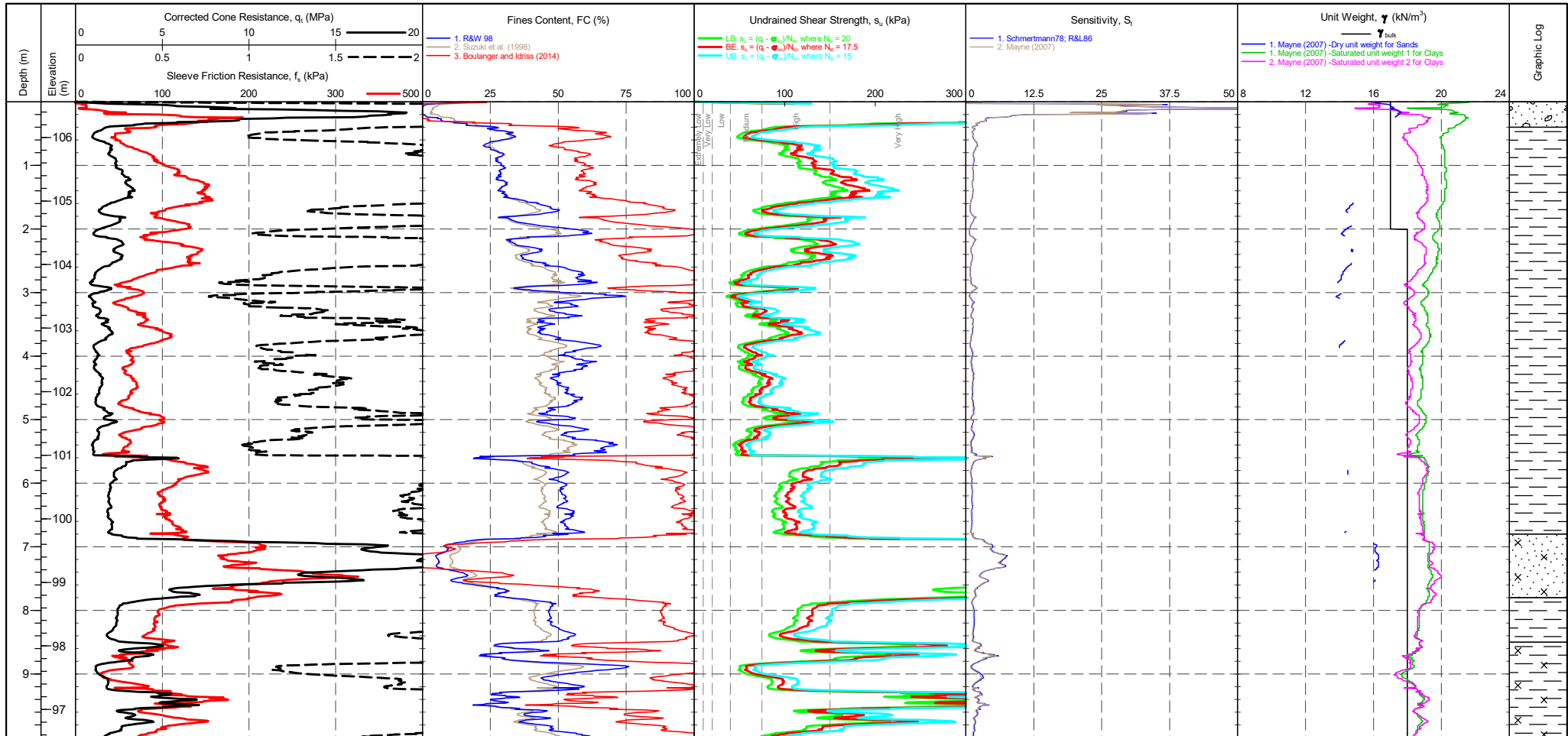
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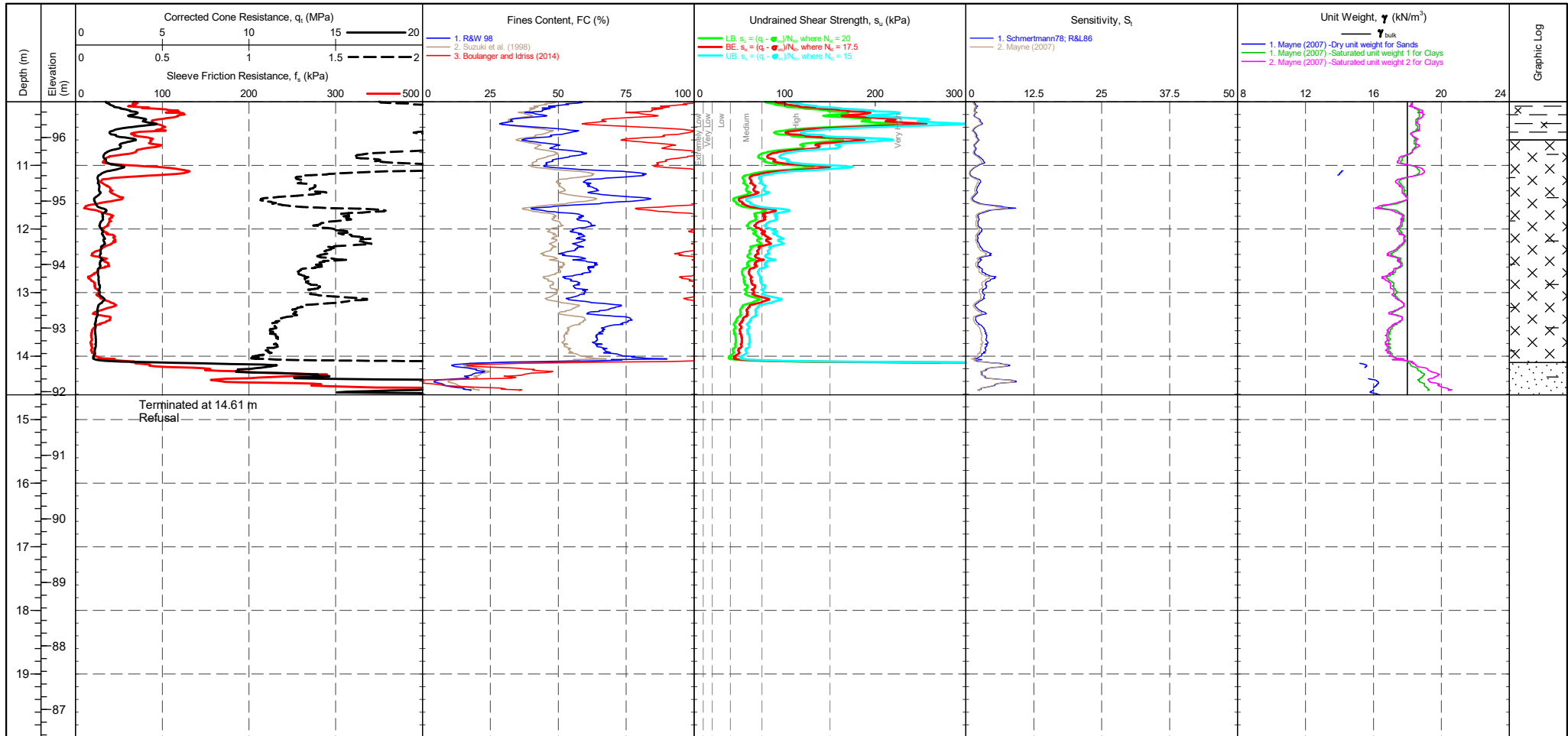


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 367 mV Sleeve: 290 mV Pore Pressure 2: 224 mV X-Y Inclinator: 2603 mV	<b>Post</b> 359 mV 287 mV 296 mV 2576 mV	<b>Difference</b> -0.089 MPa -0.002 kPa 0.017 kPa	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement su (kPa) Extremely low strength <10 Very low strength 10-20 Low strength 20-40	Term based on measurement su (kPa) Medium strength 40-75 High strength 75-150 Very high strength 150-300 Extremely high strength >300	▽ Groundwater Level  ▭ Dissipation Test
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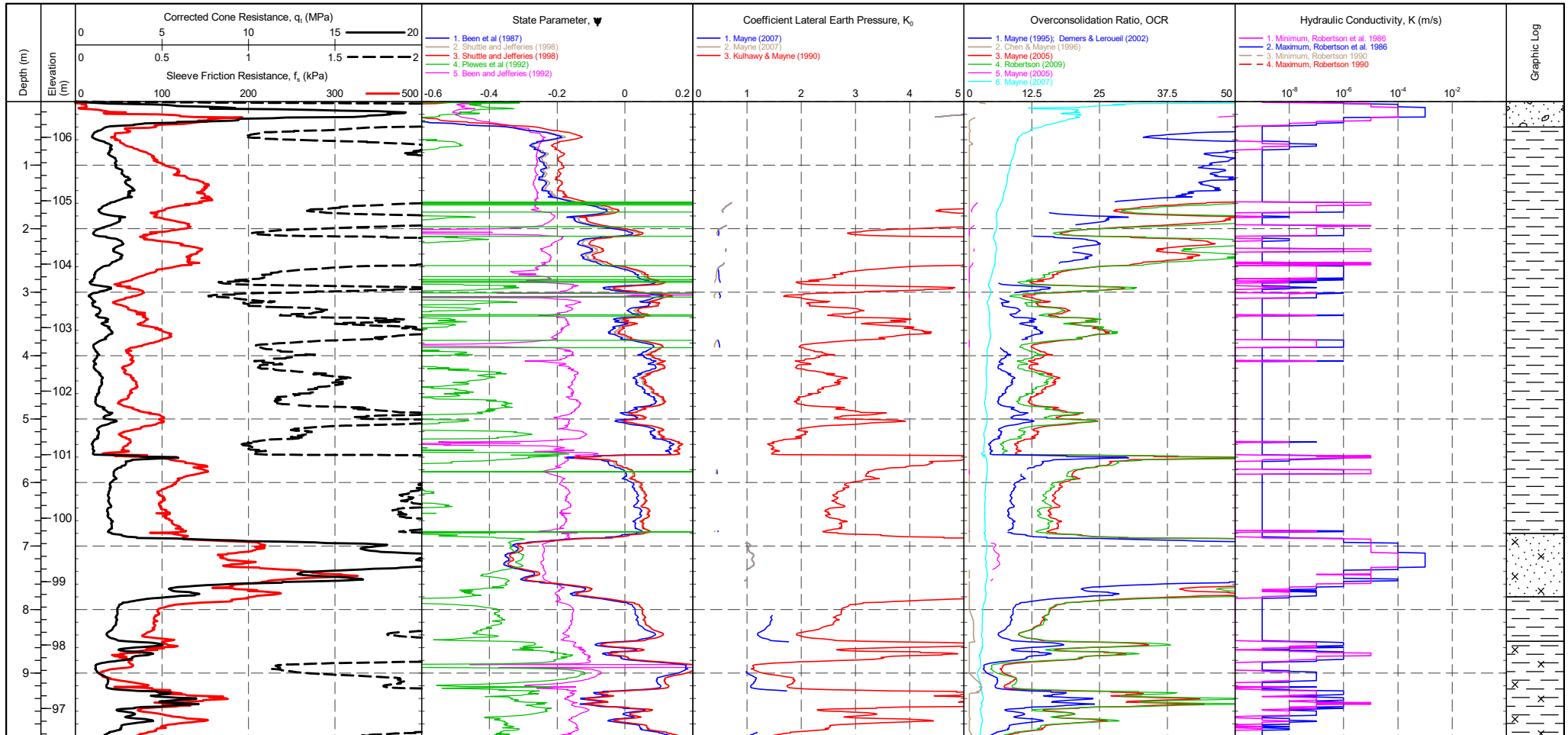


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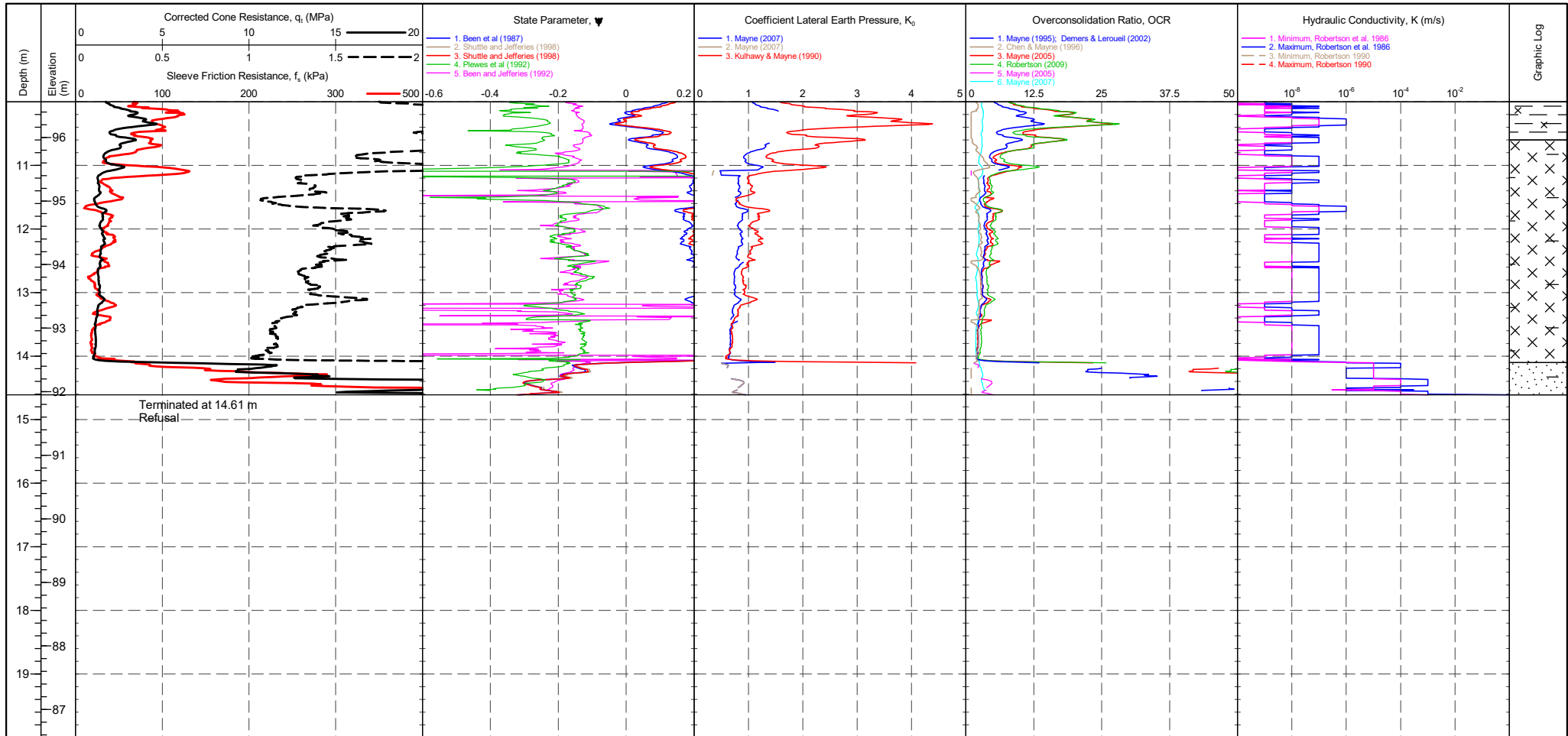
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>367 mV</td> <td>359 mV</td> <td>-0.089 MPa</td> </tr> <tr> <td>Sleeve</td> <td>290 mV</td> <td>287 mV</td> <td>-0.002 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>224 mV</td> <td>296 mV</td> <td>0.017 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2603 mV</td> <td>2576 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	367 mV	359 mV	-0.089 MPa	Sleeve	290 mV	287 mV	-0.002 kPa	Pore Pressure 2	224 mV	296 mV	0.017 kPa	X-Y Inclinator	2603 mV	2576 mV		Groundwater Level Dissipation Test
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PointID  
**CPT01A**

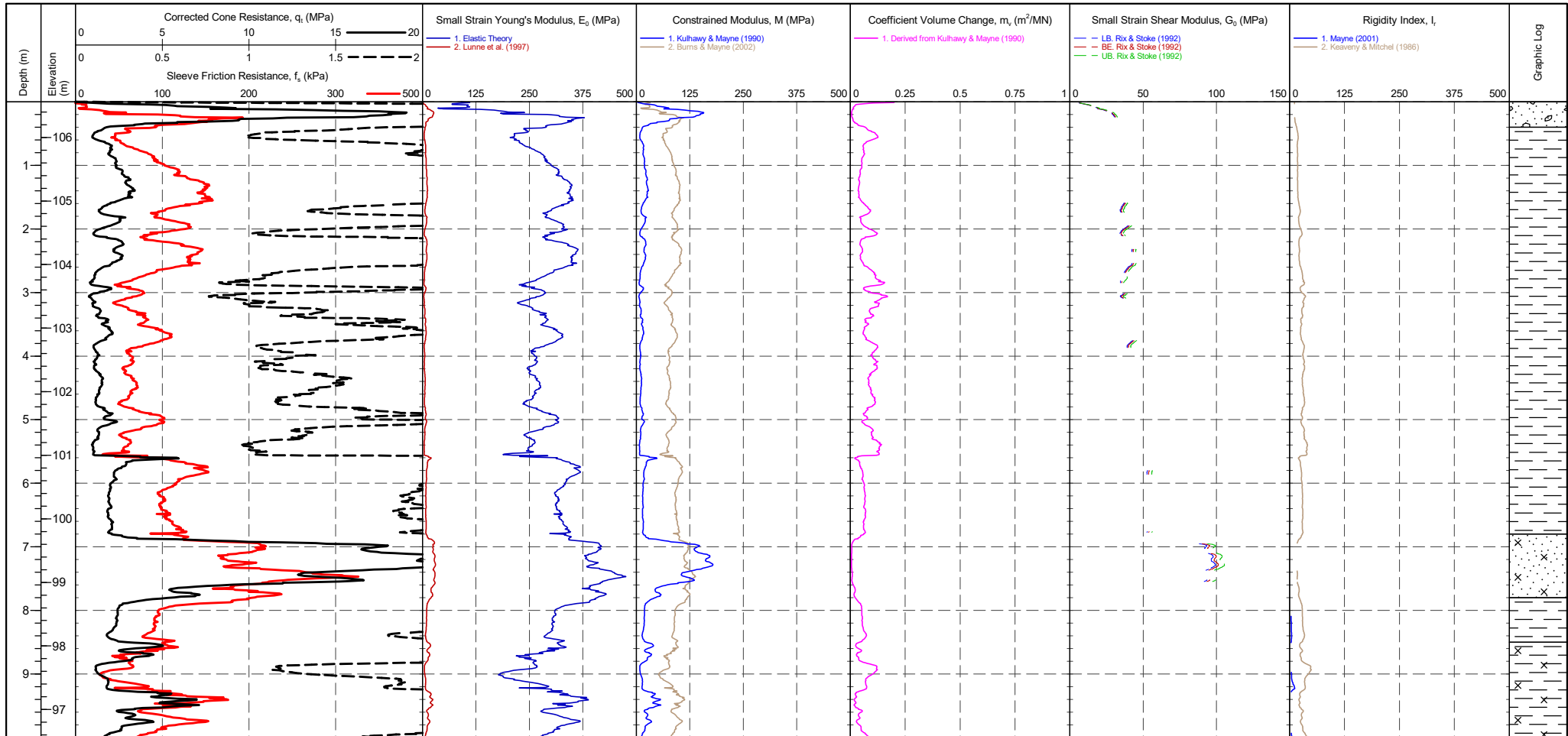
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490888.438 m <b>NORTHING</b> : 290863.511 m <b>ELEVATION</b> : 106.560 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>367 mV</td> <td>359 mV</td> <td>-0.089 MPa</td> </tr> <tr> <td>Sleeve</td> <td>290 mV</td> <td>287 mV</td> <td>-0.002 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>224 mV</td> <td>296 mV</td> <td>0.017 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2603 mV</td> <td>2576 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	367 mV	359 mV	-0.089 MPa	Sleeve	290 mV	287 mV	-0.002 kPa	Pore Pressure 2	224 mV	296 mV	0.017 kPa	X-Y Inclinator	2603 mV	2576 mV		Groundwater Level Dissipation Test
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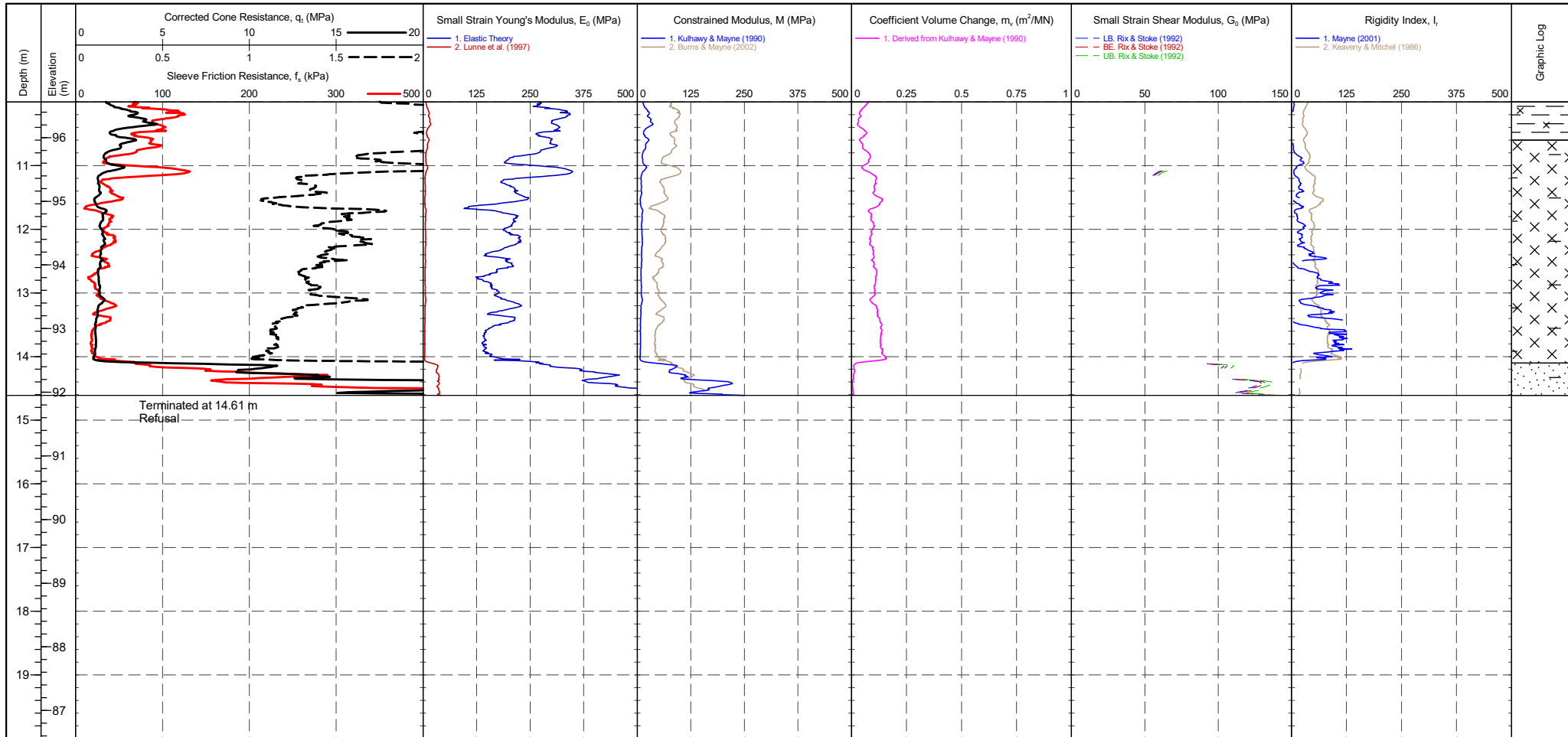
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490888.438 m <b>NORTHING</b> : 290863.511 m <b>ELEVATION</b> : 106.560 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>367 mV</td> <td>359 mV</td> <td>-0.089 MPa</td> </tr> <tr> <td>Sleeve</td> <td>290 mV</td> <td>287 mV</td> <td>-0.002 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>224 mV</td> <td>296 mV</td> <td>0.017 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2603 mV</td> <td>2576 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	367 mV	359 mV	-0.089 MPa	Sleeve	290 mV	287 mV	-0.002 kPa	Pore Pressure 2	224 mV	296 mV	0.017 kPa	X-Y Inclinator	2603 mV	2576 mV		Groundwater Level Dissipation Test
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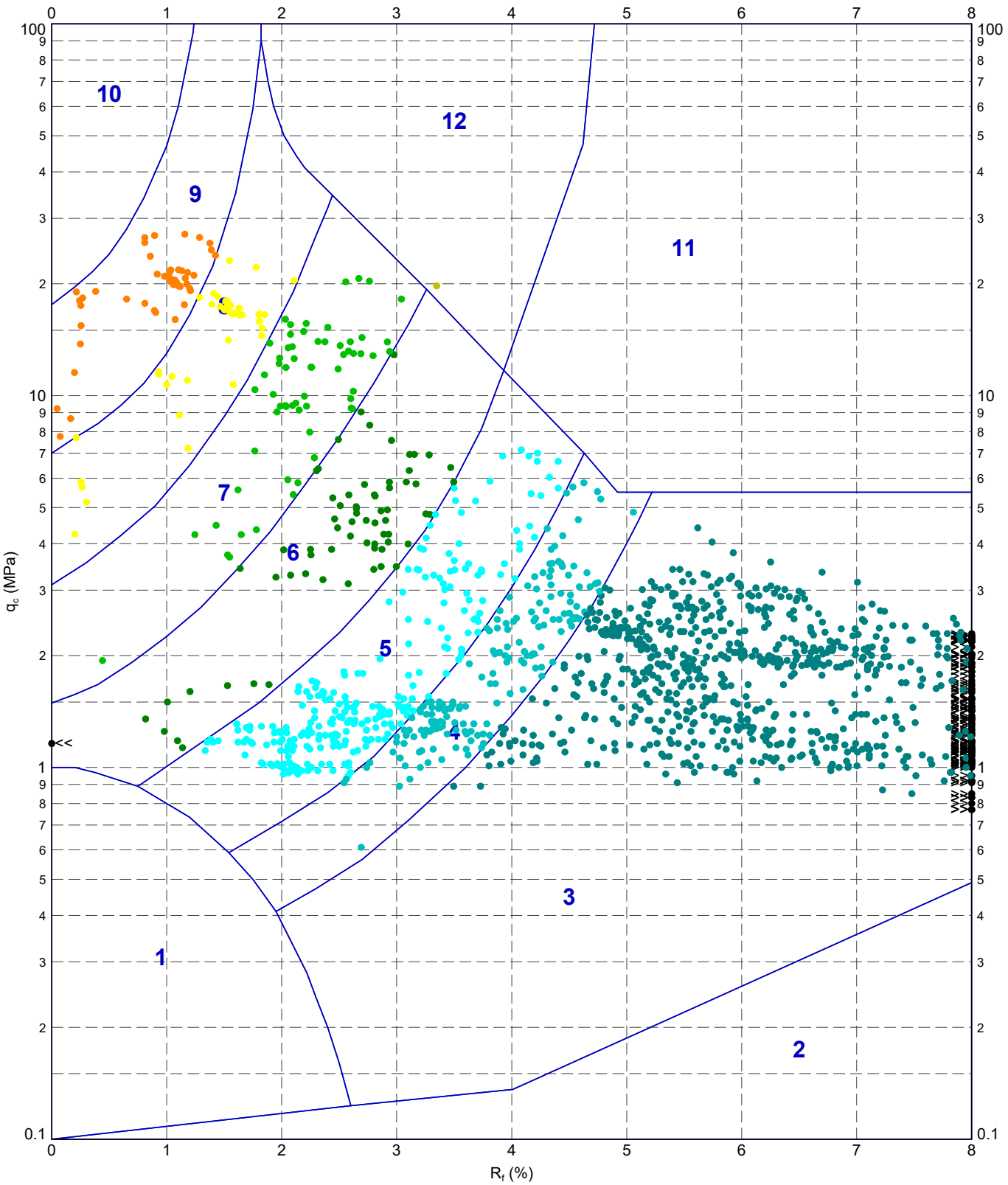
PointID  
**CPT01A**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490888.438 m <b>NORTHING</b> : 290863.511 m <b>ELEVATION</b> : 106.560 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>367 mV</td> <td>359 mV</td> <td>-0.089 MPa</td> </tr> <tr> <td>Sleeve</td> <td>290 mV</td> <td>287 mV</td> <td>-0.002 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>224 mV</td> <td>296 mV</td> <td>0.017 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2603 mV</td> <td>2576 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	367 mV	359 mV	-0.089 MPa	Sleeve	290 mV	287 mV	-0.002 kPa	Pore Pressure 2	224 mV	296 mV	0.017 kPa	X-Y Inclinator	2603 mV	2576 mV		Groundwater Level Dissipation Test
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220228-ADVANCED REPORT INSTITUTE 2.02.1 LIB - CHLOE.GLB Graph: CPT ROBERTSON ET AL. 8F QC VS. RF APF 1220144 CORBY DELTA SIMONS G.P.I. <<DrawingFile>> 04/03/2022 15:33 10.01.00.11 Datagel Lab and In Situ Tool - DGD [Lib: In Situ SI 2.02.0 2017-07-10 Proj: In Situ SI 2.02.0 2017-07-10]

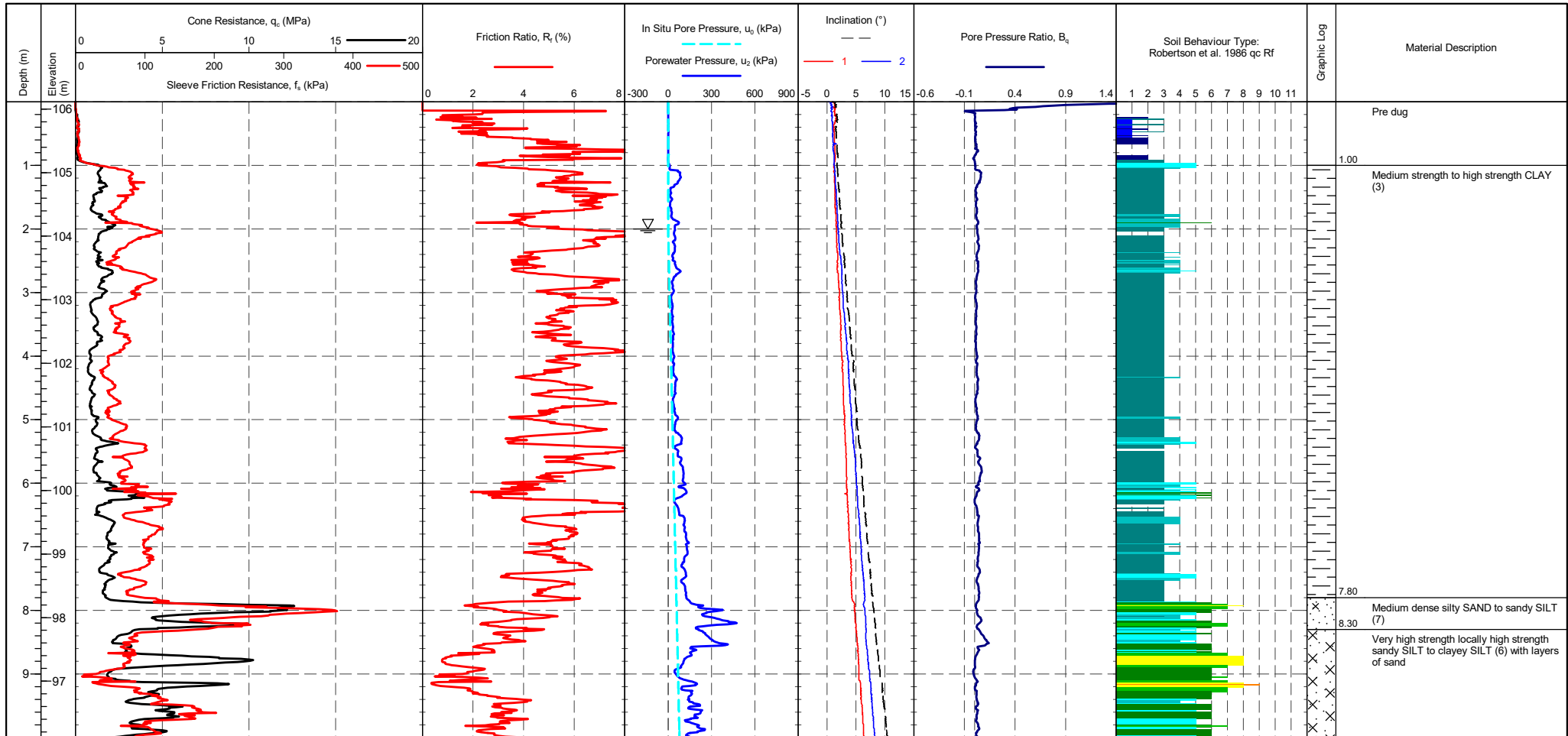


- METHOD: Robertson et al. 1986 qc Rf**
- 1 - Sensitive fine grained material
  - 4 - Silty CLAY to CLAY
  - 7 - Silty SAND to sandy SILT
  - 10 - Gravelly SAND to SAND
  - 2 - Organic material
  - 5 - Clayey SILT to silty CLAY
  - 8 - SAND to silty SAND
  - 11 - Very stiff fine grained
  - 3 - CLAY
  - 6 - Sandy SILT to clayey SILT
  - 9 - SAND
  - 12 - SAND to clayey SAND

	TITLE Delta Simons Cordby Corby Robertson et al. 1986 qc vs. Rf - CPT01A	DRAWN	DATE 04/03/2022
		CHECKED	DATE 04/03/2022
		SCALE Not To Scale	A4
		PROJECT No 1220144	FIGURE No

PointID	<b>CPT02</b>
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490949.518 m <b>NORTHING</b> : 290883.378 m <b>ELEVATION</b> : 106.114 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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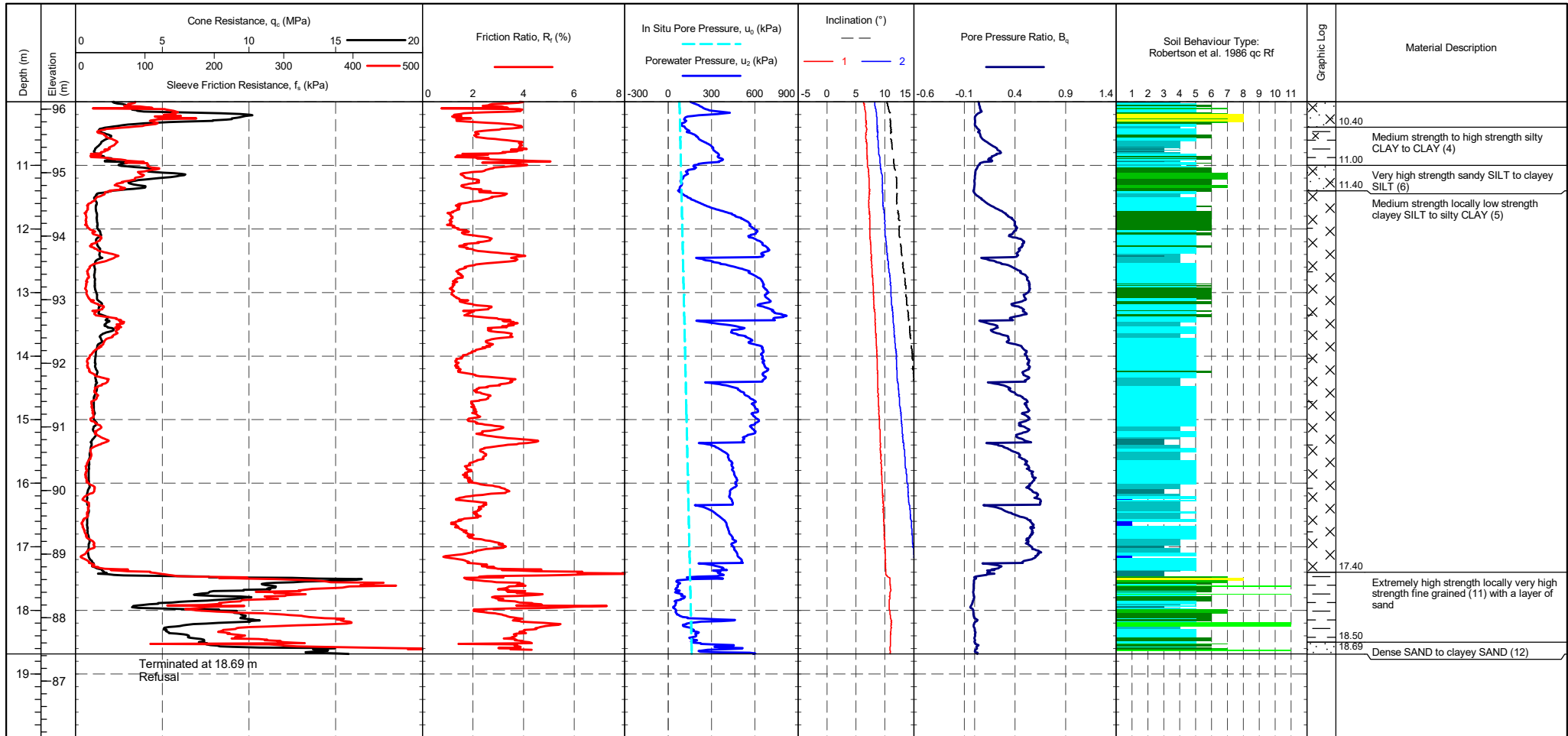


<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip: Pre 362 mV, Post 391 mV, Difference 0.321 MPa Sleeve: Pre 285 mV, Post 284 mV, Difference -0.001 kPa Pore Pressure 2: Pre 203 mV, Post 254 mV, Difference 0.012 kPa X-Y Inclinator: Pre 2671 mV, Post 2620 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravely SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID  
**CPT02**

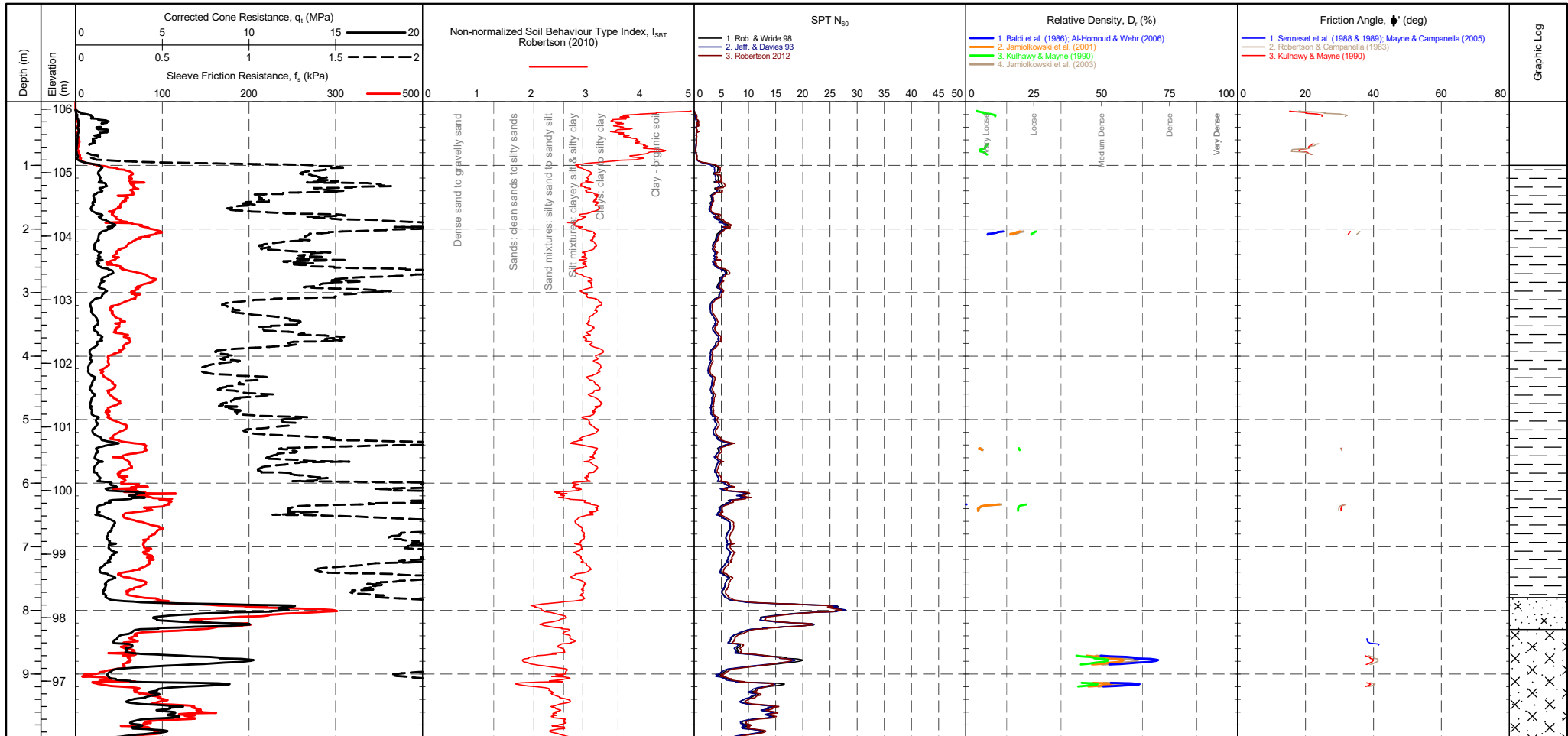
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip            Pre       Post       Difference 362 mV   391 mV   0.321 MPa Sleeve       285 mV   284 mV   -0.001 kPa Pore Pressure 2   203 mV   254 mV   0.012 kPa X-Y Inclinator   2671 mV   2620 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravely SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level  Dissipation Test
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PointID	<b>CPT02</b>
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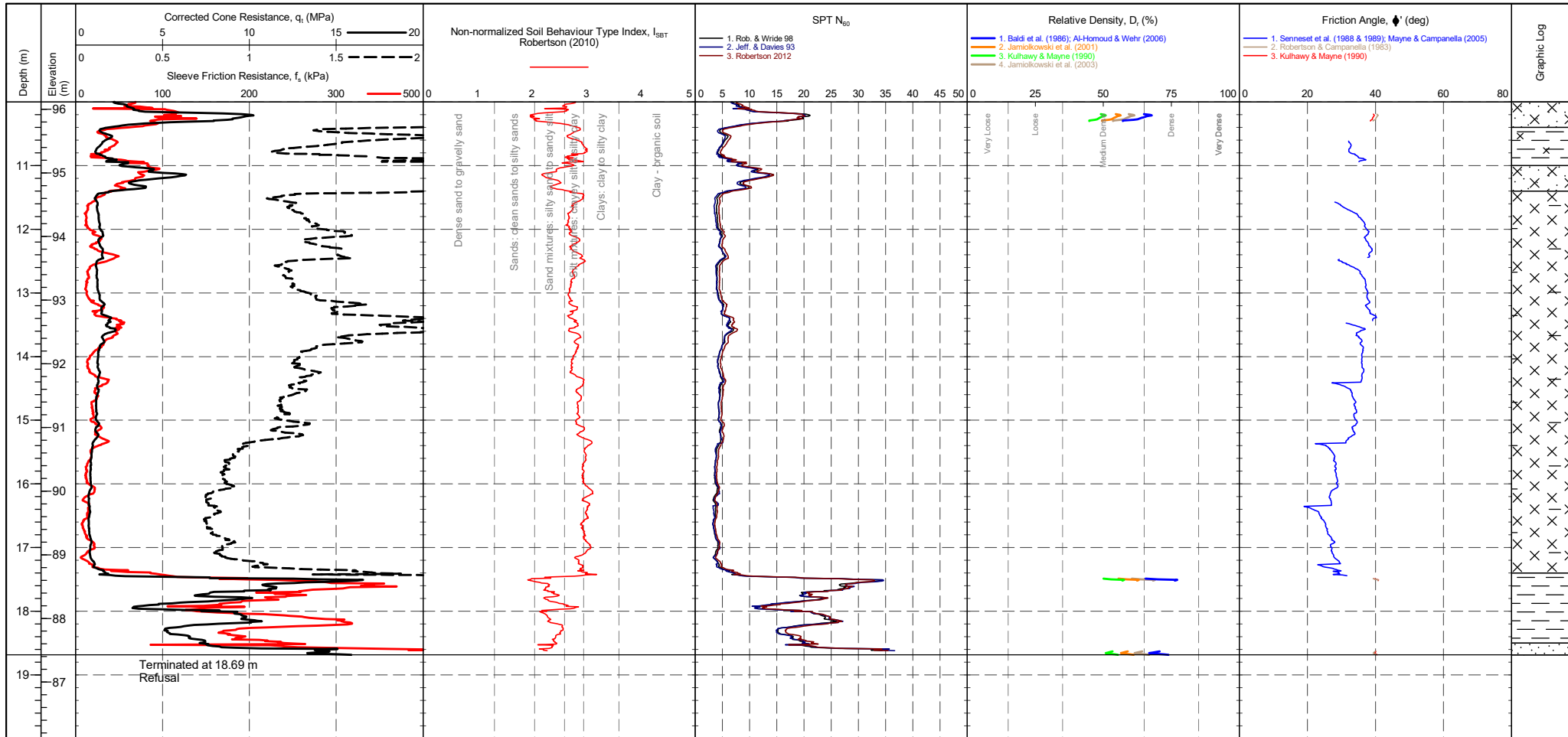
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PointID	<b>CPT02</b>
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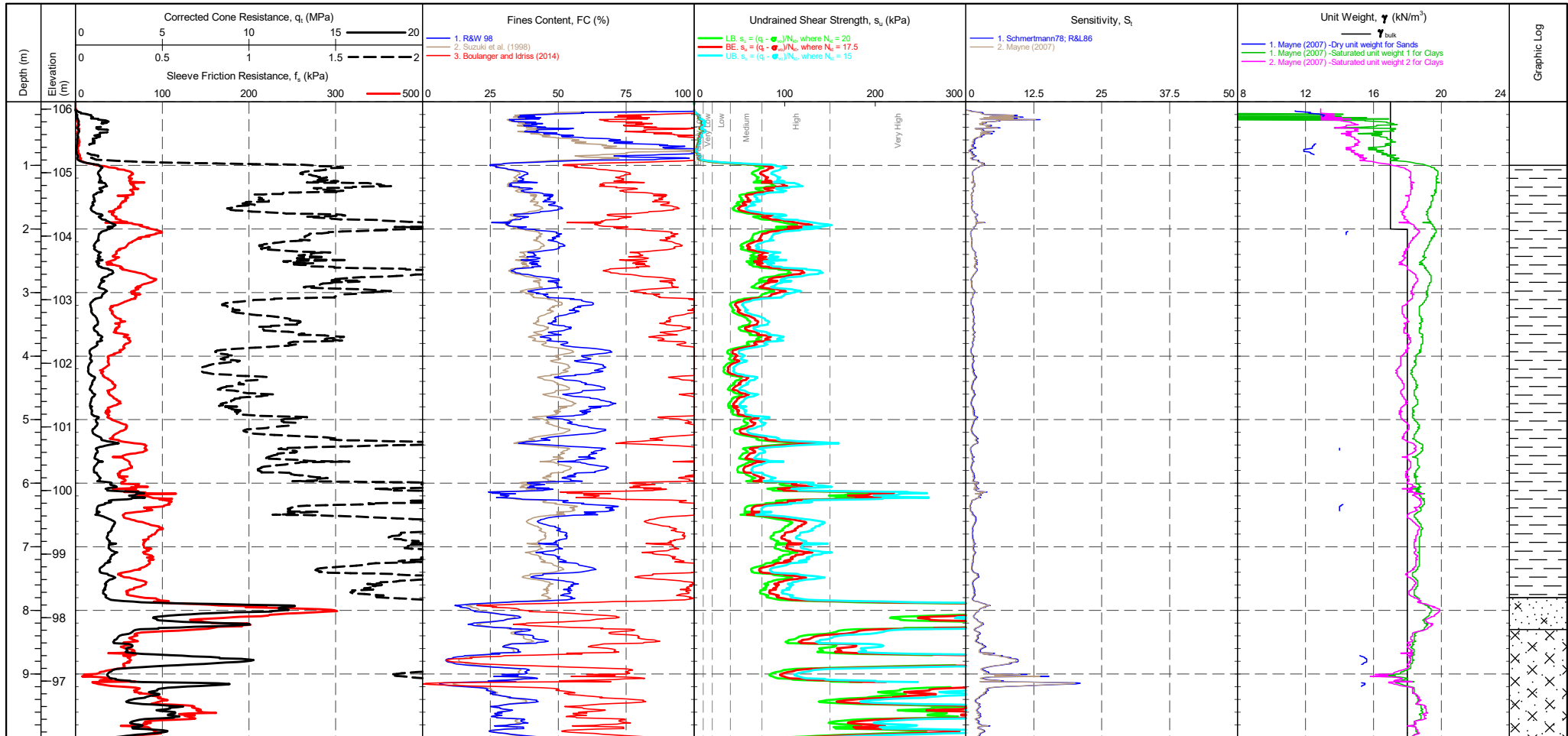
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490949.518 m <b>NORTHING</b> : 290883.378 m <b>ELEVATION</b> : 106.114 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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



<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> <b>Tip</b> : 362 mV <b>Sleeve</b> : 285 mV <b>Pore Pressure 2</b> : 203 mV <b>X-Y inclinometer</b> : 2671 mV	<b>CPTU ZERO VALUES</b> <b>Pre</b> : 391 mV <b>Post</b> : 284 mV <b>Difference</b> : 0.321 MPa <b>Difference</b> : -0.001 kPa <b>Difference</b> : 0.012 kPa <b>Difference</b> : 2620 mV	<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, I<sub>c</sub></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density D<sub>r</sub> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, I <sub>c</sub>	Description	SPT N value, NSPT	Description	Relative Density D <sub>r</sub> (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
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PointID  
**CPT02**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490949.518 m <b>NORTHING</b> : 290883.378 m <b>ELEVATION</b> : 106.114 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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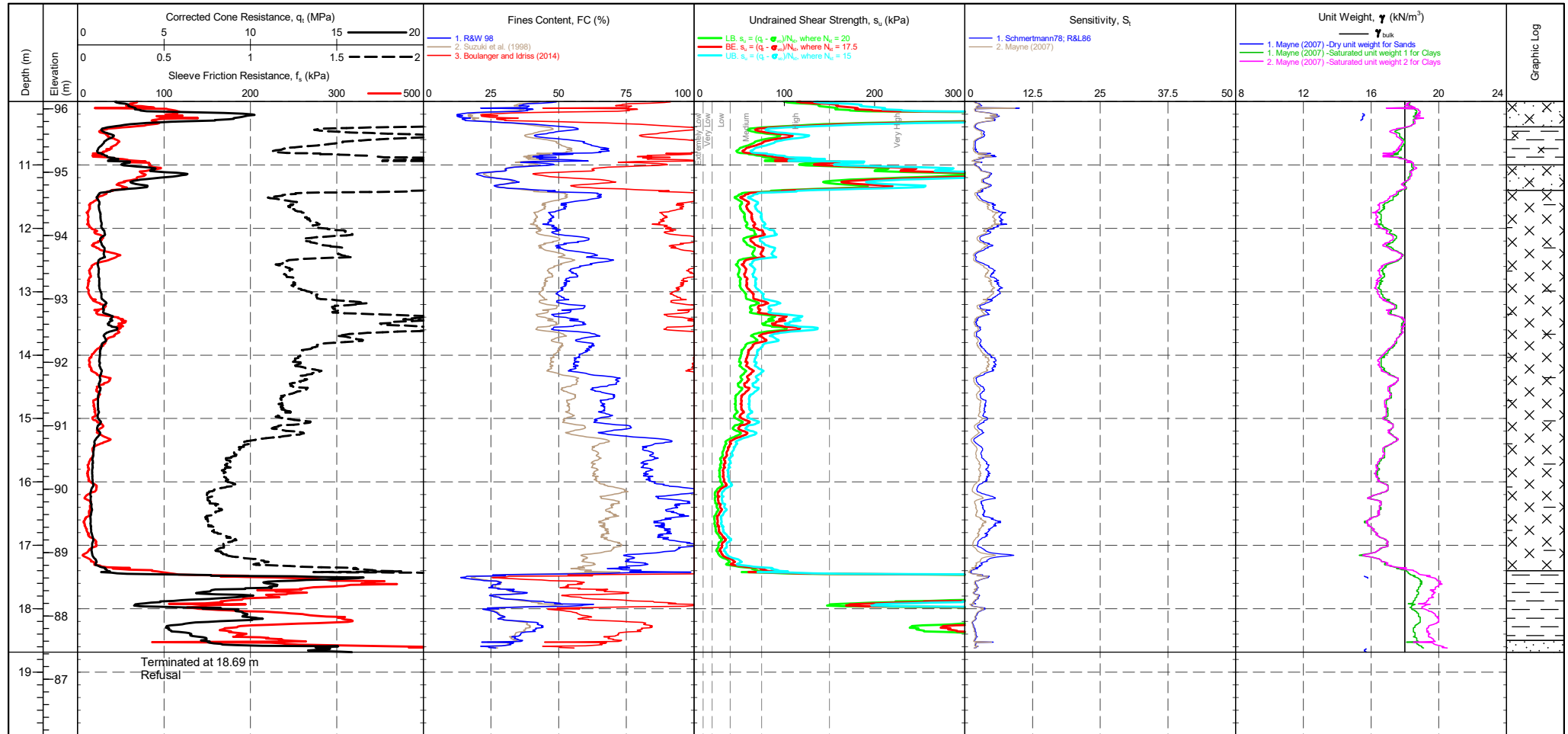


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 362 mV Sleeve: 285 mV Pore Pressure 2: 203 mV X-Y Inclinator: 2671 mV	<b>CPTU ZERO VALUES</b> Pre: 391 mV Post: 284 mV Difference: -0.001 kPa 0.321 MPa 284 mV 254 mV 2620 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> <table border="1"> <tr> <th>Term based on measurement</th> <th>su (kPa)</th> <th>Term based on measurement</th> <th>su (kPa)</th> </tr> <tr> <td>Extremely low strength</td> <td>&lt;10</td> <td>Medium strength</td> <td>40-75</td> </tr> <tr> <td>Very low strength</td> <td>10-20</td> <td>High strength</td> <td>75-150</td> </tr> <tr> <td>Low strength</td> <td>20-40</td> <td>Very high strength</td> <td>150-300</td> </tr> <tr> <td></td> <td></td> <td>Extremely high strength</td> <td>&gt;300</td> </tr> </table>	Term based on measurement	su (kPa)	Term based on measurement	su (kPa)	Extremely low strength	<10	Medium strength	40-75	Very low strength	10-20	High strength	75-150	Low strength	20-40	Very high strength	150-300			Extremely high strength	>300	<b>Groundwater Level</b>  <b>Dissipation Test</b> 
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PointID

**CPT02**

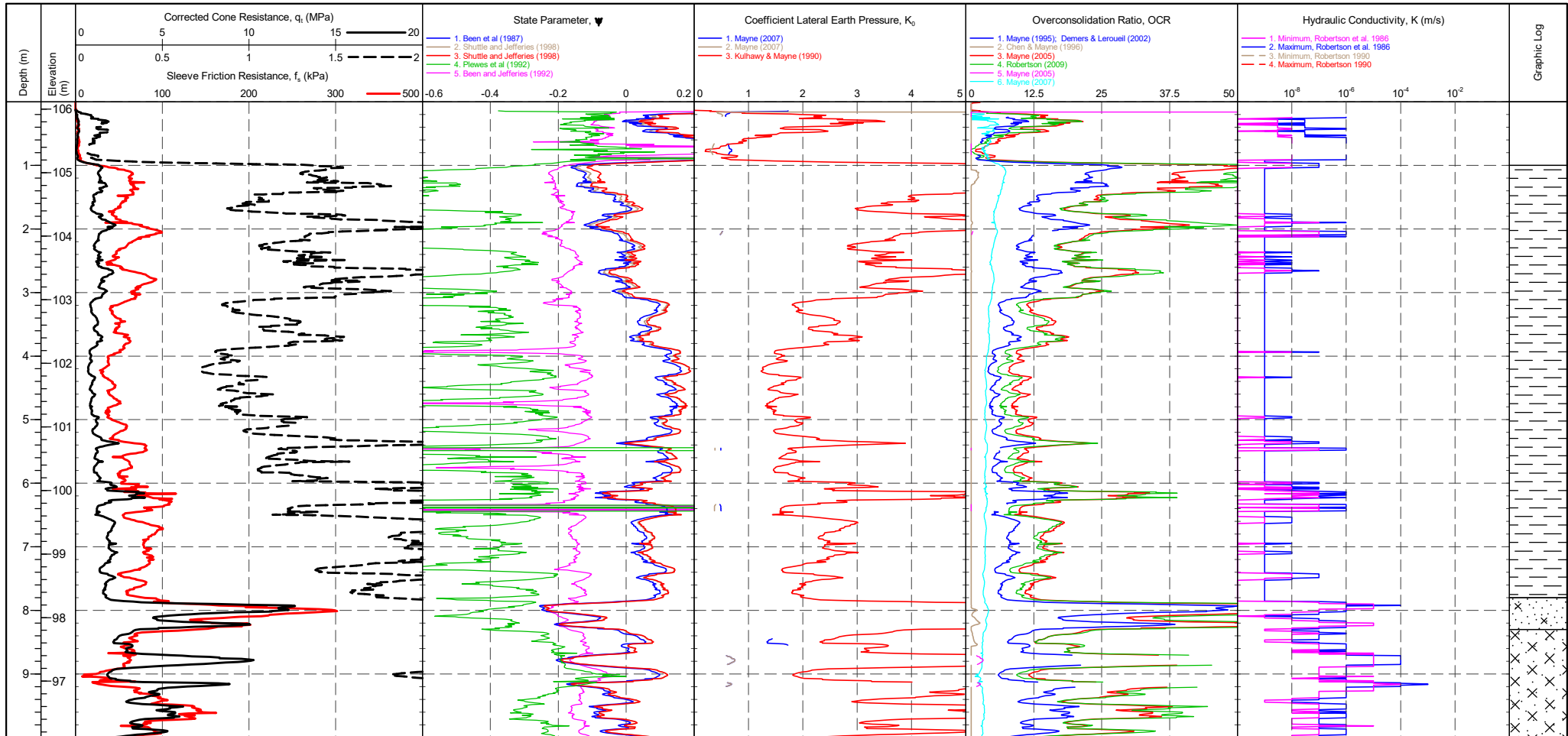
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490949.518 m <b>NORTHING</b> : 290883.378 m <b>ELEVATION</b> : 106.114 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 362 mV Sleeve: 285 mV Pore Pressure 2: 203 mV X-Y Inclinator: 2671 mV	<b>CPTU ZERO VALUES</b> Pre: 391 mV Post: 284 mV Difference: 0.321 MPa 254 mV 0.012 kPa 2620 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement su (kPa) Extremely low strength <10 Very low strength 10-20 Low strength 20-40	Term based on measurement su (kPa) Medium strength 40-75 High strength 75-150 Very high strength 150-300 Extremely high strength >300	▽ Groundwater Level ▮ Dissipation Test
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PointID  
**CPT02**

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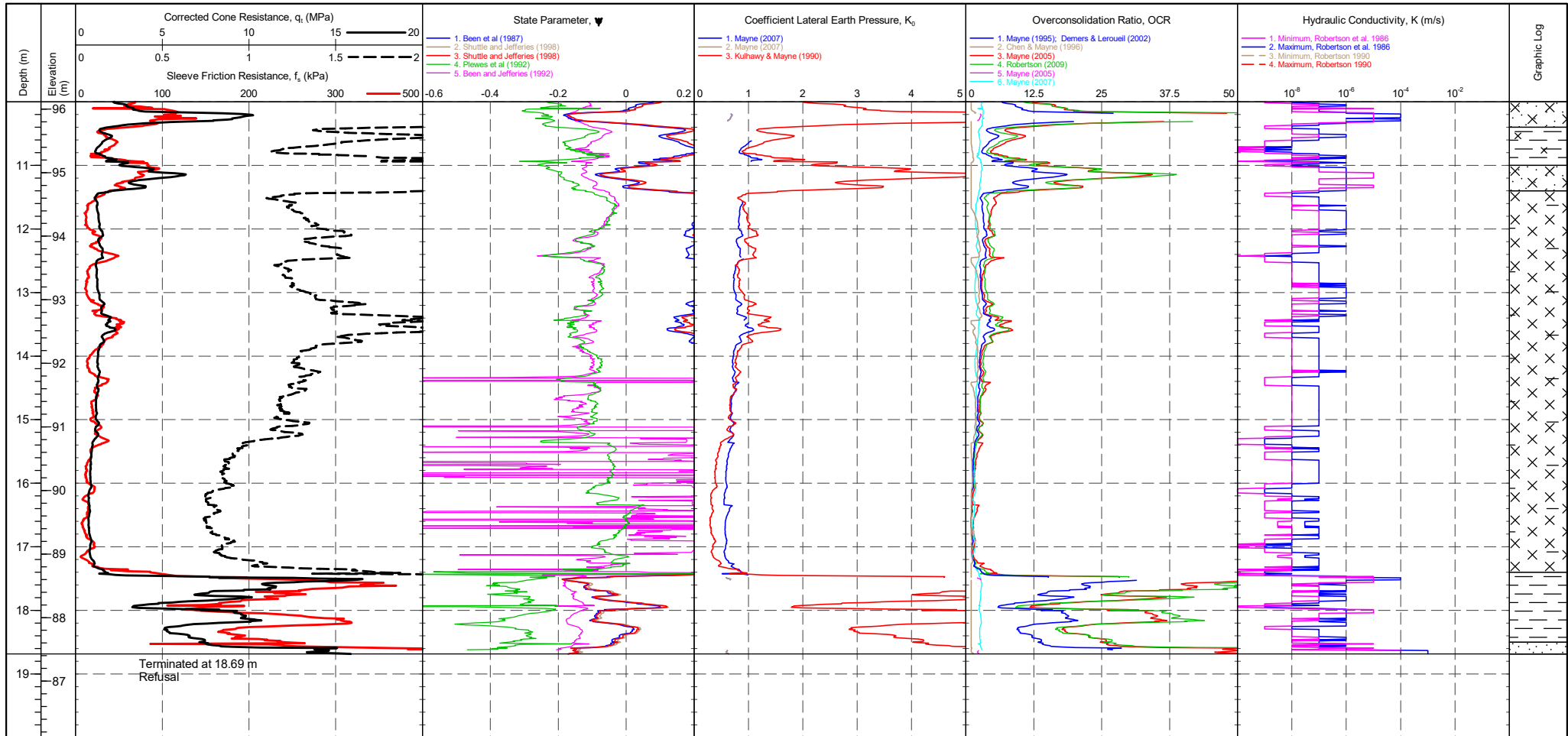


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>362 mV</td> <td>391 mV</td> <td>0.321 MPa</td> </tr> <tr> <td>Sleeve</td> <td>285 mV</td> <td>284 mV</td> <td>-0.001 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>203 mV</td> <td>254 mV</td> <td>0.012 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2671 mV</td> <td>2620 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	362 mV	391 mV	0.321 MPa	Sleeve	285 mV	284 mV	-0.001 kPa	Pore Pressure 2	203 mV	254 mV	0.012 kPa	X-Y Inclinator	2671 mV	2620 mV		Groundwater Level Dissipation Test
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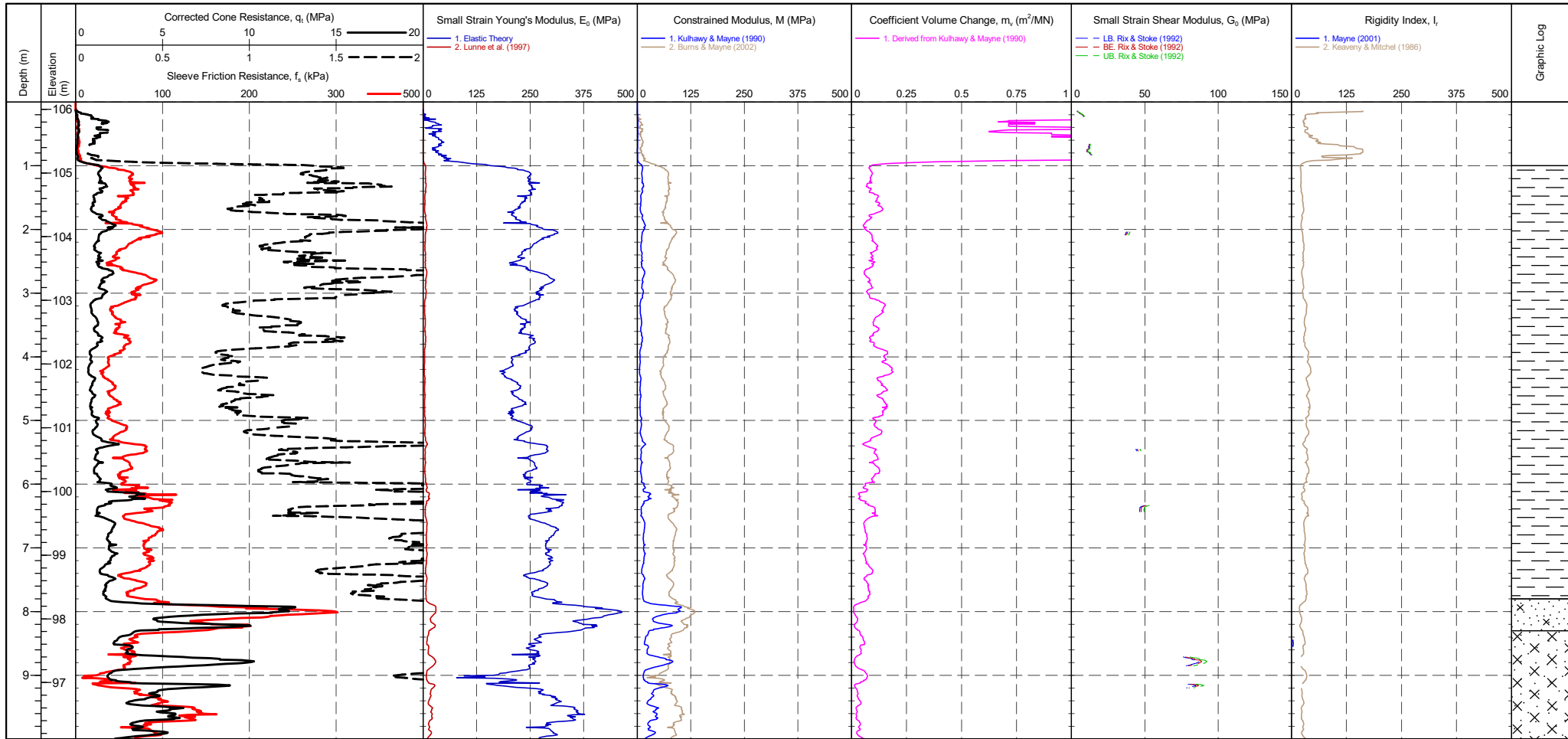


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**CPT02**

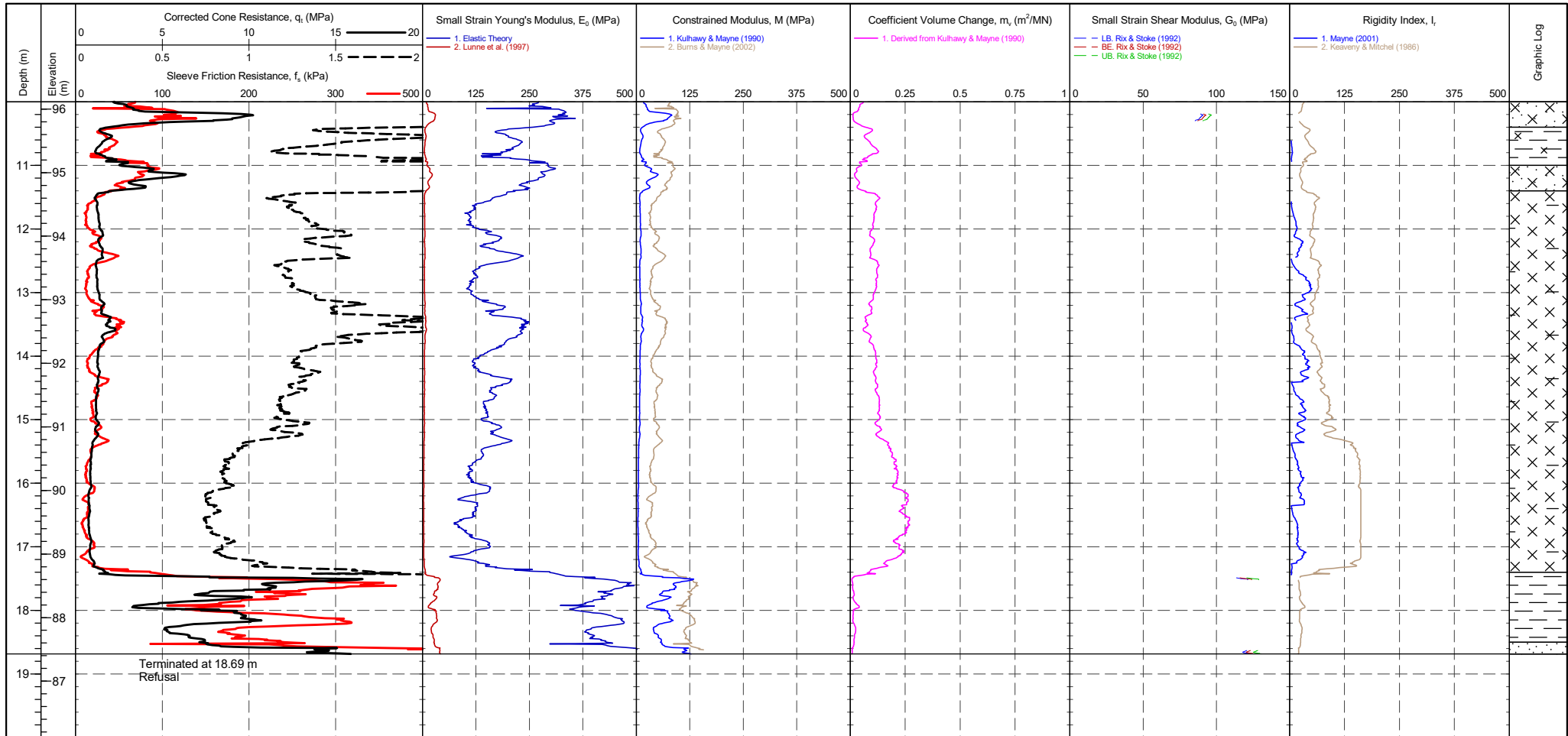
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490949.518 m <b>NORTHING</b> : 290883.378 m <b>ELEVATION</b> : 106.114 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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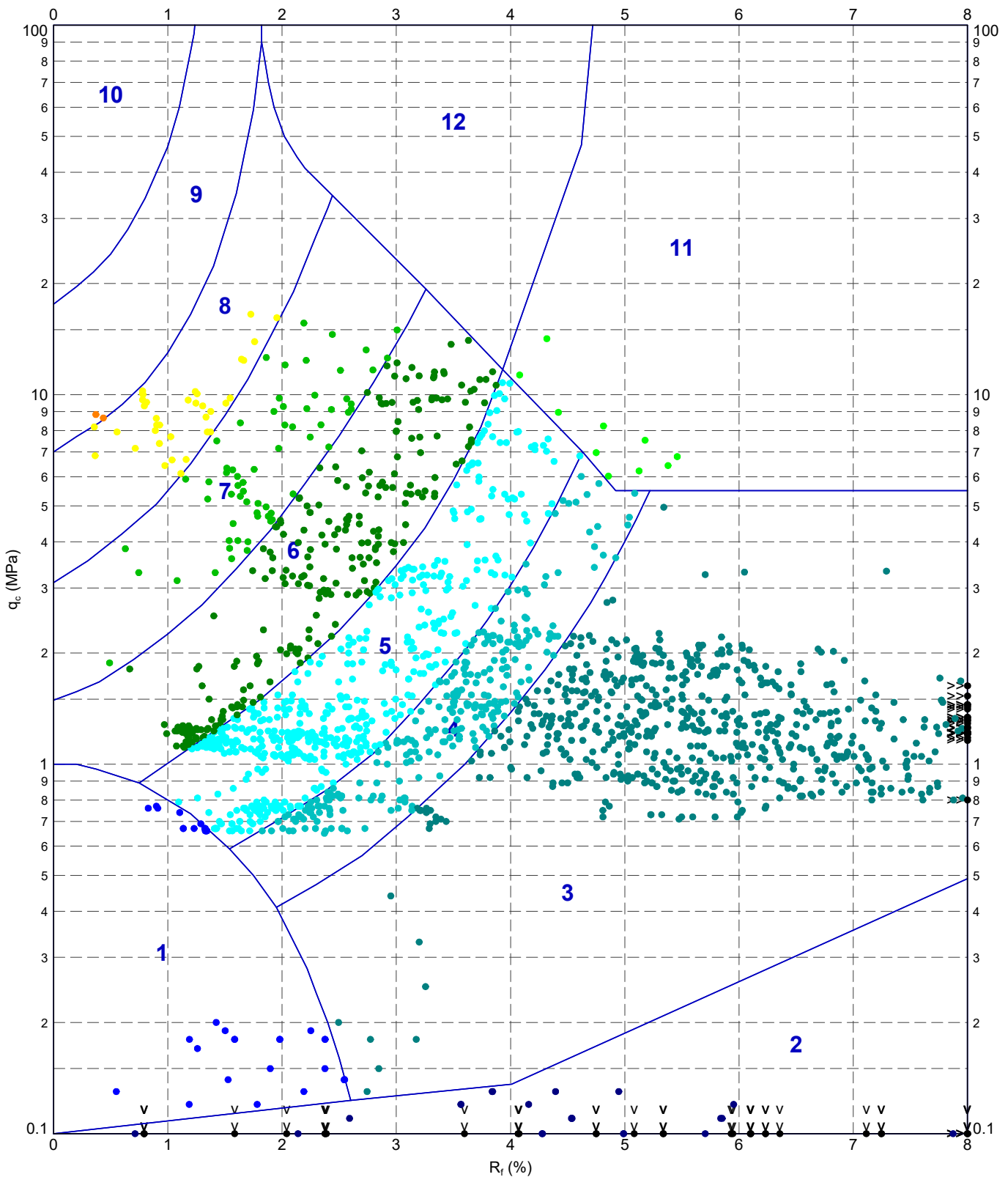
PointID	<b>CPT02</b>
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490949.518 m <b>NORTHING</b> : 290883.378 m <b>ELEVATION</b> : 106.114 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>362 mV</td> <td>391 mV</td> <td>0.321 MPa</td> </tr> <tr> <td>Sleeve</td> <td>285 mV</td> <td>284 mV</td> <td>-0.001 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>203 mV</td> <td>254 mV</td> <td>0.012 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2671 mV</td> <td>2620 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	362 mV	391 mV	0.321 MPa	Sleeve	285 mV	284 mV	-0.001 kPa	Pore Pressure 2	203 mV	254 mV	0.012 kPa	X-Y Inclinator	2671 mV	2620 mV		Groundwater Level Dissipation Test
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METHOD: Robertson et al. 1986 qc Rf

- |                                     |                               |                              |                              |
|-------------------------------------|-------------------------------|------------------------------|------------------------------|
| 1 - Sensitive fine grained material | 4 - Silty CLAY to CLAY        | 7 - Silty SAND to sandy SILT | 10 - Gravelly SAND to SAND   |
| 2 - Organic material                | 5 - Clayey SILT to silty CLAY | 8 - SAND to silty SAND       | 11 - Very stiff fine grained |
| 3 - CLAY                            | 6 - Sandy SILT to clayey SILT | 9 - SAND                     | 12 - SAND to clayey SAND     |

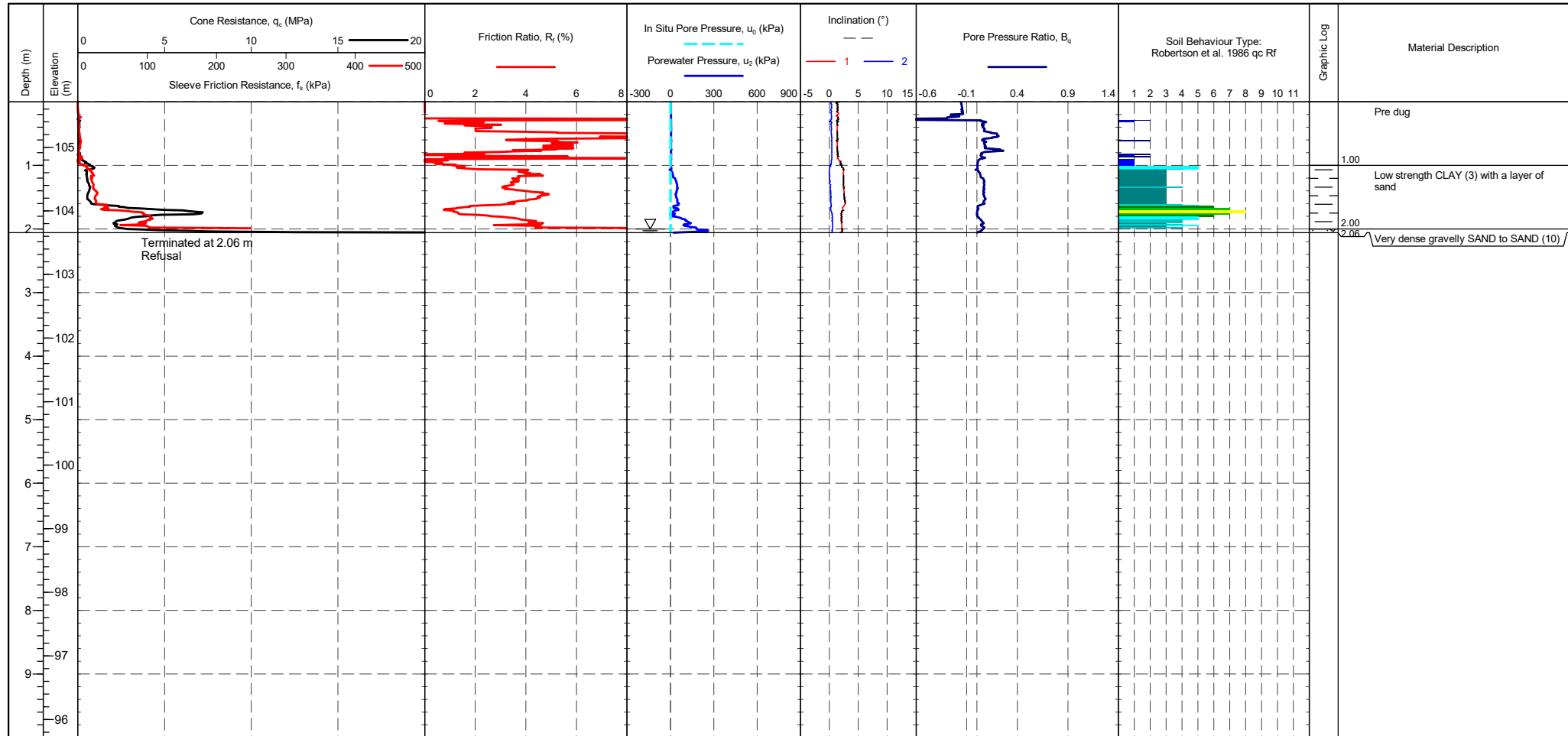


TITLE  
 Delta Simons  
 Cordby  
 Corby  
 Robertson et al. 1986 qc vs. Rf - CPT02

DRAWN	DATE	04/03/2022
CHECKED	DATE	04/03/2022
SCALE	Not To Scale	A4
PROJECT No	FIGURE No	1220144

PointID	<b>CPT03</b>
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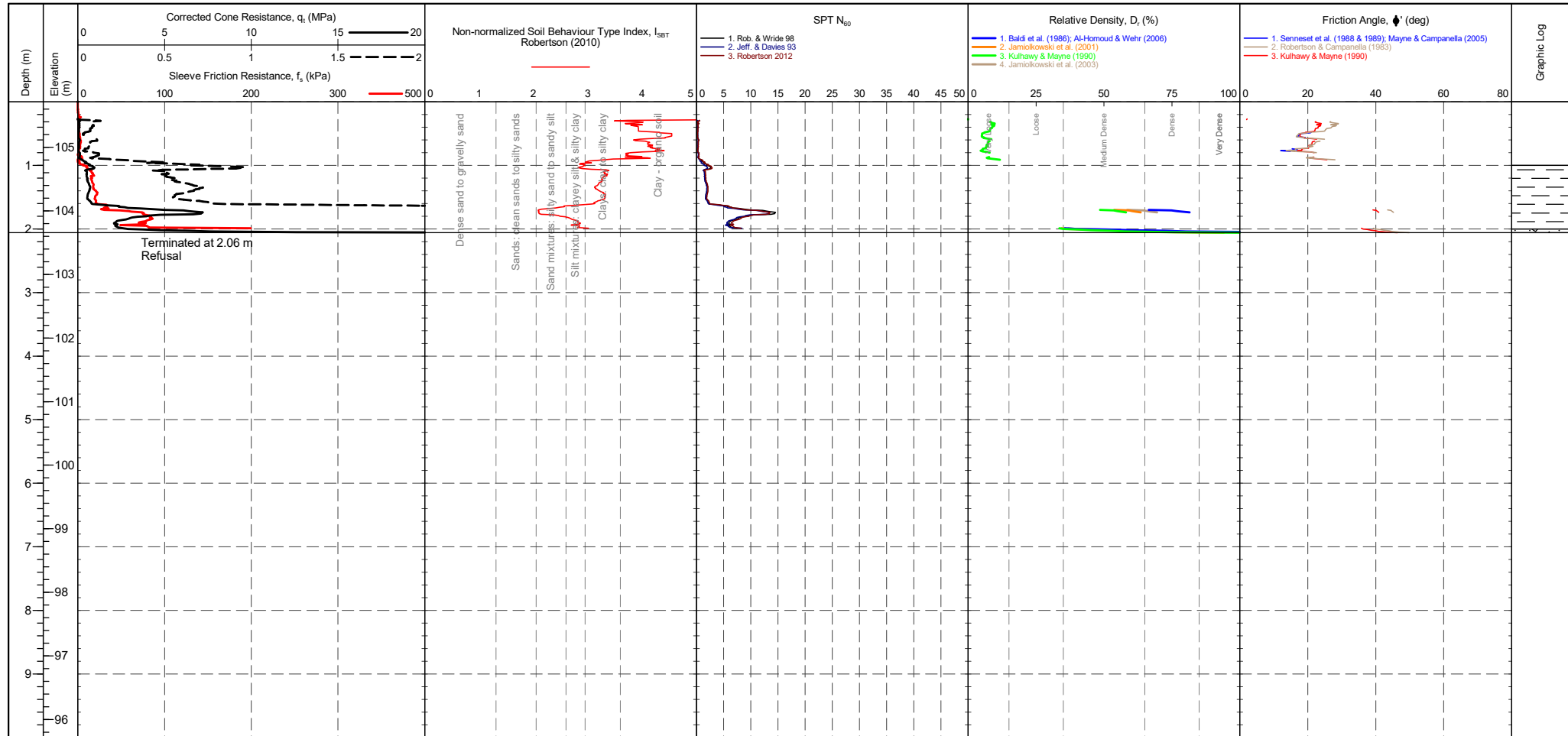
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491001.394 m <b>NORTHING</b> : 290915.219 m <b>ELEVATION</b> : 105.716 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip: Pre 360 mV, Post 361 mV, Difference 0.011 MPa Sleeve: Pre 288 mV, Post 288 mV, Difference 0 kPa Pore Pressure 2: Pre 200 mV, Post 200 mV, Difference 0 kPa X-Y Inclinator: Pre 2686 mV, Post 2655 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravelly SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID	<b>CPT03</b>
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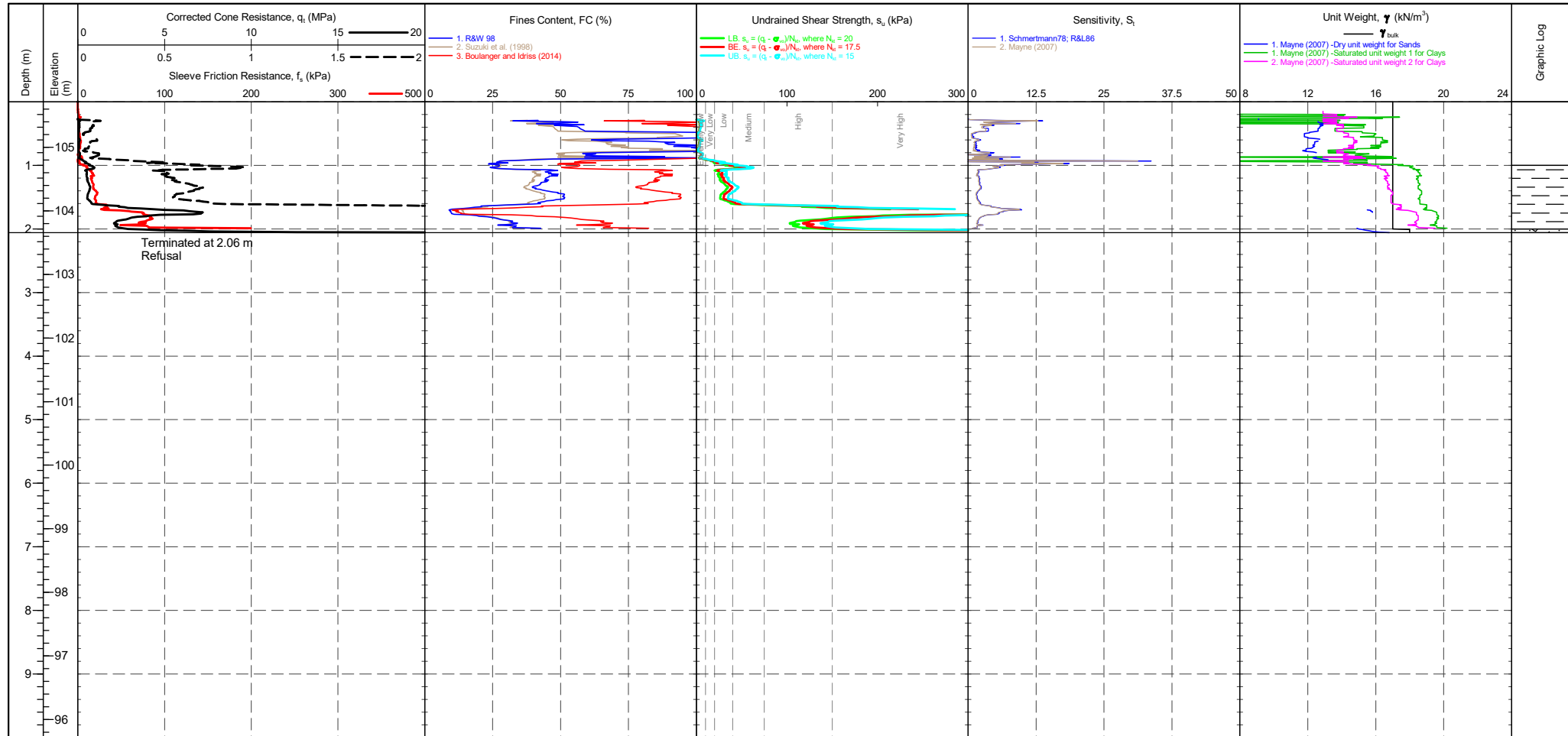
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491001.394 m <b>NORTHING</b> : 290915.219 m <b>ELEVATION</b> : 105.716 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>360 mV</td> <td>361 mV</td> <td>0.011 MPa</td> </tr> <tr> <td>Sleeve</td> <td>288 mV</td> <td>288 mV</td> <td>0 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>200 mV</td> <td>200 mV</td> <td>0 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2686 mV</td> <td>2655 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	360 mV	361 mV	0.011 MPa	Sleeve	288 mV	288 mV	0 kPa	Pore Pressure 2	200 mV	200 mV	0 kPa	X-Y Inclinator	2686 mV	2655 mV		<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, I<sub>c</sub></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density Dr (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, I <sub>c</sub>	Description	SPT N value, NSPT	Description	Relative Density Dr (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
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PointID	CPT03
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	EASTING : 491001.394 m NORTHING : 290915.219 m ELEVATION : 105.716 m OD CHECKED BY : LD TERMINATION REASON : Refusal	Remark: Test refused on tip resistance.	SHEET : 1 OF 1 STATUS : Final TEST DATE : 10/02/2022 PLOT DATE : 04/03/2022 METHOD : ISO 22476-1:2012
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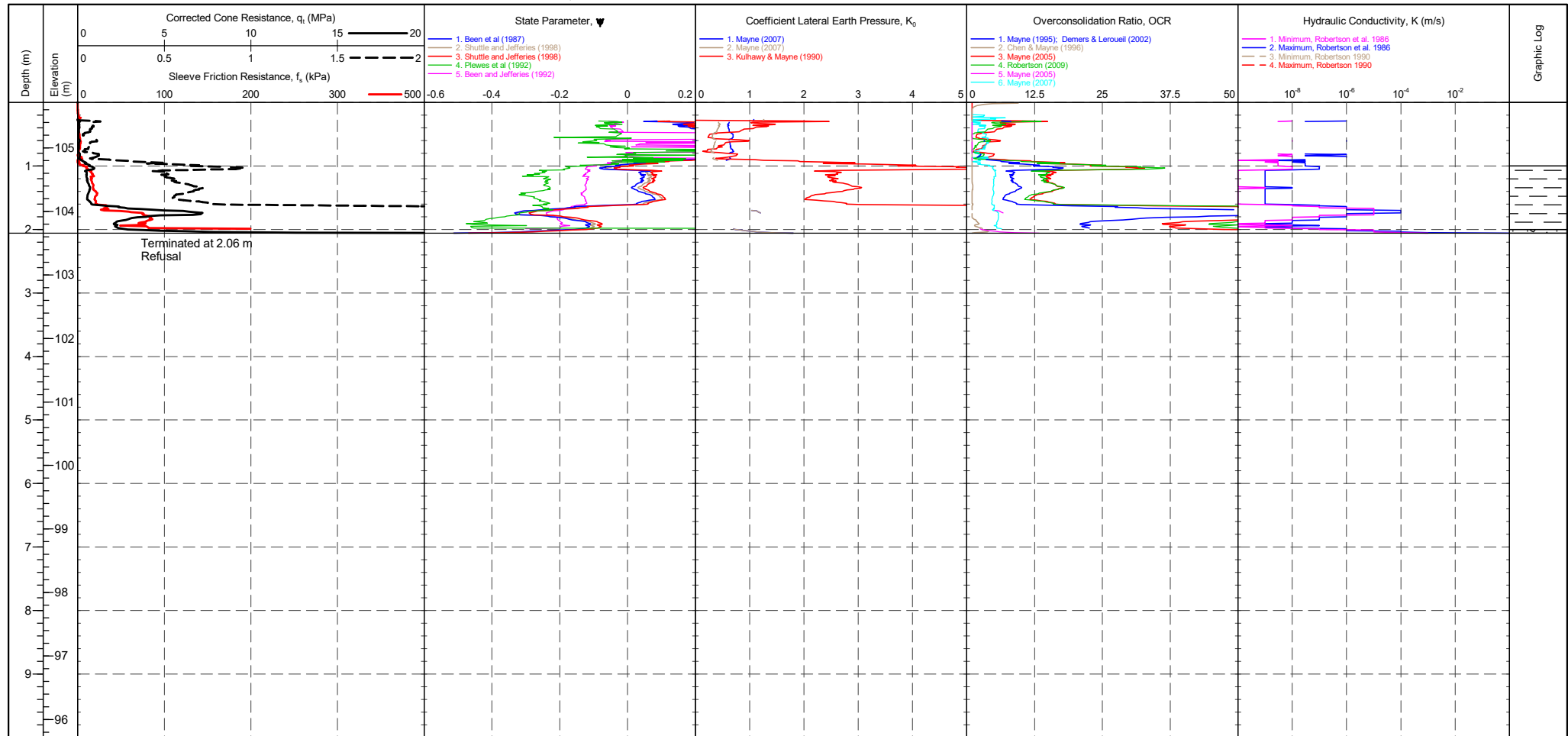


CONE ID : S15-CFIP.1867 CONE MODEL : Subtraction CONE AREA : 15cm <sup>2</sup> CONE AREA RATIO : 0.79 FILTER POSITION : u2 FILTER TYPE : HDPE	TEST TYPE : TE2 APPLICATION CLASS : 2 RIG : CPT 016 - Broomhall OPERATOR : TR FRICTION REDUCER : None WEATHER : Sunny & Hot	<b>CPTU ZERO VALUES</b> Transducer Pre Post Difference Tip 360 mV 361 mV 0.011 MPa Sleeve 288 mV 288 mV 0 kPa Pore Pressure 2 200 mV 200 mV 0 kPa X-Y Inclinator 2686 mV 2655 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> <table border="1"> <tr> <th>Term based on measurement</th> <th>su (kPa)</th> <th>Term based on measurement</th> <th>su (kPa)</th> </tr> <tr> <td>Extremely low strength</td> <td>&lt;10</td> <td>Medium strength</td> <td>40-75</td> </tr> <tr> <td>Very low strength</td> <td>10-20</td> <td>High strength</td> <td>75-150</td> </tr> <tr> <td>Low strength</td> <td>20-40</td> <td>Very high strength</td> <td>150-300</td> </tr> <tr> <td></td> <td></td> <td>Extremely high strength</td> <td>&gt;300</td> </tr> </table>	Term based on measurement	su (kPa)	Term based on measurement	su (kPa)	Extremely low strength	<10	Medium strength	40-75	Very low strength	10-20	High strength	75-150	Low strength	20-40	Very high strength	150-300			Extremely high strength	>300	Groundwater Level Dissipation Test
Term based on measurement	su (kPa)	Term based on measurement	su (kPa)																					
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PointID

CPT03

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491001.394 m <b>NORTHING</b> : 290915.219 m <b>ELEVATION</b> : 105.716 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>360 mV</td> <td>361 mV</td> <td>0.011 MPa</td> </tr> <tr> <td>Sleeve</td> <td>288 mV</td> <td>288 mV</td> <td>0 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>200 mV</td> <td>200 mV</td> <td>0 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2686 mV</td> <td>2655 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	360 mV	361 mV	0.011 MPa	Sleeve	288 mV	288 mV	0 kPa	Pore Pressure 2	200 mV	200 mV	0 kPa	X-Y Inclinator	2686 mV	2655 mV		Groundwater Level Dissipation Test
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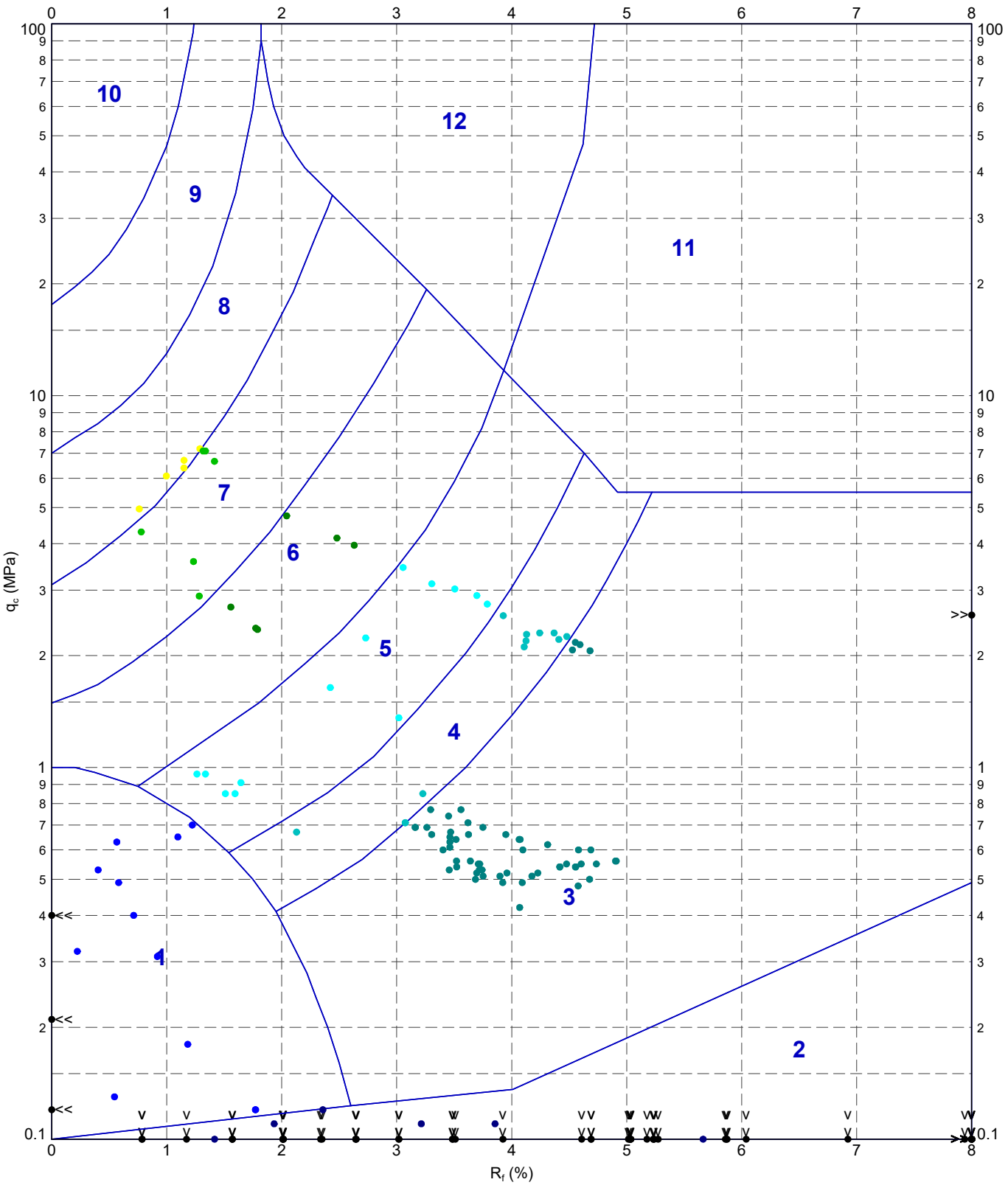
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**CPT03**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491001.394 m <b>NORTHING</b> : 290915.219 m <b>ELEVATION</b> : 105.716 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>360 mV</td> <td>361 mV</td> <td>0.011 MPa</td> </tr> <tr> <td>Sleeve</td> <td>288 mV</td> <td>288 mV</td> <td>0 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>200 mV</td> <td>200 mV</td> <td>0 kPa</td> </tr> <tr> <td>X-Y Inclinometer</td> <td>2686 mV</td> <td>2655 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	360 mV	361 mV	0.011 MPa	Sleeve	288 mV	288 mV	0 kPa	Pore Pressure 2	200 mV	200 mV	0 kPa	X-Y Inclinometer	2686 mV	2655 mV		Groundwater Level Dissipation Test
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220228-ADVANCED REPORT INSTITUTE 2.02.1 LIB - CHLOE.GLB Graph CPT ROBERTSON ET AL. 8F QC VS. RF APF 1220144 CORBY DELTA SIMONS GPJ - <<DrawingFile>> 04/03/2022 15:43 10.01.00.11 Datagel Lab and In Situ Tool - DGD [Lib: In Situ SI 2.02.0 2017-07-10 Proj: In Situ SI 2.02.0 2017-07-10]



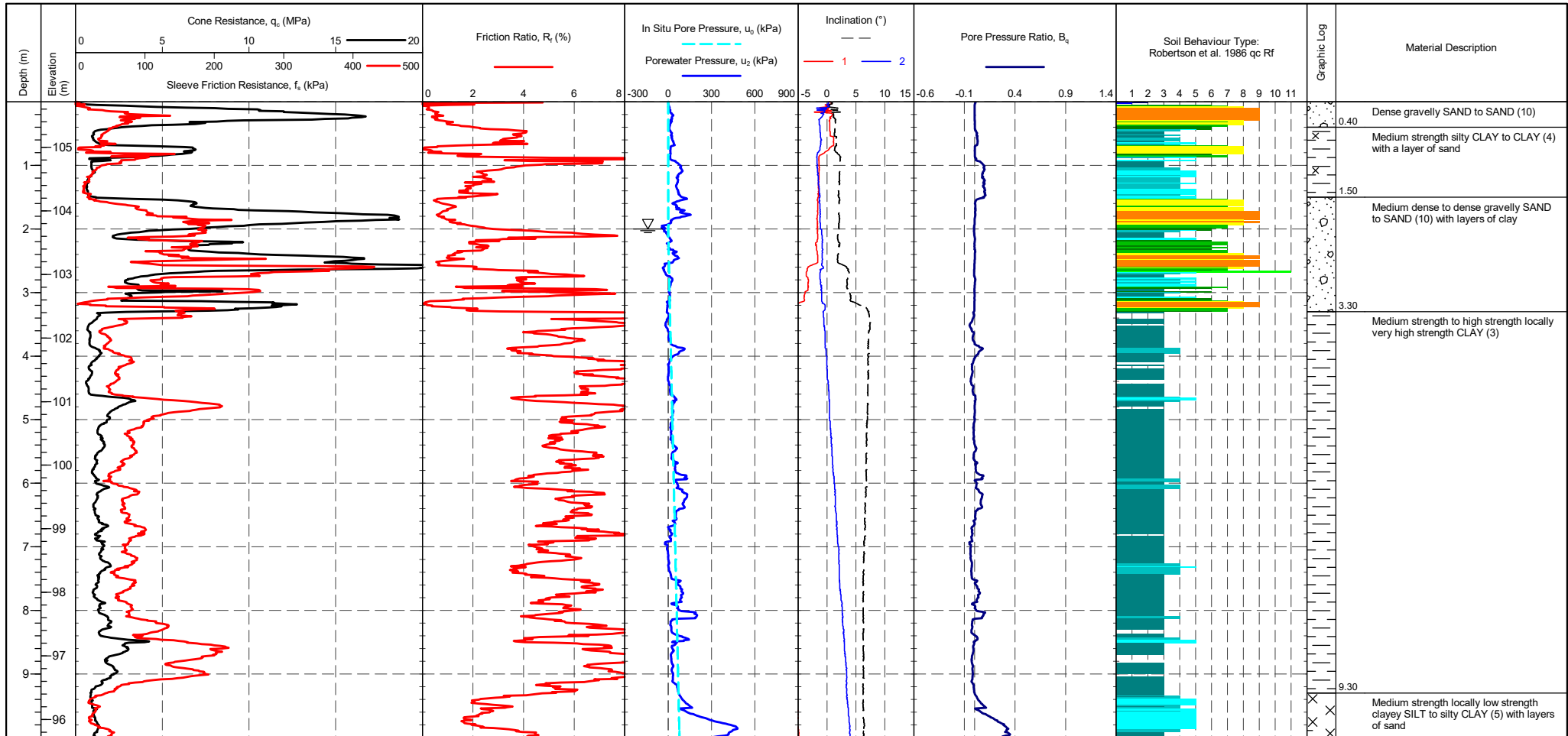
METHOD: Robertson et al. 1986 qc Rf

- 1 - Sensitive fine grained material
- 4 - Silty CLAY to CLAY
- 7 - Silty SAND to sandy SILT
- 10 - Gravelly SAND to SAND
- 2 - Organic material
- 5 - Clayey SILT to silty CLAY
- 8 - SAND to silty SAND
- 11 - Very stiff fine grained
- 3 - CLAY
- 6 - Sandy SILT to clayey SILT
- 9 - SAND
- 12 - SAND to clayey SAND

	TITLE	DRAWN	DATE
	Delta Simons Cordby Corby		04/03/2022
	Robertson et al. 1986 qc vs. Rf - CPT03	CHECKED	DATE
			04/03/2022
		SCALE	FIGURE No
		Not To Scale	A4
		PROJECT No	FIGURE No
		1220144	

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**CPT03A**

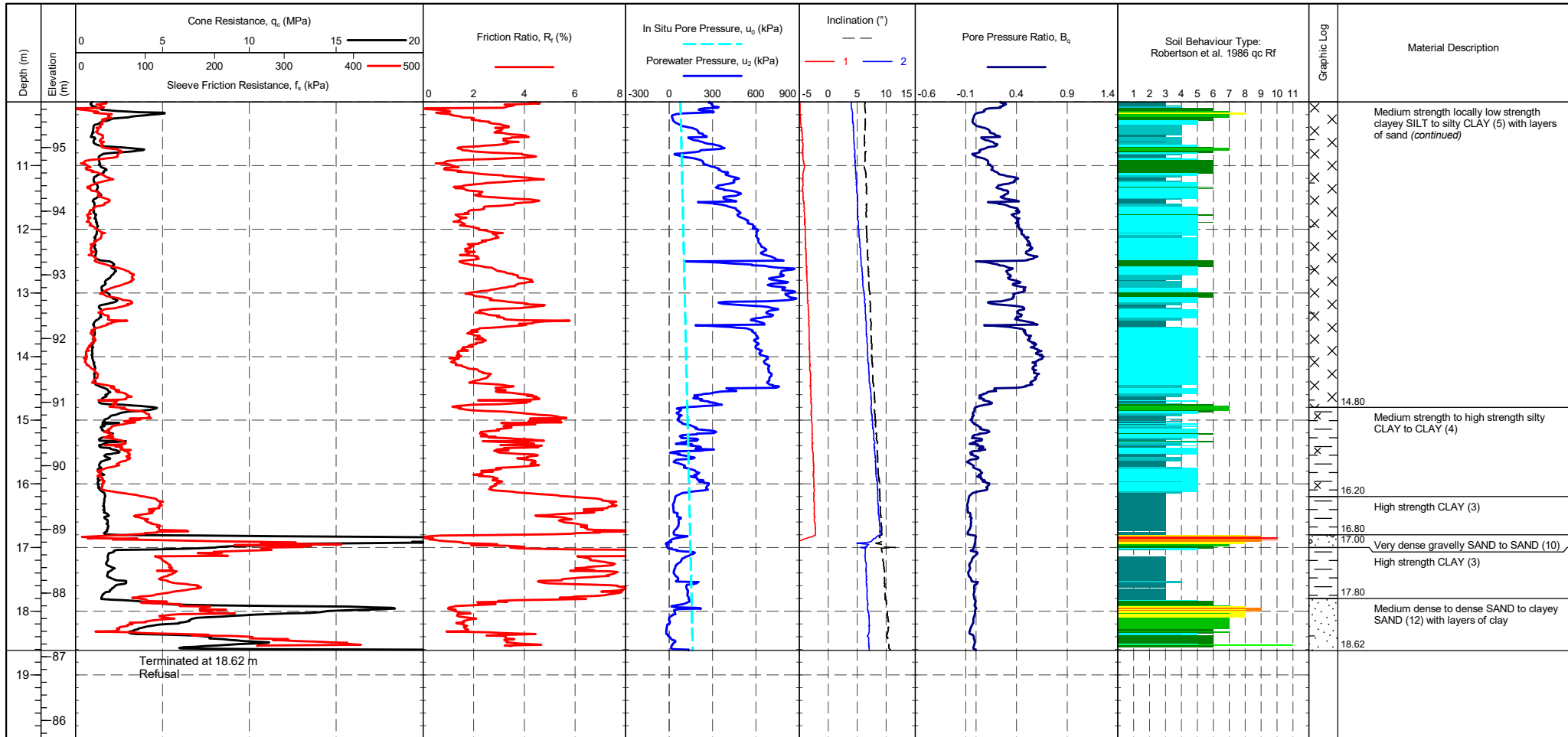
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491001.394 m <b>NORTHING</b> : 290915.219 m <b>ELEVATION</b> : 105.716 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>361 mV</td> <td>360 mV</td> <td>-0.011 MPa</td> </tr> <tr> <td>Sleeve</td> <td>289 mV</td> <td>286 mV</td> <td>-0.002 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>206 mV</td> <td>216 mV</td> <td>0.002 kPa</td> </tr> <tr> <td>X-Y Inclinometer</td> <td>2552 mV</td> <td>2612 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	361 mV	360 mV	-0.011 MPa	Sleeve	289 mV	286 mV	-0.002 kPa	Pore Pressure 2	206 mV	216 mV	0.002 kPa	X-Y Inclinometer	2552 mV	2612 mV		<b>METHOD</b> : Robertson et al. 1986 qc Rf <table border="1"> <tr> <td>1 - Sensitive fine grained material</td> <td>5 - Clayey SILT to silty CLAY</td> <td>9 - SAND</td> </tr> <tr> <td>2 - Organic material</td> <td>6 - Sandy SILT to clayey SILT</td> <td>10 - Gravelly SAND to SAND</td> </tr> <tr> <td>3 - CLAY</td> <td>7 - Silty SAND to sandy SILT</td> <td>11 - Very stiff fine grained</td> </tr> <tr> <td>4 - Silty CLAY to CLAY</td> <td>8 - SAND to silty SAND</td> <td>12 - SAND to clayey SAND</td> </tr> </table>	1 - Sensitive fine grained material	5 - Clayey SILT to silty CLAY	9 - SAND	2 - Organic material	6 - Sandy SILT to clayey SILT	10 - Gravelly SAND to SAND	3 - CLAY	7 - Silty SAND to sandy SILT	11 - Very stiff fine grained	4 - Silty CLAY to CLAY	8 - SAND to silty SAND	12 - SAND to clayey SAND	<b>Groundwater Level</b>  <b>Dissipation Test</b> 
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PointID	<b>CPT03A</b>
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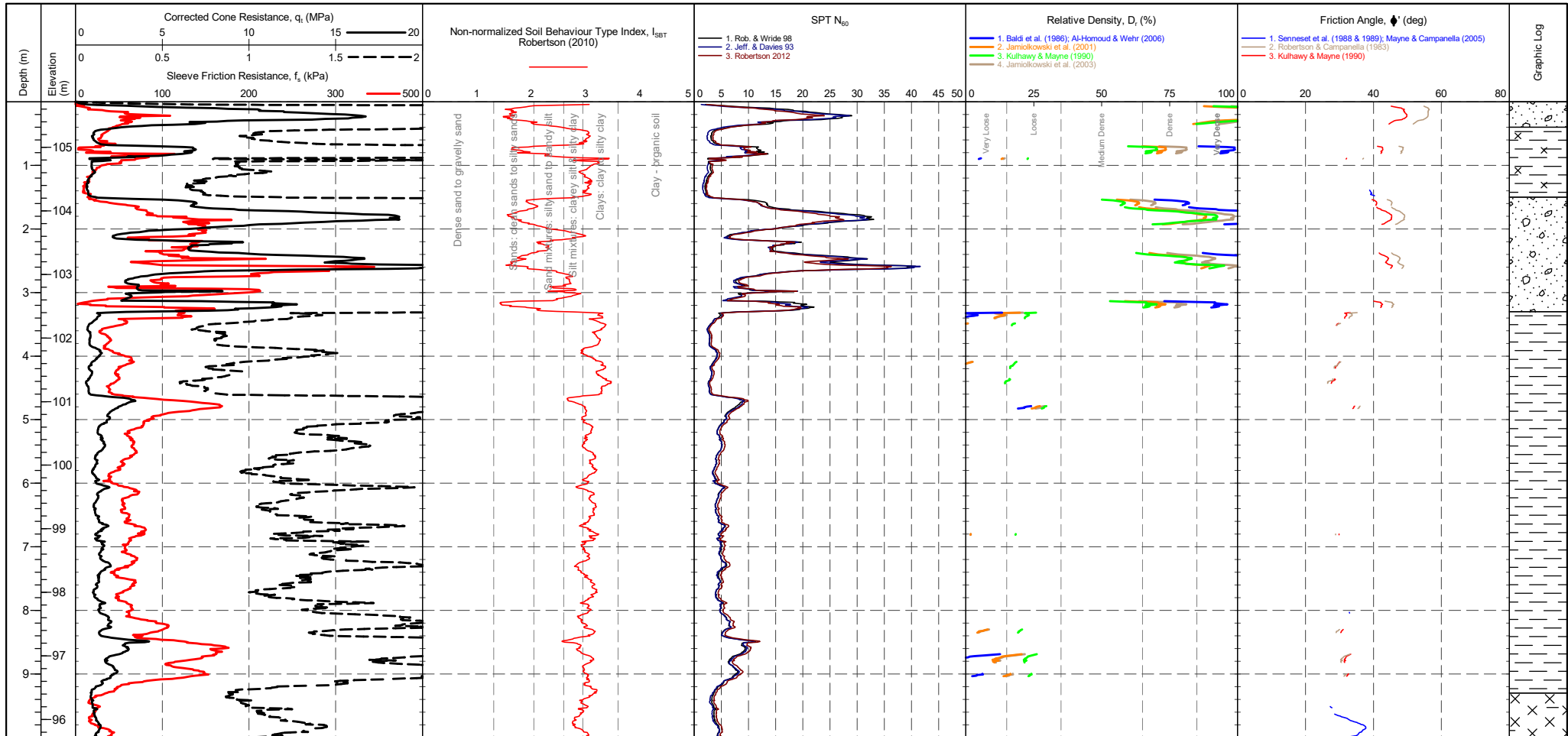
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	EASTING : 491001.394 m NORTHING : 290915.219 m ELEVATION : 105.716 m OD CHECKED BY : LD TERMINATION REASON : Refusal	Remark: Test refused on tip resistance.	SHEET : 2 OF 2 STATUS : Final TEST DATE : 10/02/2022 PLOT DATE : 04/03/2022 METHOD : ISO 22476-1:2012
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CONE ID : S15-CFIP.1867 CALIBRATION DATE : 05/03/2021 CONE MODEL : Subtraction CONE AREA : 15cm <sup>2</sup> CONE AREA RATIO : 0.79 FILTER POSITION : u2 FILTER TYPE : HDPE	TEST TYPE : TE2 APPLICATION CLASS : 2 RIG : CPT 016 - Broomhall OPERATOR : TR FRICTION REDUCER : None WEATHER : Sunny & Hot GROUNDWATER DEPTH : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip : 361 mV / 360 mV / -0.011 MPa Sleeve : 289 mV / 286 mV / -0.002 kPa Pore Pressure 2 : 206 mV / 216 mV / 0.002 kPa X-Y Inclinator : 2552 mV / 2612 mV	METHOD: Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravelly SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID	<b>CPT03A</b>
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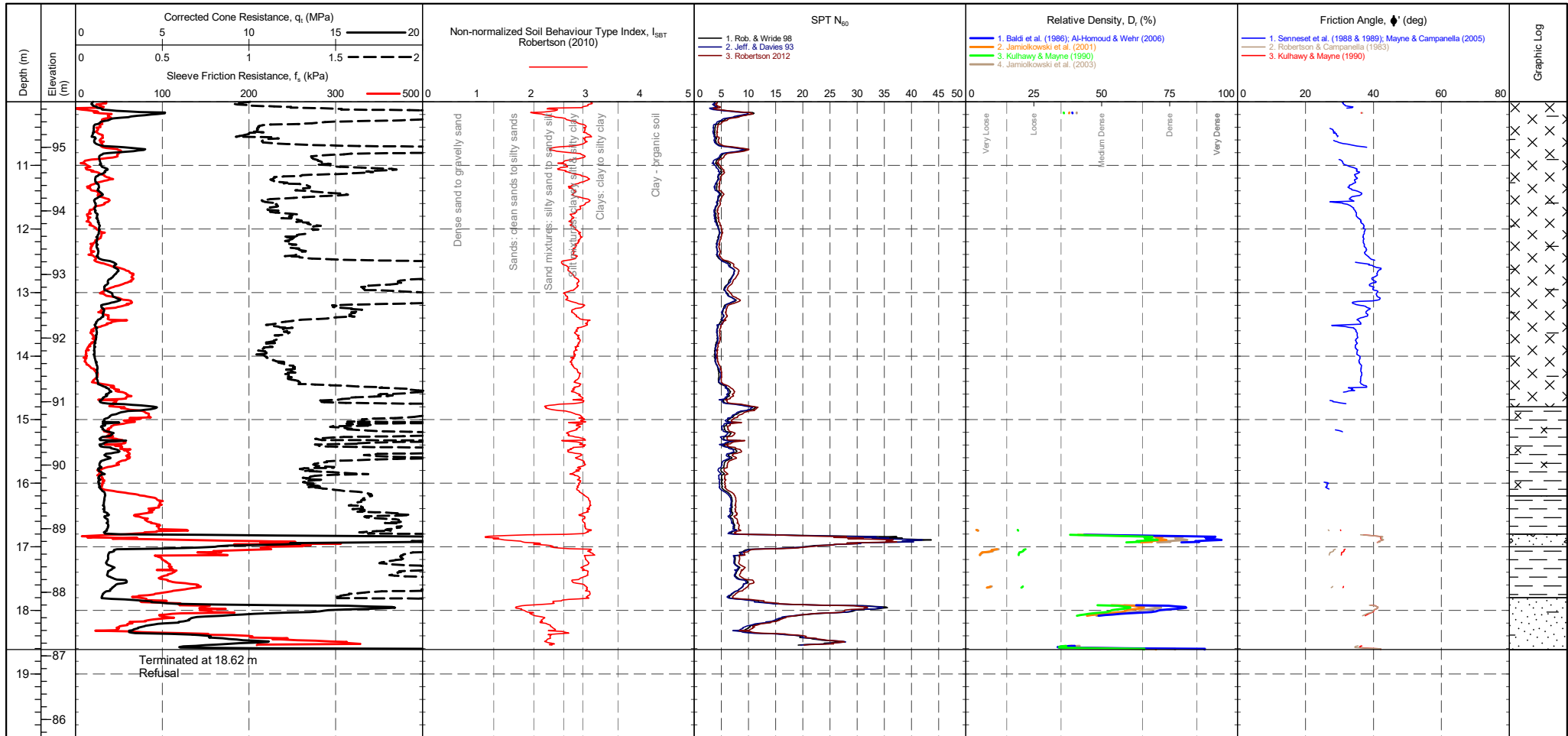
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> <b>Tip</b> : 361 mV <b>Sleeve</b> : 289 mV <b>Pore Pressure 2</b> : 206 mV <b>X-Y Inclinator</b> : 2552 mV	<b>CPTU ZERO VALUES</b> <b>Post</b> : 360 mV <b>Difference</b> : -0.011 MPa -0.002 kPa 0.002 kPa 2612 mV	<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, I<sub>c</sub></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density D<sub>r</sub> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, I <sub>c</sub>	Description	SPT N value, NSPT	Description	Relative Density D <sub>r</sub> (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	▽ Groundwater Level  ▮ Dissipation Test
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**CPT03A**

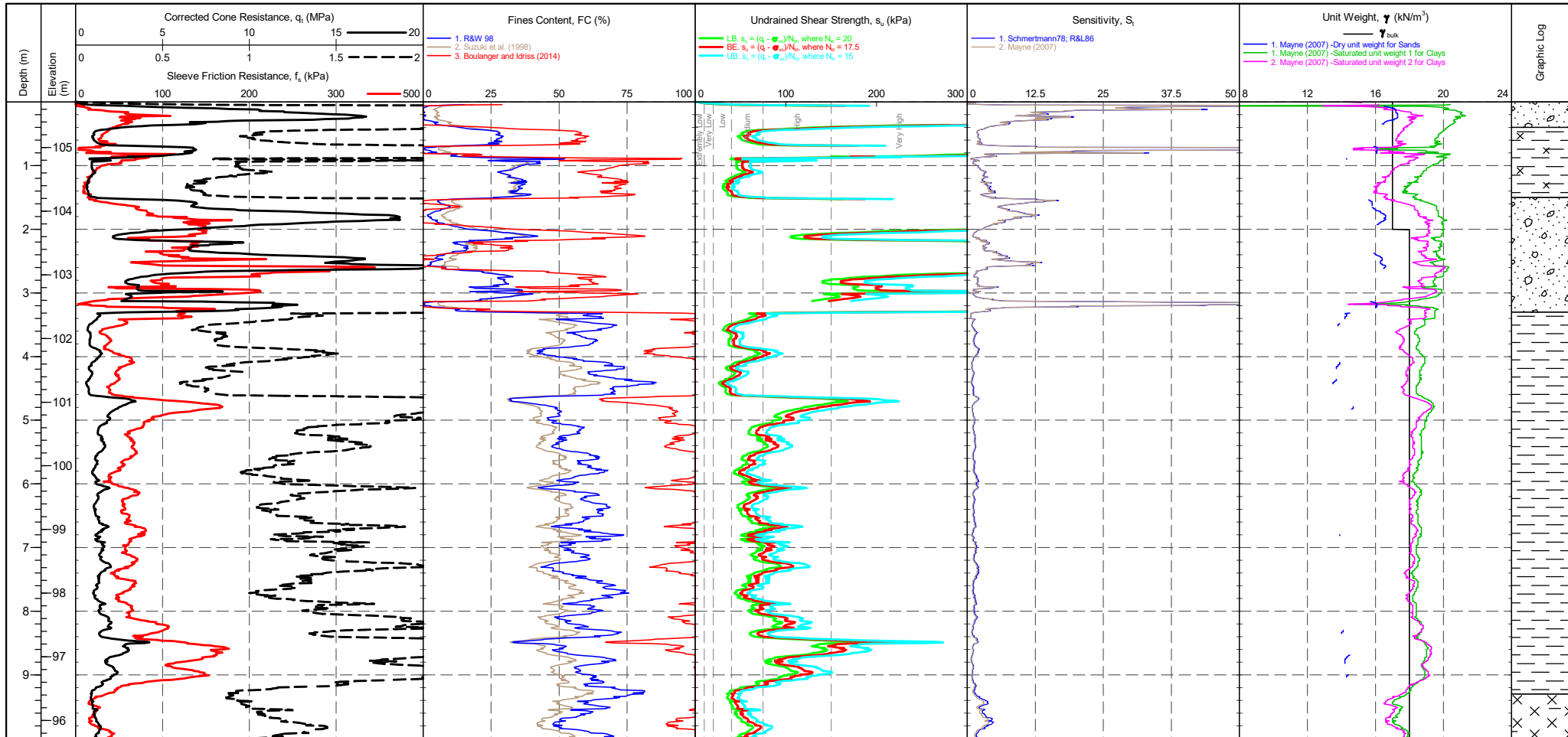
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491001.394 m <b>NORTHING</b> : 290915.219 m <b>ELEVATION</b> : 105.716 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> <b>Tip</b> : 361 mV <b>Sleeve</b> : 289 mV <b>Pore Pressure 2</b> : 206 mV <b>X-Y inclinometer</b> : 2552 mV	<b>CPTU ZERO VALUES</b> <b>Pre</b> : 360 mV <b>Post</b> : 286 mV <b>Difference</b> : -0.011 MPa <b>Difference</b> : -0.002 kPa <b>Difference</b> : 0.002 kPa <b>Difference</b> : 2612 mV	<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, <math>I_c</math></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density <math>D_r</math> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, $I_c$	Description	SPT N value, NSPT	Description	Relative Density $D_r$ (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
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PointID	CPT03A
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491001.394 m <b>NORTHING</b> : 290915.219 m <b>ELEVATION</b> : 105.716 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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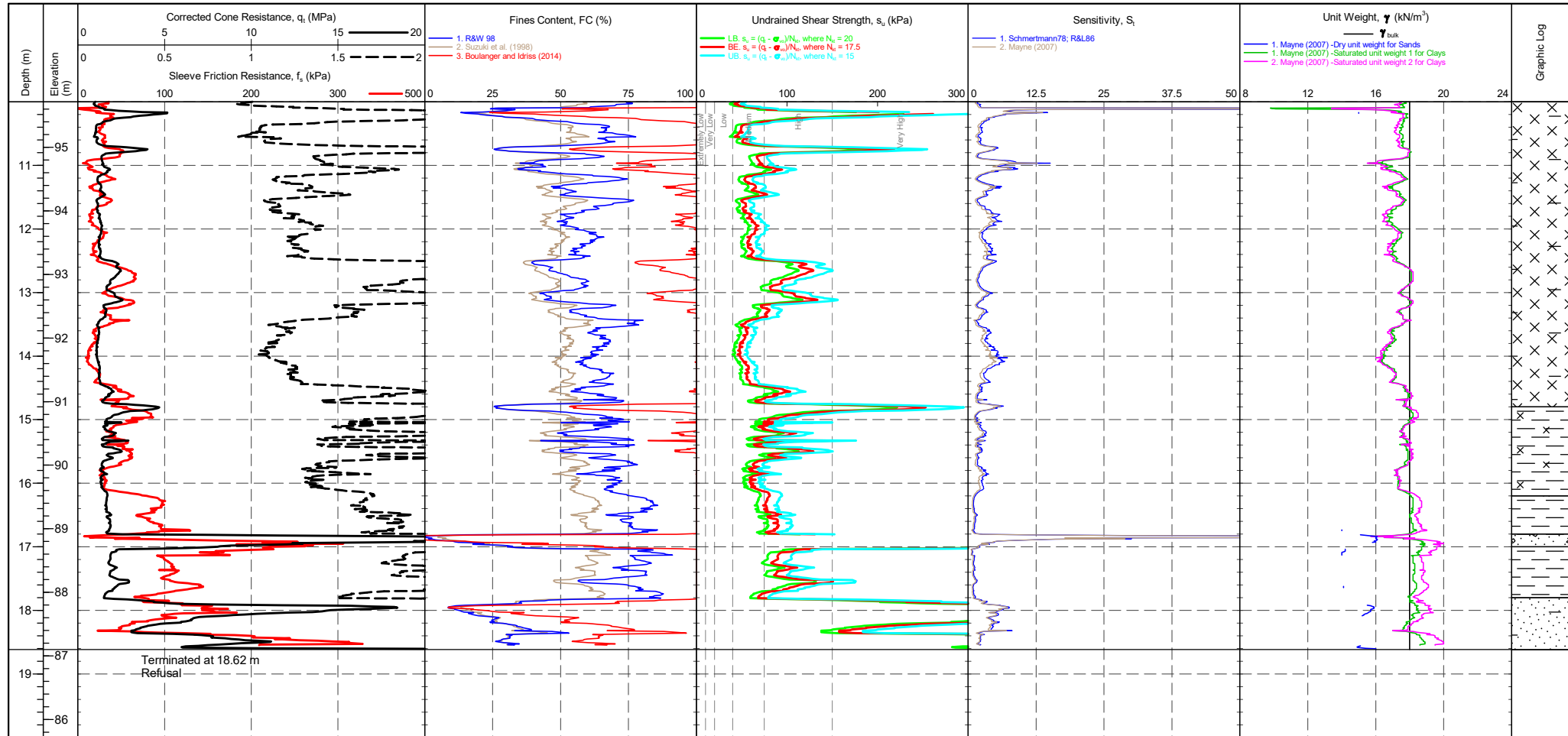


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 361 mV Sleeve: 289 mV Pore Pressure 2: 206 mV X-Y Inclinator: 2552 mV	<b>CPTU ZERO VALUES</b> Pre: 360 mV Post: 286 mV Difference: -0.011 MPa 216 mV 2612 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement su (kPa) Extremely low strength <10 Very low strength 10-20 Low strength 20-40	Term based on measurement su (kPa) Medium strength 40-75 High strength 75-150 Very high strength 150-300 Extremely high strength >300	Groundwater Level Dissipation Test
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PointID	<b>CPT03A</b>
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491001.394 m <b>NORTHING</b> : 290915.219 m <b>ELEVATION</b> : 105.716 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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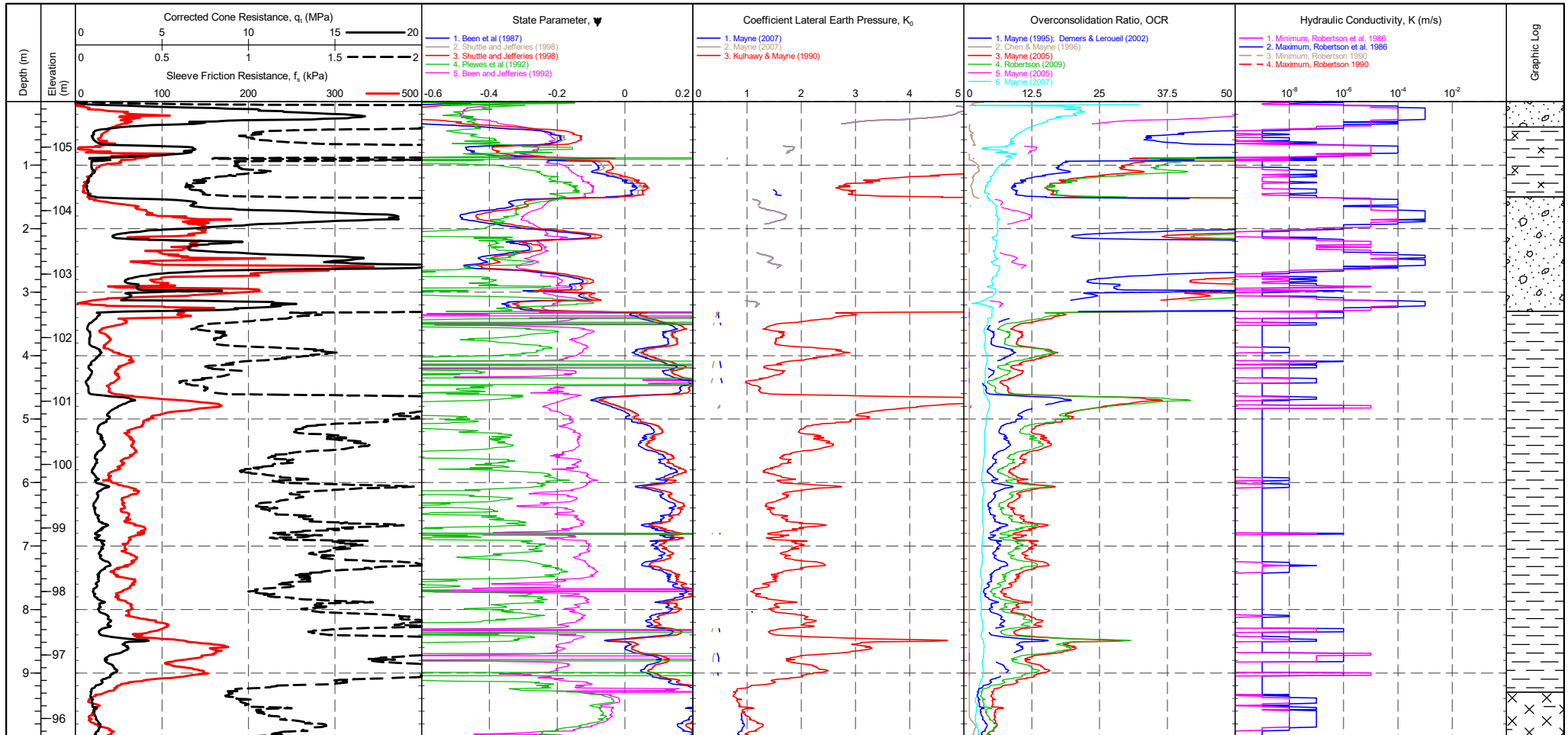


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip : 361 mV Sleeve : 289 mV Pore Pressure 2 : 206 mV X-Y Inclinator : 2552 mV	<b>CPTU ZERO VALUES</b> Pre : 360 mV Post : 286 mV Difference : -0.011 MPa 216 mV 2612 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement su (kPa) Extremely low strength <10 Very low strength 10-20 Low strength 20-40	Term based on measurement su (kPa) Medium strength 40-75 High strength 75-150 Very high strength 150-300 Extremely high strength >300	▽ Groundwater Level  ▮ Dissipation Test
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PointID

**CPT03A**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491001.394 m <b>NORTHING</b> : 290915.219 m <b>ELEVATION</b> : 105.716 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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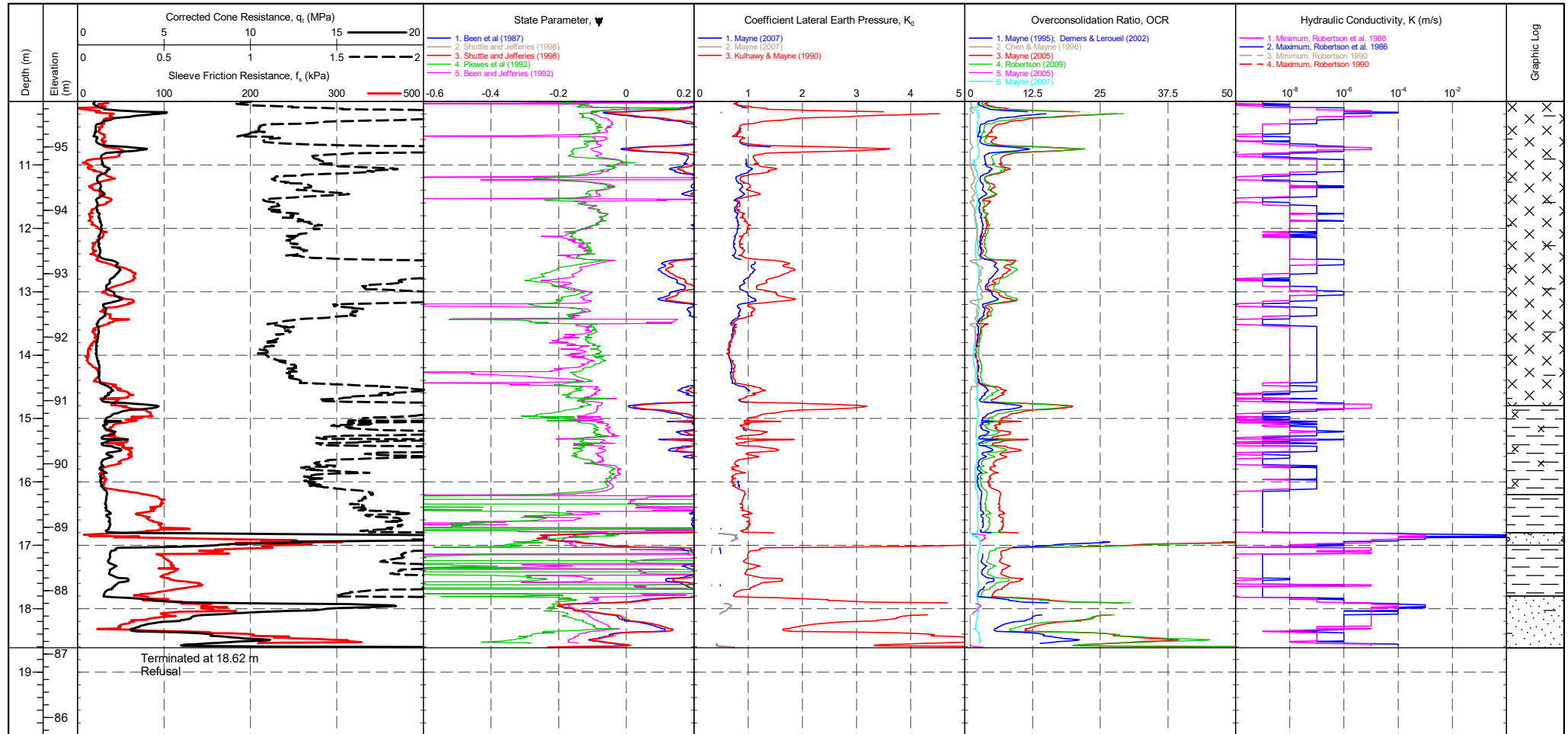


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>361 mV</td> <td>360 mV</td> <td>-0.011 MPa</td> </tr> <tr> <td>Sleeve</td> <td>289 mV</td> <td>286 mV</td> <td>-0.002 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>206 mV</td> <td>216 mV</td> <td>0.002 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2552 mV</td> <td>2612 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	361 mV	360 mV	-0.011 MPa	Sleeve	289 mV	286 mV	-0.002 kPa	Pore Pressure 2	206 mV	216 mV	0.002 kPa	X-Y Inclinator	2552 mV	2612 mV		Groundwater Level Dissipation Test
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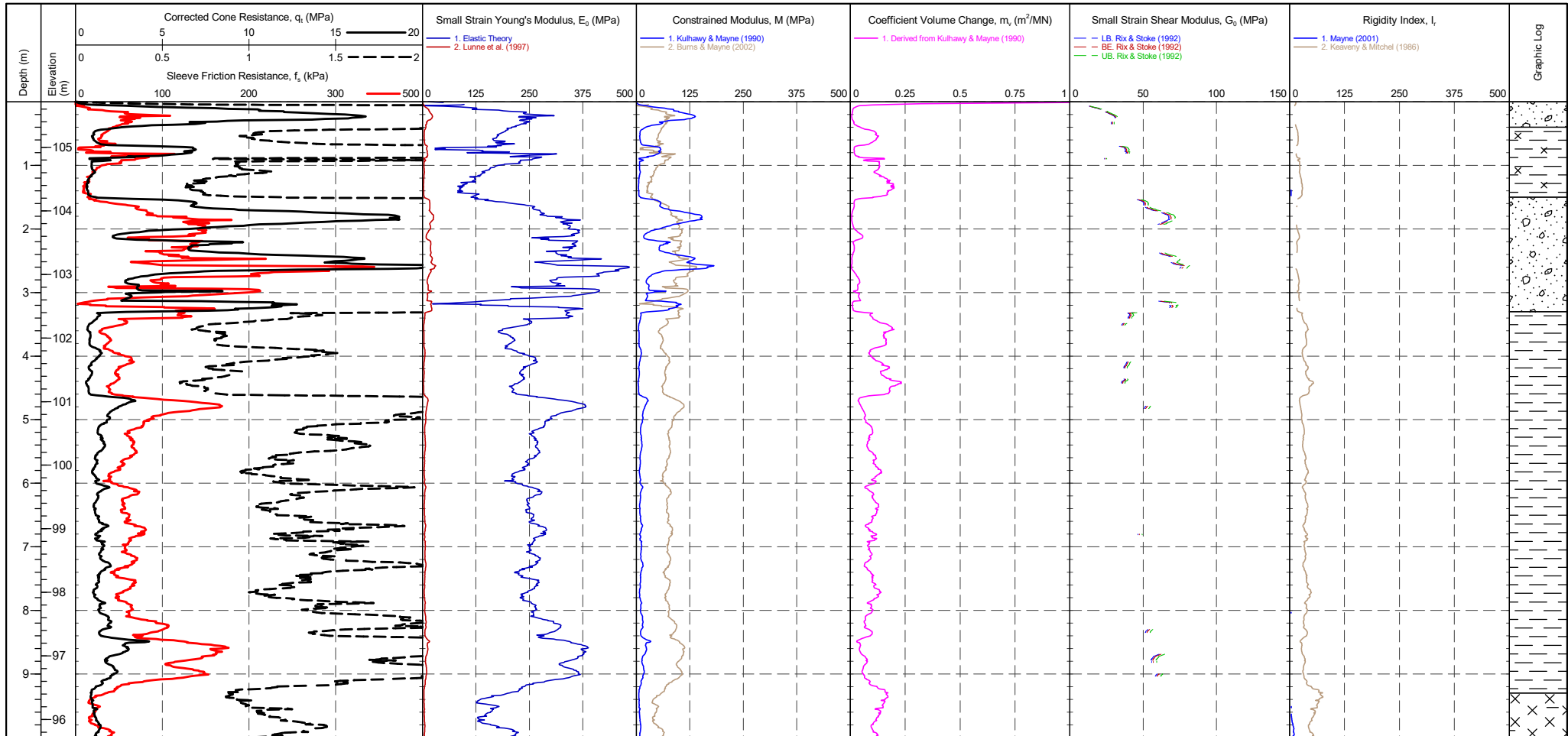
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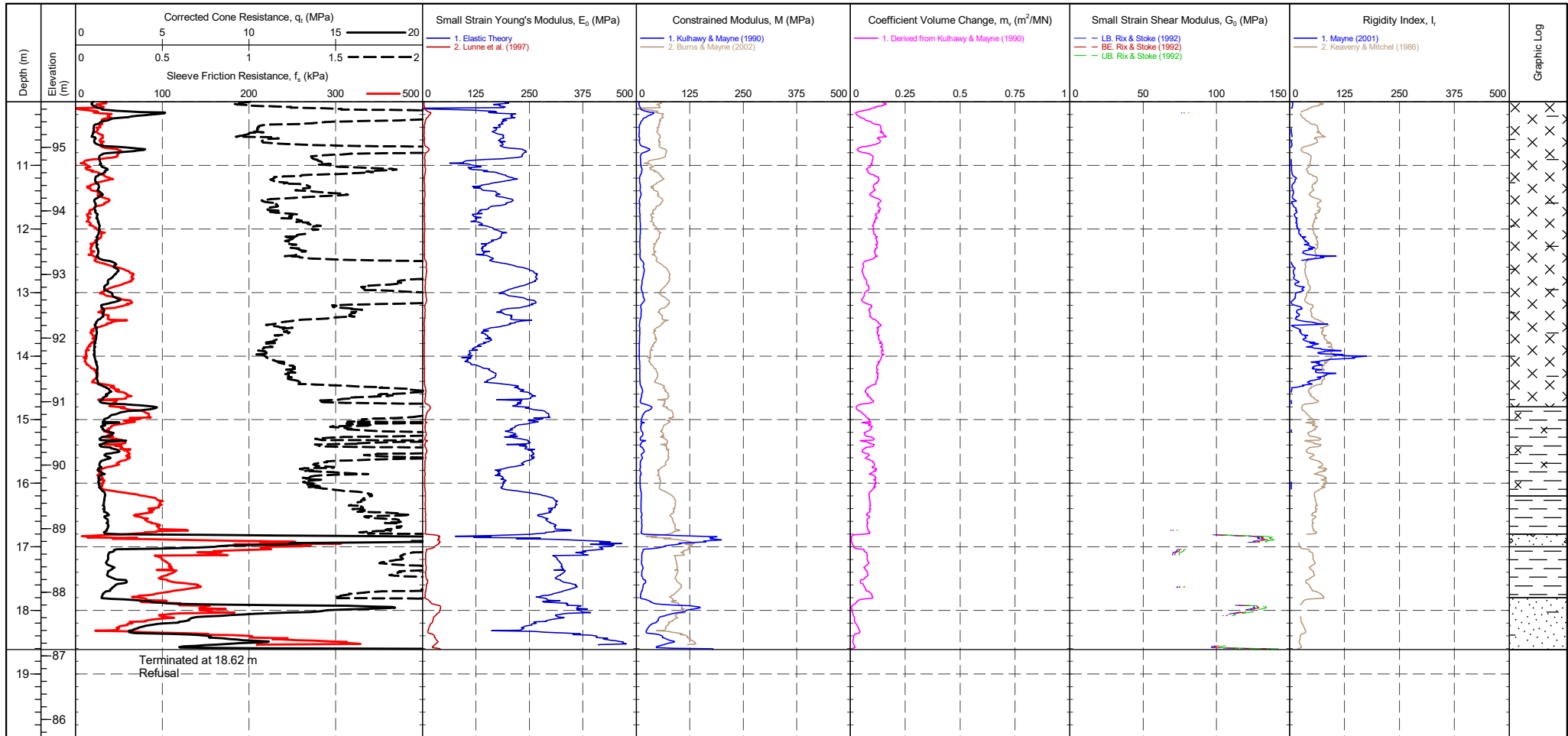
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>361 mV</td> <td>360 mV</td> <td>-0.011 MPa</td> </tr> <tr> <td>Sleeve</td> <td>289 mV</td> <td>286 mV</td> <td>-0.002 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>206 mV</td> <td>216 mV</td> <td>0.002 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2552 mV</td> <td>2612 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	361 mV	360 mV	-0.011 MPa	Sleeve	289 mV	286 mV	-0.002 kPa	Pore Pressure 2	206 mV	216 mV	0.002 kPa	X-Y Inclinator	2552 mV	2612 mV		Groundwater Level Dissipation Test
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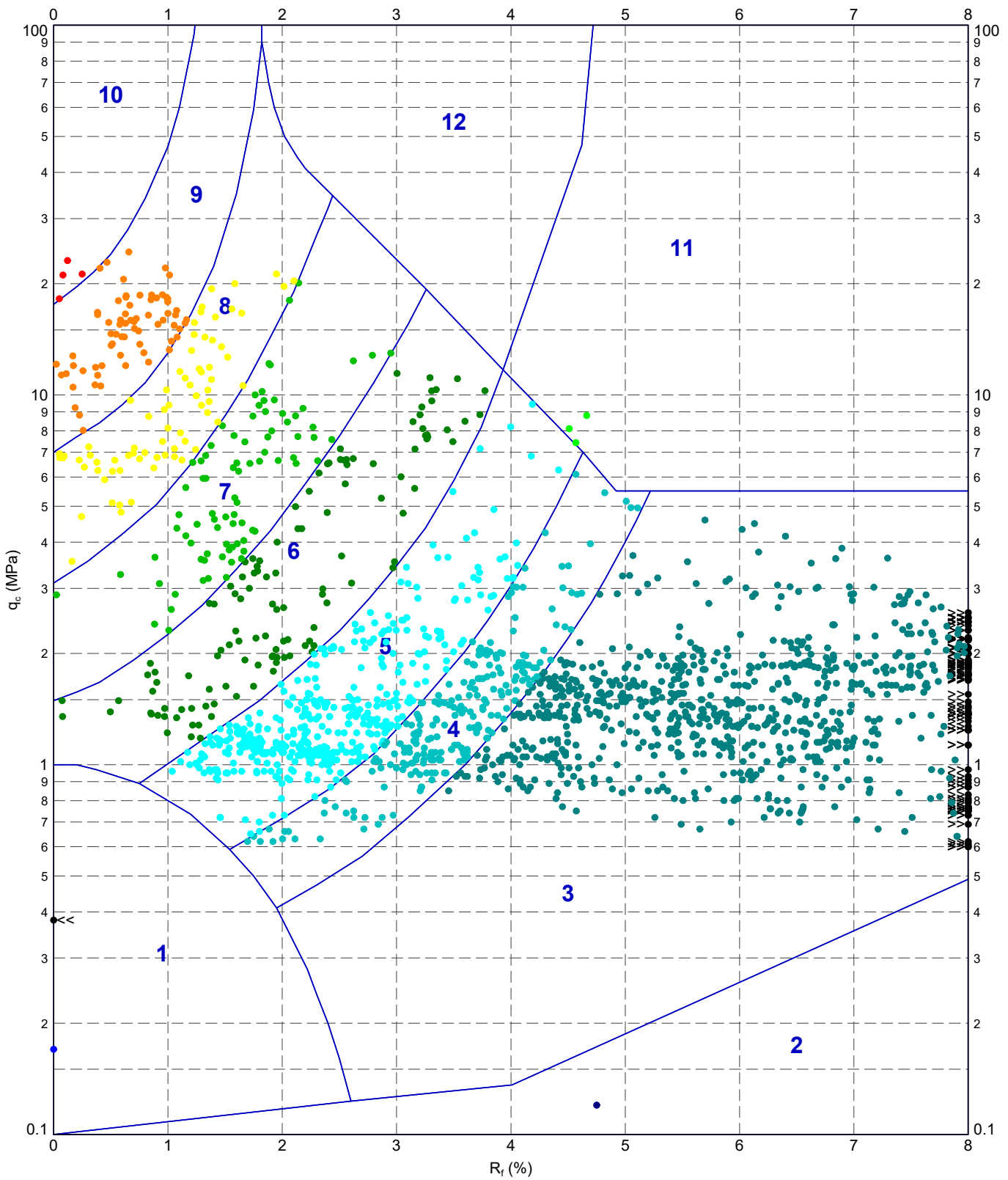
PointID  
**CPT03A**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491001.394 m <b>NORTHING</b> : 290915.219 m <b>ELEVATION</b> : 105.716 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>361 mV</td> <td>360 mV</td> <td>-0.011 MPa</td> </tr> <tr> <td>Sleeve</td> <td>289 mV</td> <td>286 mV</td> <td>-0.002 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>206 mV</td> <td>216 mV</td> <td>0.002 kPa</td> </tr> <tr> <td>X-Y Inclinometer</td> <td>2552 mV</td> <td>2612 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	361 mV	360 mV	-0.011 MPa	Sleeve	289 mV	286 mV	-0.002 kPa	Pore Pressure 2	206 mV	216 mV	0.002 kPa	X-Y Inclinometer	2552 mV	2612 mV		Groundwater Level Dissipation Test
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220228-ADVANCED REPORT INSTITUSI 2.02.1 LIB - CHLOE.GLB Graph: CPT ROBERTSON ET AL. 86 QC VS. RF APF 1220144 CORBY DELTA SIMONS.GPJ <<DrawingFile>> 04/03/2022 15:51 10.01.00.11 Datagel Lab and In Situ Tool - DGD [Lib: In Situ SI 2.02.0 2017-07-10 Proj: In Situ SI 2.02.0 2017-07-10]



METHOD: Robertson et al. 1986 qc Rf

- 1 - Sensitive fine grained material
- 4 - Silty CLAY to CLAY
- 7 - Silty SAND to sandy SILT
- 10 - Gravelly SAND to SAND
- 2 - Organic material
- 5 - Clayey SILT to silty CLAY
- 8 - SAND to silty SAND
- 11 - Very stiff fine grained
- 3 - CLAY
- 6 - Sandy SILT to clayey SILT
- 9 - SAND
- 12 - SAND to clayey SAND

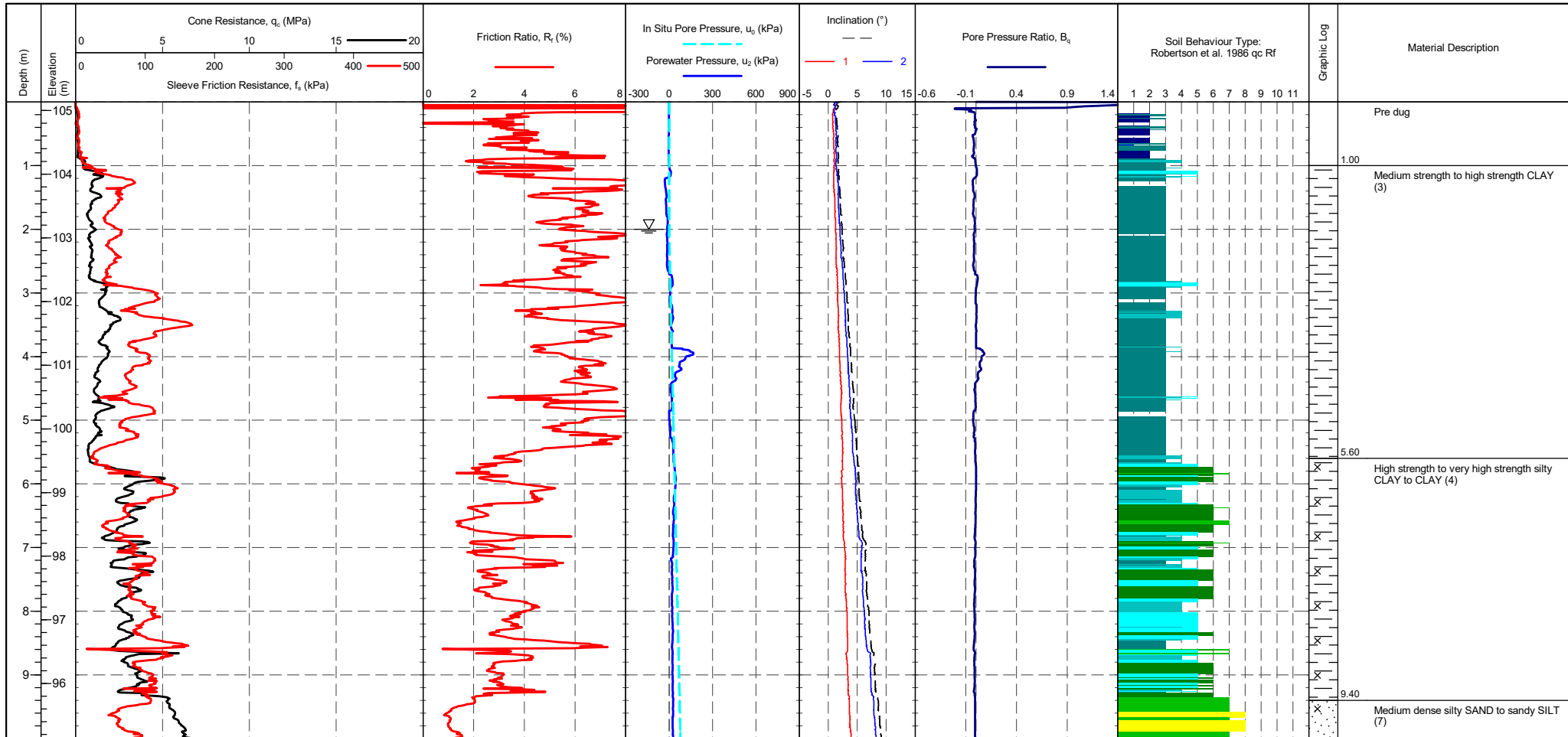


TITLE  
 Delta Simons  
 Cordby  
 Corby  
 Robertson et al. 1986 qc vs. Rf - CPT03A

DRAWN	DATE	04/03/2022
CHECKED	DATE	04/03/2022
SCALE	Not To Scale	A4
PROJECT No	FIGURE No	1220144

PointID	<b>CPT04</b>
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490956.086 m <b>NORTHING</b> : 290835.720 m <b>ELEVATION</b> : 105.136 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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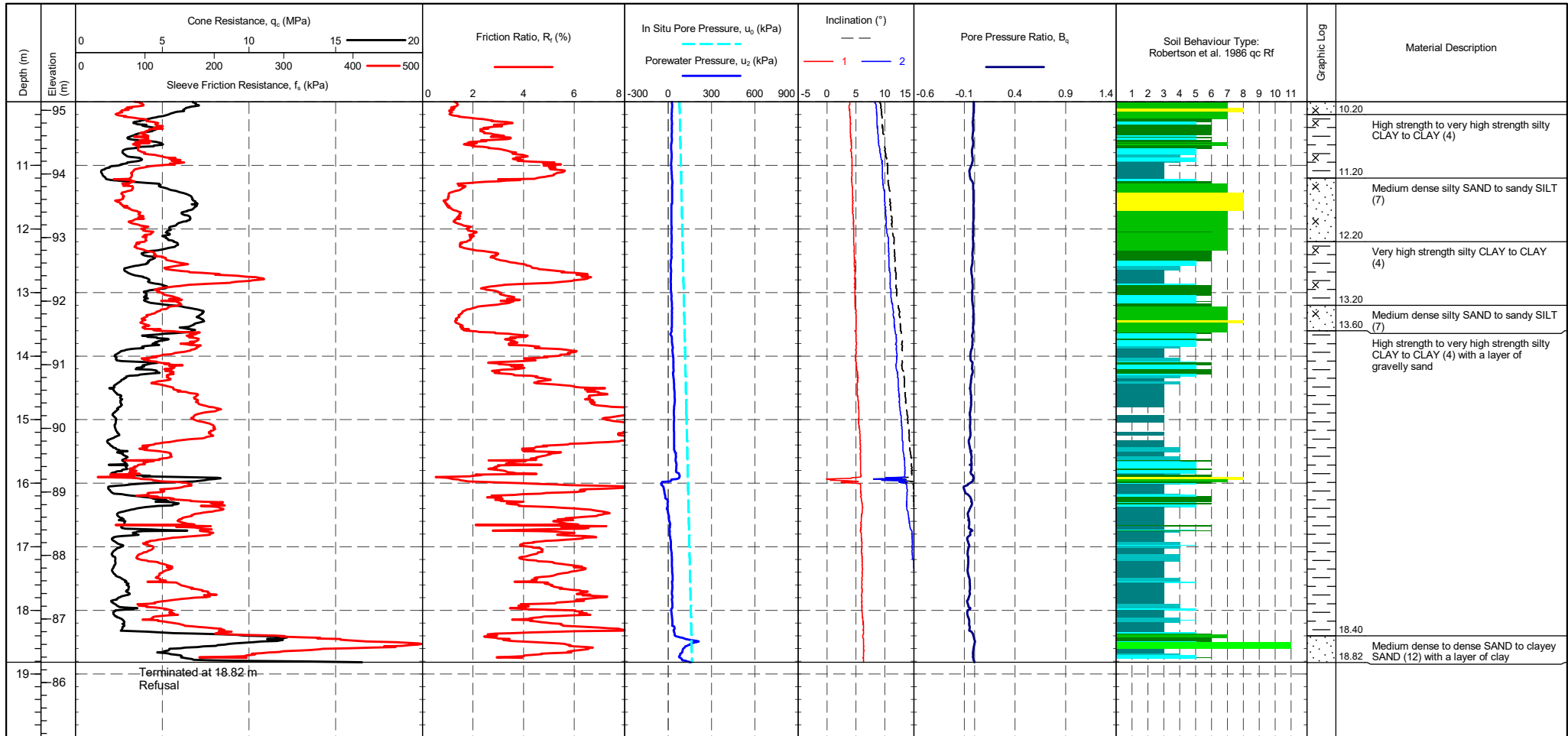


<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip: Pre 361 mV, Post 357 mV, Difference -0.044 MPa Sleeve: Pre 287 mV, Post 284 mV, Difference -0.002 kPa Pore Pressure 2: Pre 279 mV, Post 235 mV, Difference -0.01 kPa X-Y Inclinator: Pre 2664 mV, Post 2630 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravely SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID	<b>CPT04</b>
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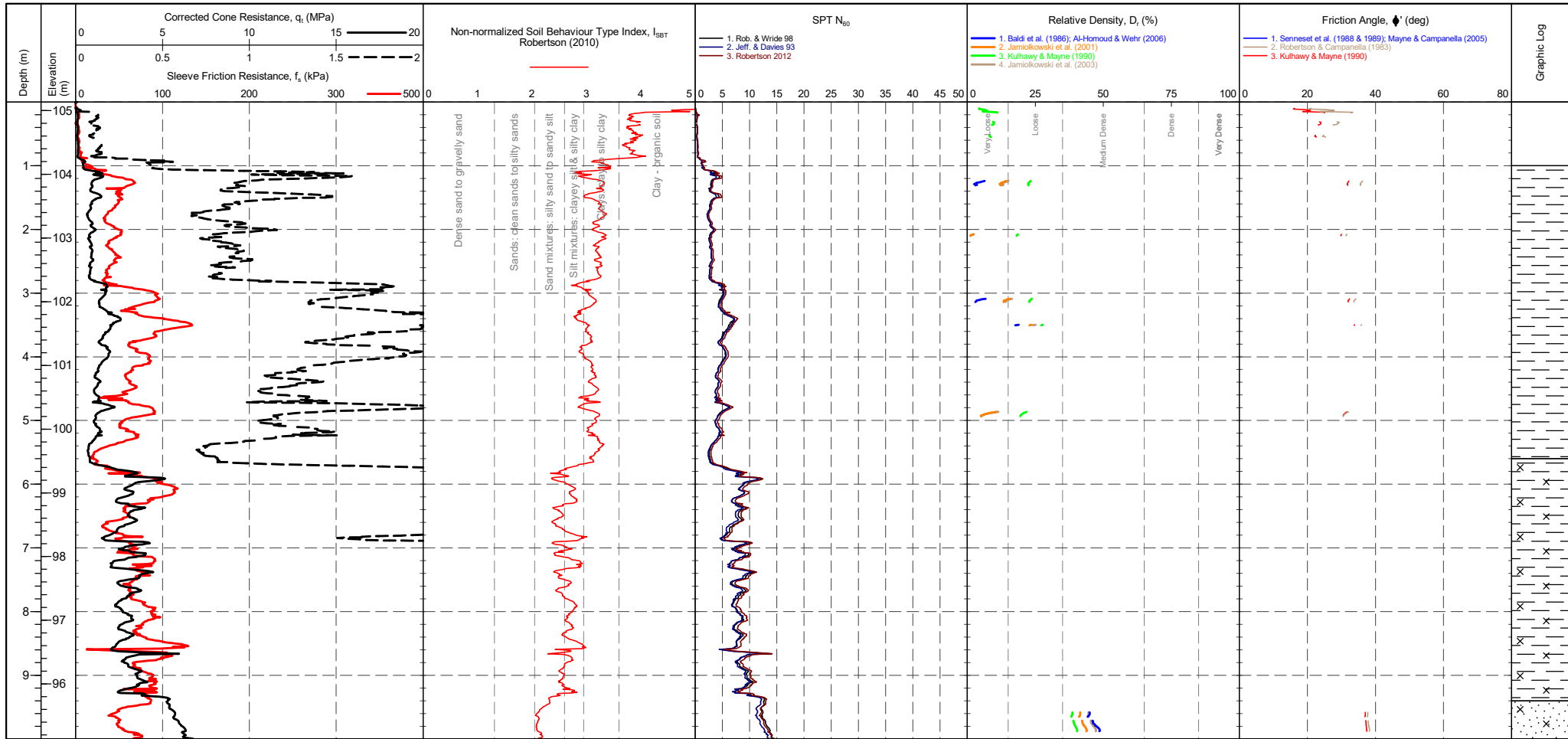
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490956.086 m <b>NORTHING</b> : 290835.720 m <b>ELEVATION</b> : 105.136 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip : 361 mV / 357 mV / -0.044 MPa Sleeve : 287 mV / 284 mV / -0.002 kPa Pore Pressure 2 : 279 mV / 235 mV / -0.01 kPa X-Y Inclinator : 2664 mV / 2630 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf Legend: Blue: 1 - Sensitive fine grained material Dark Blue: 2 - Organic material Teal: 3 - CLAY Light Blue: 4 - Silty CLAY to CLAY Cyan: 5 - Clayey SILT to silty CLAY Green: 6 - Sandy SILT to clayey SILT Light Green: 7 - Silty SAND to sandy SILT Yellow: 8 - SAND to silty SAND Orange: 9 - SAND Red: 10 - Gravelly SAND to SAND Light Green: 11 - Very stiff fine grained Yellow: 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID	<b>CPT04</b>
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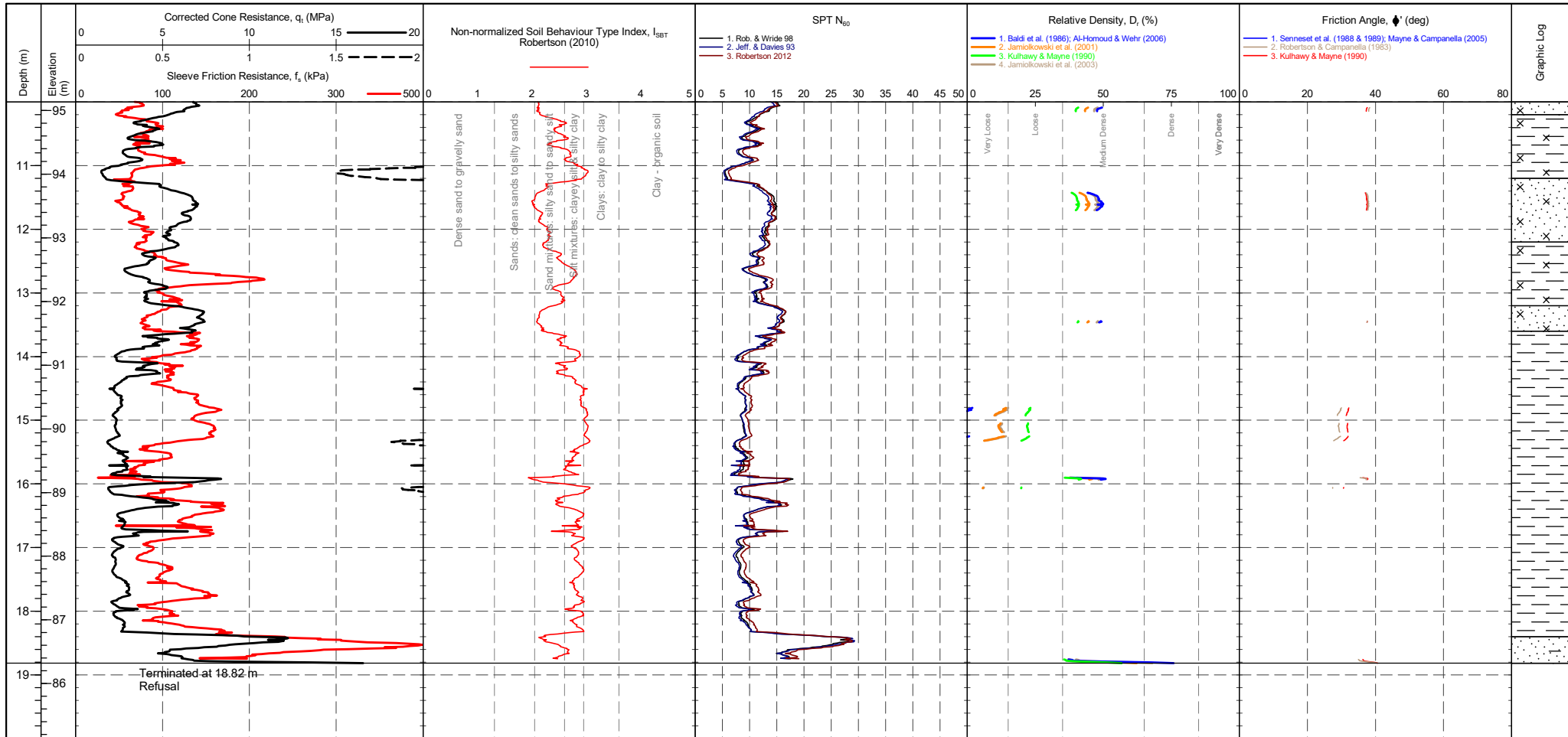
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490956.086 m <b>NORTHING</b> : 290835.720 m <b>ELEVATION</b> : 105.136 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> <b>Tip</b> : 361 mV <b>Sleeve</b> : 287 mV <b>Pore Pressure 2</b> : 279 mV <b>X-Y Inclinator</b> : 2664 mV	<b>PTU ZERO VALUES</b> <b>Pre</b> : 357 mV <b>Post</b> : 284 mV <b>Difference</b> : -0.044 MPa <b>Difference</b> : -0.002 kPa <b>Difference</b> : -0.01 kPa <b>Difference</b> : 2630 mV	<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, <math>I_c</math></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density <math>D_r</math> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, $I_c$	Description	SPT N value, NSPT	Description	Relative Density $D_r$ (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	<b>Groundwater Level</b> <b>Dissipation Test</b>
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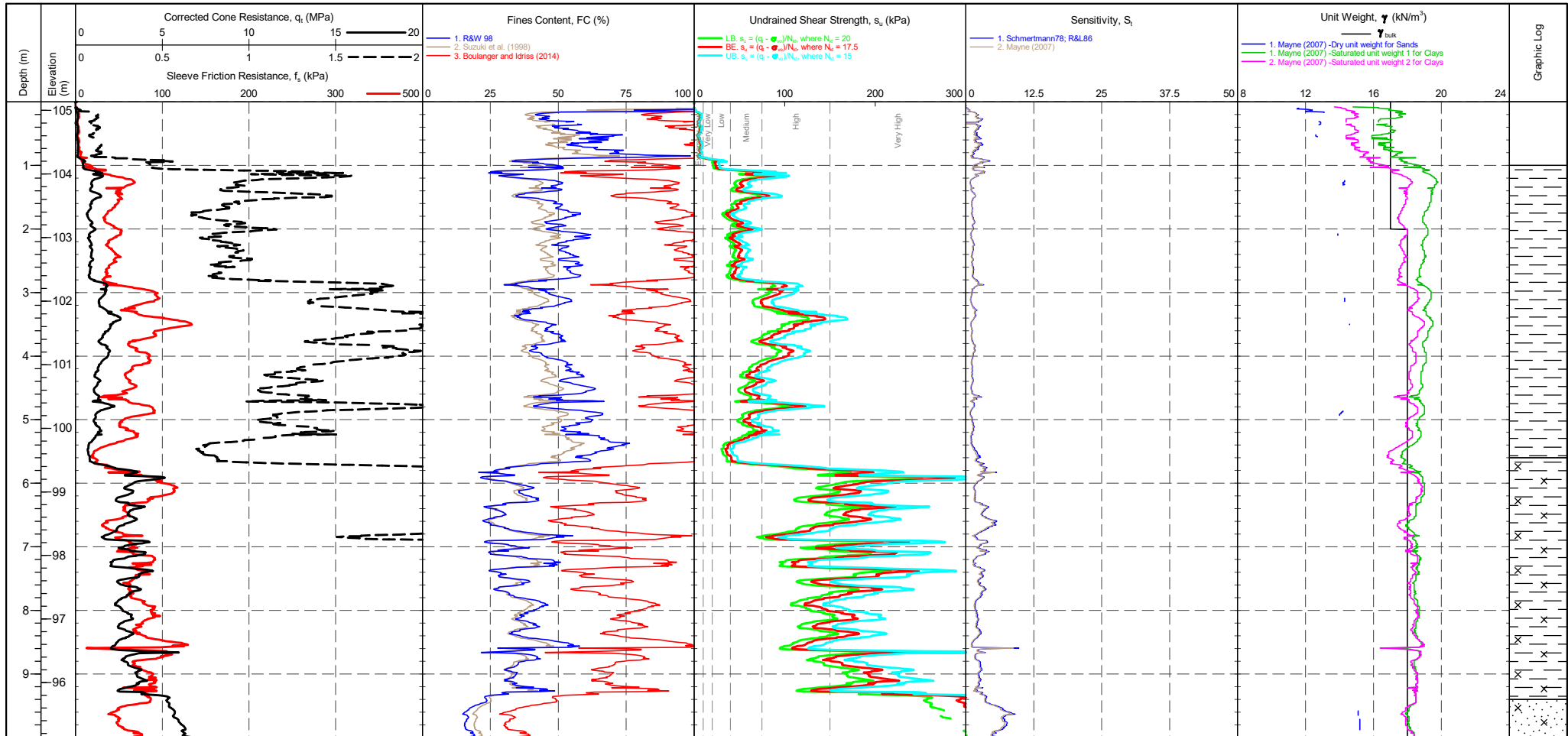
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490956.086 m <b>NORTHING</b> : 290835.720 m <b>ELEVATION</b> : 105.136 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>361 mV</td> <td>357 mV</td> <td>-0.044 MPa</td> </tr> <tr> <td>Sleeve</td> <td>287 mV</td> <td>284 mV</td> <td>-0.002 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>279 mV</td> <td>235 mV</td> <td>-0.01 kPa</td> </tr> <tr> <td>X-Y inclinometer</td> <td>2664 mV</td> <td>2630 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	361 mV	357 mV	-0.044 MPa	Sleeve	287 mV	284 mV	-0.002 kPa	Pore Pressure 2	279 mV	235 mV	-0.01 kPa	X-Y inclinometer	2664 mV	2630 mV		<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, <math>I_c</math></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density <math>D_r</math> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, $I_c$	Description	SPT N value, NSPT	Description	Relative Density $D_r$ (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
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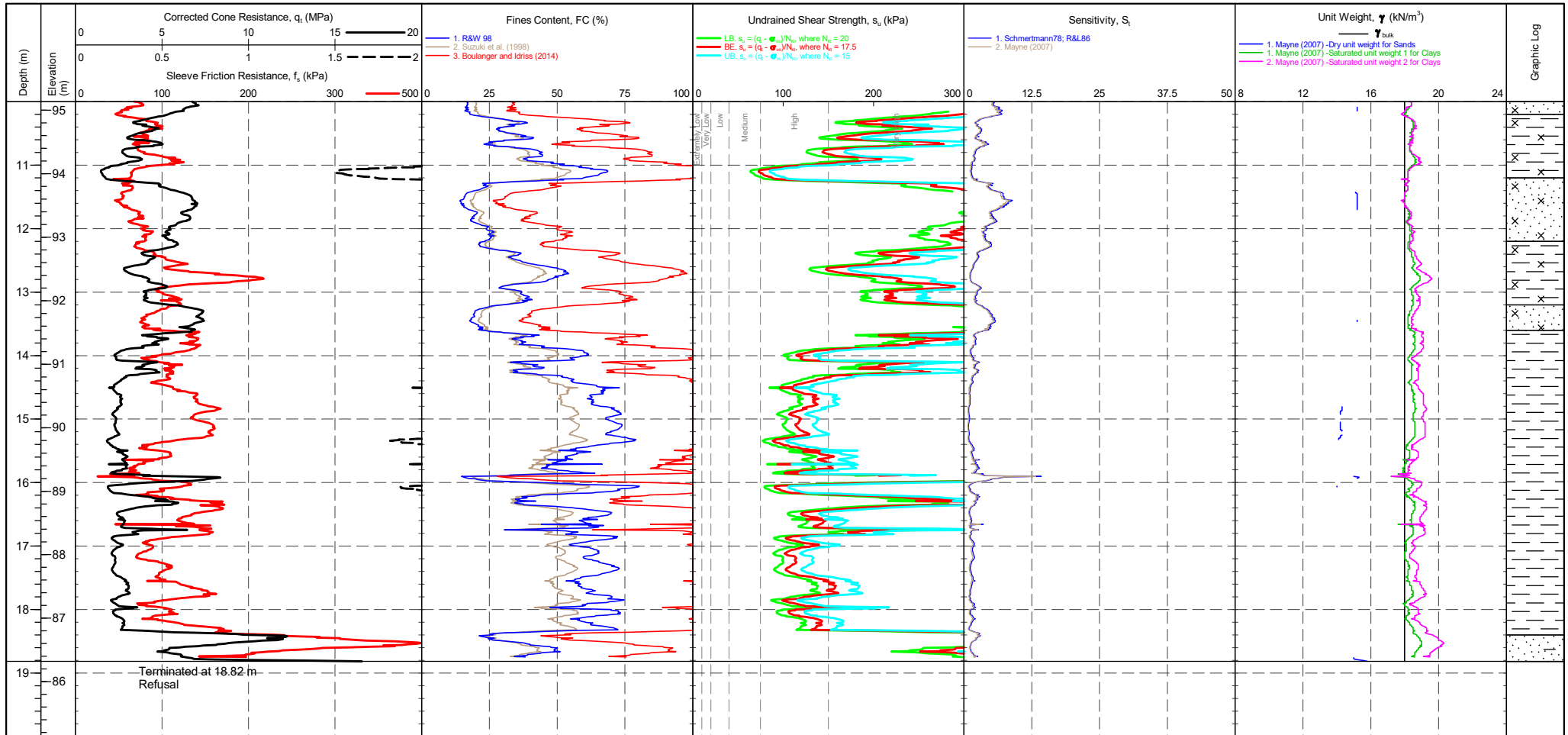


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 361 mV / 357 mV / -0.044 MPa Sleeve: 287 mV / 284 mV / -0.002 kPa Pore Pressure 2: 279 mV / 235 mV / -0.01 kPa X-Y Inclinator: 2664 mV / 2630 mV	<b>CPTU ZERO VALUES</b> Pre: 361 mV, Post: 357 mV, Difference: -0.044 MPa Sleeve: 287 mV, Post: 284 mV, Difference: -0.002 kPa Pore Pressure 2: 279 mV, Post: 235 mV, Difference: -0.01 kPa X-Y Inclinator: 2664 mV, Post: 2630 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement   $s_u$ (kPa)   Term based on measurement   $s_u$ (kPa) Extremely low strength   <10   Medium strength   40-75 Very low strength   10-20   High strength   75-150 Low strength   20-40   Very high strength   150-300     Extremely high strength   >300	▽ Groundwater Level ▮ Dissipation Test
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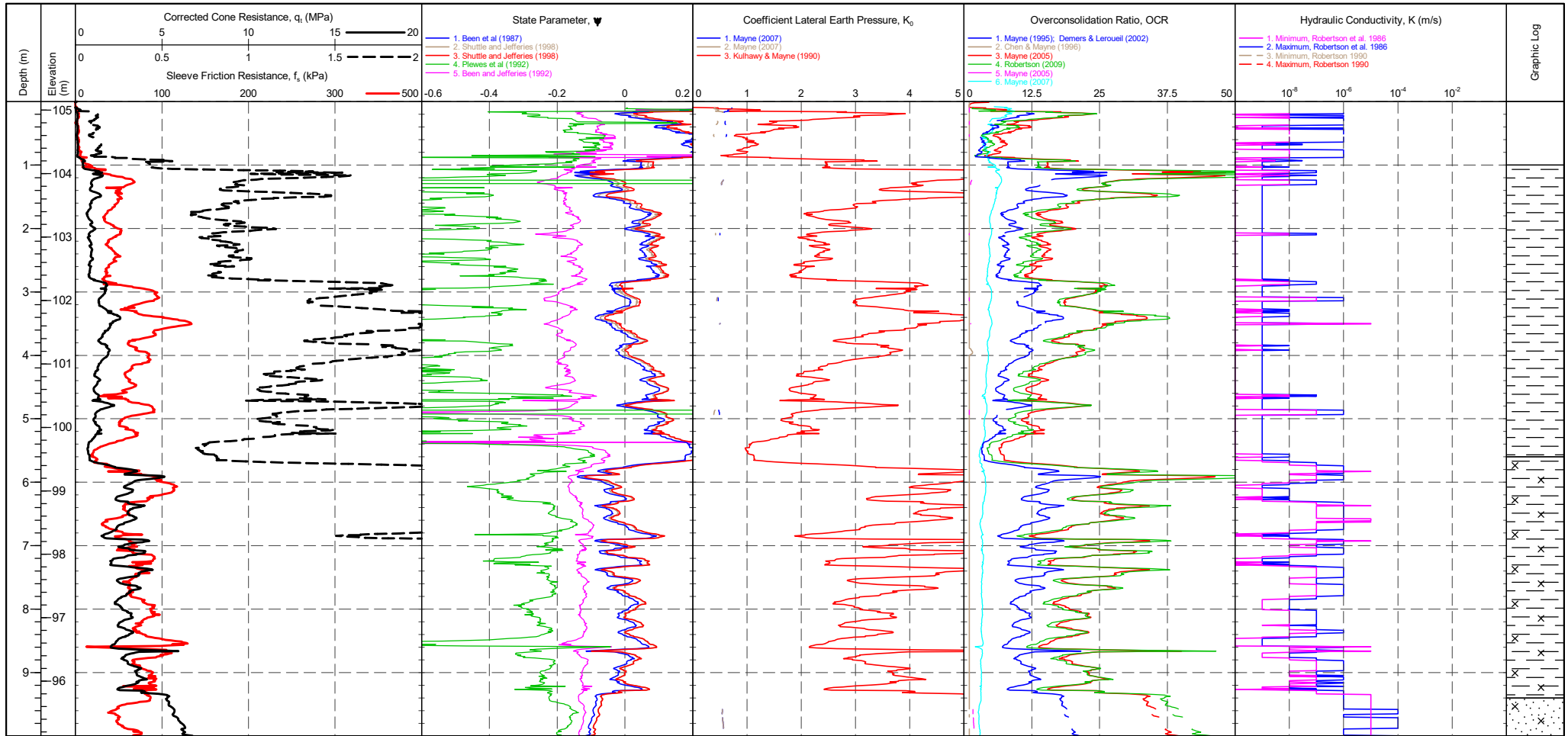


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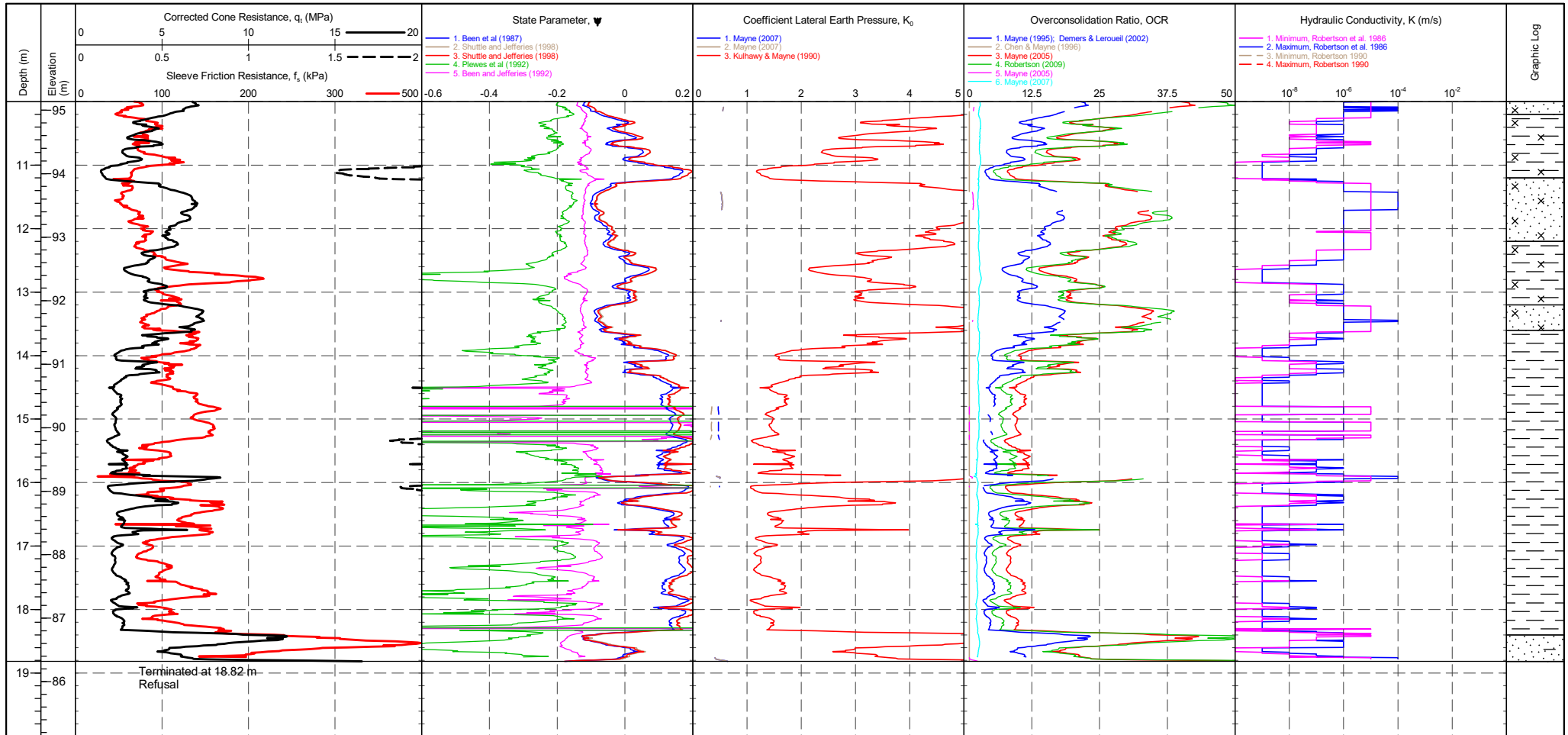
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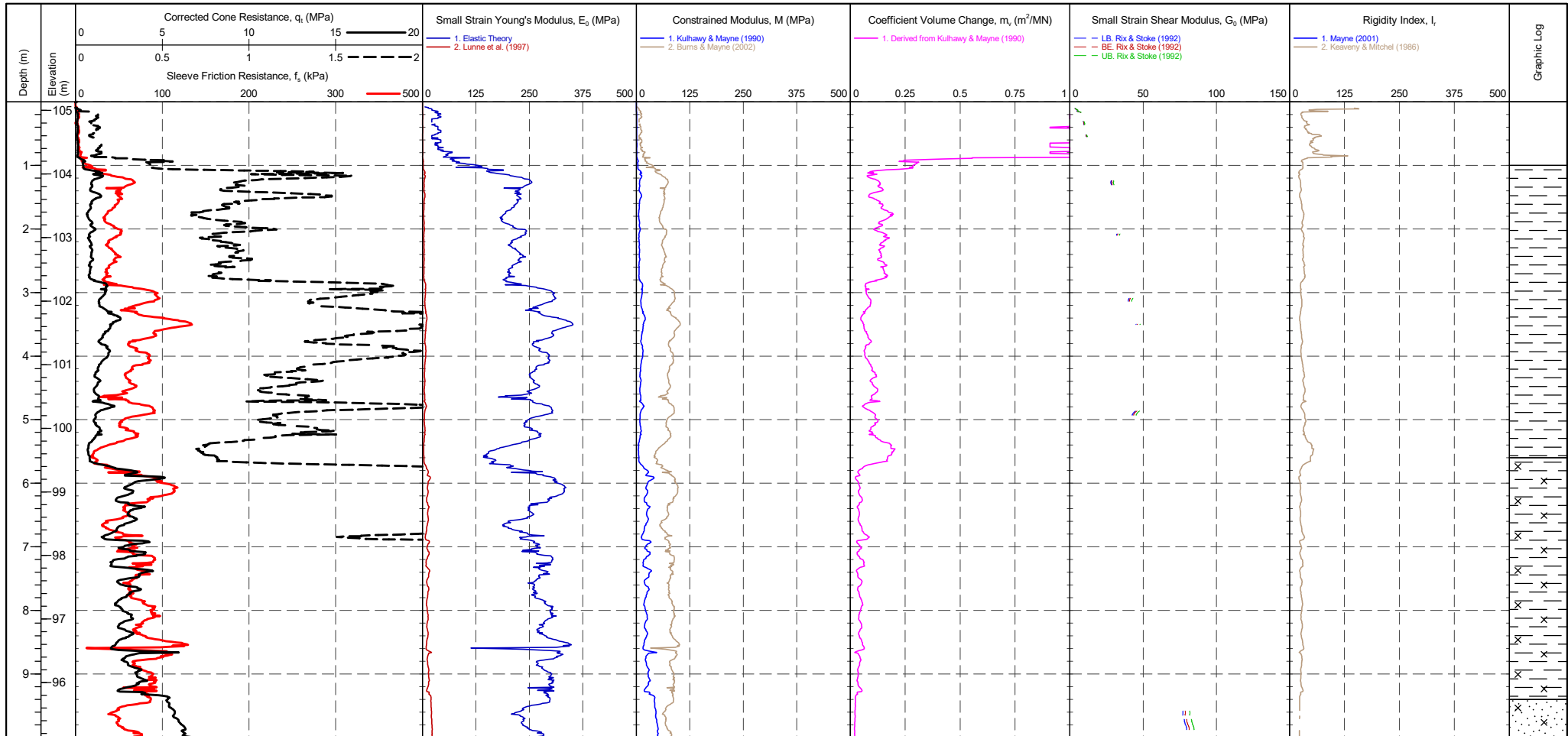


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 361 mV (Pre), 357 mV (Post), -0.044 MPa (Difference) Sleeve: 287 mV (Pre), 284 mV (Post), -0.002 kPa (Difference) Pore Pressure 2: 279 mV (Pre), 235 mV (Post), -0.01 kPa (Difference) X-Y Inclinator: 2664 mV (Pre), 2630 mV (Post)	<b>CPTU ZERO VALUES</b> Tip: 361 mV (Pre), 357 mV (Post), -0.044 MPa (Difference) Sleeve: 287 mV (Pre), 284 mV (Post), -0.002 kPa (Difference) Pore Pressure 2: 279 mV (Pre), 235 mV (Post), -0.01 kPa (Difference) X-Y Inclinator: 2664 mV (Pre), 2630 mV (Post)	Groundwater Level Dissipation Test
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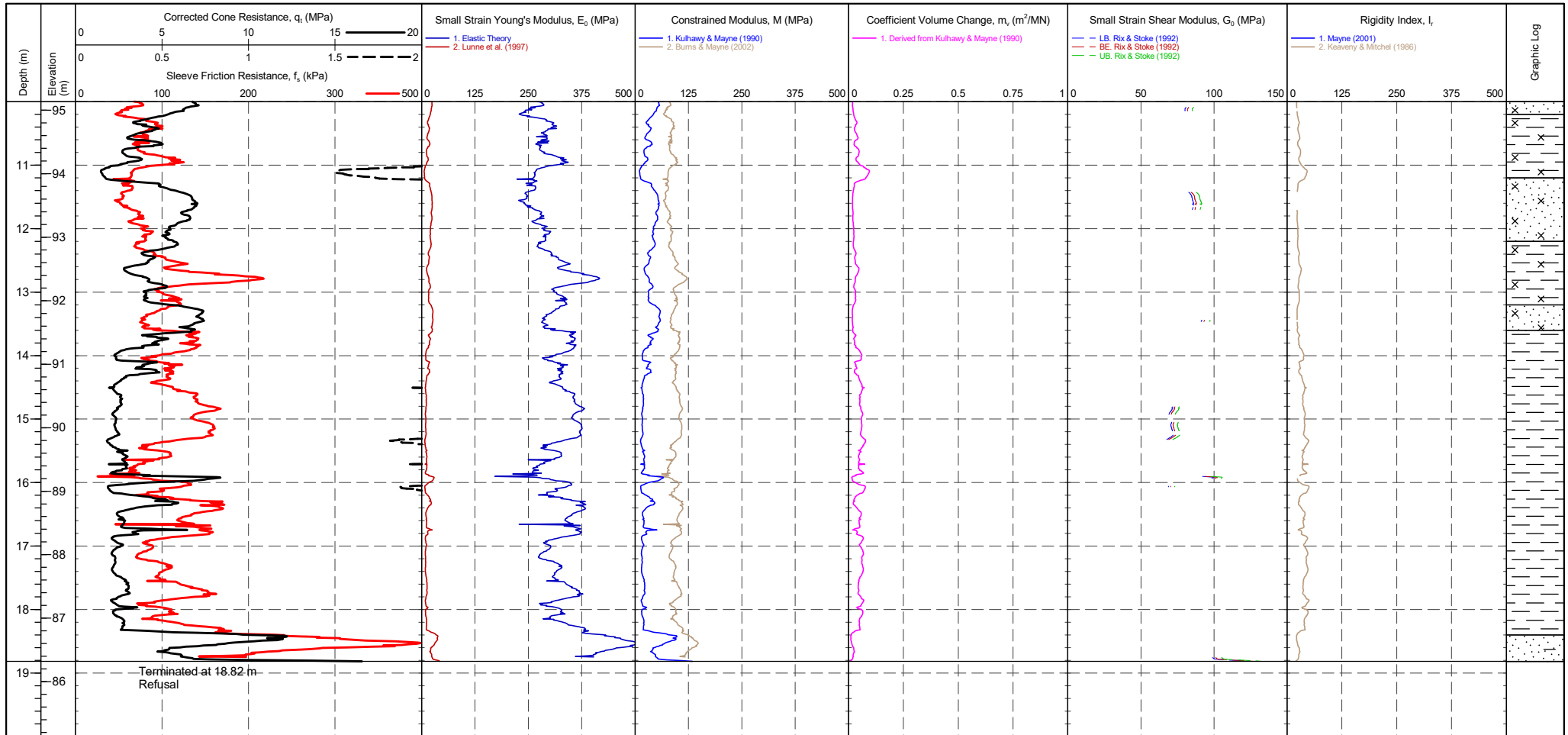


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PointID

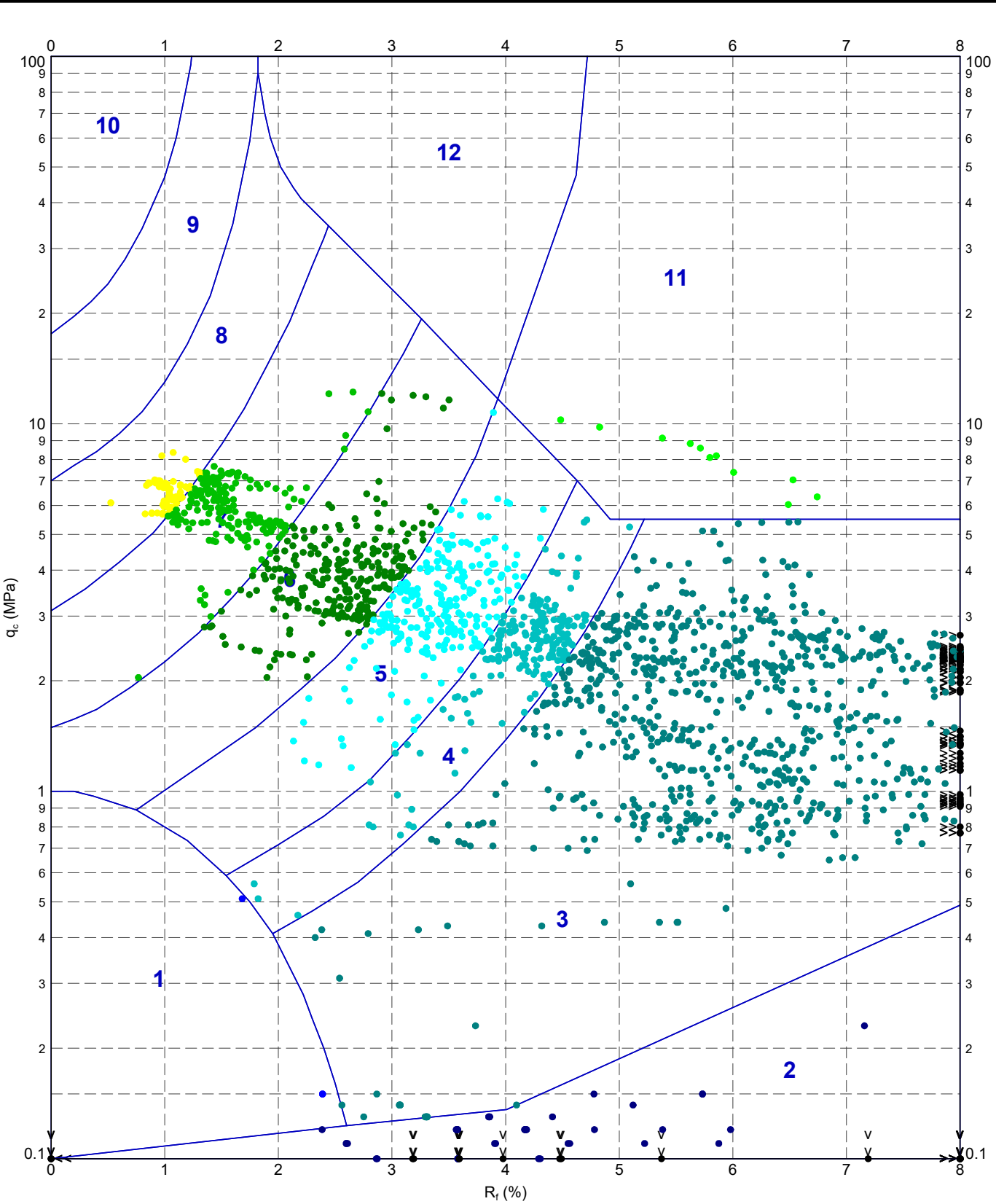
**CPT04**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490956.086 m <b>NORTHING</b> : 290835.720 m <b>ELEVATION</b> : 105.136 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> Transducer Pre Post Difference Tip 361 mV 357 mV -0.044 MPa Sleeve 287 mV 284 mV -0.002 kPa Pore Pressure 2 279 mV 235 mV -0.01 kPa X-Y Inclinator 2664 mV 2630 mV	Groundwater Level Dissipation Test
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220228-ADVANCED REPORT INSTITUTE 2.02.1 LIB - CHLOE.GLB Graph: CPT ROBERTSON ET AL. 8F QC VS. RF APF 1220144 CORBY DELTA SIMONS.GPJ <<DrawingFile>> 04/03/2022 15:57 10.01.00.11 Datagel Lab and In Situ Tool - DGD [Lib: In Situ SI 2.02.0 2017-07-10 Proj: In Situ SI 2.02.0 2017-07-10]



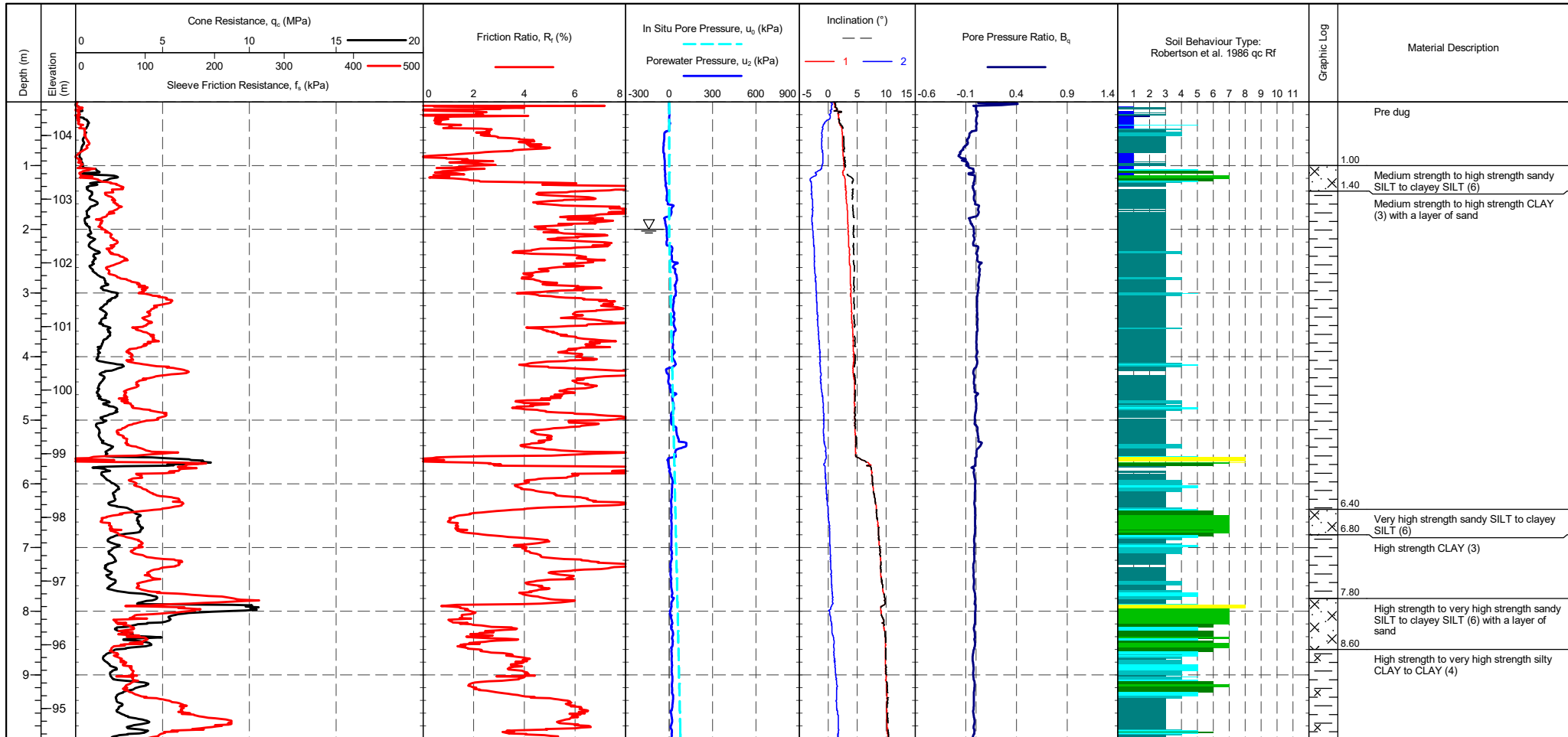
**METHOD: Robertson et al. 1986  $q_c$  vs  $R_f$**

1 - Sensitive fine grained material	4 - Silty CLAY to CLAY	7 - Silty SAND to sandy SILT	10 - Gravelly SAND to SAND
2 - Organic material	5 - Clayey SILT to silty CLAY	8 - SAND to silty SAND	11 - Very stiff fine grained
3 - CLAY	6 - Sandy SILT to clayey SILT	9 - SAND	12 - SAND to clayey SAND

	TITLE	DRAWN	DATE
	Delta Simons Cordby Corby Robertson et al. 1986 $q_c$ vs. $R_f$ - CPT04	CHECKED	DATE
		SCALE	FIGURE No
		PROJECT No	
		1220144	A4

PointID	<b>CPT05</b>
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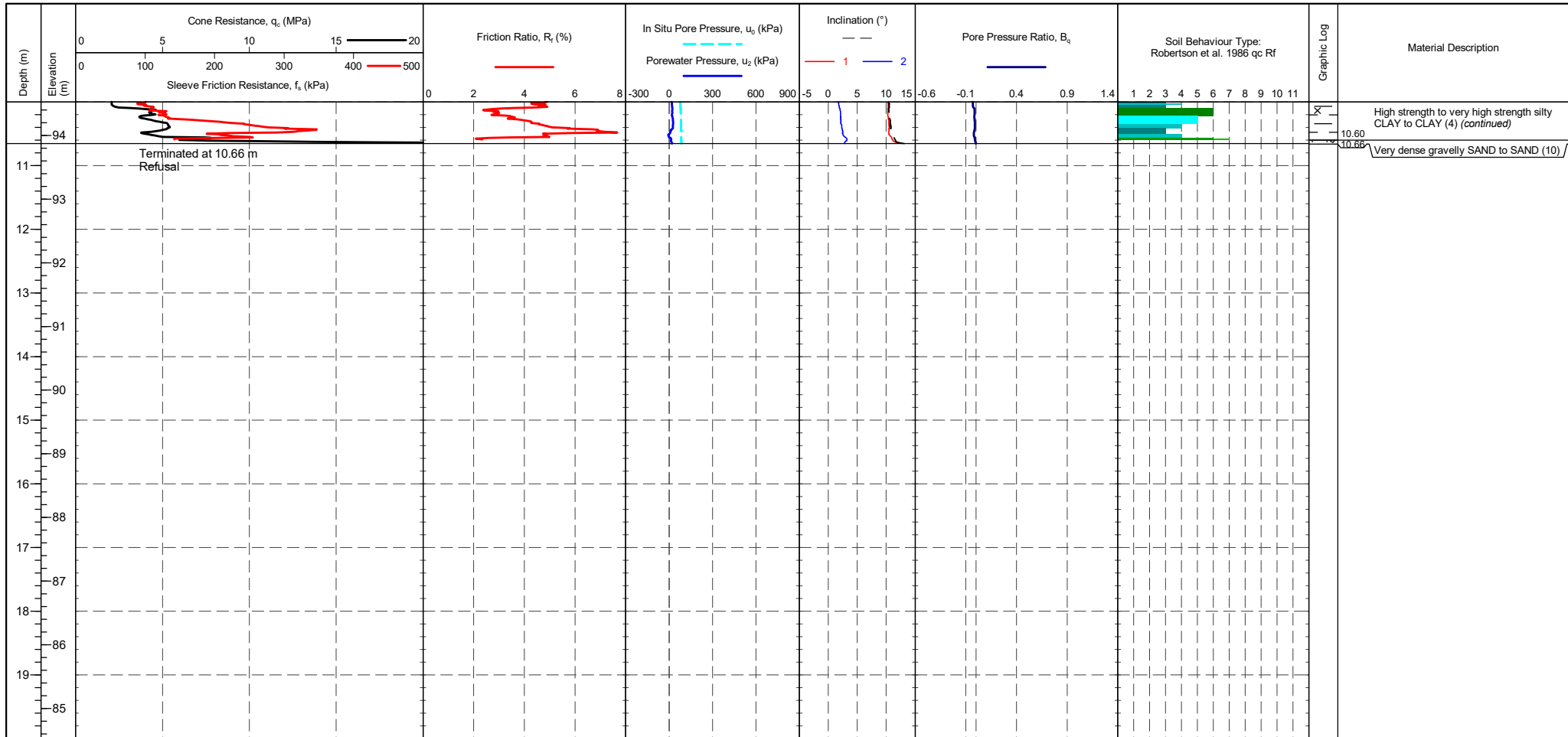
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip: Pre 363 mV, Post 358 mV, Difference -0.055 MPa Sleeve: Pre 291 mV, Post 284 mV, Difference -0.005 kPa Pore Pressure 2: Pre 218 mV, Post 218 mV, Difference 0 kPa X-Y Inclinator: Pre 2641 mV, Post 2643 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravely SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID	<b>CPT05</b>
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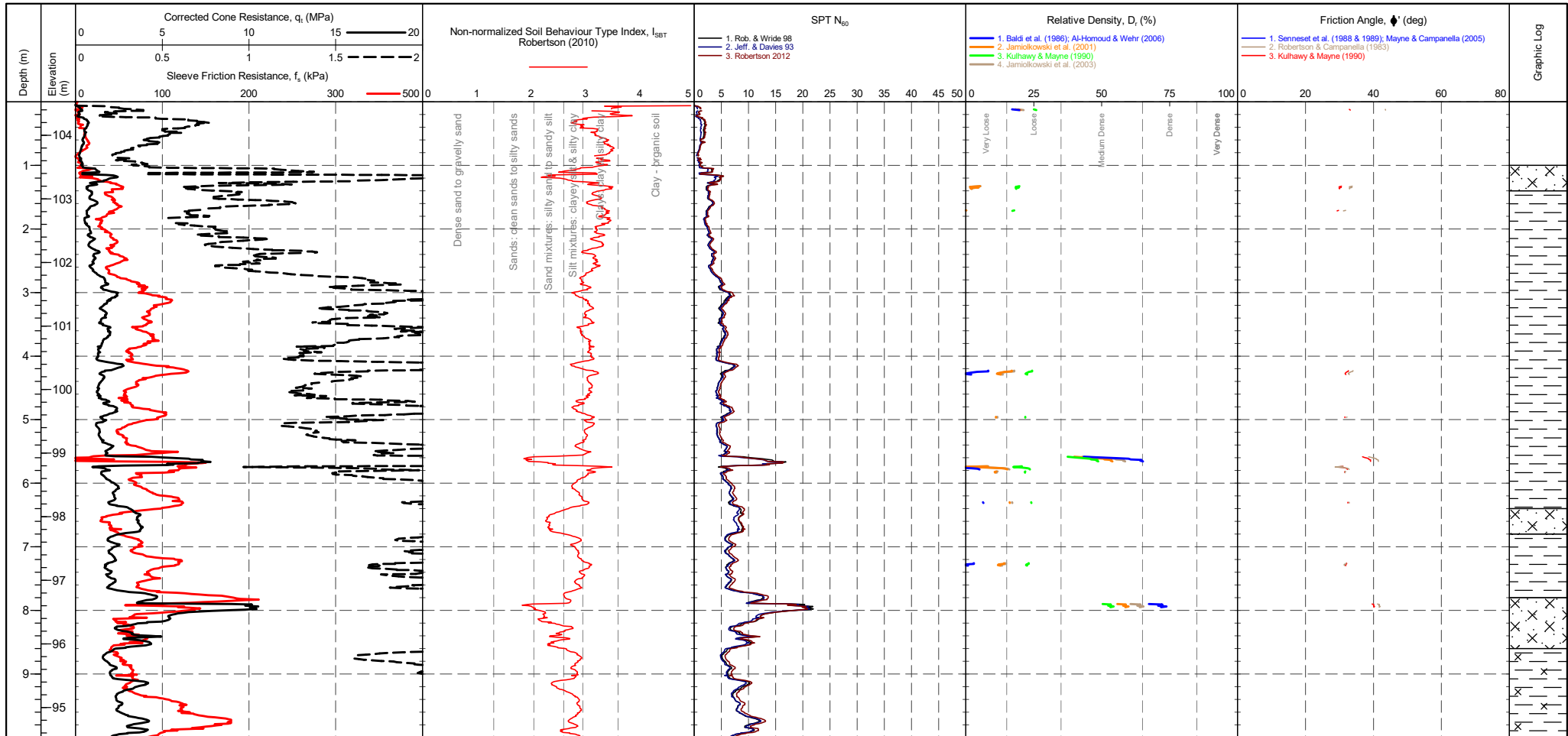
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip: Pre 363 mV, Post 358 mV, Difference -0.055 MPa Sleeve: Pre 291 mV, Post 284 mV, Difference -0.005 kPa Pore Pressure 2: Pre 218 mV, Post 218 mV, Difference 0 kPa X-Y Inclinator: Pre 2641 mV, Post 2643 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravely SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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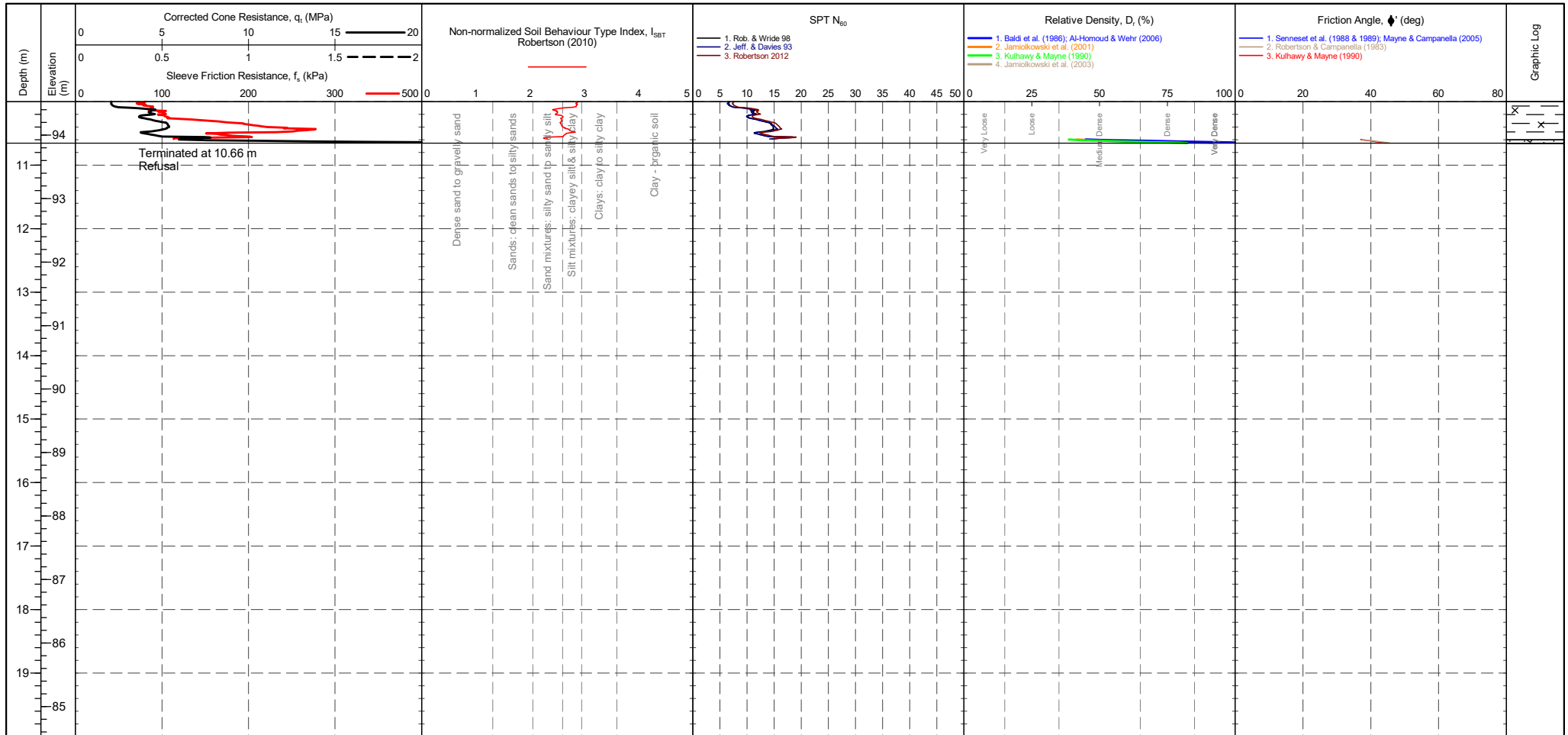


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> <b>Tip</b> : 363 mV <b>Sleeve</b> : 291 mV <b>Pore Pressure 2</b> : 218 mV <b>X-Y Inclinator</b> : 2641 mV	<b>CPTU ZERO VALUES</b> <b>Post</b> : 358 mV <b>Difference</b> : -0.055 MPa <b>0 kPa</b> : -0.005 kPa <b>2643 mV</b> : 2643 mV	<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, <math>I_c</math></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density <math>D_r</math> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, $I_c$	Description	SPT N value, NSPT	Description	Relative Density $D_r$ (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	▽ Groundwater Level ▮ Dissipation Test
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PointID

**CPT05**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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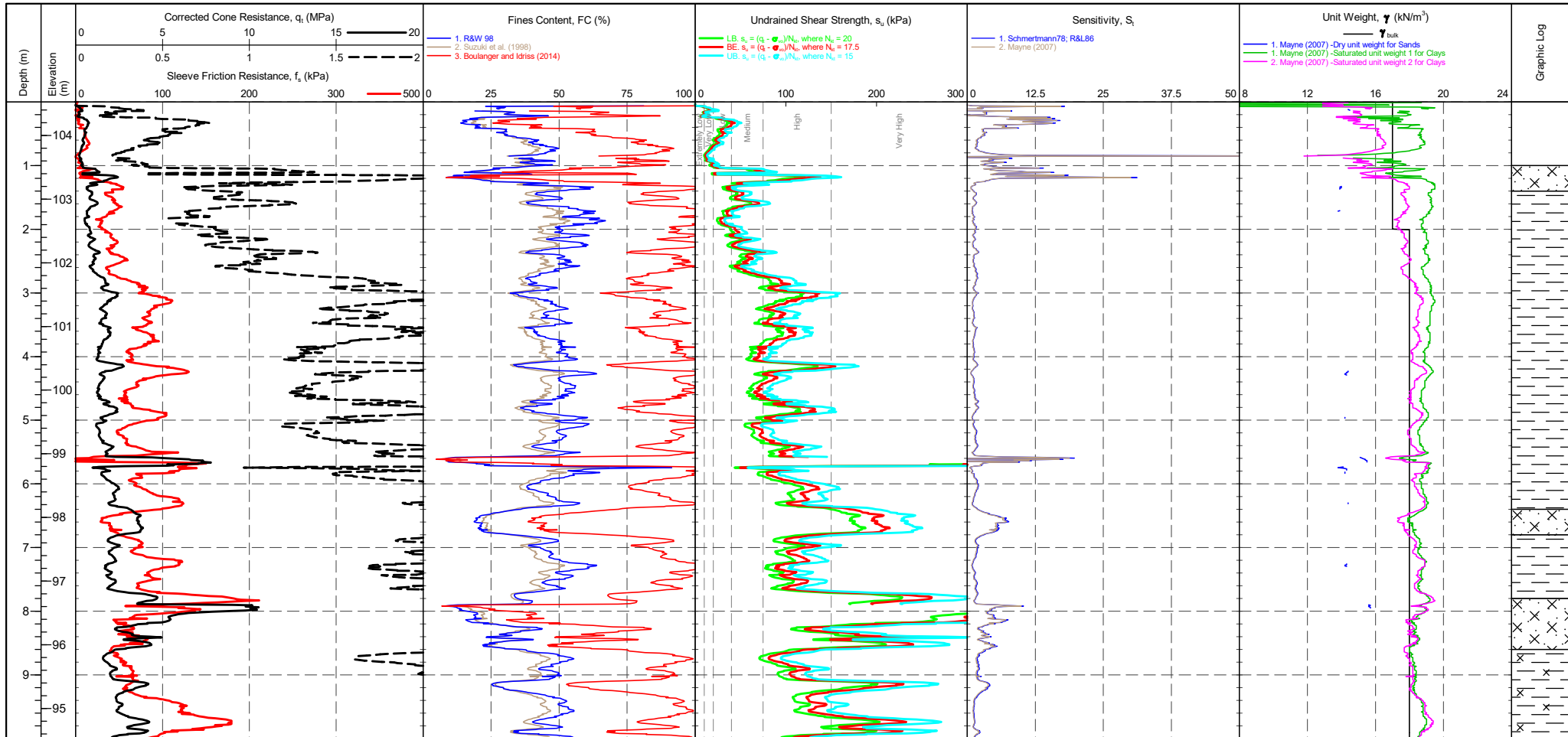




<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>363 mV</td> <td>358 mV</td> <td>-0.055 MPa</td> </tr> <tr> <td>Sleeve</td> <td>291 mV</td> <td>284 mV</td> <td>-0.005 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>218 mV</td> <td>218 mV</td> <td>0 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2641 mV</td> <td>2643 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	363 mV	358 mV	-0.055 MPa	Sleeve	291 mV	284 mV	-0.005 kPa	Pore Pressure 2	218 mV	218 mV	0 kPa	X-Y Inclinator	2641 mV	2643 mV		<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, I<sub>c</sub></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density D<sub>r</sub> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, I <sub>c</sub>	Description	SPT N value, NSPT	Description	Relative Density D <sub>r</sub> (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
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PointID	<b>CPT05</b>
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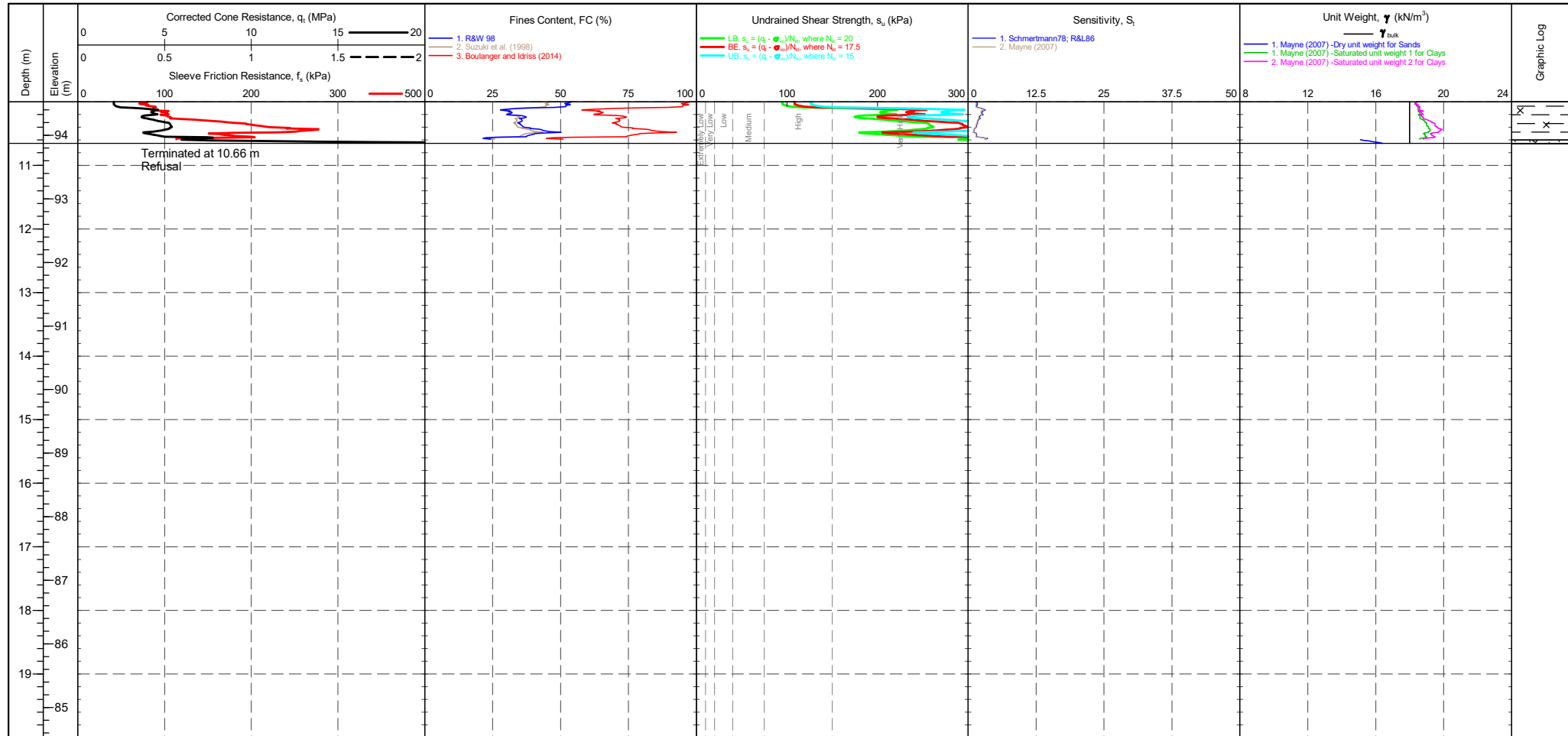
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 363 mV / 358 mV Sleeve: 291 mV / 284 mV Pore Pressure 2: 218 mV / 218 mV X-Y Inclinator: 2641 mV / 2643 mV	<b>CPTU ZERO VALUES</b> Difference: -0.055 MPa Difference: -0.005 kPa Difference: 0 kPa	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> <table border="1"> <tr> <th>Term based on measurement</th> <th>su (kPa)</th> <th>Term based on measurement</th> <th>su (kPa)</th> </tr> <tr> <td>Extremely low strength</td> <td>&lt;10</td> <td>Medium strength</td> <td>40-75</td> </tr> <tr> <td>Very low strength</td> <td>10-20</td> <td>High strength</td> <td>75-150</td> </tr> <tr> <td>Low strength</td> <td>20-40</td> <td>Very high strength</td> <td>150-300</td> </tr> <tr> <td></td> <td></td> <td>Extremely high strength</td> <td>&gt;300</td> </tr> </table>	Term based on measurement	su (kPa)	Term based on measurement	su (kPa)	Extremely low strength	<10	Medium strength	40-75	Very low strength	10-20	High strength	75-150	Low strength	20-40	Very high strength	150-300			Extremely high strength	>300	<b>Groundwater Level</b>  <b>Dissipation Test</b> 
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PointID	<b>CPT05</b>
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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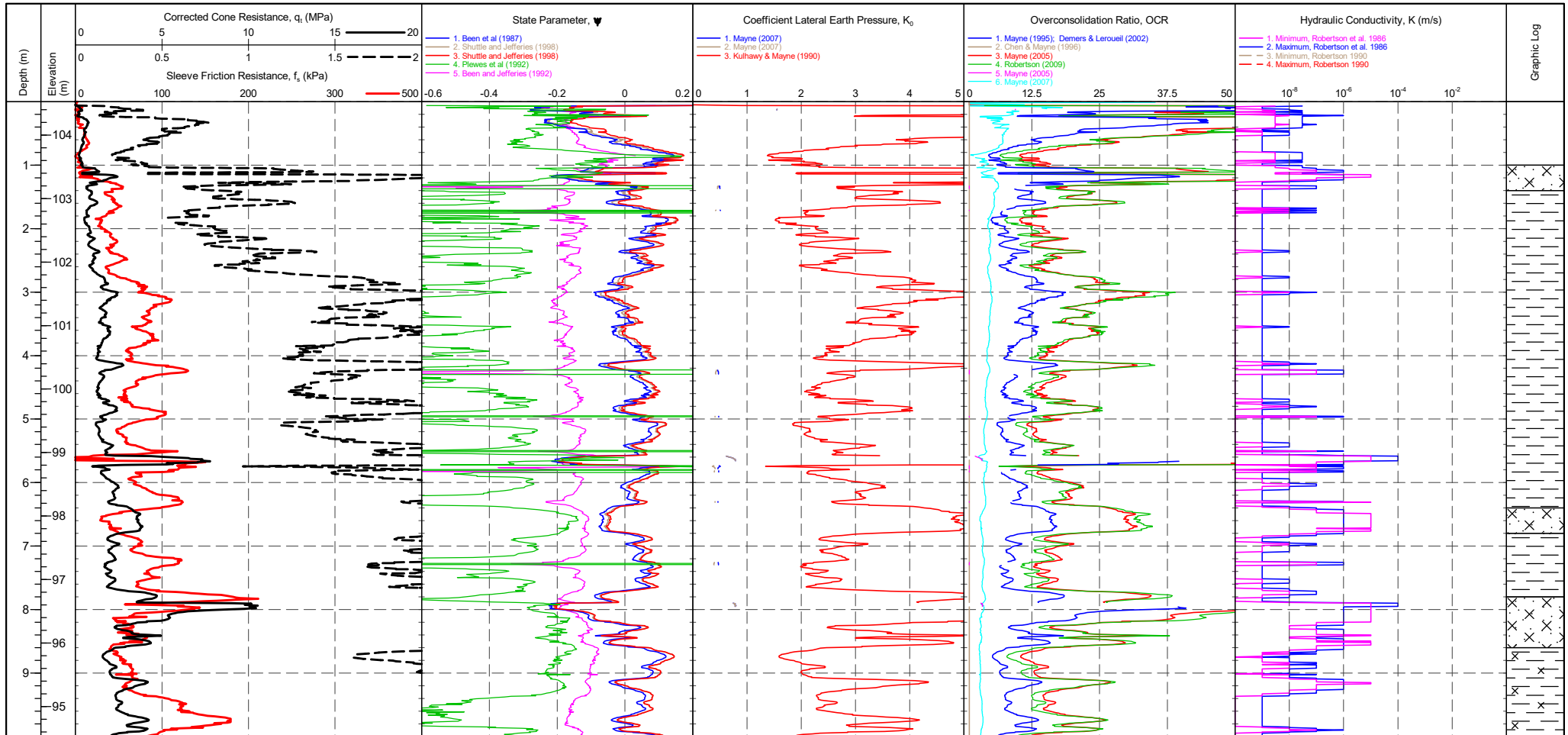


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 363 mV Sleeve: 291 mV Pore Pressure 2: 218 mV X-Y inclinometer: 2641 mV	<b>CPTU ZERO VALUES</b> Post: 358 mV Difference: -0.055 MPa 284 mV -0.005 kPa 218 mV 0 kPa 2643 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement su (kPa) Extremely low strength <10 Very low strength 10-20 Low strength 20-40	Term based on measurement su (kPa) Medium strength 40-75 High strength 75-150 Very high strength 150-300 Extremely high strength >300	Groundwater Level Dissipation Test
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PointID

**CPT05**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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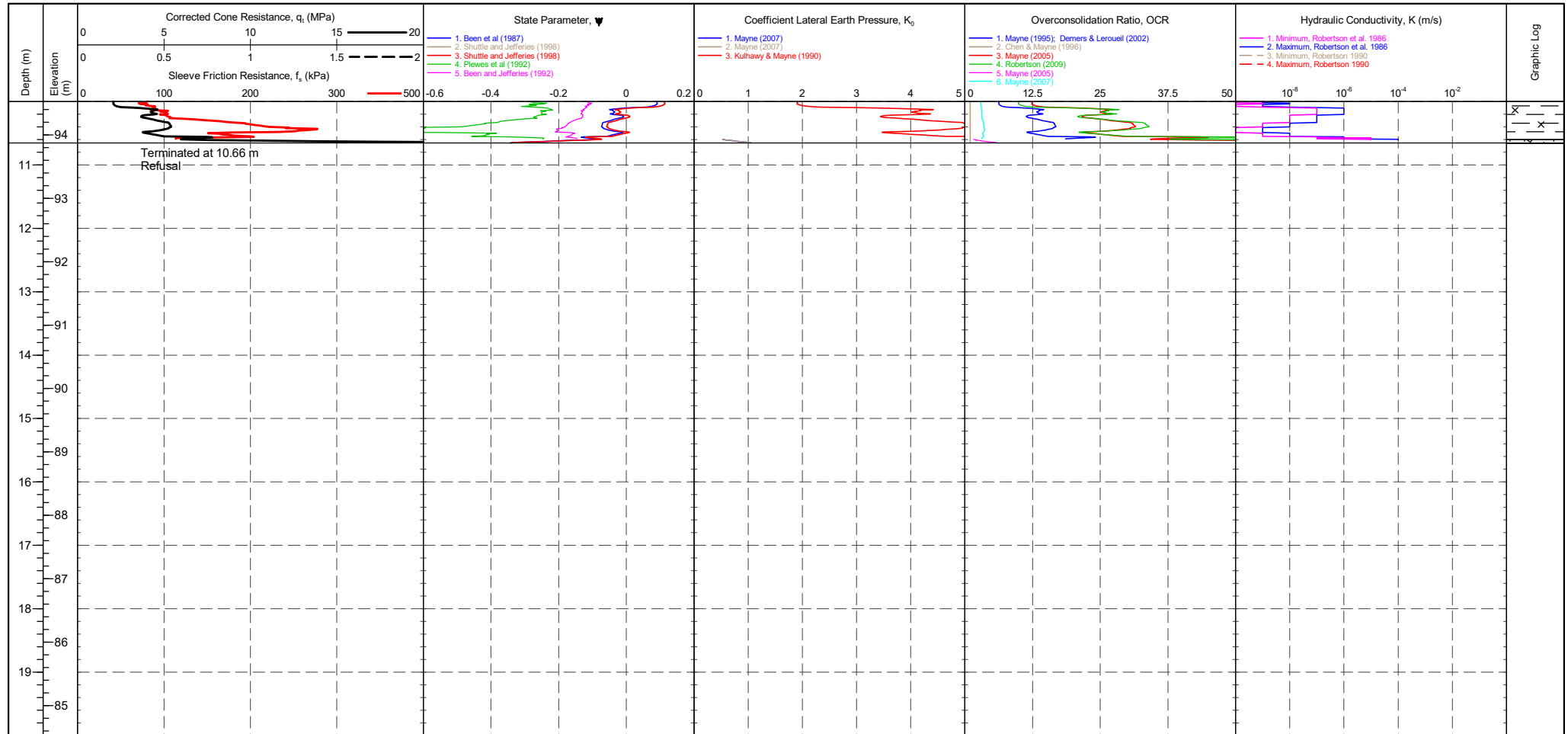


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>363 mV</td> <td>358 mV</td> <td>-0.055 MPa</td> </tr> <tr> <td>Sleeve</td> <td>291 mV</td> <td>284 mV</td> <td>-0.005 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>218 mV</td> <td>218 mV</td> <td>0 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2641 mV</td> <td>2643 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	363 mV	358 mV	-0.055 MPa	Sleeve	291 mV	284 mV	-0.005 kPa	Pore Pressure 2	218 mV	218 mV	0 kPa	X-Y Inclinator	2641 mV	2643 mV		Groundwater Level Dissipation Test
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PointID

CPT05

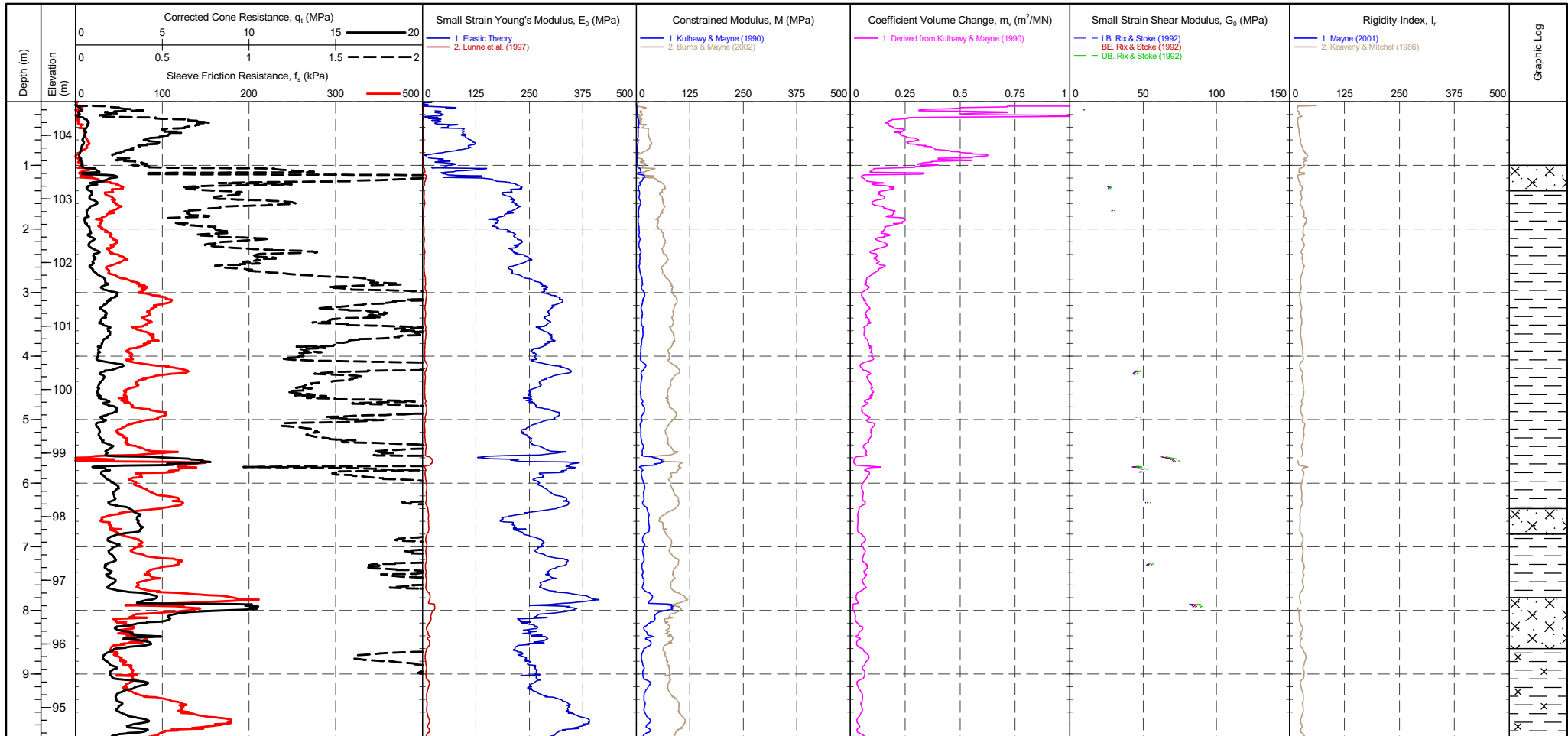
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>363 mV</td> <td>358 mV</td> <td>-0.055 MPa</td> </tr> <tr> <td>Sleeve</td> <td>291 mV</td> <td>284 mV</td> <td>-0.005 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>218 mV</td> <td>218 mV</td> <td>0 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2641 mV</td> <td>2643 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	363 mV	358 mV	-0.055 MPa	Sleeve	291 mV	284 mV	-0.005 kPa	Pore Pressure 2	218 mV	218 mV	0 kPa	X-Y Inclinator	2641 mV	2643 mV		Groundwater Level Dissipation Test
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PointID  
**CPT05**

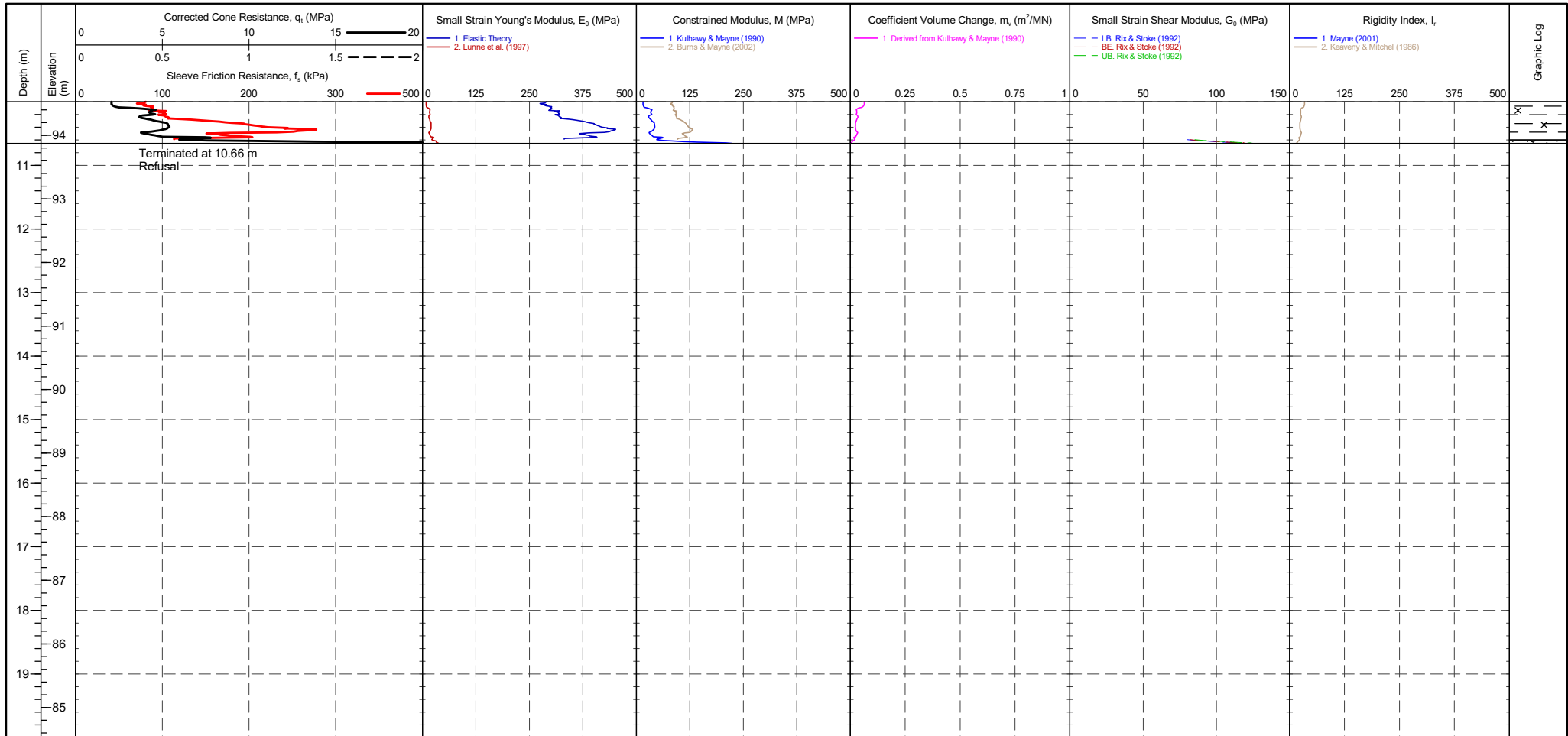
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>363 mV</td> <td>358 mV</td> <td>-0.055 MPa</td> </tr> <tr> <td>Sleeve</td> <td>291 mV</td> <td>284 mV</td> <td>-0.005 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>218 mV</td> <td>218 mV</td> <td>0 kPa</td> </tr> <tr> <td>X-Y inclinometer</td> <td>2641 mV</td> <td>2643 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	363 mV	358 mV	-0.055 MPa	Sleeve	291 mV	284 mV	-0.005 kPa	Pore Pressure 2	218 mV	218 mV	0 kPa	X-Y inclinometer	2641 mV	2643 mV		Groundwater Level Dissipation Test
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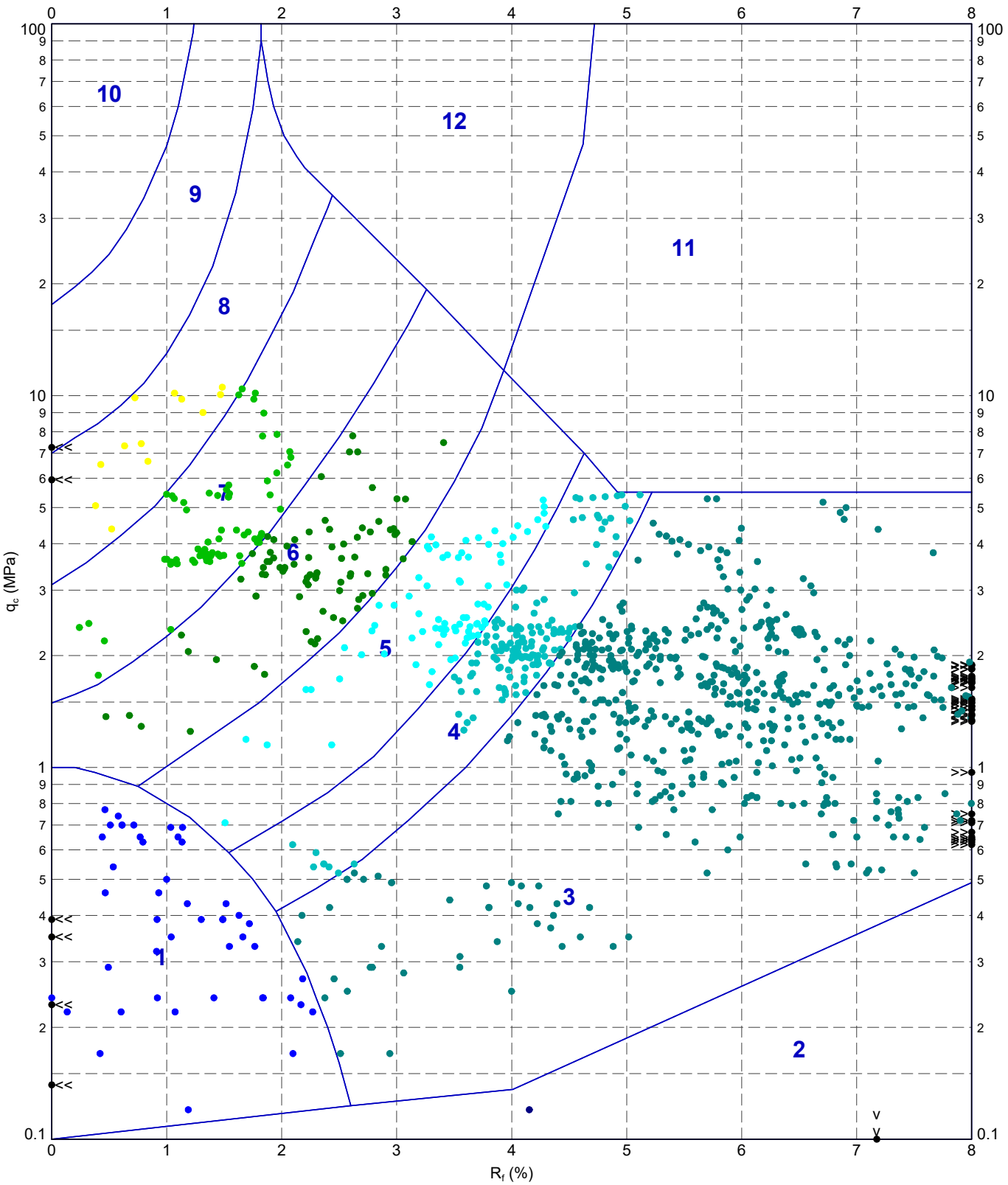
PointID	<b>CPT05</b>
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>363 mV</td> <td>358 mV</td> <td>-0.055 MPa</td> </tr> <tr> <td>Sleeve</td> <td>291 mV</td> <td>284 mV</td> <td>-0.005 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>218 mV</td> <td>218 mV</td> <td>0 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2641 mV</td> <td>2643 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	363 mV	358 mV	-0.055 MPa	Sleeve	291 mV	284 mV	-0.005 kPa	Pore Pressure 2	218 mV	218 mV	0 kPa	X-Y Inclinator	2641 mV	2643 mV		Groundwater Level Dissipation Test
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METHOD: Robertson et al. 1986 qc Rf

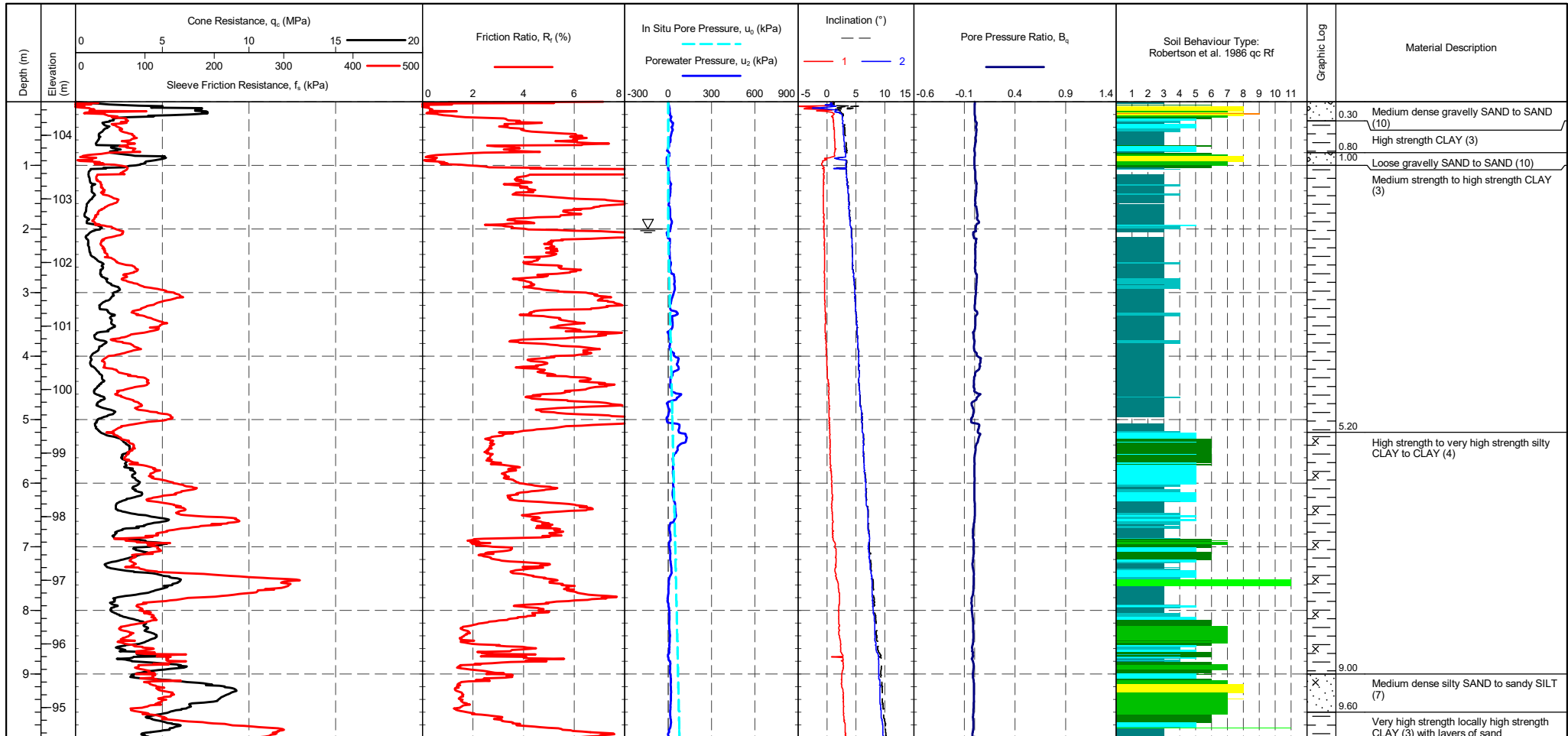
- 1 - Sensitive fine grained material
- 4 - Silty CLAY to CLAY
- 7 - Silty SAND to sandy SILT
- 10 - Gravelly SAND to SAND
- 2 - Organic material
- 5 - Clayey SILT to silty CLAY
- 8 - SAND to silty SAND
- 11 - Very stiff fine grained
- 3 - CLAY
- 6 - Sandy SILT to clayey SILT
- 9 - SAND
- 12 - SAND to clayey SAND

	TITLE	DRAWN	DATE
	Delta Simons Cordby Corby	CHECKED	DATE
	Robertson et al. 1986 qc vs. Rf - CPT05	SCALE	FIGURE No
		PROJECT No 1220144	A4



PointID	<b>CPT05A</b>
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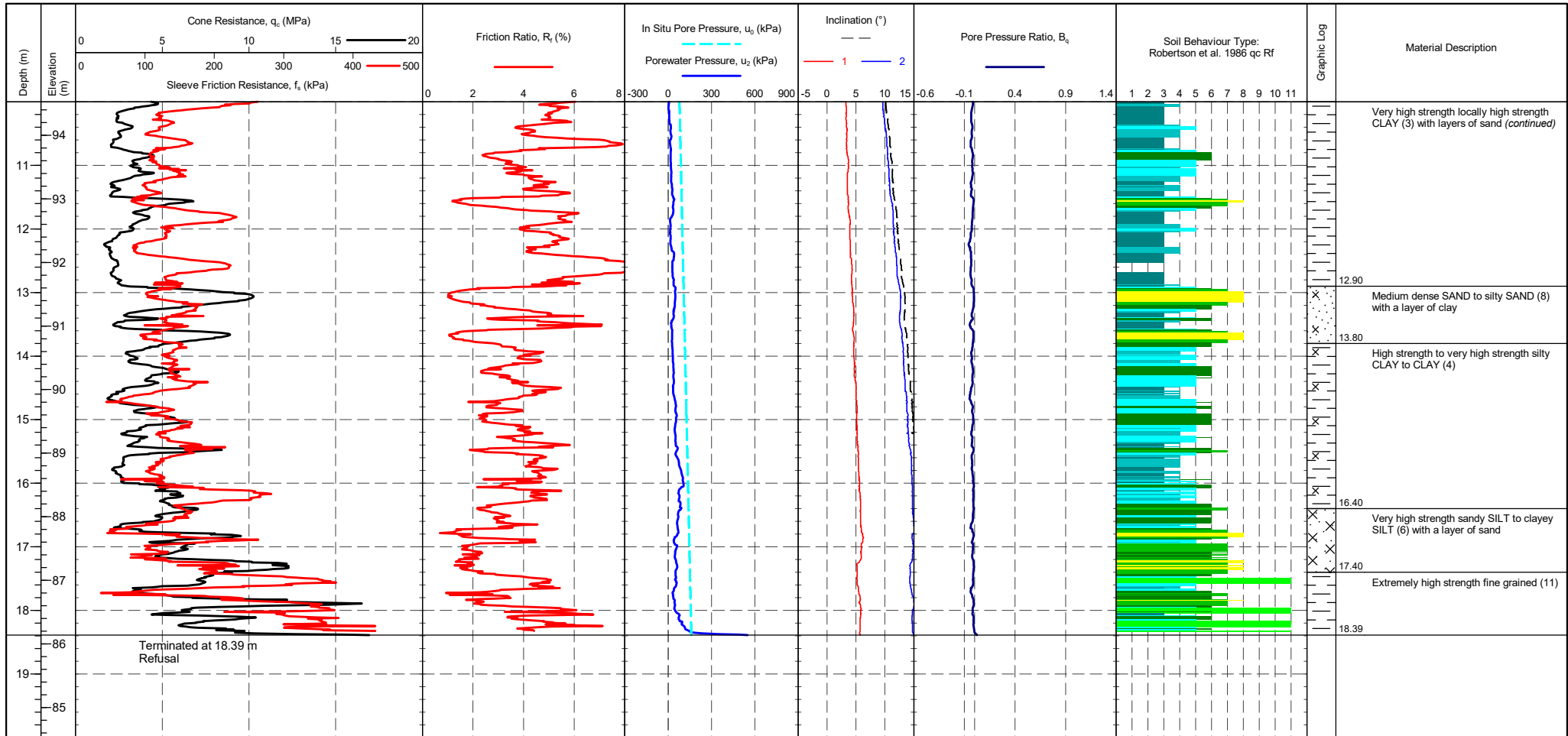
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip: Pre 360 mV, Post 359 mV, Difference -0.011 MPa Sleeve: Pre 286 mV, Post 284 mV, Difference -0.001 kPa Pore Pressure 2: Pre 225 mV, Post 294 mV, Difference 0.016 kPa X-Y Inclinator: Pre 2529 mV, Post 2633 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravelly SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID	<b>CPT05A</b>
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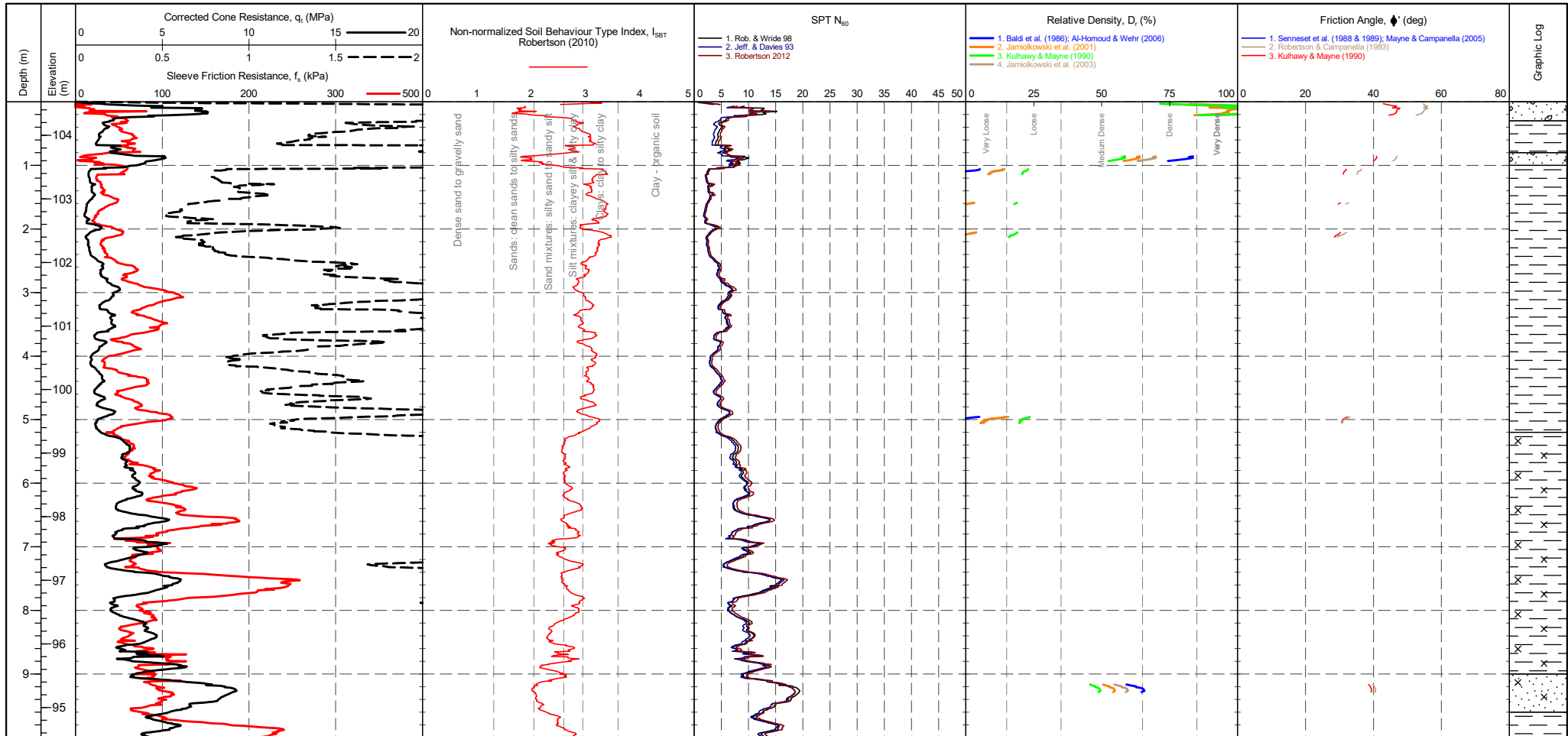
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PointID  
**CPT05A**

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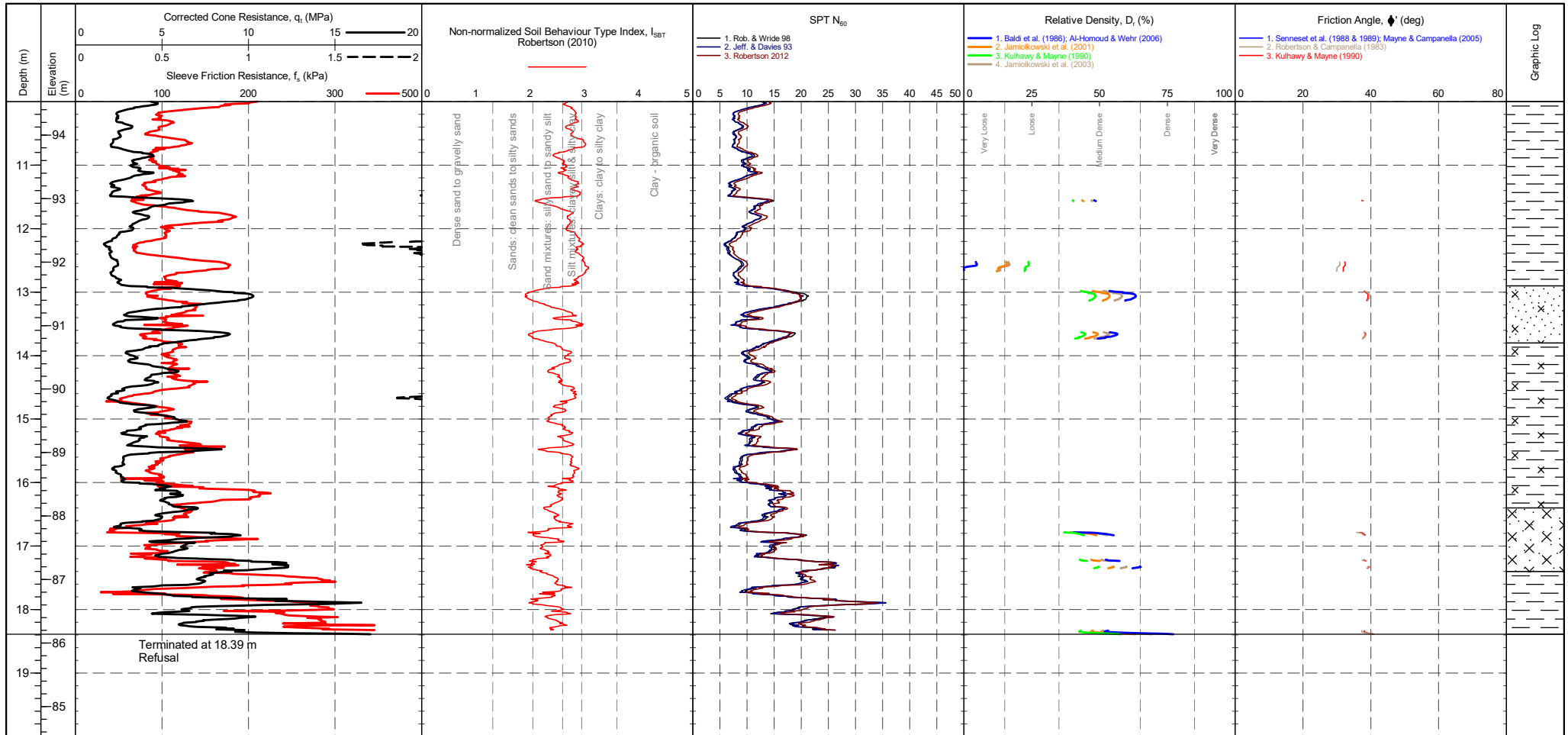


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PointID

**CPT05A**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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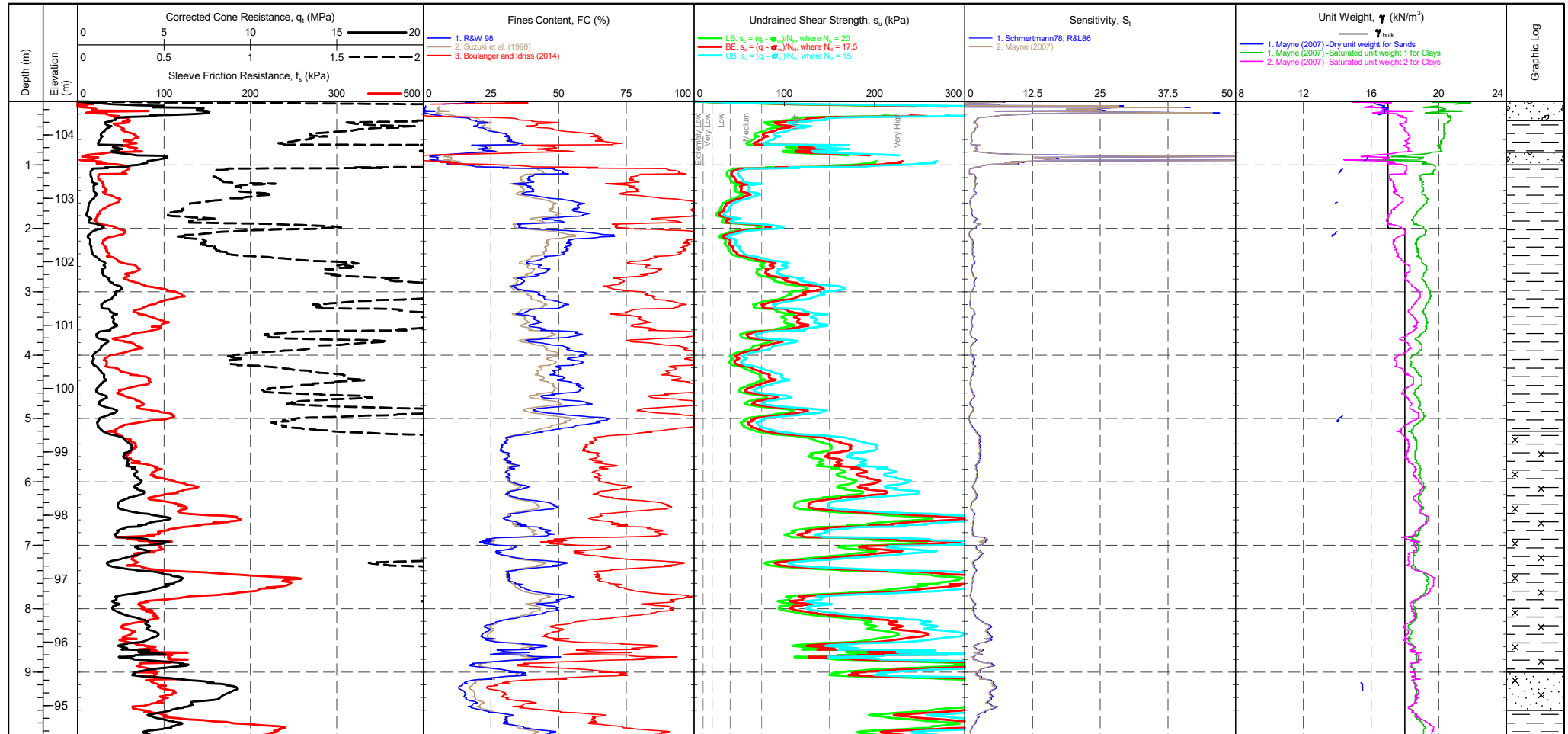


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> <b>Tip</b> : 360 mV <b>Sleeve</b> : 286 mV <b>Pore Pressure 2</b> : 225 mV <b>X-Y inclinometer</b> : 2529 mV	<b>CPTU ZERO VALUES</b> <b>Post</b> : 359 mV <b>Difference</b> : -0.011 MPa <b>284 mV</b> <b>294 mV</b> <b>2633 mV</b>	<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, <math>I_c</math></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density <math>D_r</math> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, $I_c$	Description	SPT N value, NSPT	Description	Relative Density $D_r$ (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
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CPT05A

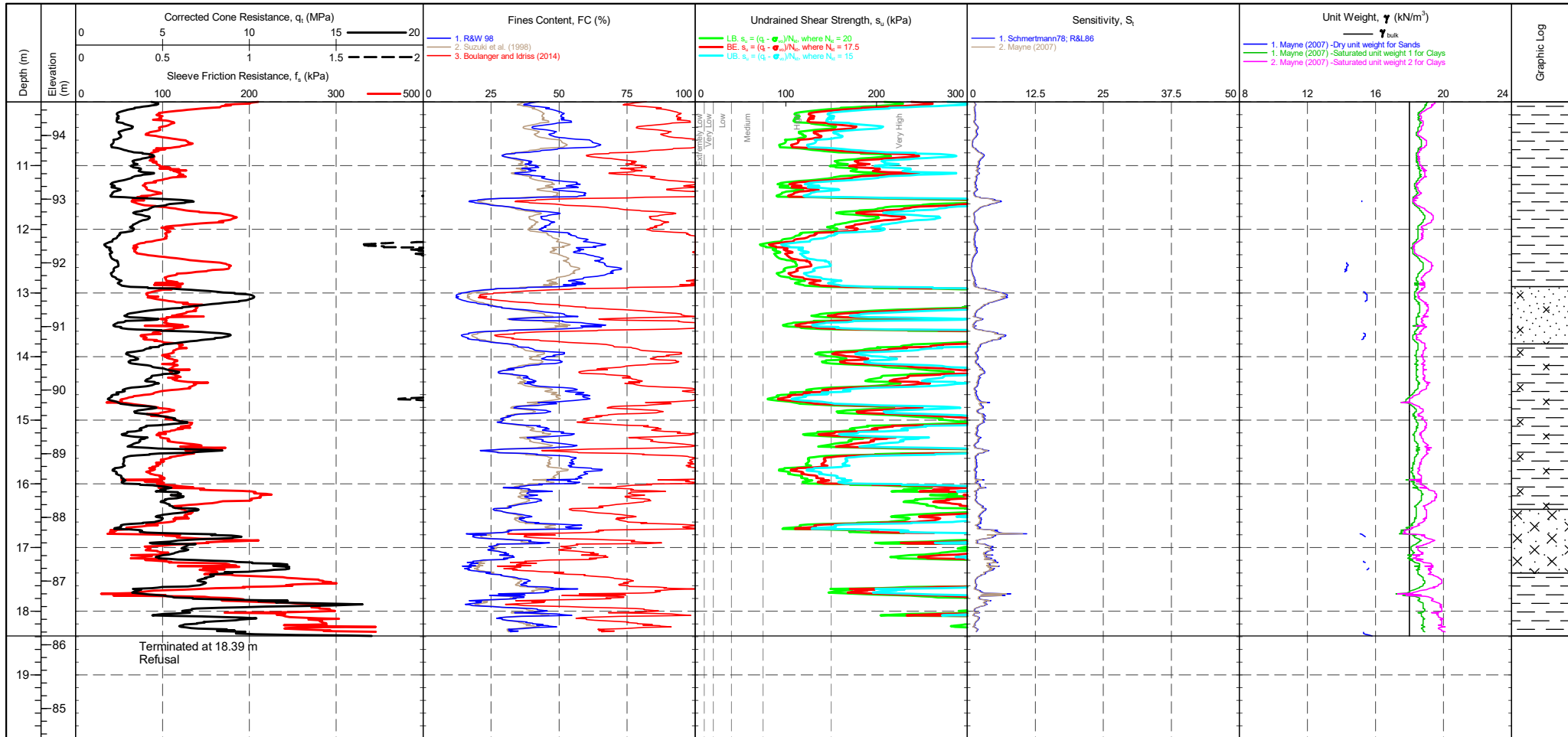
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 360 mV Sleeve: 286 mV Pore Pressure 2: 225 mV X-Y Inclinator: 2529 mV	<b>CPTU ZERO VALUES</b> Pre: 359 mV Post: 284 mV Difference: -0.011 MPa 294 mV 0.016 kPa 2633 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement su (kPa) Extremely low strength <10 Very low strength 10-20 Low strength 20-40	Term based on measurement su (kPa) Medium strength 40-75 High strength 75-150 Very high strength 150-300 Extremely high strength >300	Groundwater Level Dissipation Test
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PointID	<b>CPT05A</b>
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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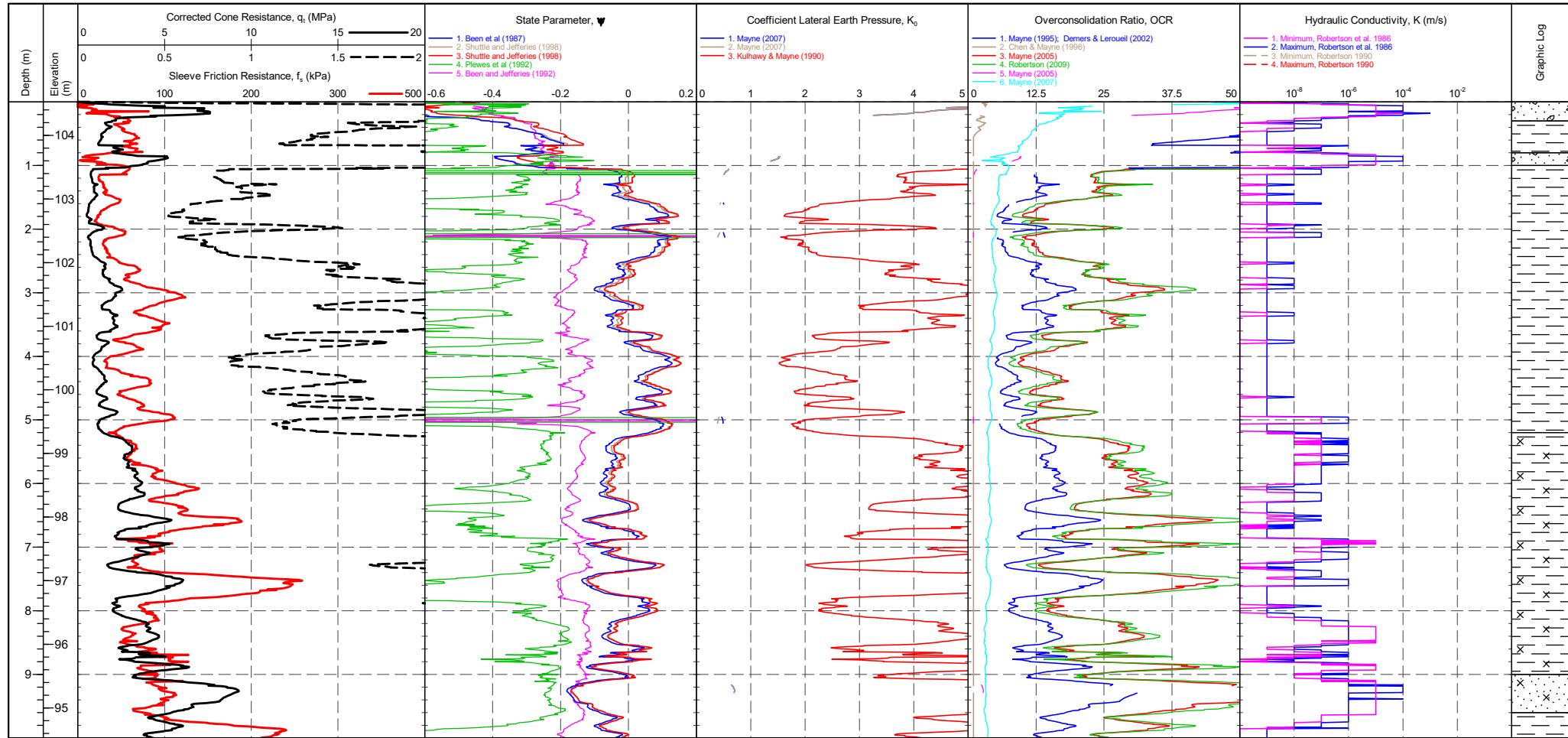


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 360 mV Sleeve: 286 mV Pore Pressure 2: 225 mV X-Y Inclinator: 2529 mV	<b>CPTU ZERO VALUES</b> Post: 359 mV Difference: -0.011 MPa 284 mV -0.001 kPa 294 mV 0.016 kPa 2633 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement su (kPa) Extremely low strength <10 Very low strength 10-20 Low strength 20-40	Term based on measurement su (kPa) Medium strength 40-75 High strength 75-150 Very high strength 150-300 Extremely high strength >300	Groundwater Level Dissipation Test
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PointID  
**CPT05A**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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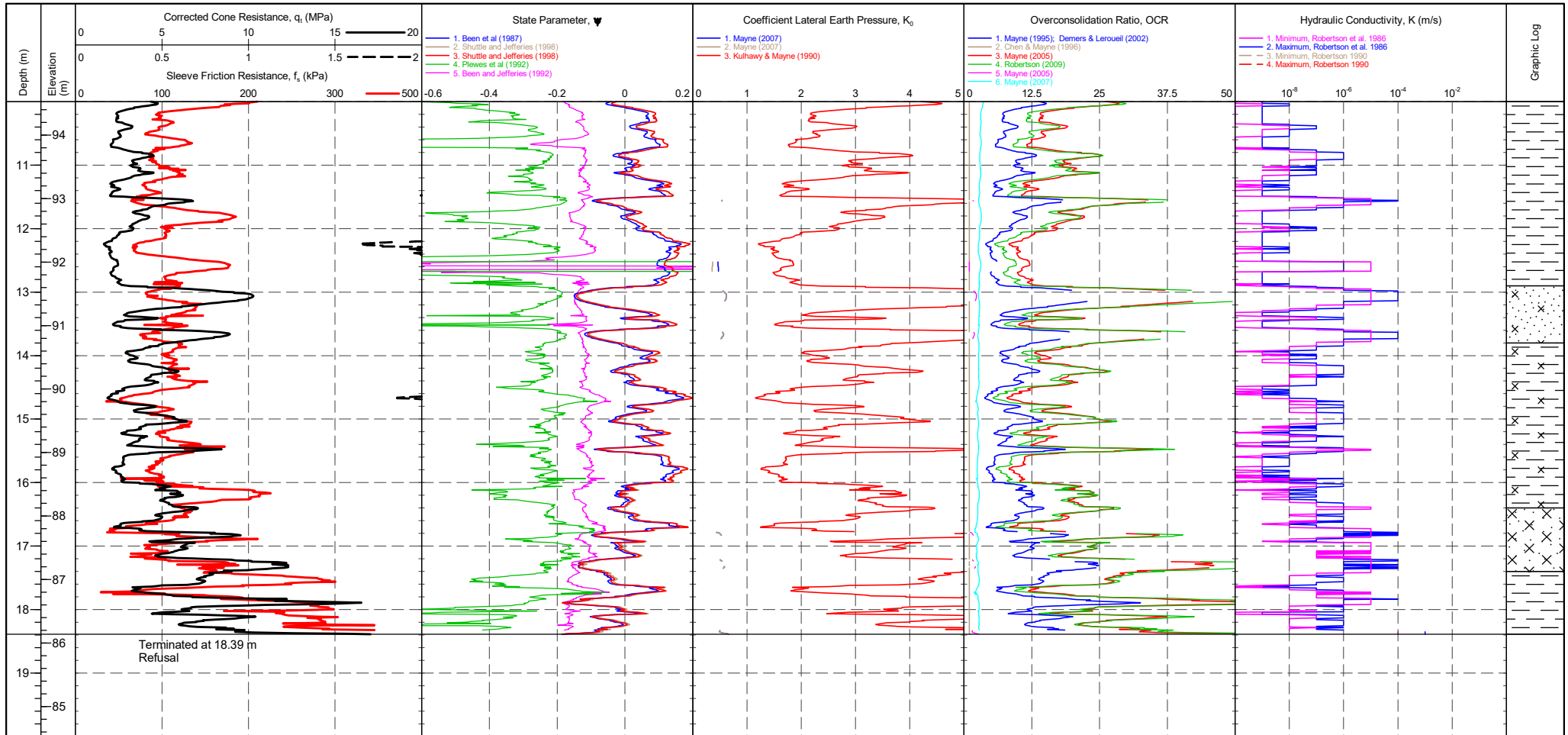
<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>360 mV</td> <td>359 mV</td> <td>-0.011 MPa</td> </tr> <tr> <td>Sleeve</td> <td>286 mV</td> <td>284 mV</td> <td>-0.001 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>225 mV</td> <td>294 mV</td> <td>0.016 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2529 mV</td> <td>2633 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	360 mV	359 mV	-0.011 MPa	Sleeve	286 mV	284 mV	-0.001 kPa	Pore Pressure 2	225 mV	294 mV	0.016 kPa	X-Y Inclinator	2529 mV	2633 mV		Groundwater Level Dissipation Test
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PointID

CPT05A

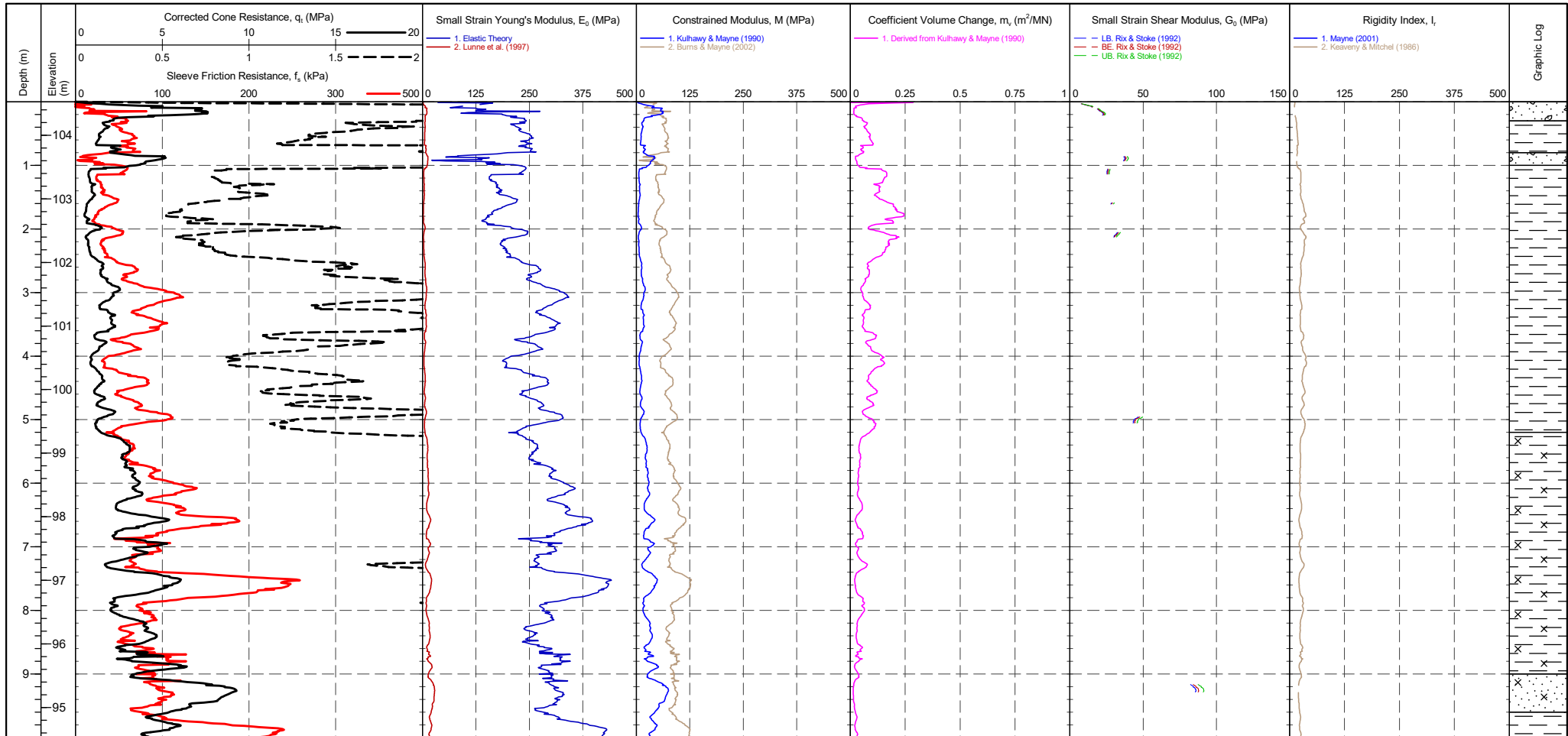
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 360 mV Sleeve: 286 mV Pore Pressure 2: 225 mV X-Y Inclinator: 2529 mV	<b>CPTU ZERO VALUES</b> Pre: 359 mV Post: 284 mV Difference: 294 mV Difference: 2633 mV	Groundwater Level Dissipation Test
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PointID  
**CPT05A**

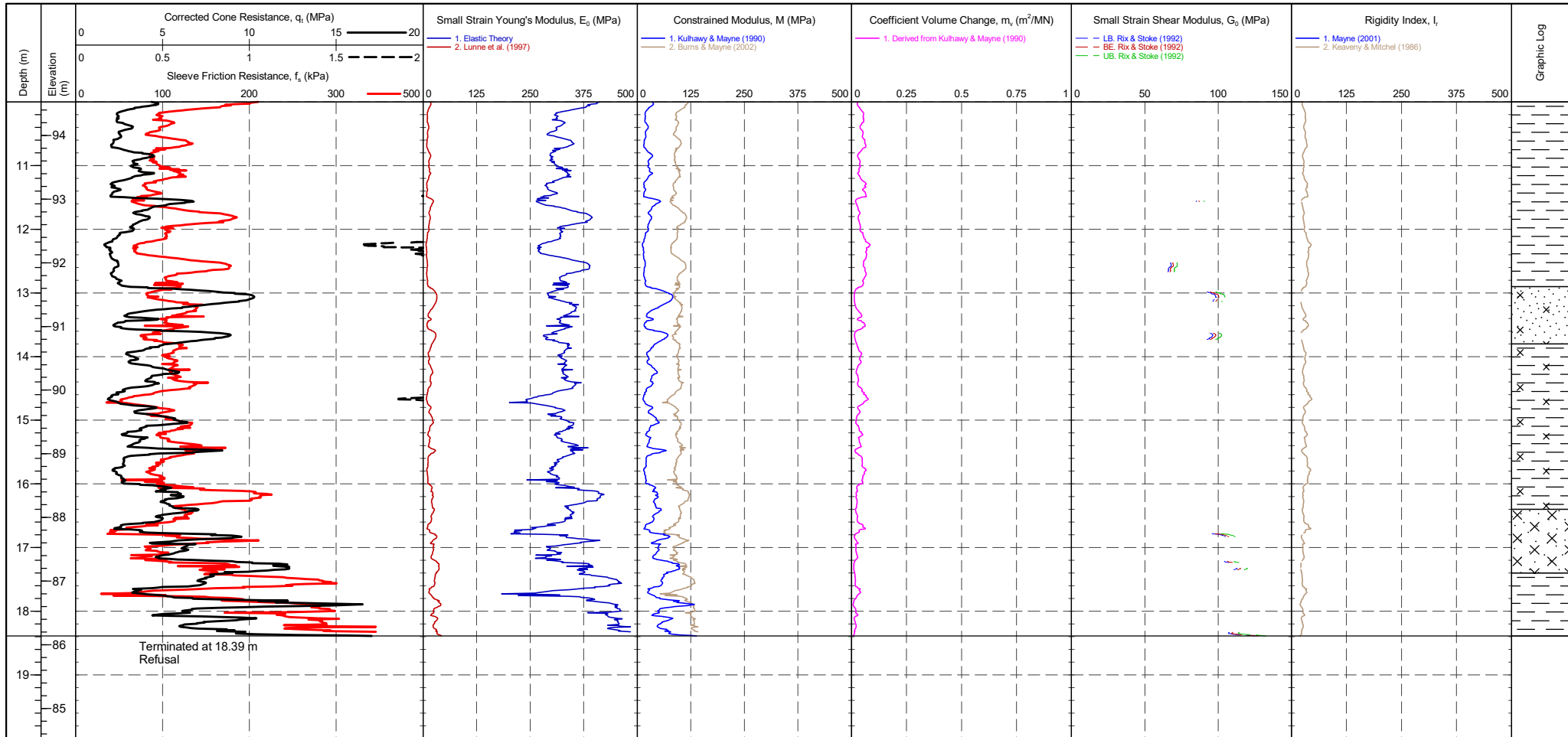
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>360 mV</td> <td>359 mV</td> <td>-0.011 MPa</td> </tr> <tr> <td>Sleeve</td> <td>286 mV</td> <td>284 mV</td> <td>-0.001 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>225 mV</td> <td>294 mV</td> <td>0.016 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2529 mV</td> <td>2633 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	360 mV	359 mV	-0.011 MPa	Sleeve	286 mV	284 mV	-0.001 kPa	Pore Pressure 2	225 mV	294 mV	0.016 kPa	X-Y Inclinator	2529 mV	2633 mV		Groundwater Level Dissipation Test
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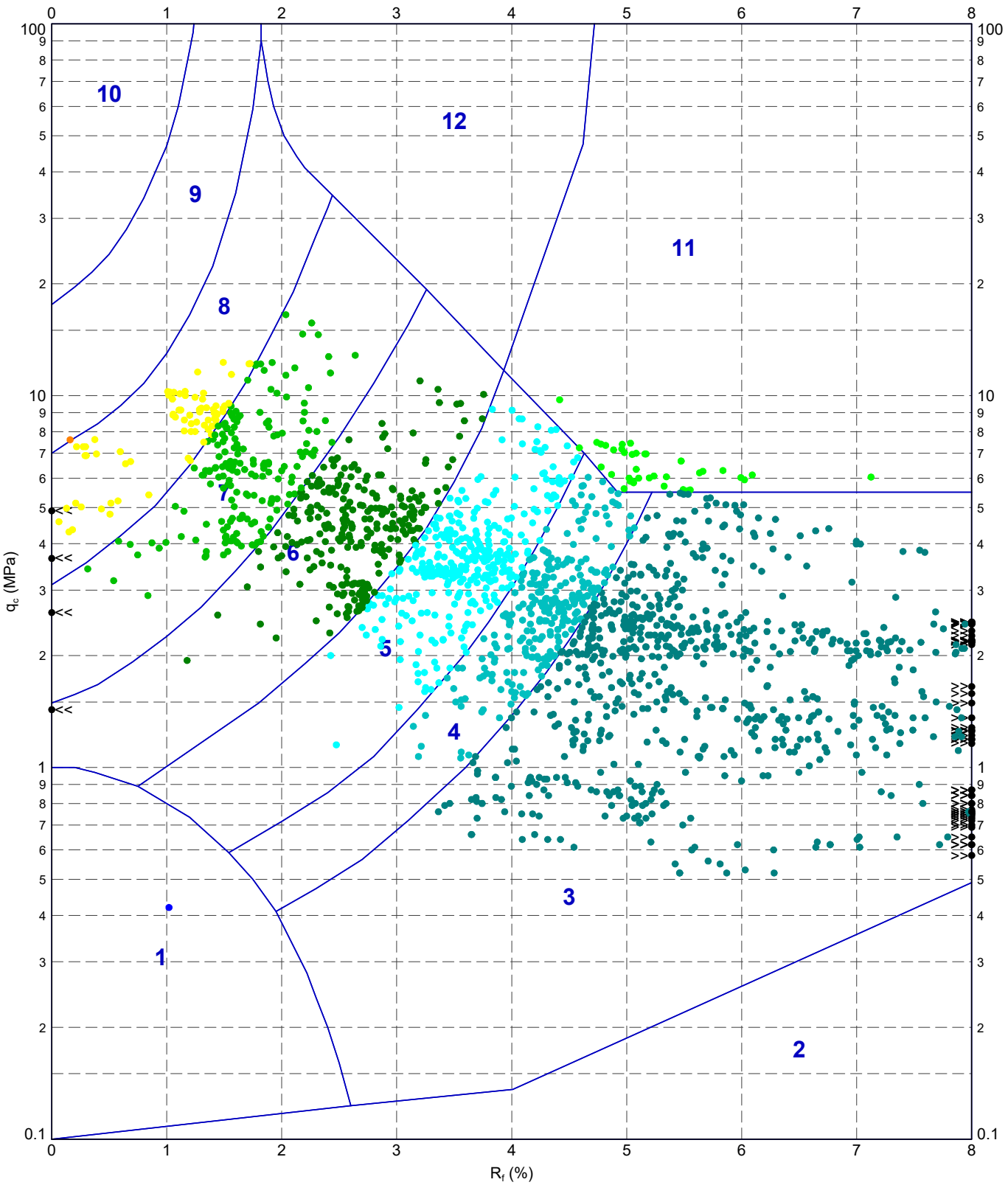
PointID	<b>CPT05A</b>
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491009.419 m <b>NORTHING</b> : 290857.935 m <b>ELEVATION</b> : 104.527 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> Transducer Pre Post Difference Tip 360 mV 359 mV -0.011 MPa Sleeve 286 mV 284 mV -0.001 kPa Pore Pressure 2 225 mV 294 mV 0.016 kPa X-Y inclinometer 2529 mV 2633 mV	Groundwater Level Dissipation Test
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220228-ADVANCED REPORT INSTITUTE 2.02.1 LIB - CHLOE.GLB Graph CPT ROBERTSON ET AL. 8F QC VS. RF APF 1220144 CORBY DELTA SIMONS G.P.J. <<DrawingFile>> 04/03/2022 16:11 10.01.00.11 Datagel Lab and In Situ Tool - DGD [Lib: In Situ SI 2.02.0 2017-07-10 Proj: In Situ SI 2.02.0 2017-07-10]



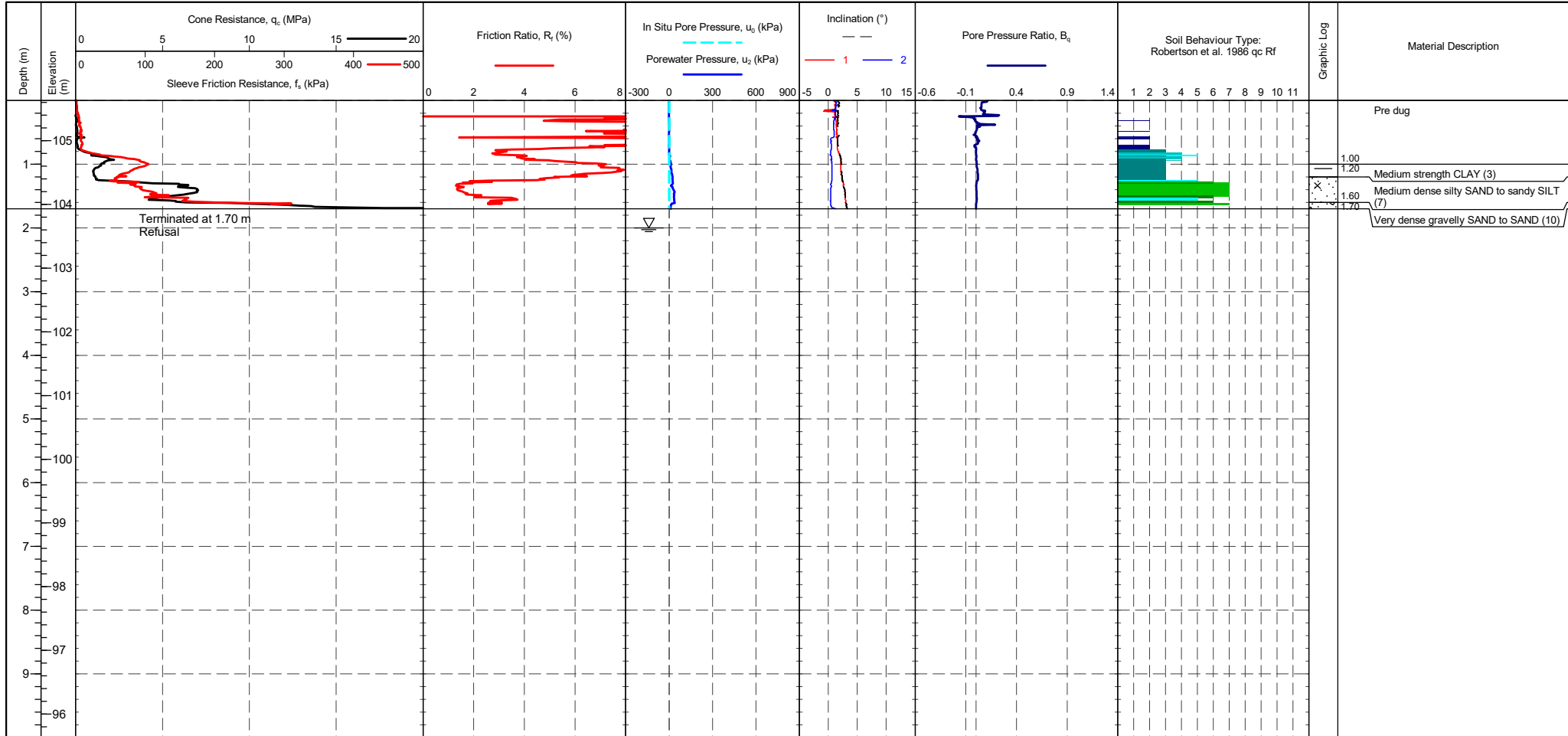
**METHOD: Robertson et al. 1986 qc Rf**

1 - Sensitive fine grained material	4 - Silty CLAY to CLAY	7 - Silty SAND to sandy SILT	10 - Gravelly SAND to SAND
2 - Organic material	5 - Clayey SILT to silty CLAY	8 - SAND to silty SAND	11 - Very stiff fine grained
3 - CLAY	6 - Sandy SILT to clayey SILT	9 - SAND	12 - SAND to clayey SAND

	TITLE	DRAWN	DATE
	Delta Simons Cordby Corby	CHECKED	DATE
	Robertson et al. 1986 qc vs. Rf - CPT05A	SCALE	Not To Scale
		PROJECT No 1220144	FIGURE No
			A4

PointID	<b>CPT06</b>
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490993.287 m <b>NORTHING</b> : 290892.523 m <b>ELEVATION</b> : 105.632 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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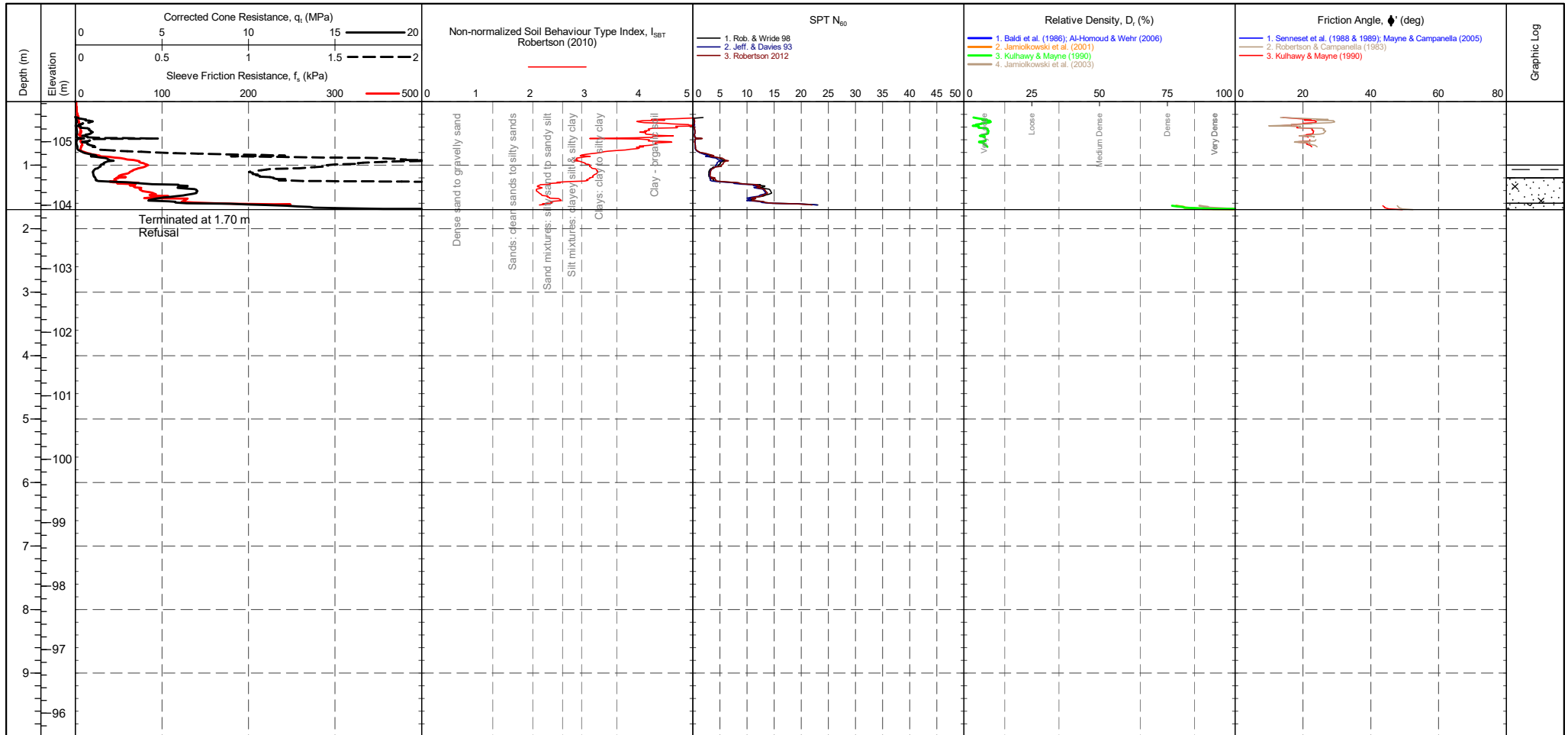
Depth (m)	Material Description
105.632	Pre dug
1.00	Medium strength CLAY (3)
1.20	Medium dense silty SAND to sandy SILT (7)
1.60	Very dense gravelly SAND to SAND (10)

<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip: Pre 388 mV, Post 390 mV, Difference 0.022 MPa Sleeve: Pre 286 mV, Post 286 mV, Difference 0 kPa Pore Pressure 2: Pre 246 mV, Post 195 mV, Difference -0.012 kPa X-Y Inclinator: Pre 2631 mV, Post 2622 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravelly SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID

**CPT06**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490993.287 m <b>NORTHING</b> : 290892.523 m <b>ELEVATION</b> : 105.632 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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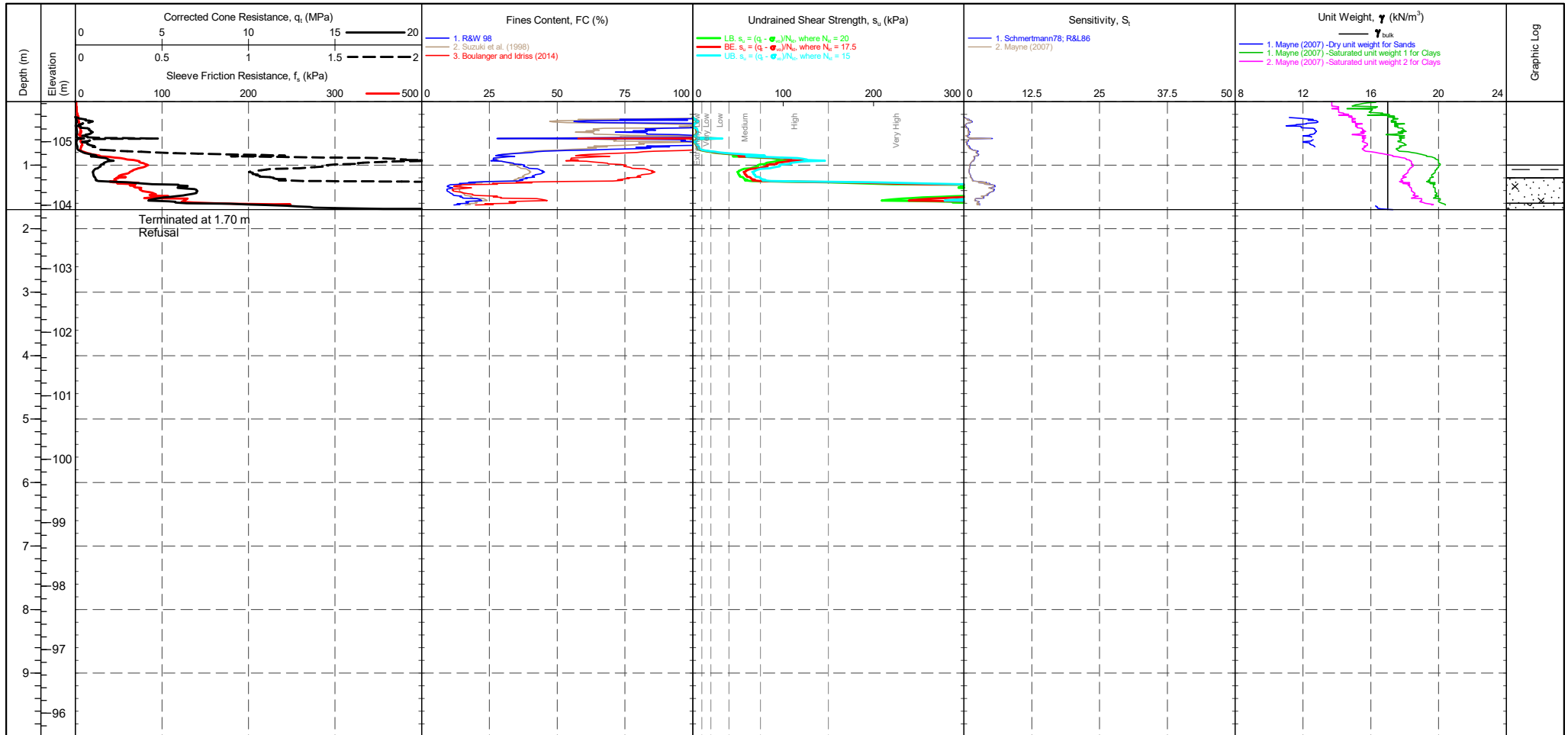


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>388 mV</td> <td>390 mV</td> <td>0.022 MPa</td> </tr> <tr> <td>Sleeve</td> <td>286 mV</td> <td>286 mV</td> <td>0 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>246 mV</td> <td>195 mV</td> <td>-0.012 kPa</td> </tr> <tr> <td>X-Y inclinometer</td> <td>2631 mV</td> <td>2622 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	388 mV	390 mV	0.022 MPa	Sleeve	286 mV	286 mV	0 kPa	Pore Pressure 2	246 mV	195 mV	-0.012 kPa	X-Y inclinometer	2631 mV	2622 mV		<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, I<sub>c</sub></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density D<sub>r</sub> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, I <sub>c</sub>	Description	SPT N value, NSPT	Description	Relative Density D <sub>r</sub> (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
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PointID

**CPT06**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490993.287 m <b>NORTHING</b> : 290892.523 m <b>ELEVATION</b> : 105.632 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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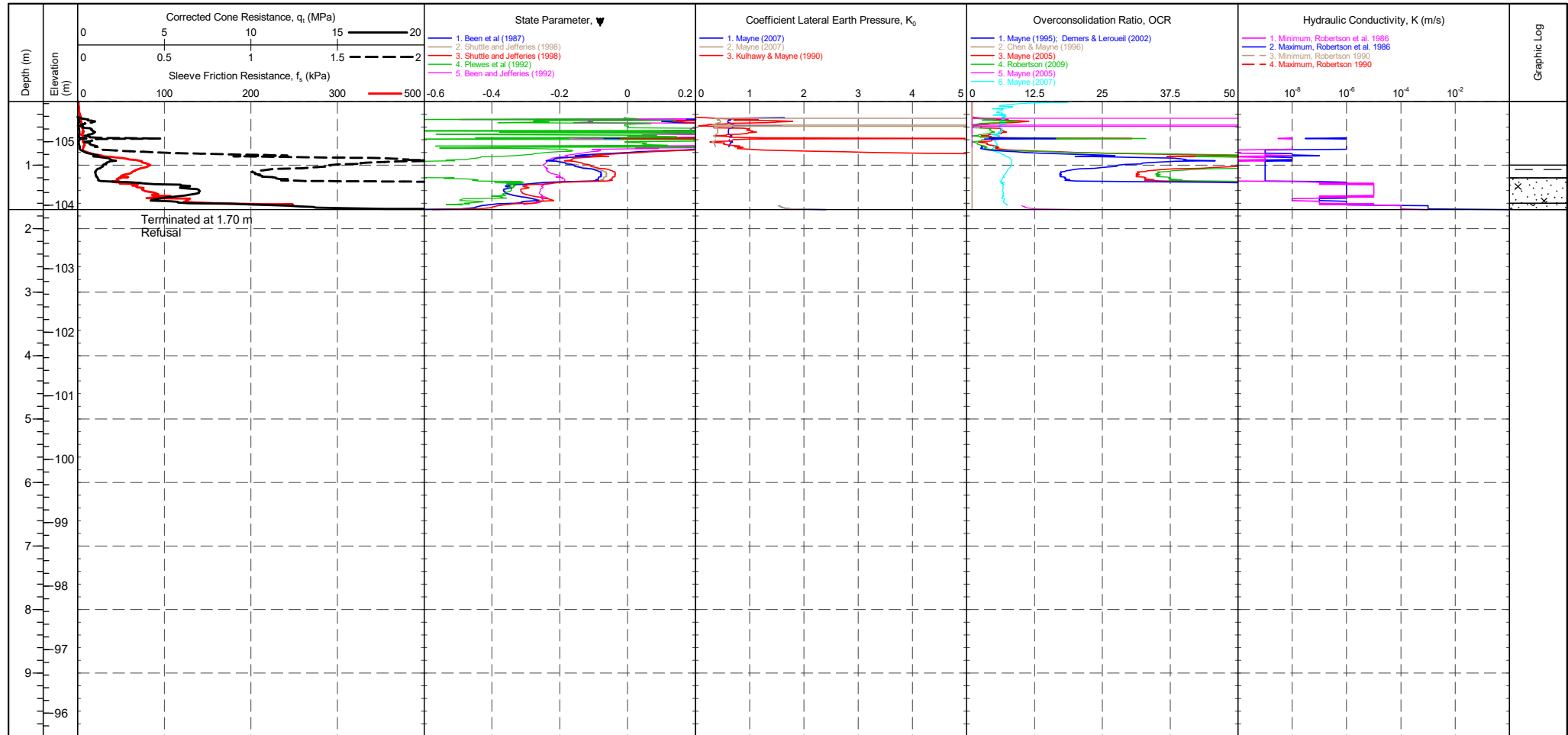
<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> Transducer Pre Post Difference Tip 388 mV 390 mV 0.022 MPa Sleeve 286 mV 286 mV 0 kPa Pore Pressure 2 246 mV 195 mV -0.012 kPa X-Y Inclinator 2631 mV 2622 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement $s_u$ (kPa)   Term based on measurement $s_u$ (kPa) Extremely low strength <10   Medium strength 40-75 Very low strength 10-20   High strength 75-150 Low strength 20-40   Very high strength 150-300   Extremely high strength >300	▽ Groundwater Level ▭ Dissipation Test
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PointID

CPT06

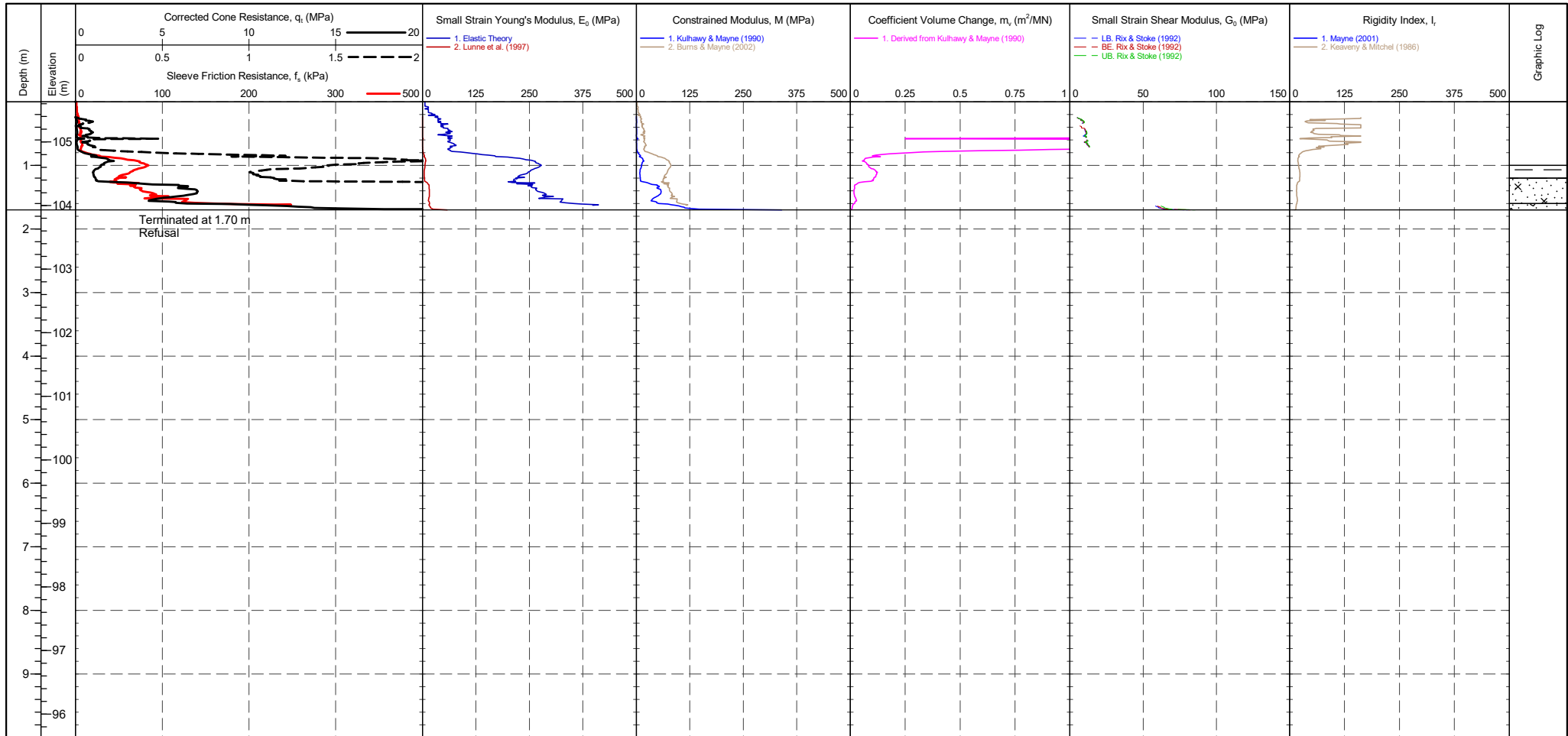
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490993.287 m <b>NORTHING</b> : 290892.523 m <b>ELEVATION</b> : 105.632 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>388 mV</td> <td>390 mV</td> <td>0.022 MPa</td> </tr> <tr> <td>Sleeve</td> <td>286 mV</td> <td>286 mV</td> <td>0 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>246 mV</td> <td>195 mV</td> <td>-0.012 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2631 mV</td> <td>2622 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	388 mV	390 mV	0.022 MPa	Sleeve	286 mV	286 mV	0 kPa	Pore Pressure 2	246 mV	195 mV	-0.012 kPa	X-Y Inclinator	2631 mV	2622 mV		Groundwater Level Dissipation Test
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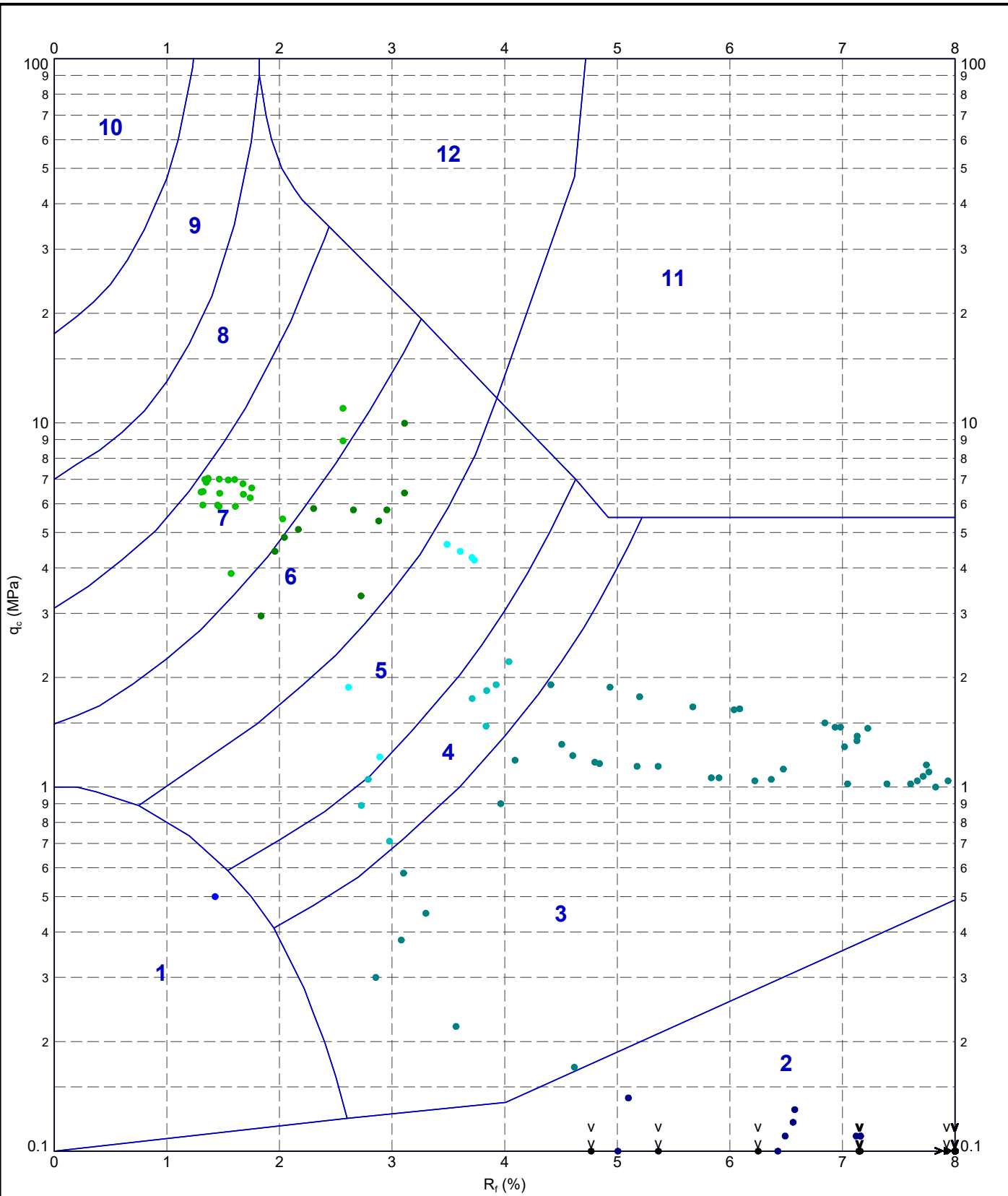
PointID  
**CPT06**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490993.287 m <b>NORTHING</b> : 290892.523 m <b>ELEVATION</b> : 105.632 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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22028-ADVANCED REPORT INSTITUTE 2.02.1 LIB - CHLOE.GLB Graph: CPT ROBERTSON ET AL. 8F QC VS. RF APF 1220144 CORBY DELTA SIMONS.GPJ <<DrawingFile>> 04/03/2022 16:15 10.01.00.11 Datagel Lab and In Situ Tool - DGD [Lib: In Situ SI 2.02.0 2017-07-10 Proj: In Situ SI 2.02.0 2017-07-10]



METHOD: Robertson et al. 1986  $q_c$   $R_f$

- 1 - Sensitive fine grained material
- 4 - Silty CLAY to CLAY
- 7 - Silty SAND to sandy SILT
- 10 - Gravelly SAND to SAND
- 2 - Organic material
- 5 - Clayey SILT to silty CLAY
- 8 - SAND to silty SAND
- 11 - Very stiff fine grained
- 3 - CLAY
- 6 - Sandy SILT to clayey SILT
- 9 - SAND
- 12 - SAND to clayey SAND

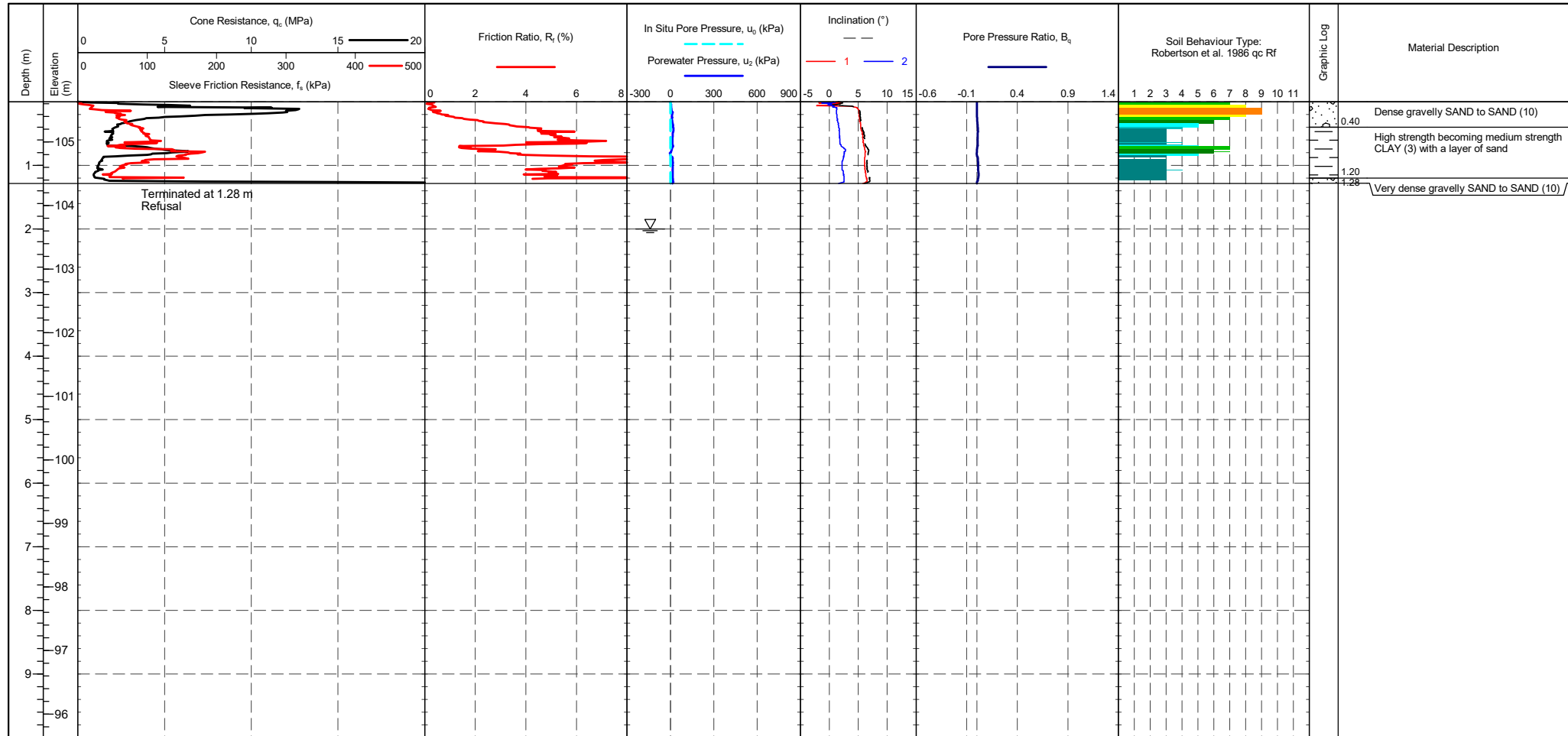


TITLE  
 Delta Simons  
 Cordby  
 Corby  
 Robertson et al. 1986  $q_c$  vs.  $R_f$  - CPT06

DRAWN	DATE	04/03/2022
CHECKED	DATE	04/03/2022
SCALE	Not To Scale	
PROJECT No	1220144	
FIGURE No	A4	

PointID	<b>CPT06A</b>
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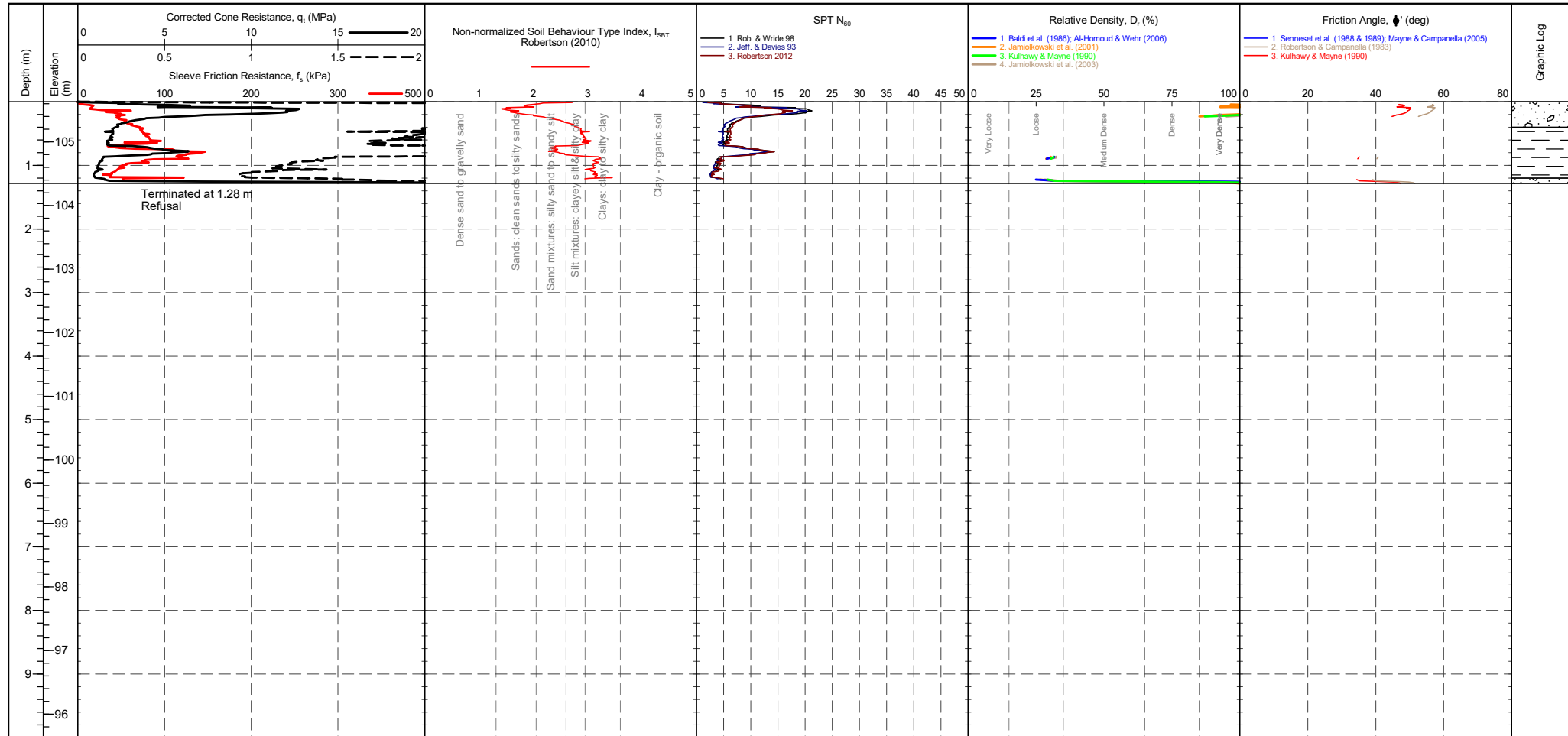
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490993.287 m <b>NORTHING</b> : 290892.523 m <b>ELEVATION</b> : 105.632 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : CPT <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip: Pre 389 mV, Post 392 mV, Difference 0.033 MPa Sleeve: Pre 288 mV, Post 289 mV, Difference 0.001 kPa Pore Pressure 2: Pre 204 mV, Post 199 mV, Difference -0.001 kPa X-Y Inclinator: Pre 2672 mV, Post 2665 mV	<b>METHOD:</b> Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravelly SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID  
**CPT06A**

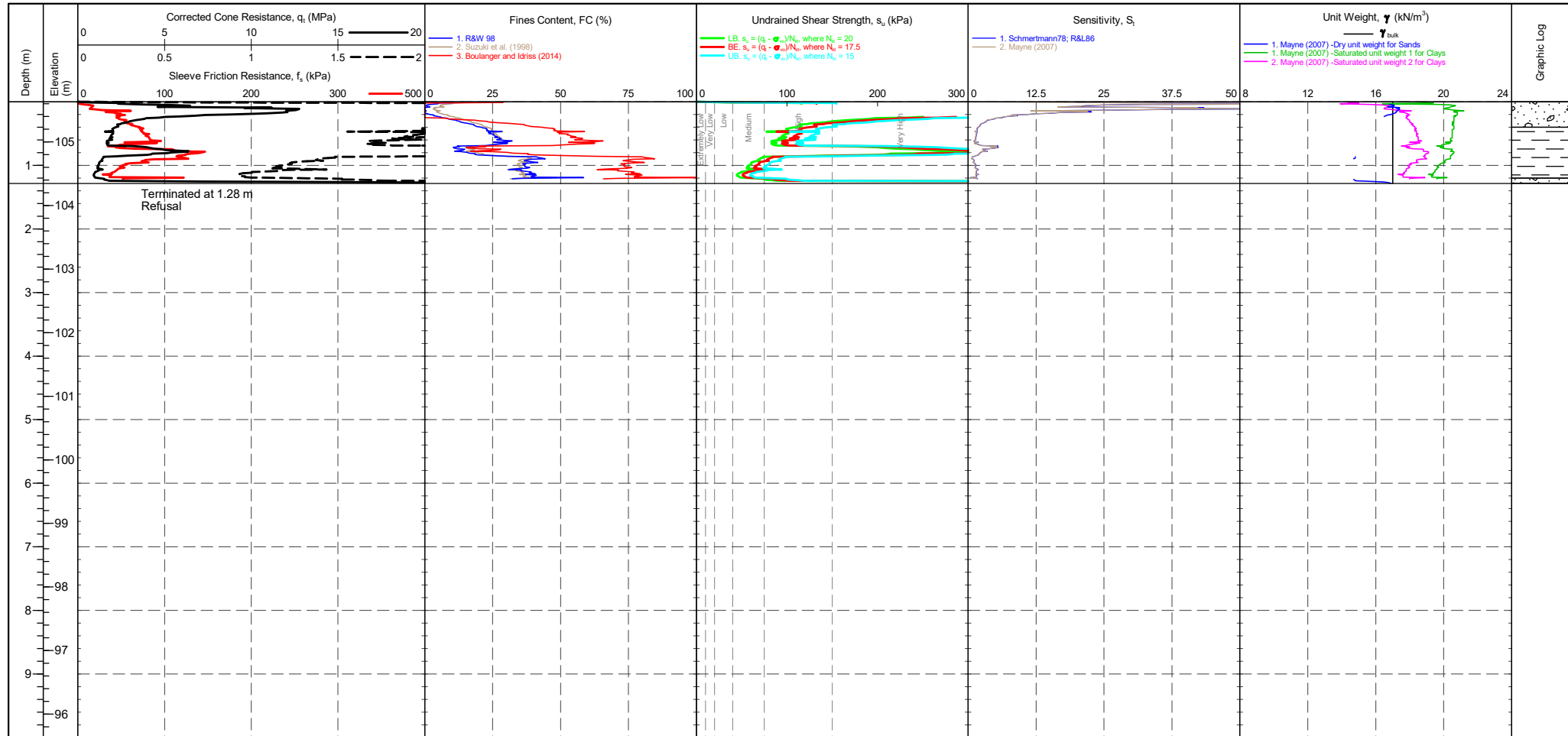
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490993.287 m <b>NORTHING</b> : 290892.523 m <b>ELEVATION</b> : 105.632 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>389 mV</td> <td>392 mV</td> <td>0.033 MPa</td> </tr> <tr> <td>Sleeve</td> <td>288 mV</td> <td>289 mV</td> <td>0.001 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>204 mV</td> <td>199 mV</td> <td>-0.001 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2672 mV</td> <td>2665 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	389 mV	392 mV	0.033 MPa	Sleeve	288 mV	289 mV	0.001 kPa	Pore Pressure 2	204 mV	199 mV	-0.001 kPa	X-Y Inclinator	2672 mV	2665 mV		<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, I<sub>c</sub></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density D<sub>r</sub> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, I <sub>c</sub>	Description	SPT N value, NSPT	Description	Relative Density D <sub>r</sub> (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
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PointID  
**CPT06A**

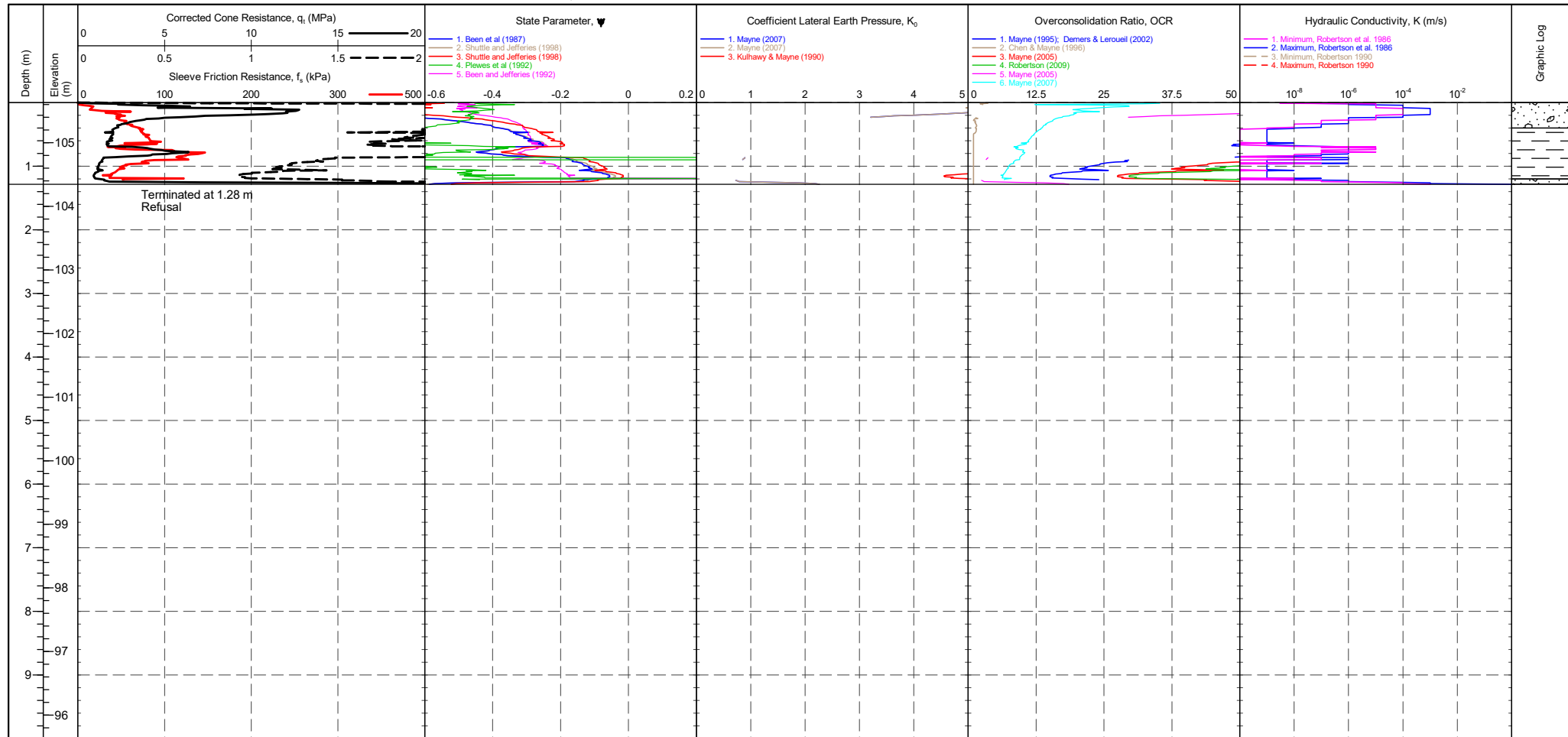
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490993.287 m <b>NORTHING</b> : 290892.523 m <b>ELEVATION</b> : 105.632 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 389 mV Sleeve: 288 mV Pore Pressure 2: 204 mV X-Y Inclinator: 2672 mV	<b>CPTU ZERO VALUES</b> Post: 392 mV Difference: 0.033 MPa 289 mV 0.001 kPa 199 mV -0.001 kPa 2665 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> <table border="1"> <tr> <th>Term based on measurement</th> <th>su (kPa)</th> <th>Term based on measurement</th> <th>su (kPa)</th> </tr> <tr> <td>Extremely low strength</td> <td>&lt;10</td> <td>Medium strength</td> <td>40-75</td> </tr> <tr> <td>Very low strength</td> <td>10-20</td> <td>High strength</td> <td>75-150</td> </tr> <tr> <td>Low strength</td> <td>20-40</td> <td>Very high strength</td> <td>150-300</td> </tr> <tr> <td></td> <td></td> <td>Extremely high strength</td> <td>&gt;300</td> </tr> </table>	Term based on measurement	su (kPa)	Term based on measurement	su (kPa)	Extremely low strength	<10	Medium strength	40-75	Very low strength	10-20	High strength	75-150	Low strength	20-40	Very high strength	150-300			Extremely high strength	>300	Groundwater Level Dissipation Test
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PointID	<b>CPT06A</b>
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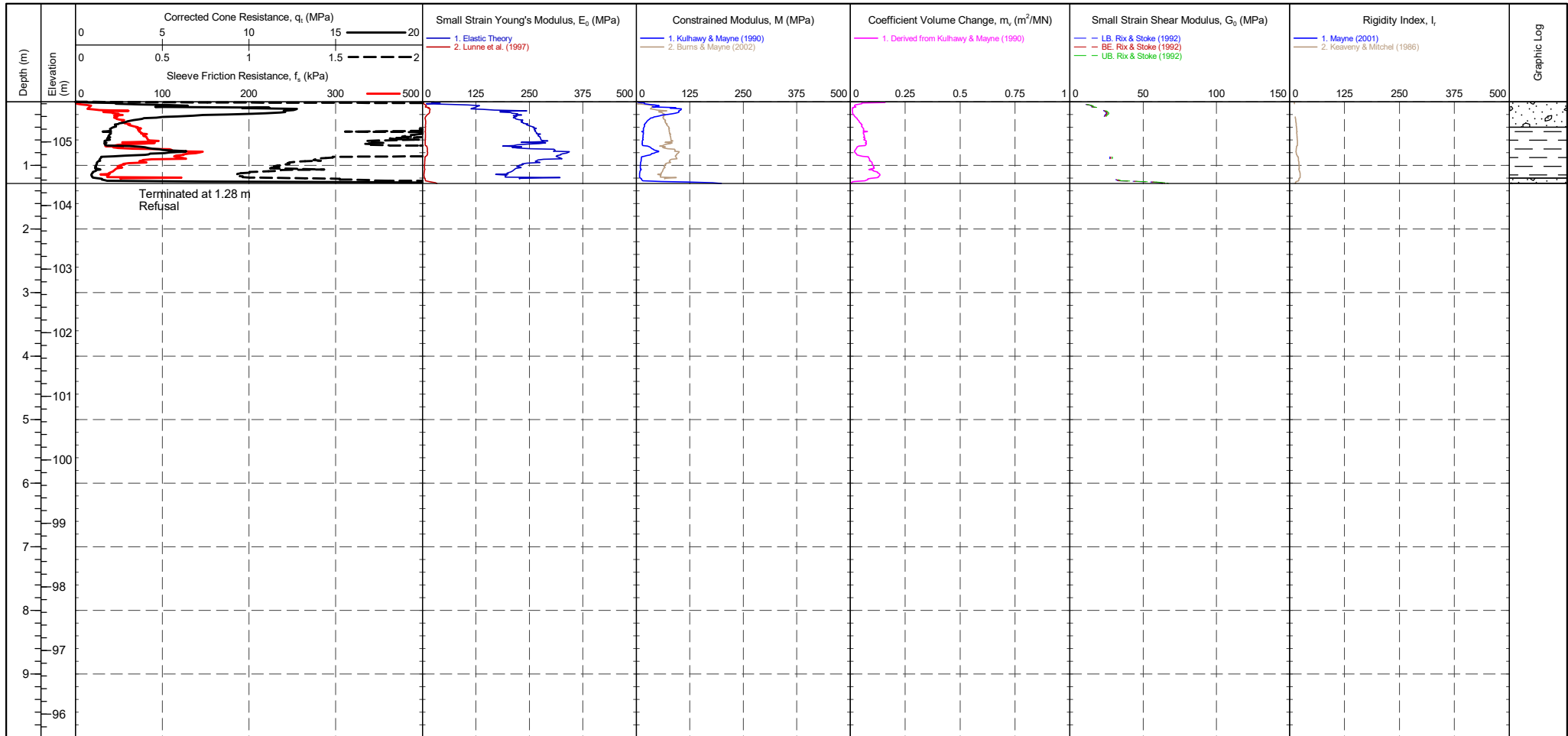


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>389 mV</td> <td>392 mV</td> <td>0.033 MPa</td> </tr> <tr> <td>Sleeve</td> <td>288 mV</td> <td>289 mV</td> <td>0.001 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>204 mV</td> <td>199 mV</td> <td>-0.001 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2672 mV</td> <td>2665 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	389 mV	392 mV	0.033 MPa	Sleeve	288 mV	289 mV	0.001 kPa	Pore Pressure 2	204 mV	199 mV	-0.001 kPa	X-Y Inclinator	2672 mV	2665 mV		Groundwater Level Dissipation Test
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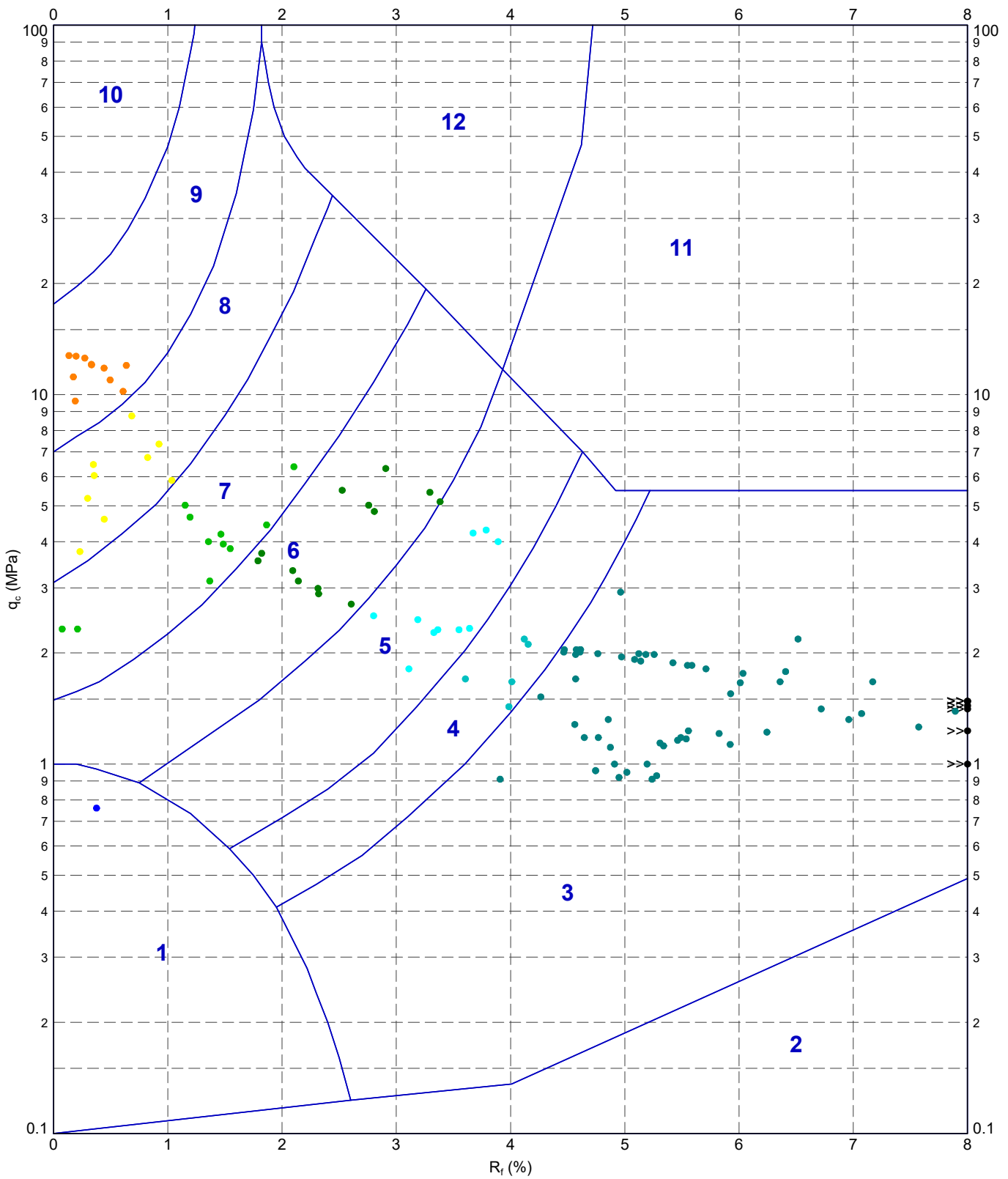
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**CPT06A**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490993.287 m <b>NORTHING</b> : 290892.523 m <b>ELEVATION</b> : 105.632 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>389 mV</td> <td>392 mV</td> <td>0.033 MPa</td> </tr> <tr> <td>Sleeve</td> <td>288 mV</td> <td>289 mV</td> <td>0.001 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>204 mV</td> <td>199 mV</td> <td>-0.001 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2672 mV</td> <td>2665 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	389 mV	392 mV	0.033 MPa	Sleeve	288 mV	289 mV	0.001 kPa	Pore Pressure 2	204 mV	199 mV	-0.001 kPa	X-Y Inclinator	2672 mV	2665 mV		Groundwater Level Dissipation Test
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220228-ADVANCED REPORT INSTITUTE 2.02.1 LIB - CHLOE.GLB Graph: CPT ROBERTSON ET AL. 8F QC VS. RF APF 1220144 CORBY DELTA SIMONS GPJ <<DrawingFile>> 04/03/2022 16:19 10.01.00.11 Datagel Lab and In Situ Tool - DGD [Lib: In Situ SI 2.02.0 2017-07-10 Proj: In Situ SI 2.02.0 2017-07-10]



METHOD: Robertson et al. 1986 qc Rf

- 1 - Sensitive fine grained material
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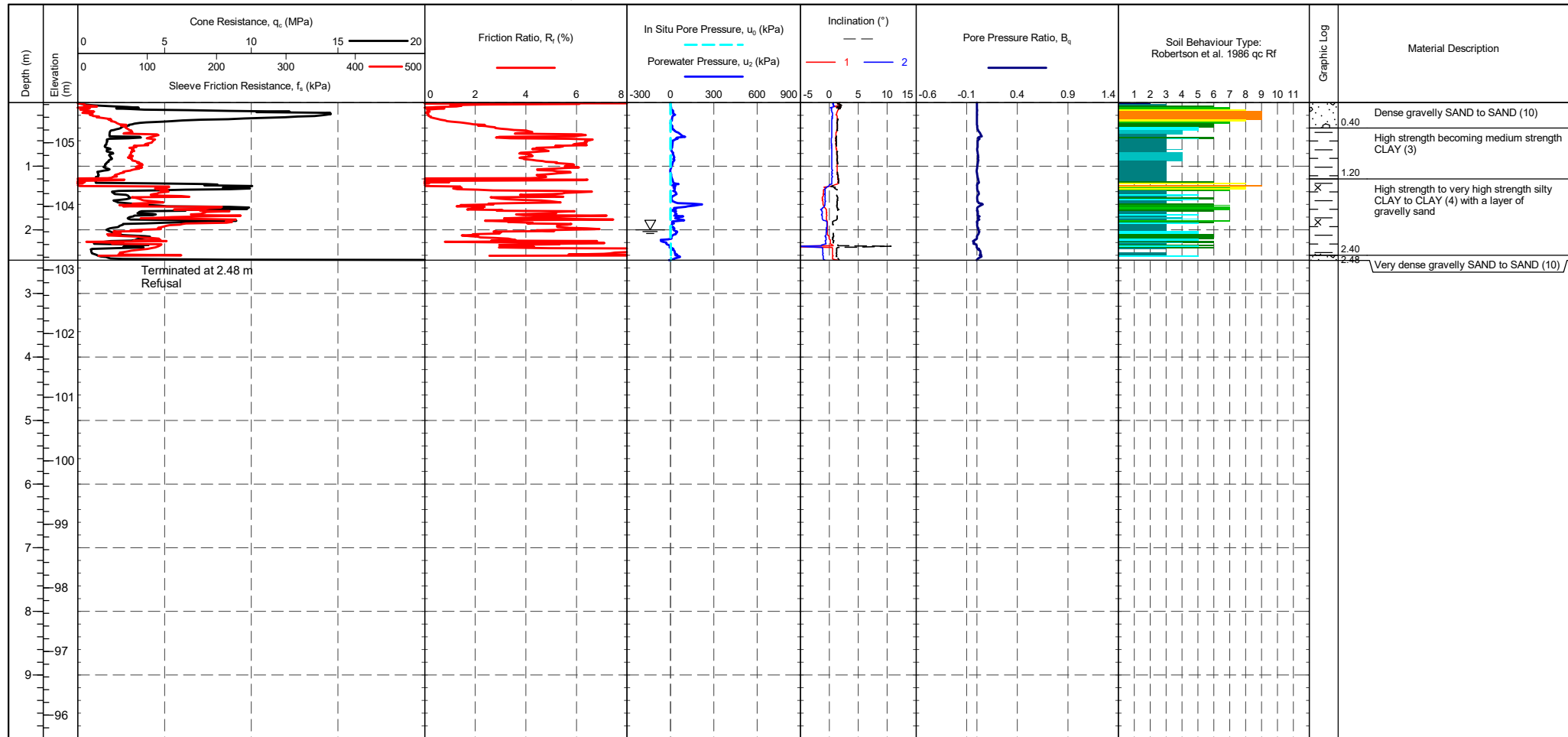


TITLE  
 Delta Simons  
 Cordby  
 Corby  
 Robertson et al. 1986 qc vs. Rf - CPT06A

DRAWN	DATE	04/03/2022
CHECKED	DATE	04/03/2022
SCALE	Not To Scale	
PROJECT No	1220144	
FIGURE No	A4	

PointID	<b>CPT06B</b>
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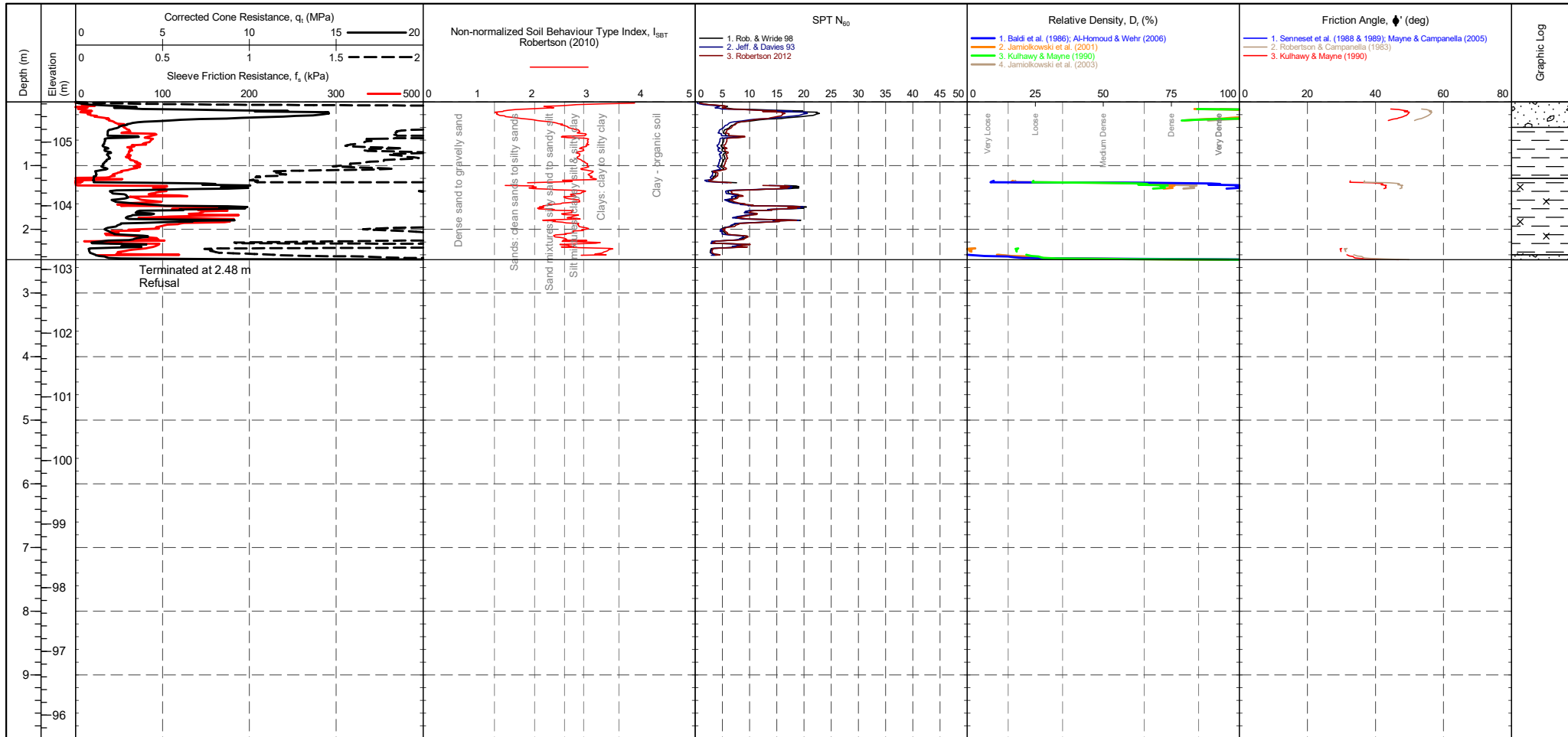
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490993.287 m <b>NORTHING</b> : 290892.523 m <b>ELEVATION</b> : 105.632 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>Transducer</b> Tip: 367 mV / 366 mV / -0.011 MPa Sleeve: 291 mV / 290 mV / -0.001 kPa Pore Pressure 2: 232 mV / 216 mV / -0.004 kPa X-Y Inclinator: 2702 mV / 2639 mV	<b>CPTU ZERO VALUES</b> Tip: 367 mV / 366 mV / -0.011 MPa Sleeve: 291 mV / 290 mV / -0.001 kPa Pore Pressure 2: 232 mV / 216 mV / -0.004 kPa X-Y Inclinator: 2702 mV / 2639 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravelly SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID  
**CPT06B**

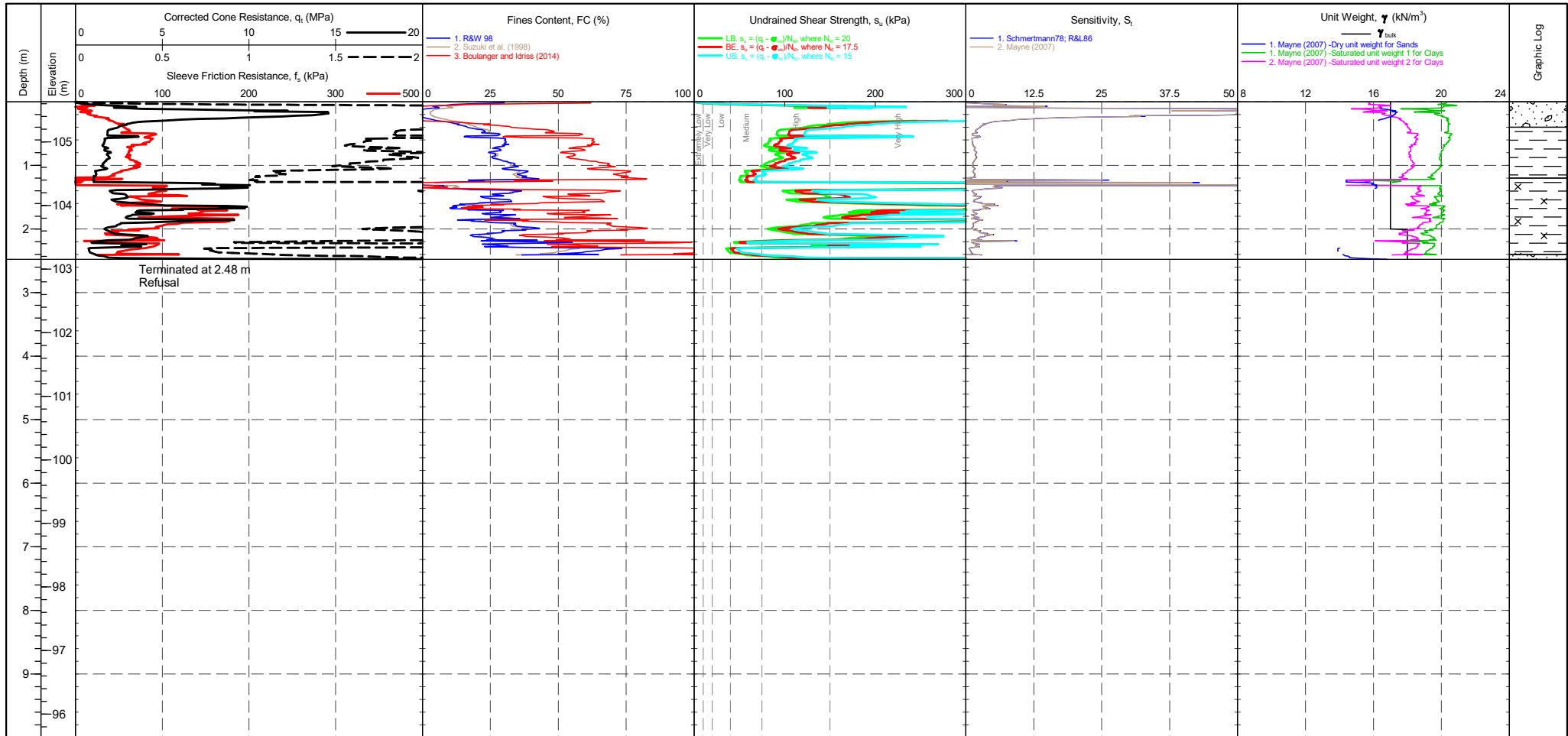
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490993.287 m <b>NORTHING</b> : 290892.523 m <b>ELEVATION</b> : 105.632 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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**CPT06B**

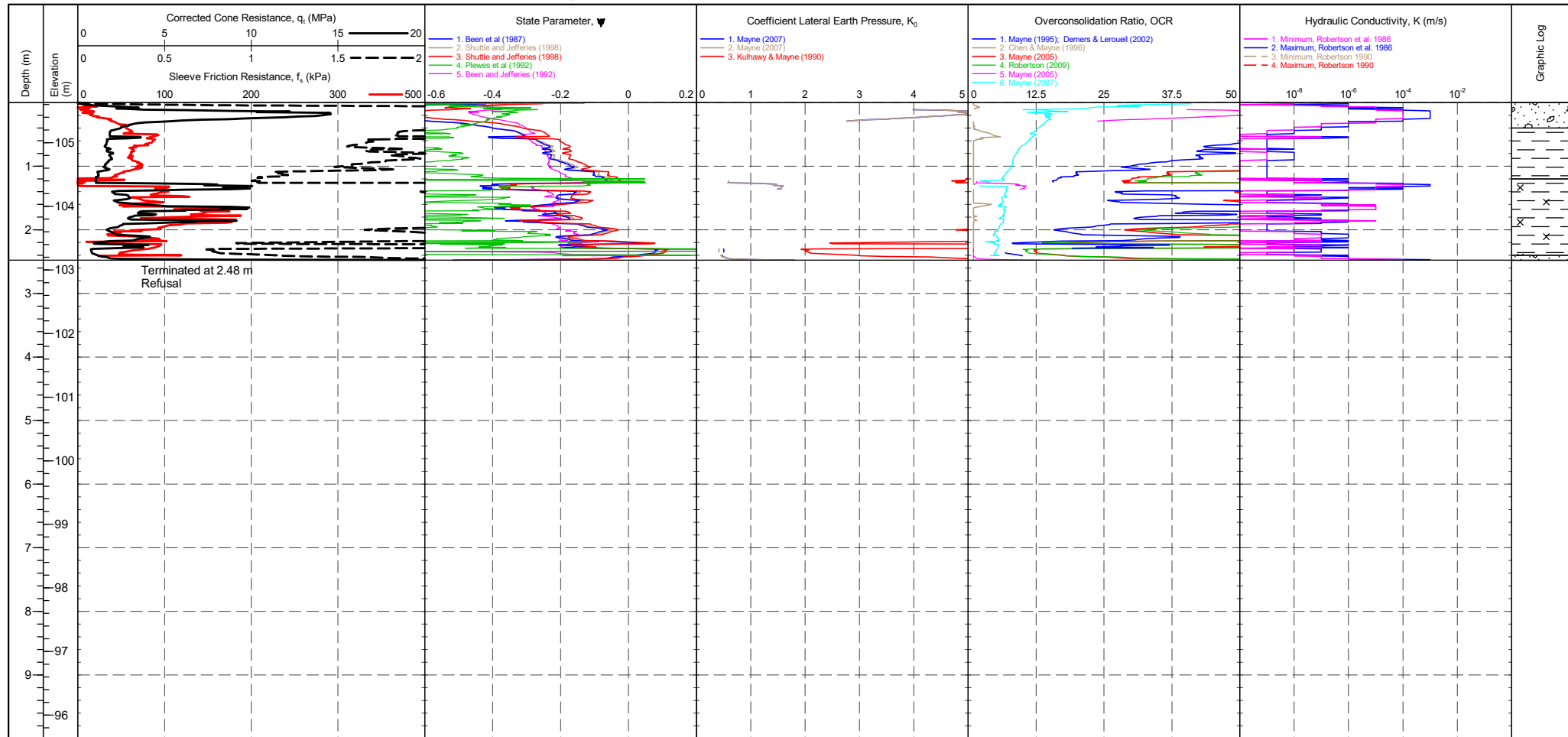
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490993.287 m <b>NORTHING</b> : 290892.523 m <b>ELEVATION</b> : 105.632 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip Sleeve Pore Pressure 2 X-Y Inclinator	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>367 mV</td> <td>366 mV</td> <td>-0.011 MPa</td> </tr> <tr> <td>291 mV</td> <td>290 mV</td> <td>-0.001 kPa</td> </tr> <tr> <td>232 mV</td> <td>216 mV</td> <td>-0.004 kPa</td> </tr> <tr> <td>2702 mV</td> <td>2639 mV</td> <td></td> </tr> </table>	Pre	Post	Difference	367 mV	366 mV	-0.011 MPa	291 mV	290 mV	-0.001 kPa	232 mV	216 mV	-0.004 kPa	2702 mV	2639 mV		<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> <table border="1"> <tr> <th>Term based on measurement</th> <th>su (kPa)</th> <th>Term based on measurement</th> <th>su (kPa)</th> </tr> <tr> <td>Extremely low strength</td> <td>&lt;10</td> <td>Medium strength</td> <td>40-75</td> </tr> <tr> <td>Very low strength</td> <td>10-20</td> <td>High strength</td> <td>75-150</td> </tr> <tr> <td>Low strength</td> <td>20-40</td> <td>Very high strength</td> <td>150-300</td> </tr> <tr> <td></td> <td></td> <td>Extremely high strength</td> <td>&gt;300</td> </tr> </table>	Term based on measurement	su (kPa)	Term based on measurement	su (kPa)	Extremely low strength	<10	Medium strength	40-75	Very low strength	10-20	High strength	75-150	Low strength	20-40	Very high strength	150-300			Extremely high strength	>300	<b>Groundwater Level</b>  <b>Dissipation Test</b> 
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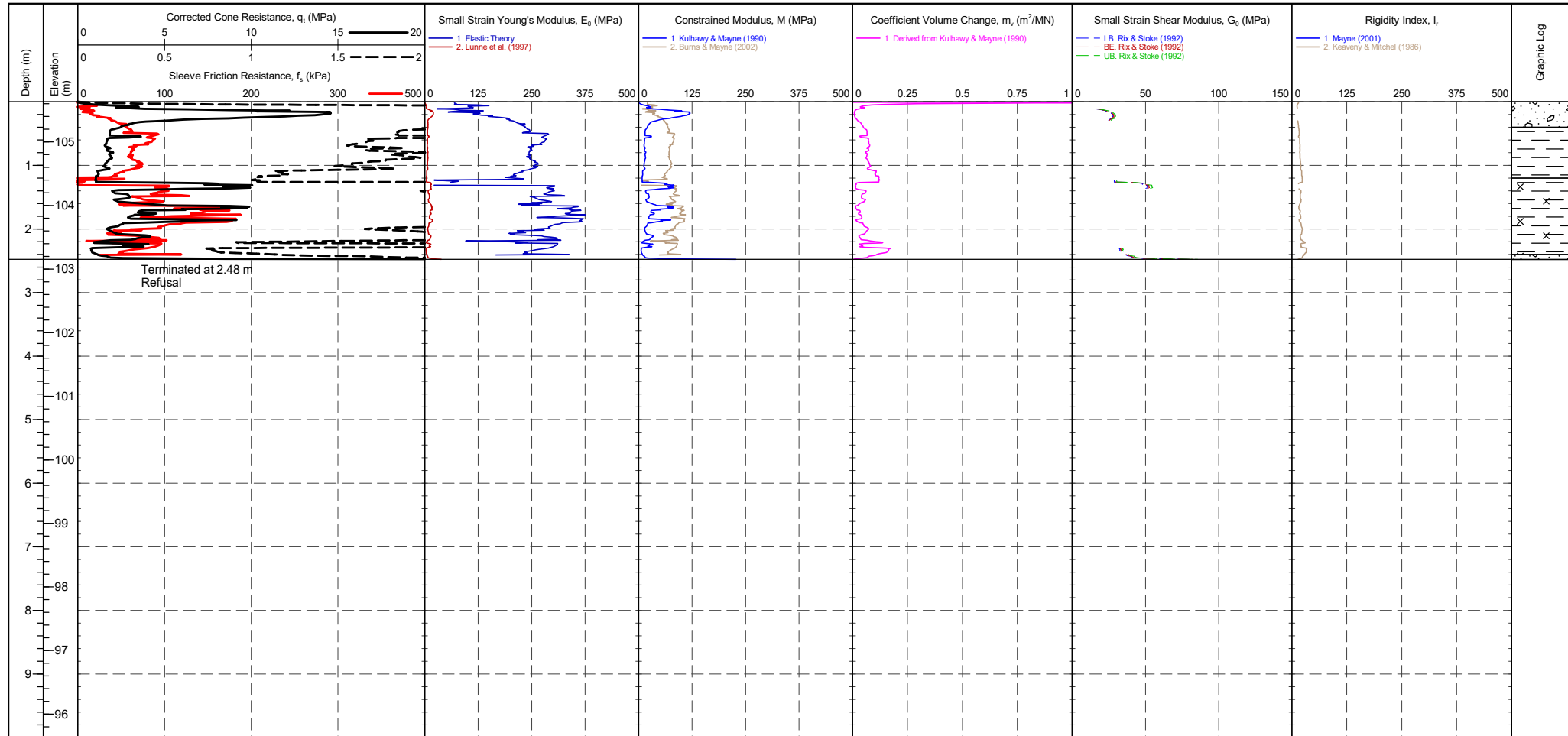
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490993.287 m <b>NORTHING</b> : 290892.523 m <b>ELEVATION</b> : 105.632 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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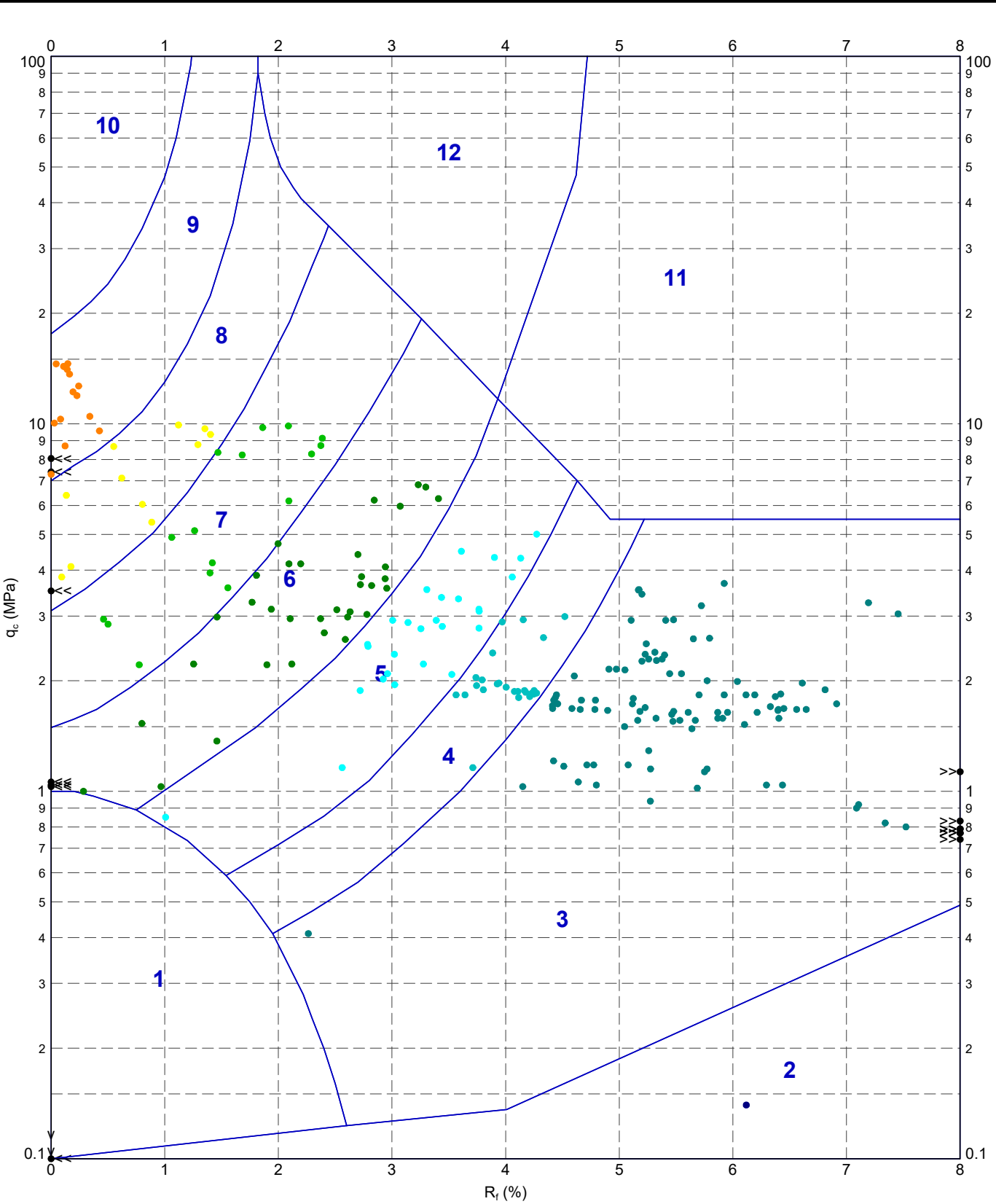
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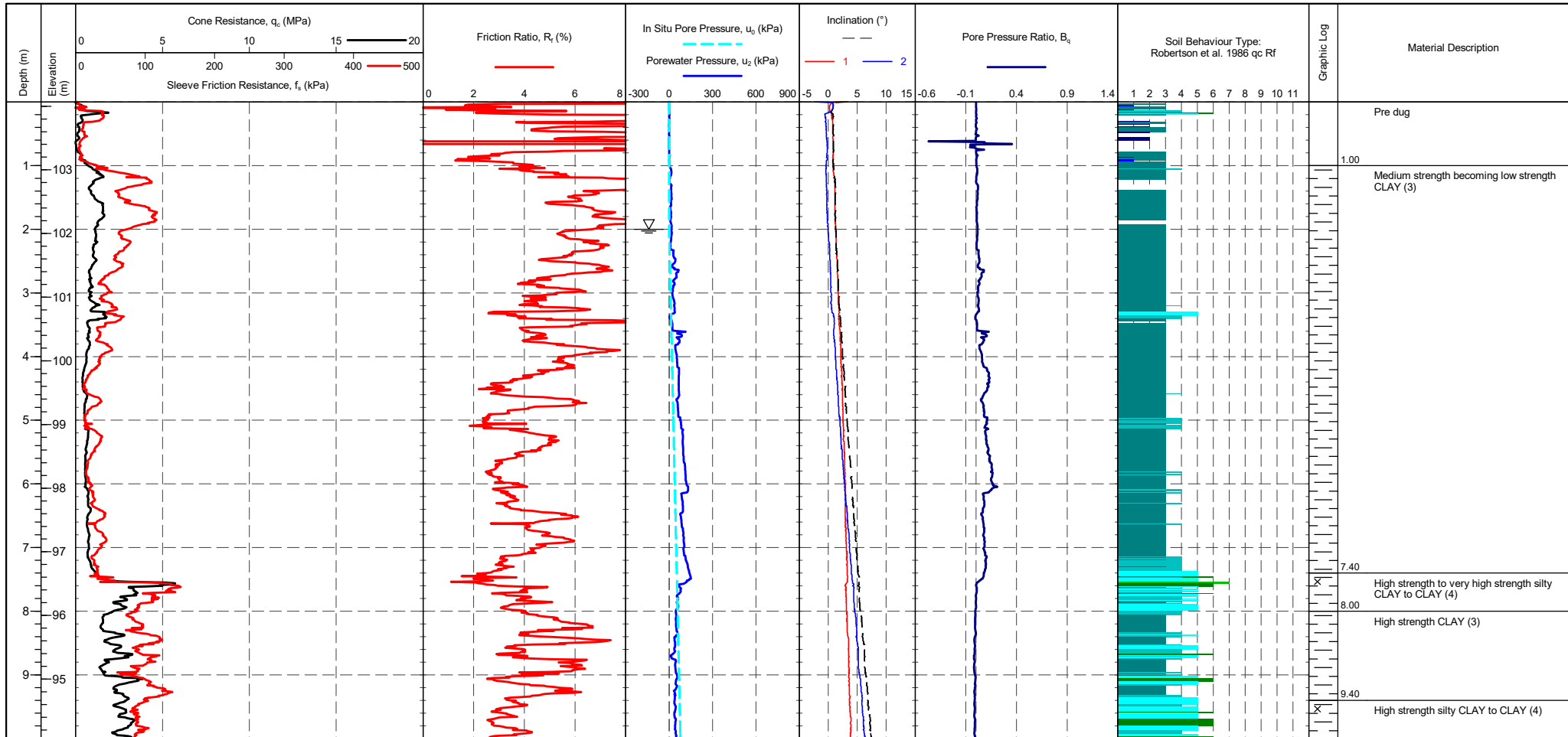
METHOD: Robertson et al. 1986 qc Rf

- 1 - Sensitive fine grained material
- 4 - Silty CLAY to CLAY
- 7 - Silty SAND to sandy SILT
- 10 - Gravelly SAND to SAND
- 2 - Organic material
- 5 - Clayey SILT to silty CLAY
- 8 - SAND to silty SAND
- 11 - Very stiff fine grained
- 3 - CLAY
- 6 - Sandy SILT to clayey SILT
- 9 - SAND
- 12 - SAND to clayey SAND

	TITLE Delta Simons Cordby Corby Robertson et al. 1986 qc vs. Rf - CPT06B	DRAWN	DATE 04/03/2022
		CHECKED	DATE 04/03/2022
		SCALE Not To Scale	A4
		PROJECT No 1220144	FIGURE No

PointID	<b>CPT07</b>
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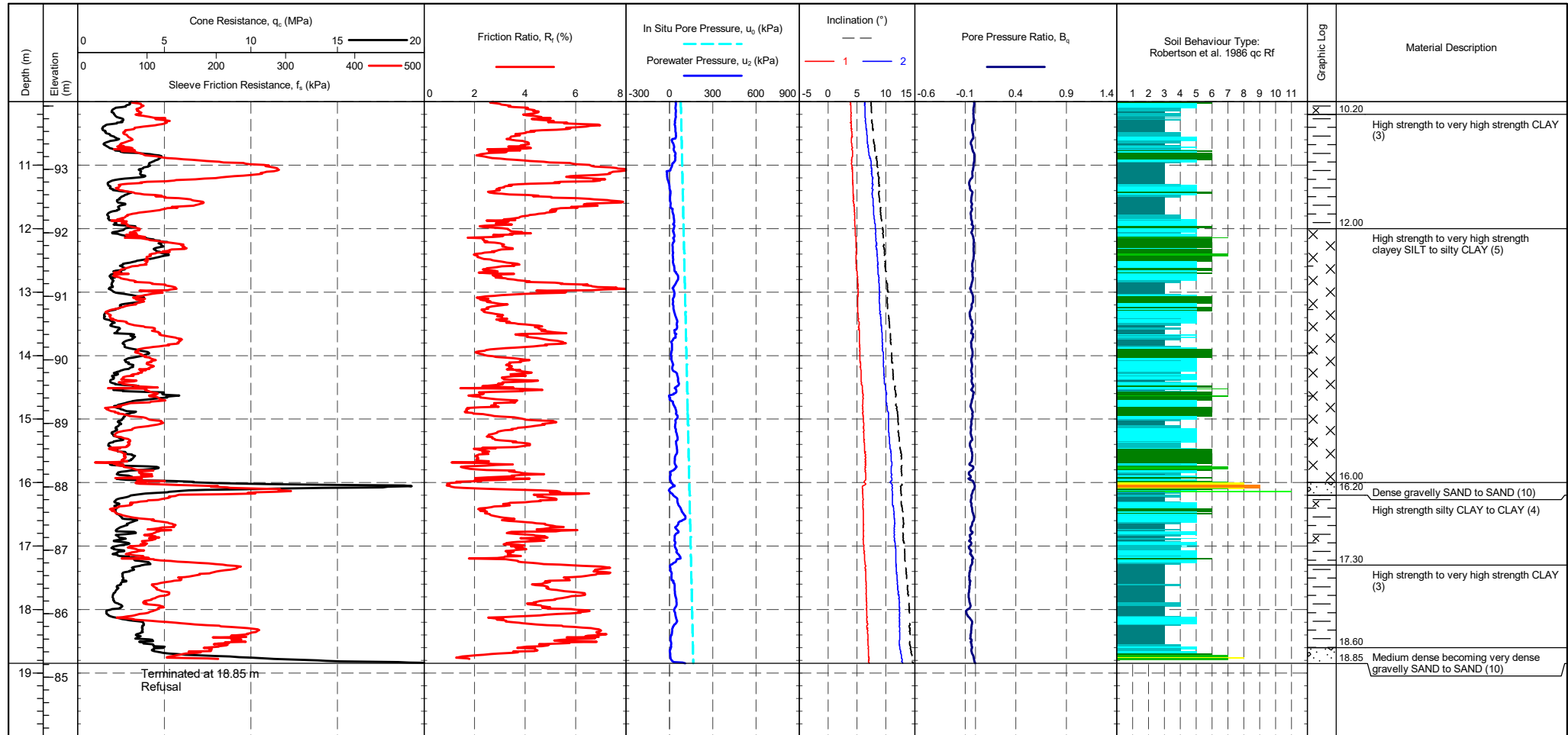
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491084.703 m <b>NORTHING</b> : 290876.351 m <b>ELEVATION</b> : 104.067 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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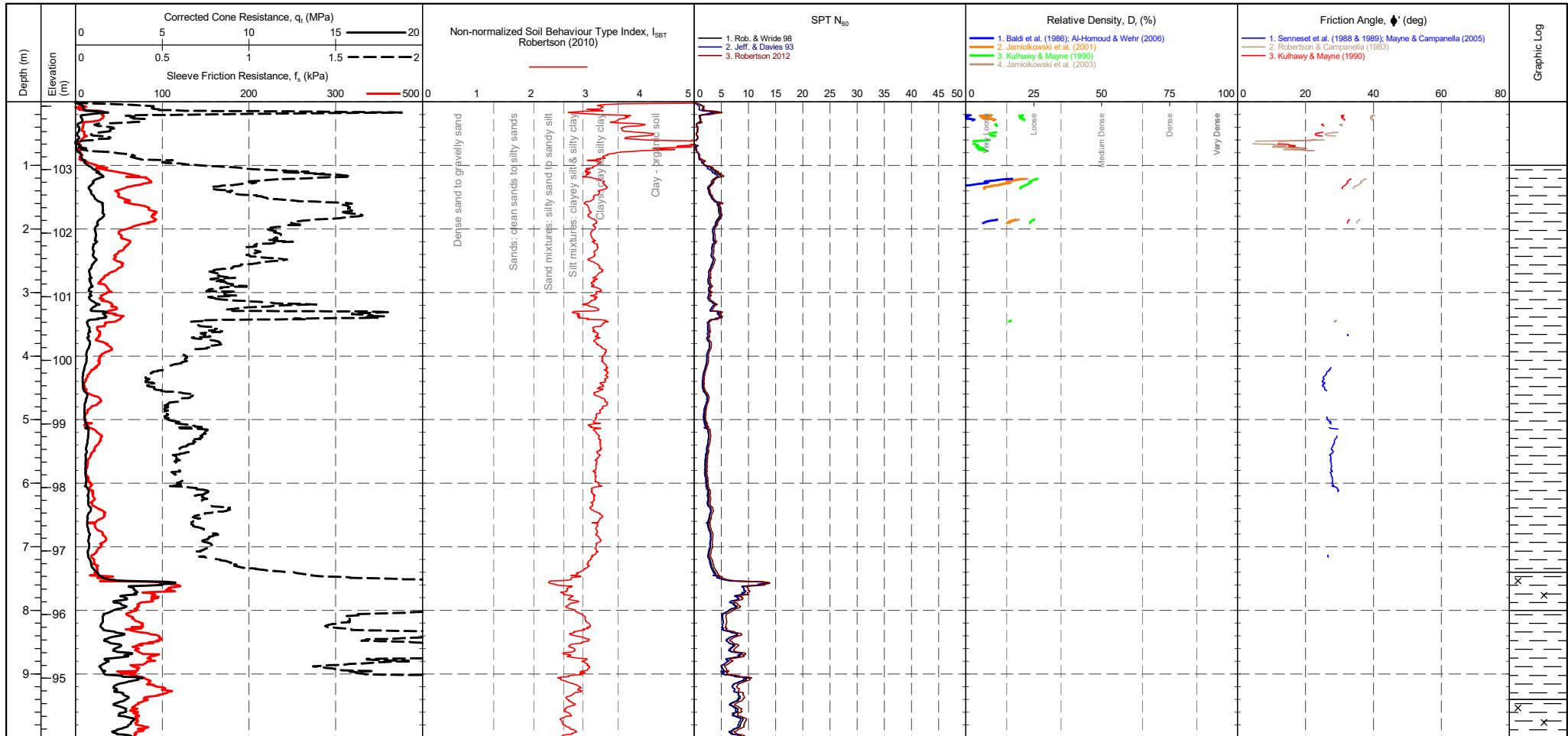
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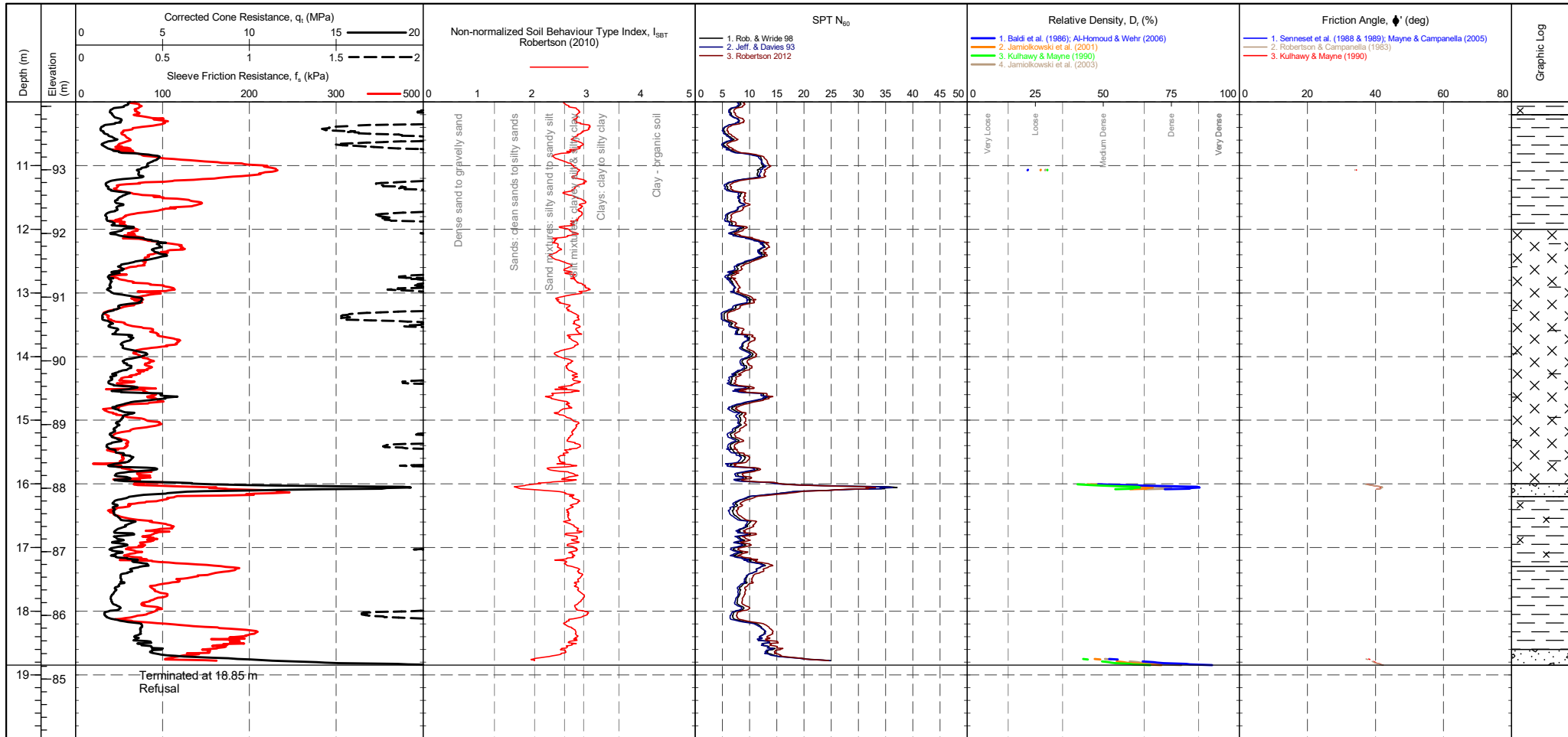
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491084.703 m <b>NORTHING</b> : 290876.351 m <b>ELEVATION</b> : 104.067 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> <b>Tip</b> : 363 mV <b>Sleeve</b> : 287 mV <b>Pore Pressure 2</b> : 248 mV <b>X-Y inclinometer</b> : 2762 mV	<b>CPTU ZERO VALUES</b> <b>Post</b> : 363 mV <b>Difference</b> : 0 MPa 0 kPa 0 kPa 2588 mV	<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, <math>I_c</math></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density <math>D_r</math> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, $I_c$	Description	SPT N value, NSPT	Description	Relative Density $D_r$ (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
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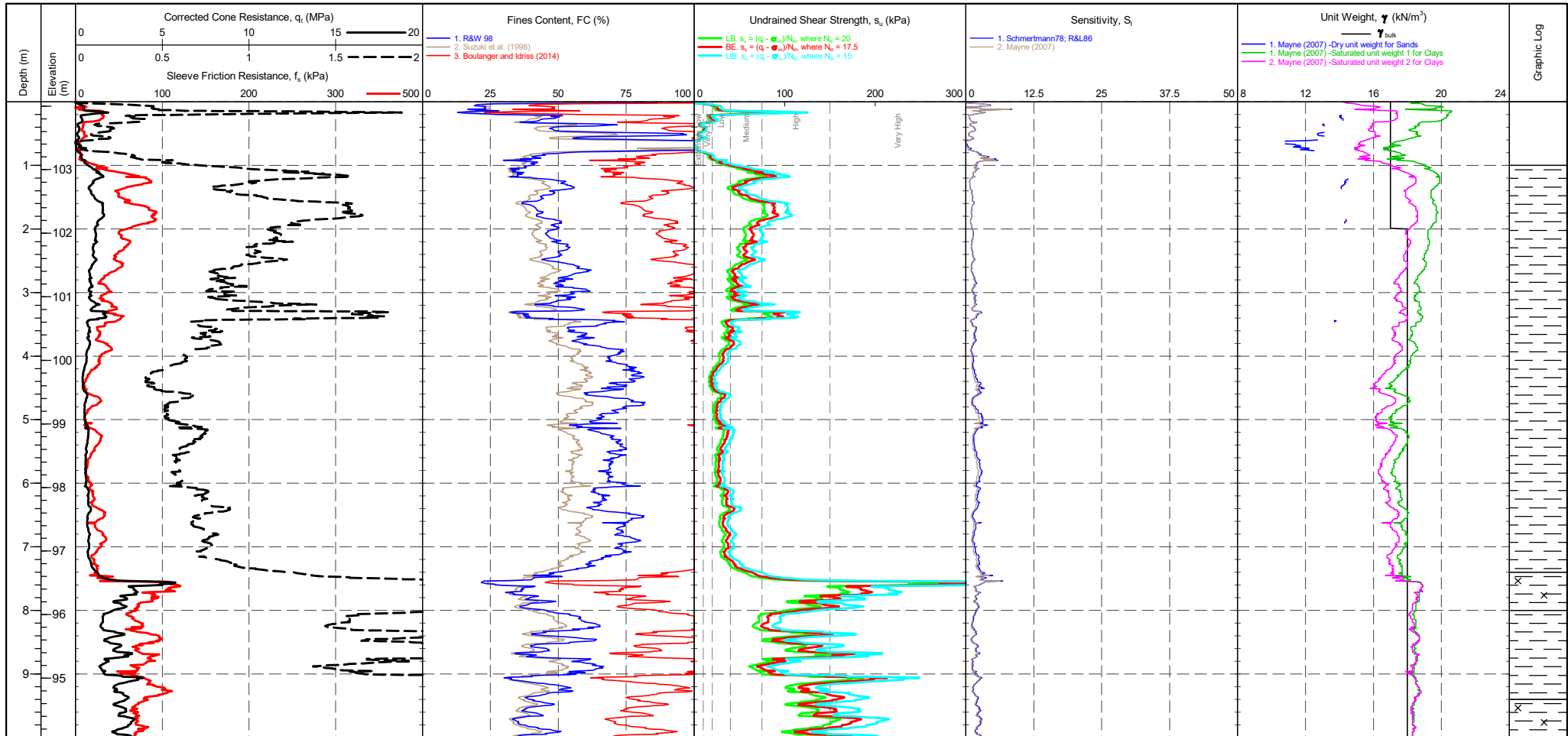
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491084.703 m <b>NORTHING</b> : 290876.351 m <b>ELEVATION</b> : 104.067 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> <b>Tip</b> : 363 mV <b>Sleeve</b> : 287 mV <b>Pore Pressure 2</b> : 248 mV <b>X-Y inclinometer</b> : 2762 mV	<b>CPTU ZERO VALUES</b> <b>Post</b> : 363 mV <b>Difference</b> : 0 MPa <b>0 kPa</b> <b>0 kPa</b> <b>2588 mV</b>	<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, I<sub>c</sub></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density Dr (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, I <sub>c</sub>	Description	SPT N value, NSPT	Description	Relative Density Dr (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
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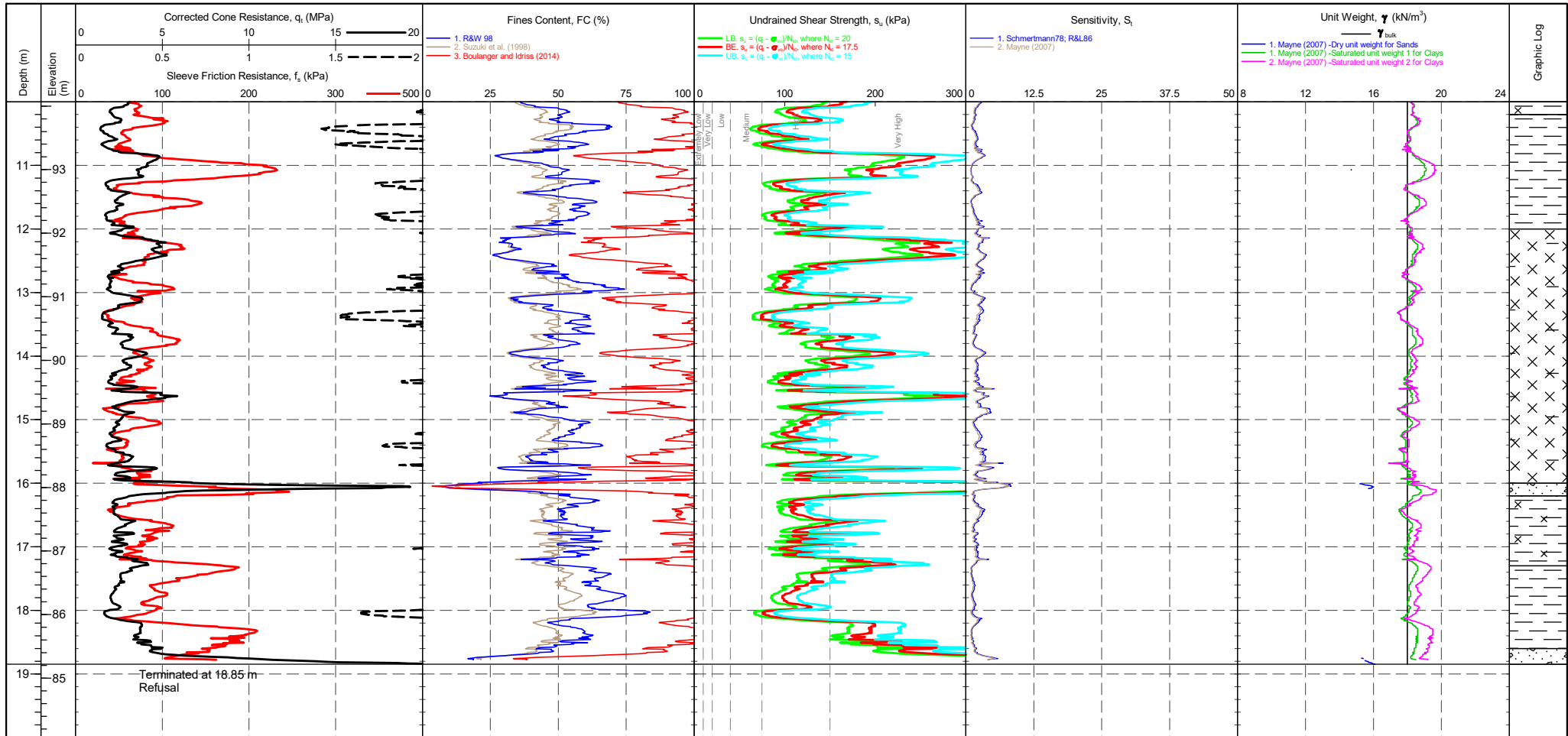
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491084.703 m <b>NORTHING</b> : 290876.351 m <b>ELEVATION</b> : 104.067 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 363 mV / 363 mV / 0 MPa Sleeve: 287 mV / 287 mV / 0 kPa Pore Pressure 2: 248 mV / 246 mV / 0 kPa X-Y Inclinator: 2762 mV / 2588 mV	<b>CPTU ZERO VALUES</b> Pre: 363 mV, Post: 363 mV, Difference: 0 MPa Pre: 287 mV, Post: 287 mV, Difference: 0 kPa Pre: 248 mV, Post: 246 mV, Difference: 0 kPa Pre: 2762 mV, Post: 2588 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> <table border="1"> <tr> <th>Term based on measurement</th> <th>su (kPa)</th> <th>Term based on measurement</th> <th>su (kPa)</th> </tr> <tr> <td>Extremely low strength</td> <td>&lt;10</td> <td>Medium strength</td> <td>40-75</td> </tr> <tr> <td>Very low strength</td> <td>10-20</td> <td>High strength</td> <td>75-150</td> </tr> <tr> <td>Low strength</td> <td>20-40</td> <td>Very high strength</td> <td>150-300</td> </tr> <tr> <td></td> <td></td> <td>Extremely high strength</td> <td>&gt;300</td> </tr> </table>	Term based on measurement	su (kPa)	Term based on measurement	su (kPa)	Extremely low strength	<10	Medium strength	40-75	Very low strength	10-20	High strength	75-150	Low strength	20-40	Very high strength	150-300			Extremely high strength	>300	▽ Groundwater Level ▮ Dissipation Test
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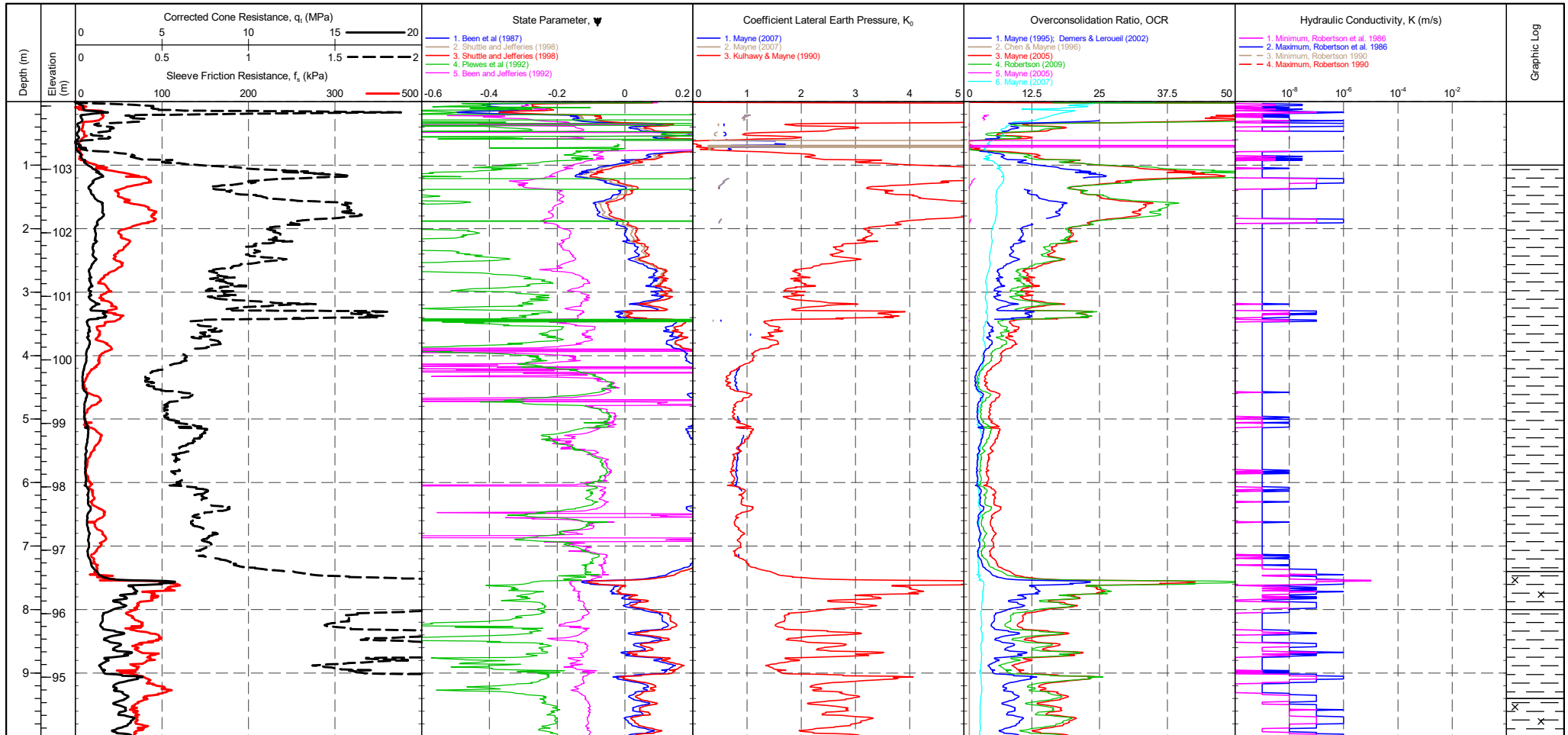
<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 363 mV Sleeve: 287 mV Pore Pressure 2: 248 mV X-Y Inclinator: 2762 mV	<b>CPTU ZERO VALUES</b> Post: 363 mV Difference: 0 MPa 287 mV 0 kPa 246 mV 0 kPa 2588 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement su (kPa) Extremely low strength <10 Very low strength 10-20 Low strength 20-40	Term based on measurement su (kPa) Medium strength 40-75 High strength 75-150 Very high strength 150-300 Extremely high strength >300	Groundwater Level Dissipation Test
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



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**CPT07**

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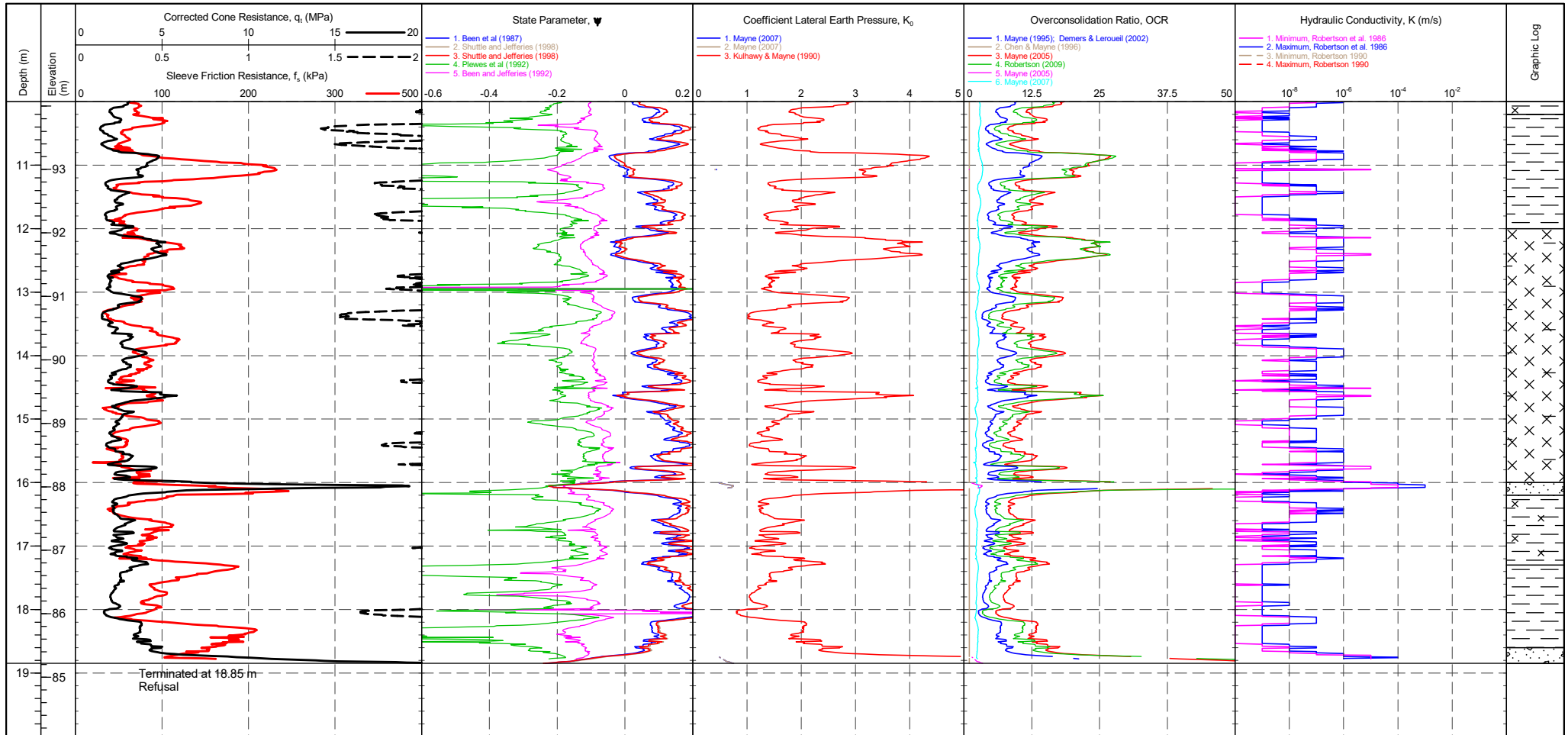


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>363 mV</td> <td>363 mV</td> <td>0 MPa</td> </tr> <tr> <td>Sleeve</td> <td>287 mV</td> <td>287 mV</td> <td>0 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>248 mV</td> <td>246 mV</td> <td>0 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2762 mV</td> <td>2588 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	363 mV	363 mV	0 MPa	Sleeve	287 mV	287 mV	0 kPa	Pore Pressure 2	248 mV	246 mV	0 kPa	X-Y Inclinator	2762 mV	2588 mV		 Groundwater Level   Dissipation Test
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**CPT07**

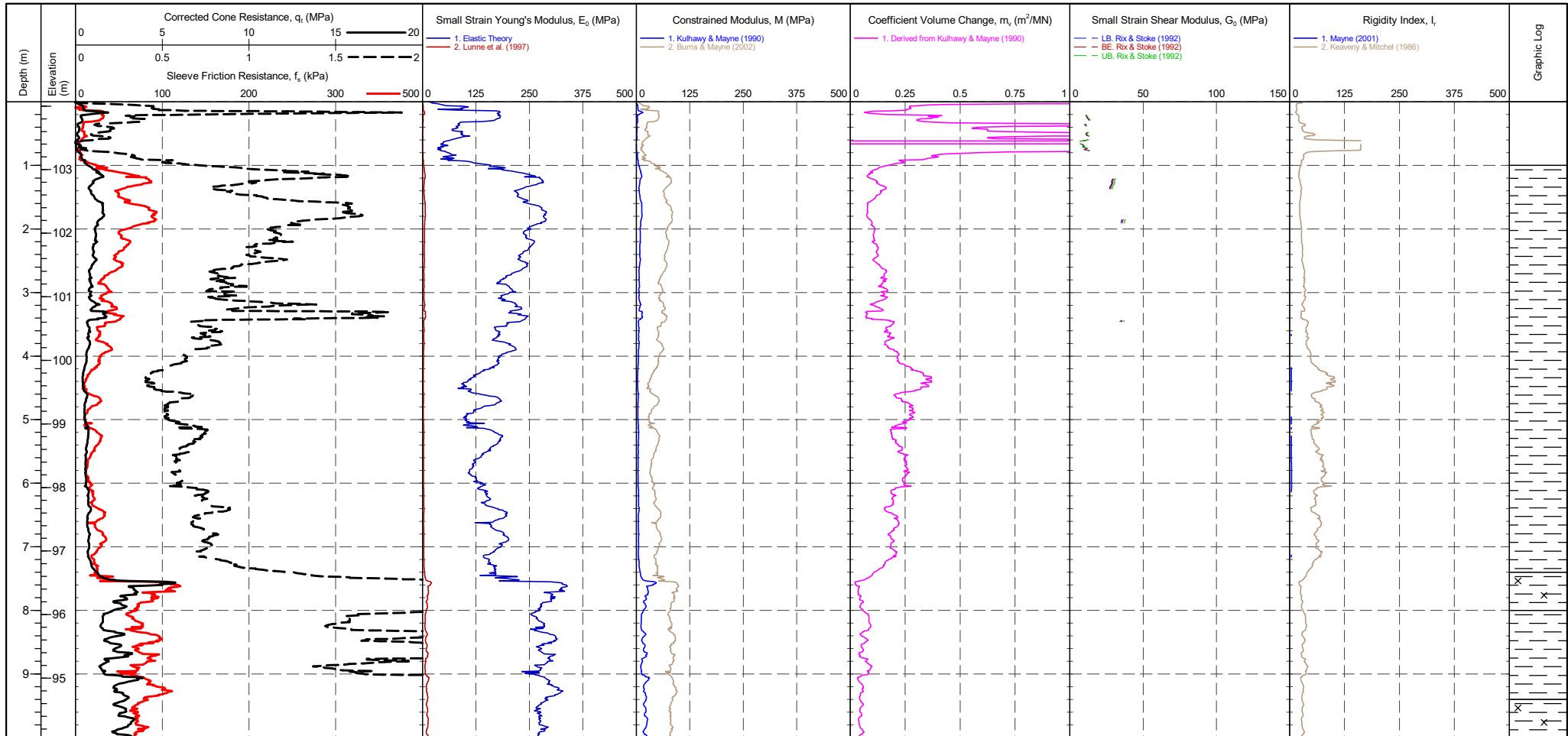
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> Transducer Pre Post Difference Tip 363 mV 363 mV 0 MPa Sleeve 287 mV 287 mV 0 kPa Pore Pressure 2 248 mV 246 mV 0 kPa X-Y Inclinator 2762 mV 2588 mV	Groundwater Level Dissipation Test
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PointID  
**CPT07**

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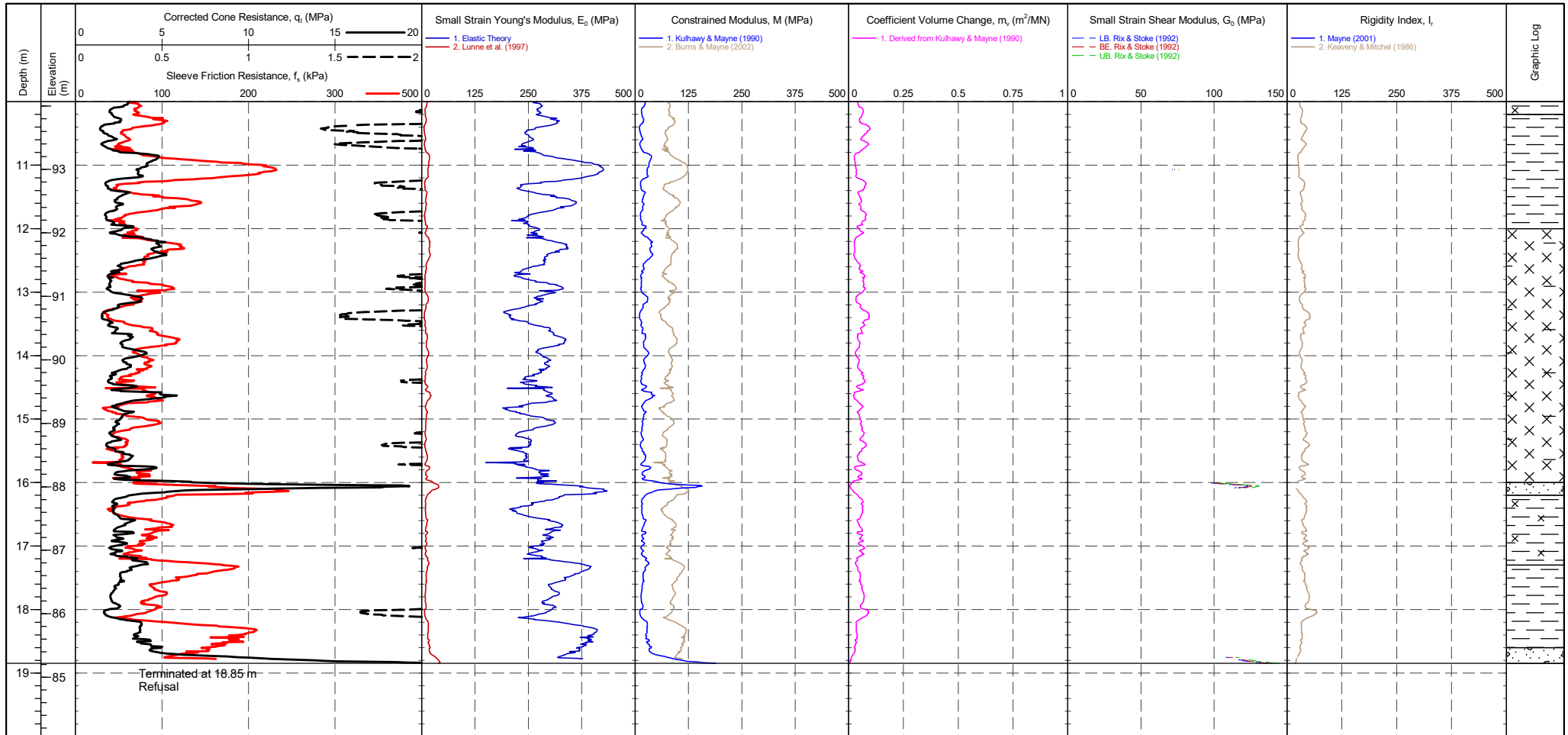


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>363 mV</td> <td>363 mV</td> <td>0 MPa</td> </tr> <tr> <td>Sleeve</td> <td>287 mV</td> <td>287 mV</td> <td>0 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>248 mV</td> <td>246 mV</td> <td>0 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2762 mV</td> <td>2588 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	363 mV	363 mV	0 MPa	Sleeve	287 mV	287 mV	0 kPa	Pore Pressure 2	248 mV	246 mV	0 kPa	X-Y Inclinator	2762 mV	2588 mV		Groundwater Level Dissipation Test
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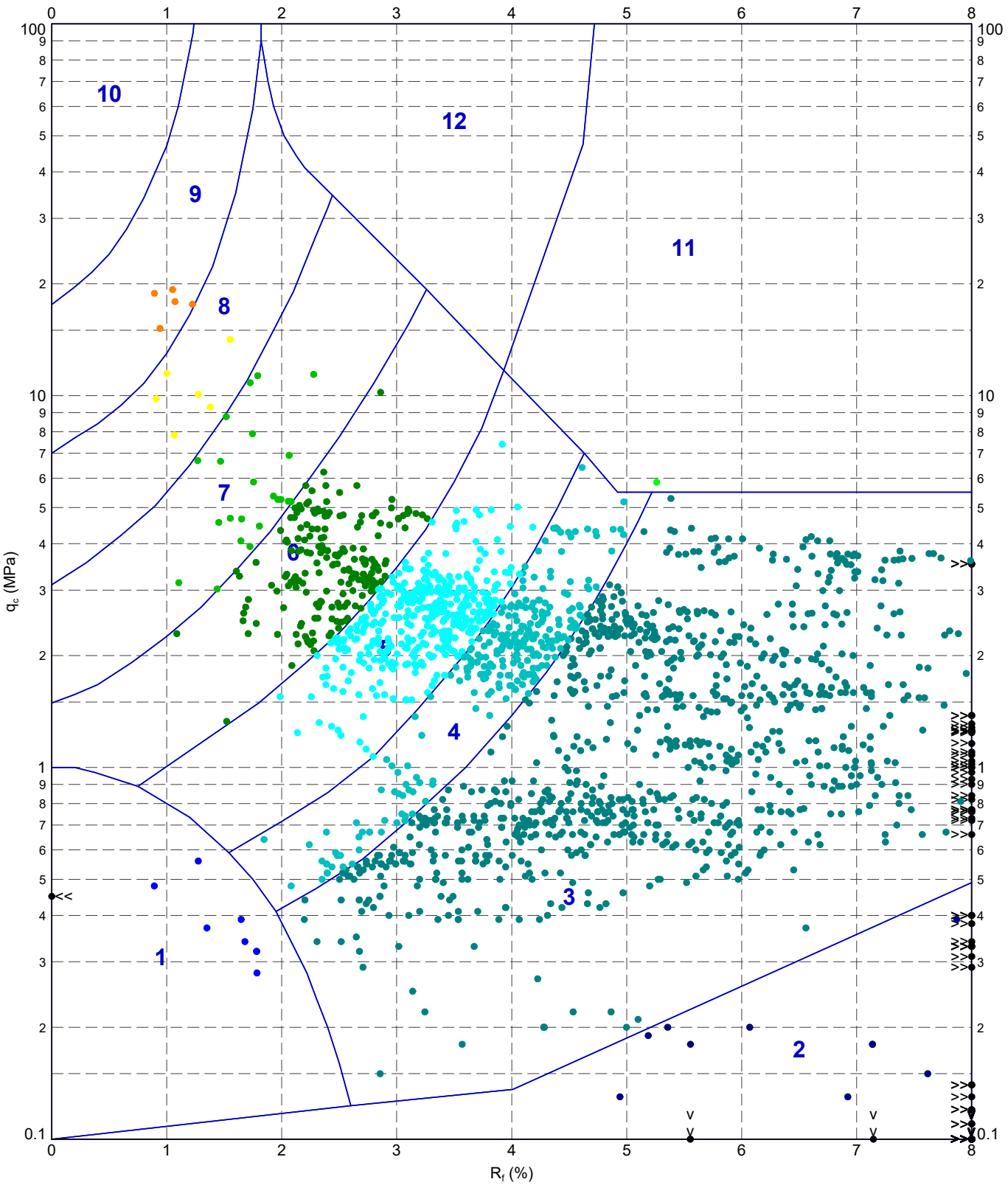
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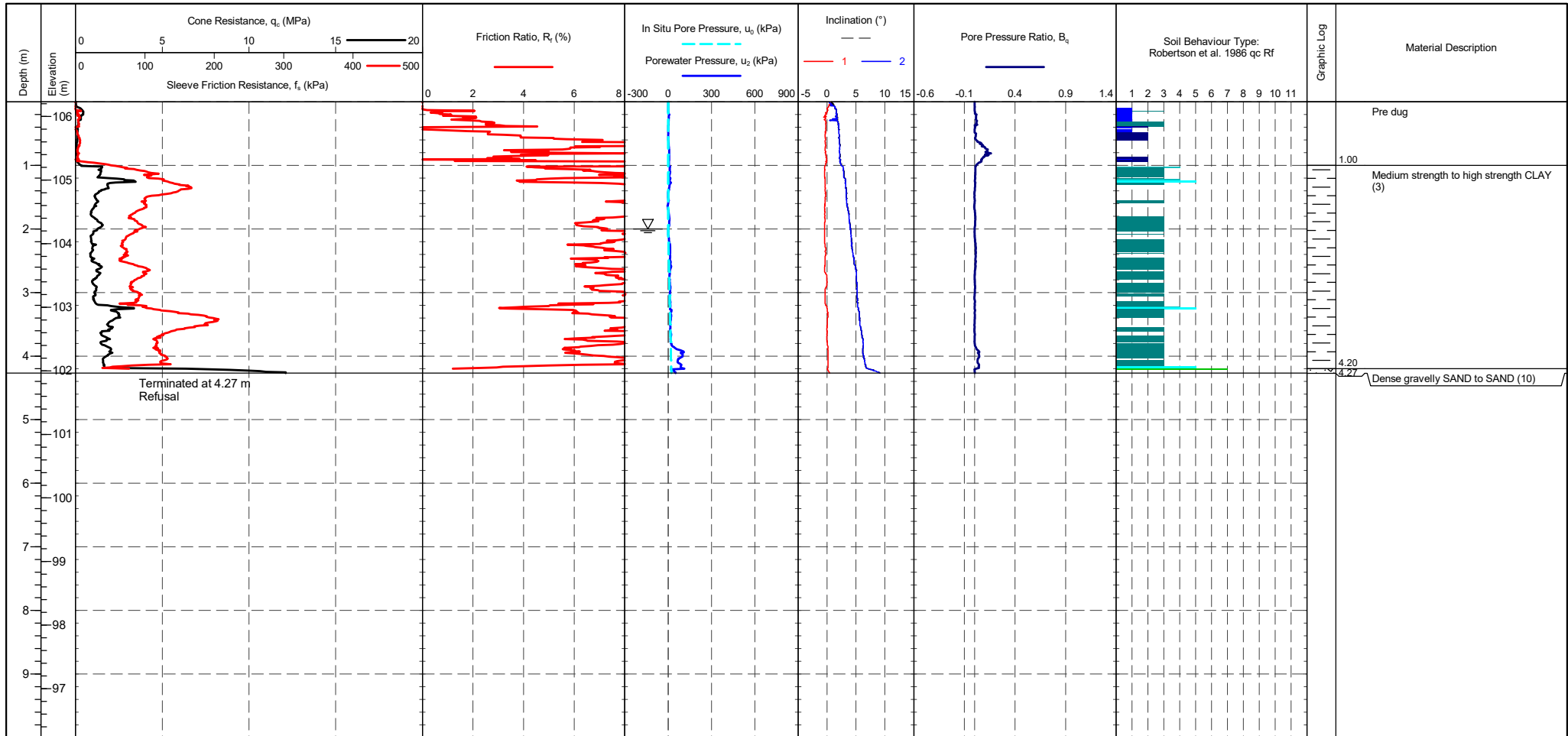


- METHOD: Robertson et al. 1986 q<sub>c</sub> R<sub>f</sub>**
- 1 - Sensitive fine grained material
  - 2 - Organic material
  - 3 - CLAY
  - 4 - Silty CLAY to CLAY
  - 5 - Clayey SILT to silty CLAY
  - 6 - Sandy SILT to clayey SILT
  - 7 - Silty SAND to sandy SILT
  - 8 - SAND to silty SAND
  - 9 - SAND
  - 10 - Gravelly SAND to SAND
  - 11 - Very stiff fine grained
  - 12 - SAND to clayey SAND

	<b>TITLE</b> Delta Simons Cordby Corby Robertson et al. 1986 q <sub>c</sub> vs. R <sub>f</sub> - CPT07	<b>DRAWN</b> _____	<b>DATE</b> 04/03/2022	
		<b>CHECKED</b> _____	<b>DATE</b> 04/03/2022	
		<b>SCALE</b> Not To Scale		<b>A4</b>
		<b>PROJECT No</b> 1220144	<b>FIGURE No</b> _____	

PointID	<b>CPT08</b>
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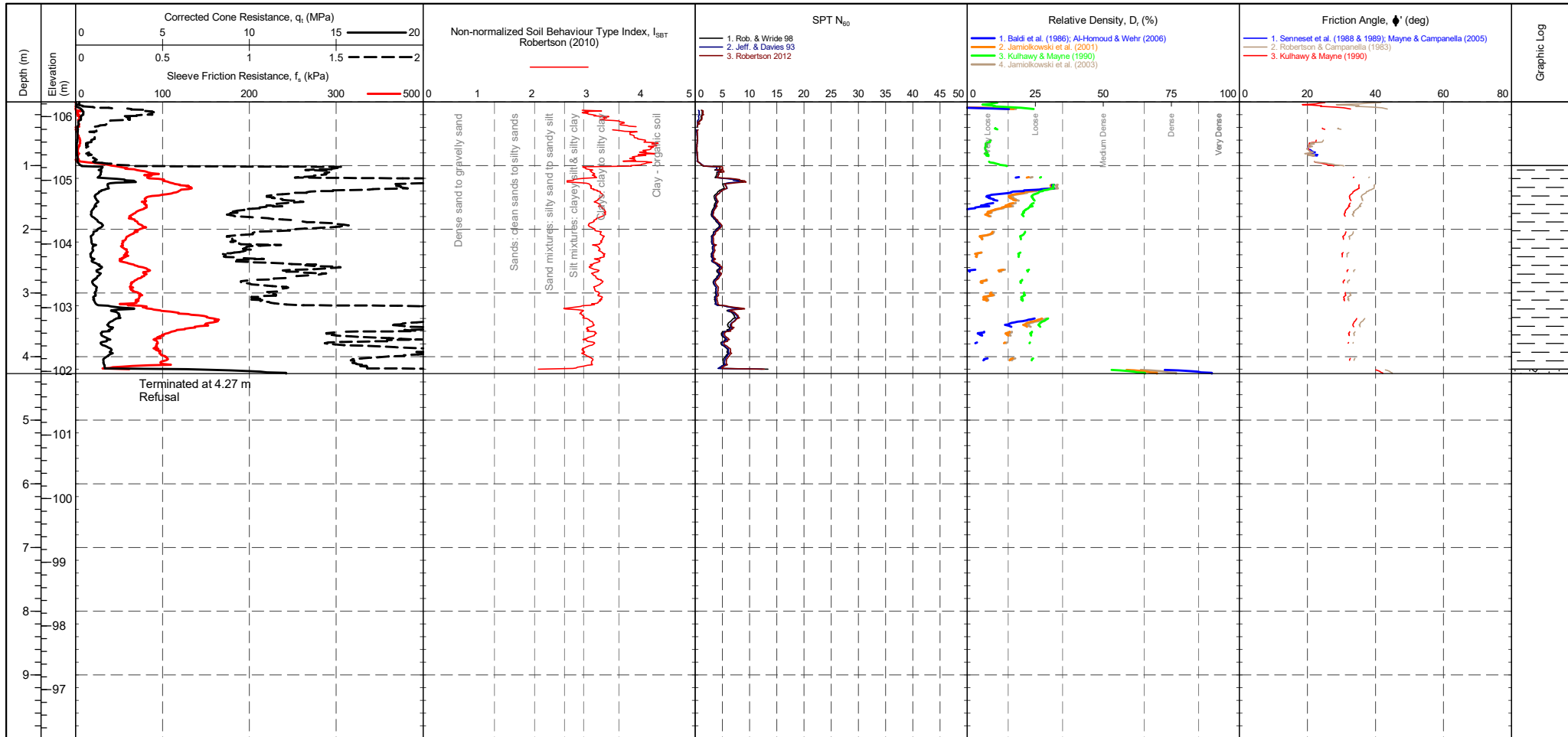
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490892.029 m <b>NORTHING</b> : 290837.383 m <b>ELEVATION</b> : 106.232 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on inclination.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Pre Post Difference Tip 375 mV 372 mV -0.033 MPa Sleeve 291 mV 288 mV -0.002 kPa Pore Pressure 2 206 mV 246 mV 0.009 kPa X-Y Inclinator 2587 mV 2569 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravelly SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490892.029 m <b>NORTHING</b> : 290837.383 m <b>ELEVATION</b> : 106.232 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on inclination.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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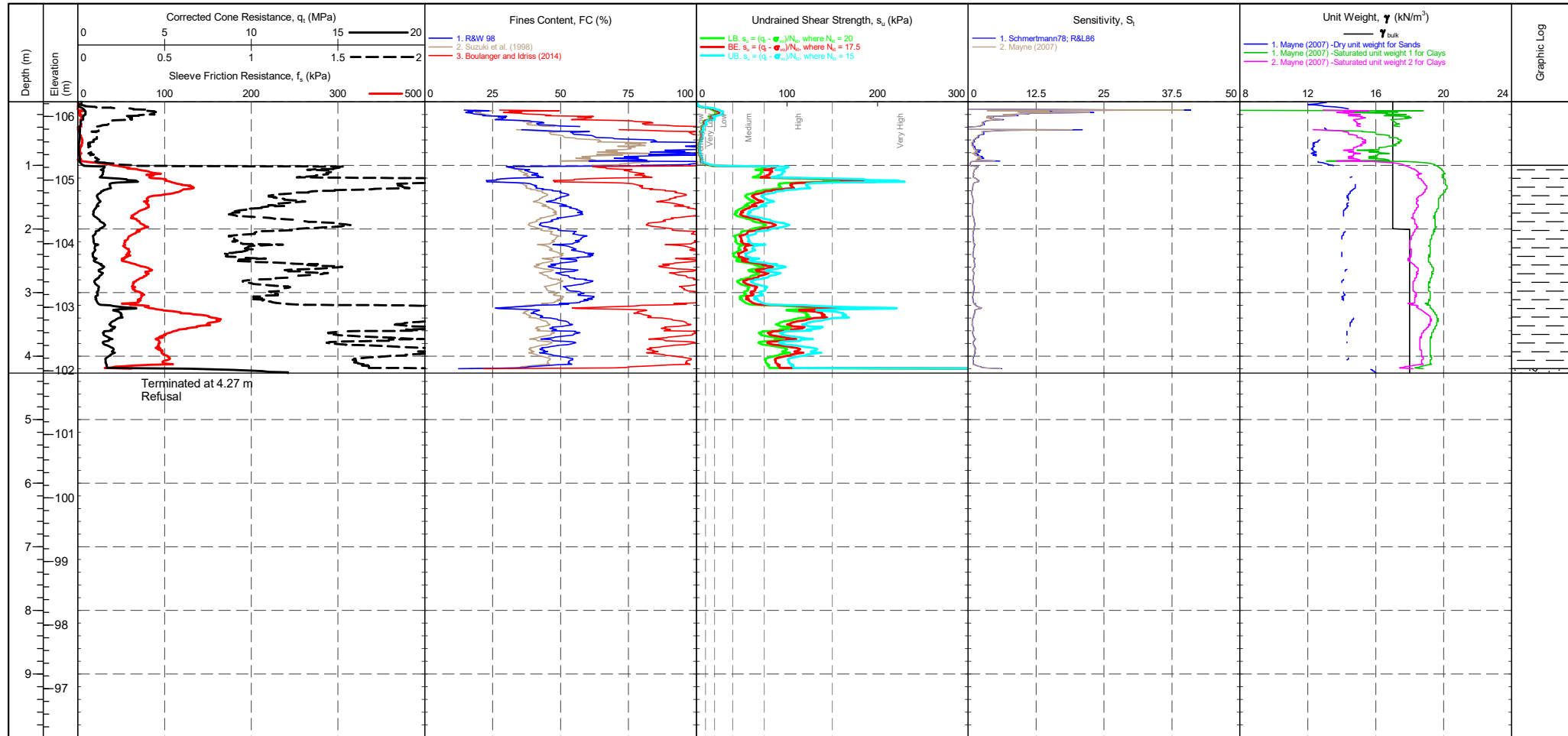


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> <b>Tip</b> : 375 mV <b>Sleeve</b> : 291 mV <b>Pore Pressure 2</b> : 206 mV <b>X-Y Inclinator</b> : 2587 mV	<b>CPTU ZERO VALUES</b> <b>Post</b> : 372 mV <b>Difference</b> : -0.033 MPa <b>0.002 kPa</b> <b>0.009 kPa</b> <b>2569 mV</b>	<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, <math>I_c</math></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density <math>D_r</math> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, $I_c$	Description	SPT N value, NSPT	Description	Relative Density $D_r$ (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	<b>Groundwater Level</b> <b>Dissipation Test</b>
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PointID	<b>CPT08</b>
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490892.029 m <b>NORTHING</b> : 290837.383 m <b>ELEVATION</b> : 106.232 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on inclination.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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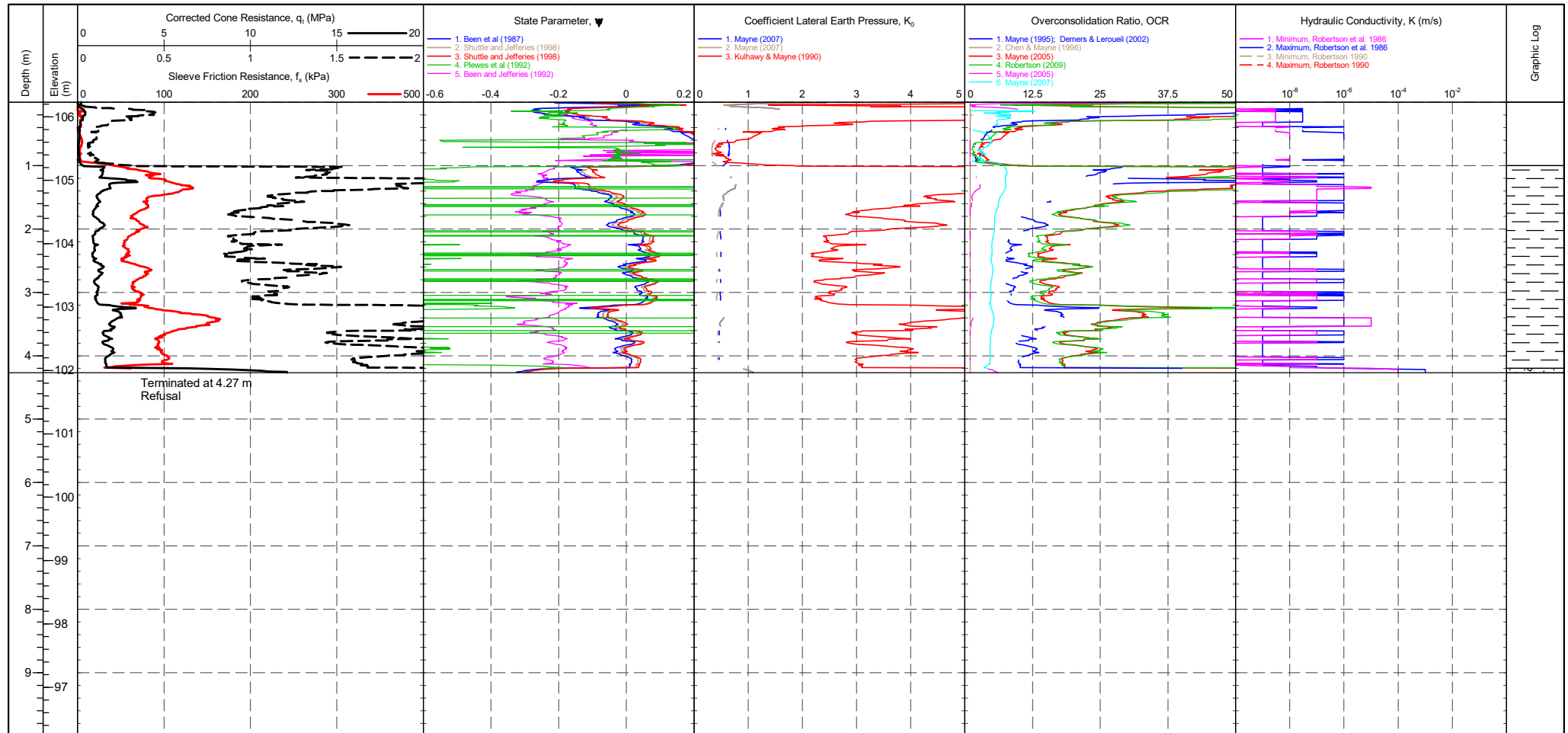


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> Transducer Pre Post Difference Tip 375 mV 372 mV -0.033 MPa Sleeve 291 mV 288 mV -0.002 kPa Pore Pressure 2 206 mV 246 mV 0.009 kPa X-Y Inclinator 2587 mV 2569 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement $s_u$ (kPa) Term based on measurement $s_u$ (kPa) Extremely low strength <10 Medium strength 40-75 Very low strength 10-20 High strength 75-150 Low strength 20-40 Very high strength 150-300 Extremely high strength >300	▽ Groundwater Level ▮ Dissipation Test
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PointID

**CPT08**

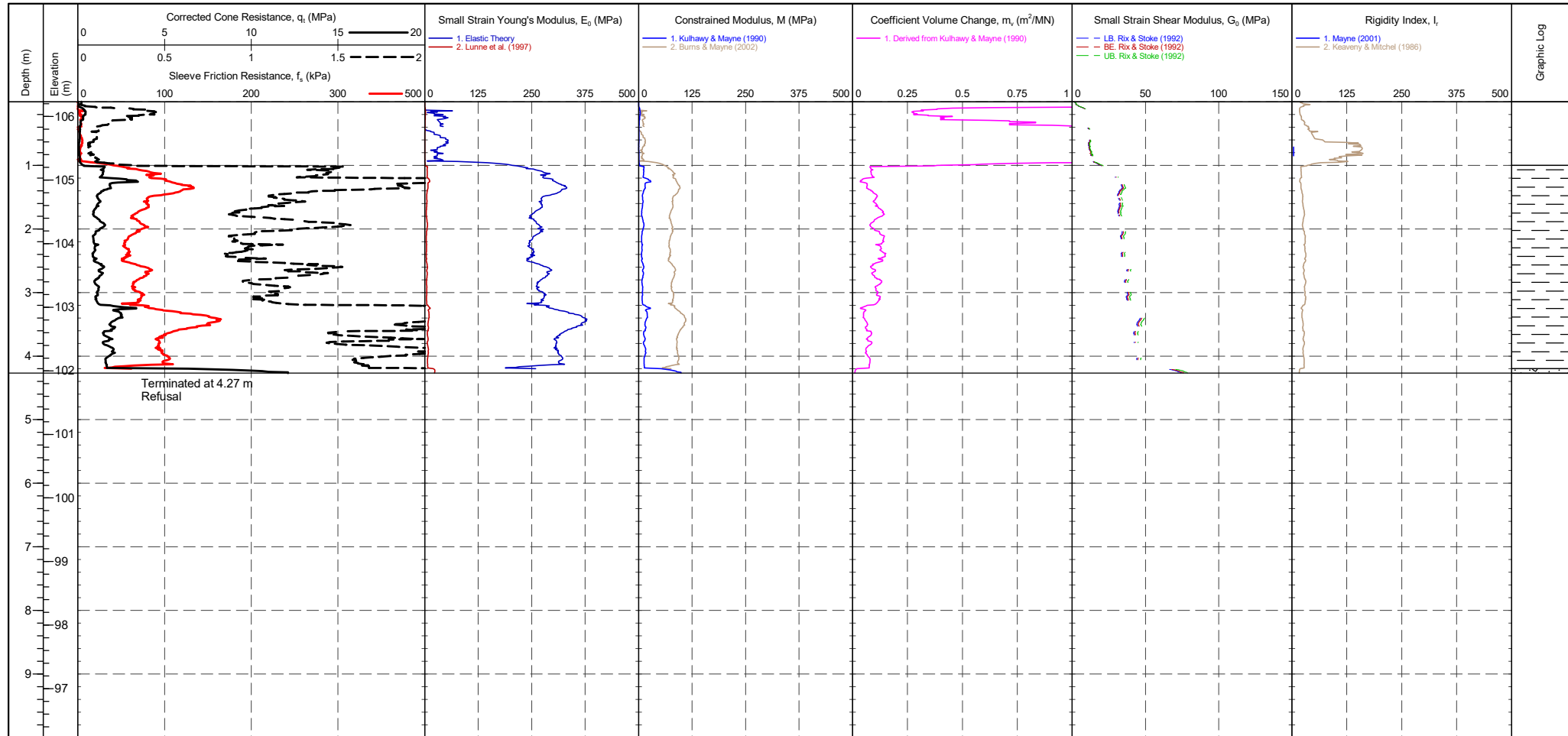
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490892.029 m <b>NORTHING</b> : 290837.383 m <b>ELEVATION</b> : 106.232 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on inclination.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>375 mV</td> <td>372 mV</td> <td>-0.033 MPa</td> </tr> <tr> <td>Sleeve</td> <td>291 mV</td> <td>288 mV</td> <td>-0.002 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>206 mV</td> <td>246 mV</td> <td>0.009 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2587 mV</td> <td>2569 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	375 mV	372 mV	-0.033 MPa	Sleeve	291 mV	288 mV	-0.002 kPa	Pore Pressure 2	206 mV	246 mV	0.009 kPa	X-Y Inclinator	2587 mV	2569 mV		Groundwater Level Dissipation Test
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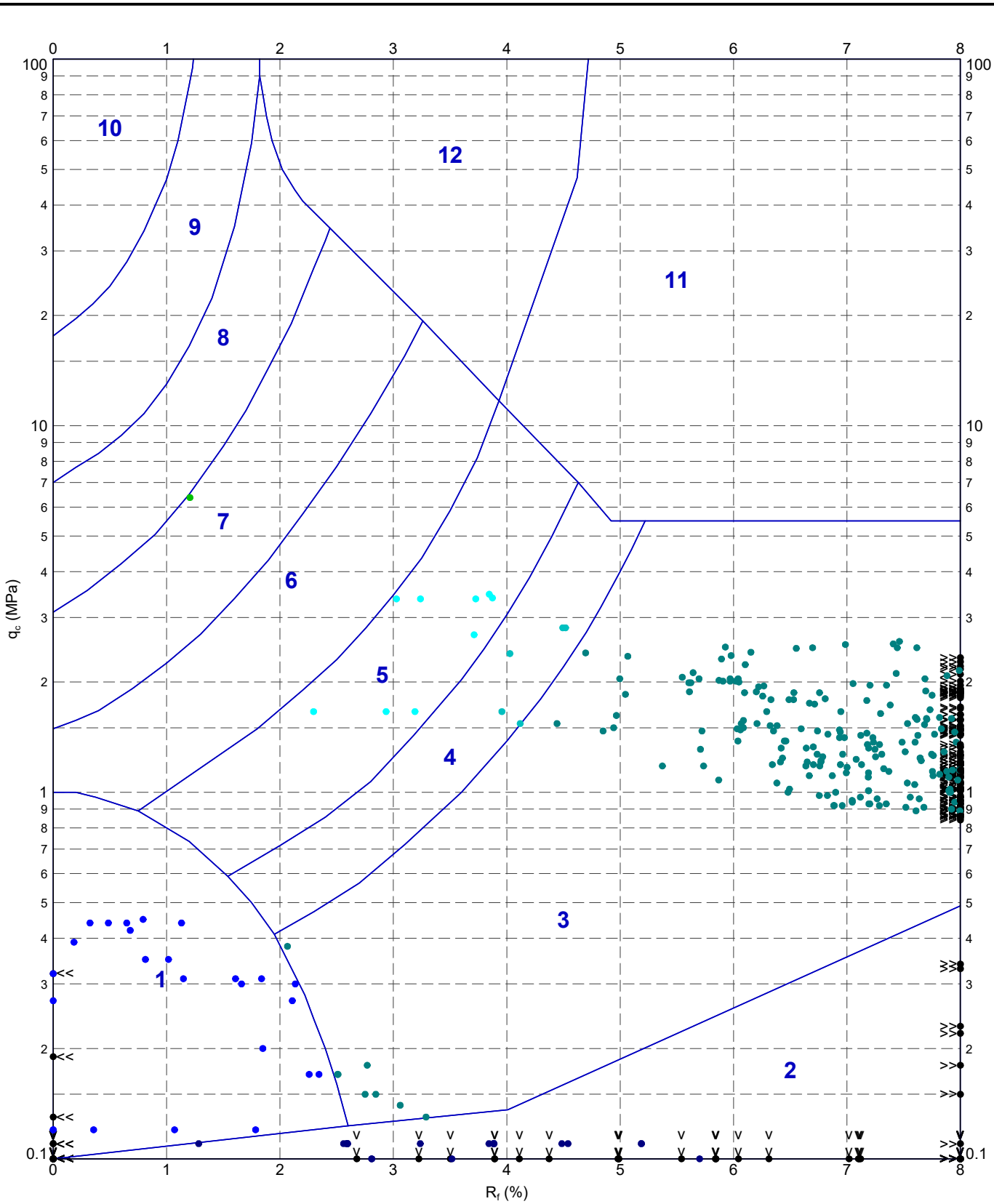
PointID	<b>CPT08</b>
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490892.029 m <b>NORTHING</b> : 290837.383 m <b>ELEVATION</b> : 106.232 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on inclination.	<b>SHEET</b> : 1 OF 1 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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22028-ADVANCED REPORT INSTITUTE 2.02.1 LIB - CHLOE.GLB Graph CPT ROBERTSON ET AL. 8F QC VS. RF APF 1220144 CORBY DELTA SIMONS G.P.J. <<DrawingFile>> 04/03/2022 17:13 10.01.00.11 Datagel Lab and In Situ Tool - DGD [Lib: In Situ SI 2.02.0/2017-07-10 Proj: In Situ SI 2.02.0 2017-07-10]



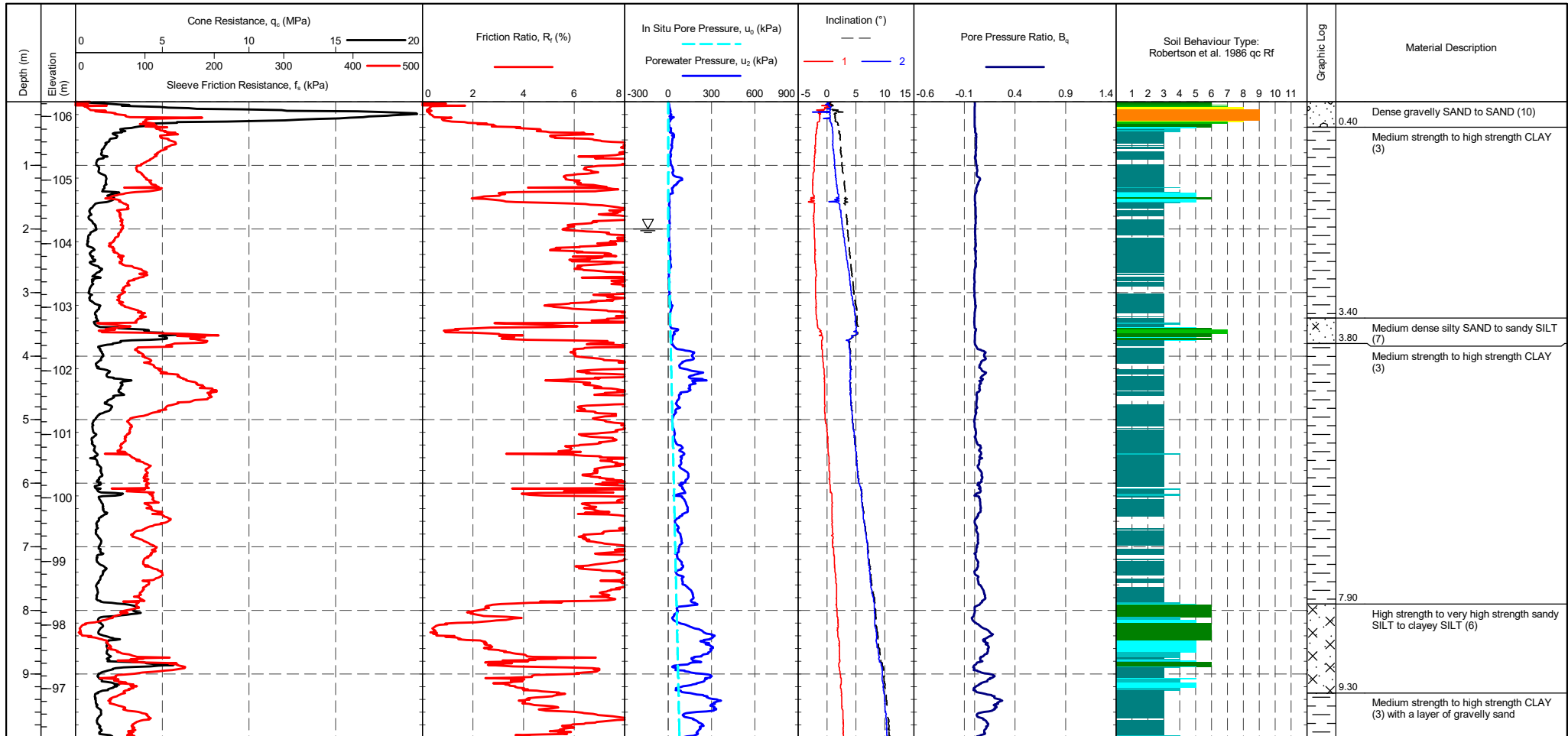
METHOD: Robertson et al. 1986 qc Rf

- 1 - Sensitive fine grained material
- 4 - Silty CLAY to CLAY
- 7 - Silty SAND to sandy SILT
- 10 - Gravelly SAND to SAND
- 2 - Organic material
- 5 - Clayey SILT to silty CLAY
- 8 - SAND to silty SAND
- 11 - Very stiff fine grained
- 3 - CLAY
- 6 - Sandy SILT to clayey SILT
- 9 - SAND
- 12 - SAND to clayey SAND

	TITLE <b>Delta Simons Cordby Corby</b> Robertson et al. 1986 qc vs. Rf - CPT08	DRAWN	DATE	04/03/2022	
		CHECKED	DATE	04/03/2022	
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		PROJECT No	FIGURE No		
	1220144				

PointID  
**CPT08A**

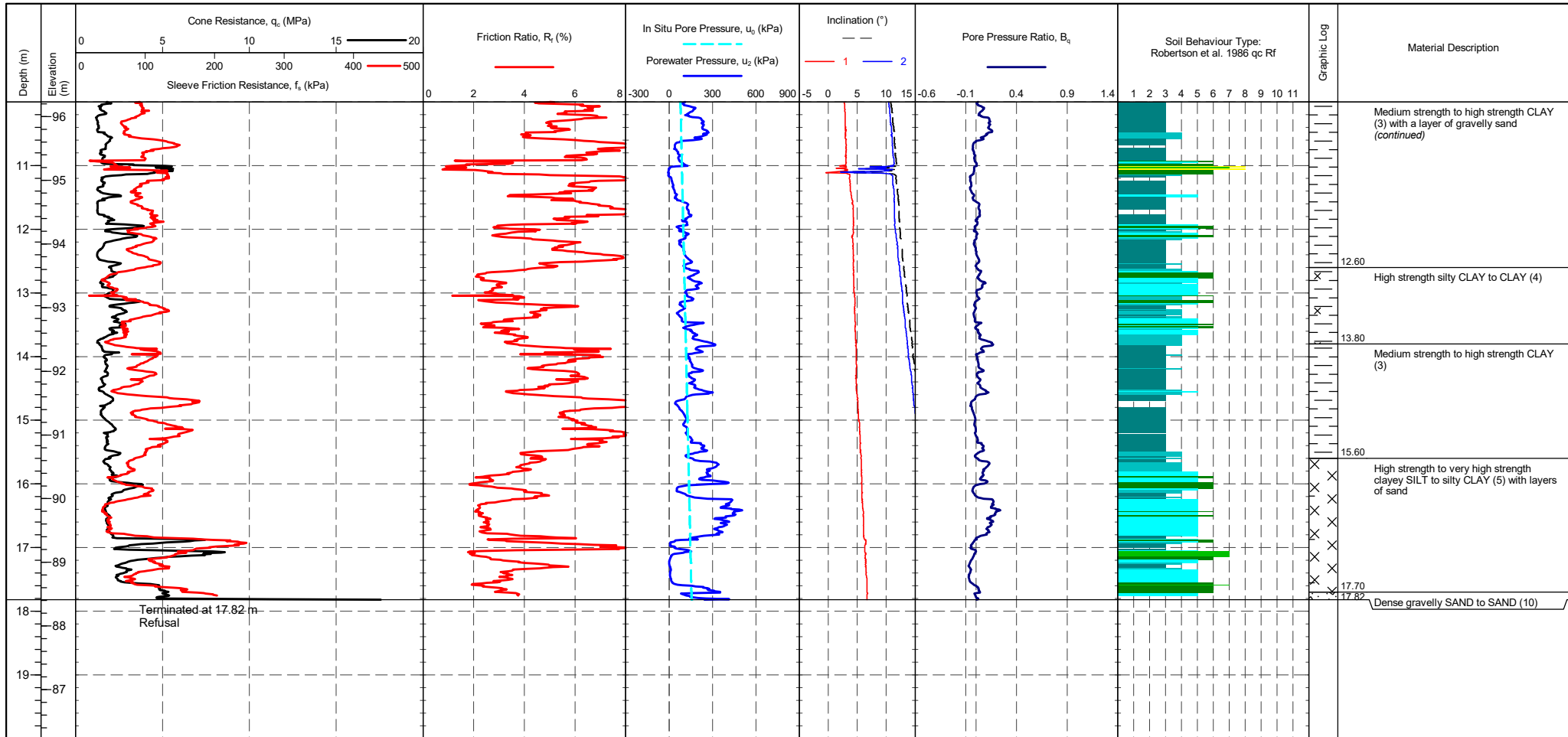
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490892.029 m <b>NORTHING</b> : 290837.383 m <b>ELEVATION</b> : 106.232 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip : 372 mV / 363 mV / -0.1 MPa Sleeve : 290 mV / 287 mV / -0.002 kPa Pore Pressure 2 : 220 mV / 243 mV / 0.005 kPa X-Y Inclinator : 2593 mV / 2686 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravelly SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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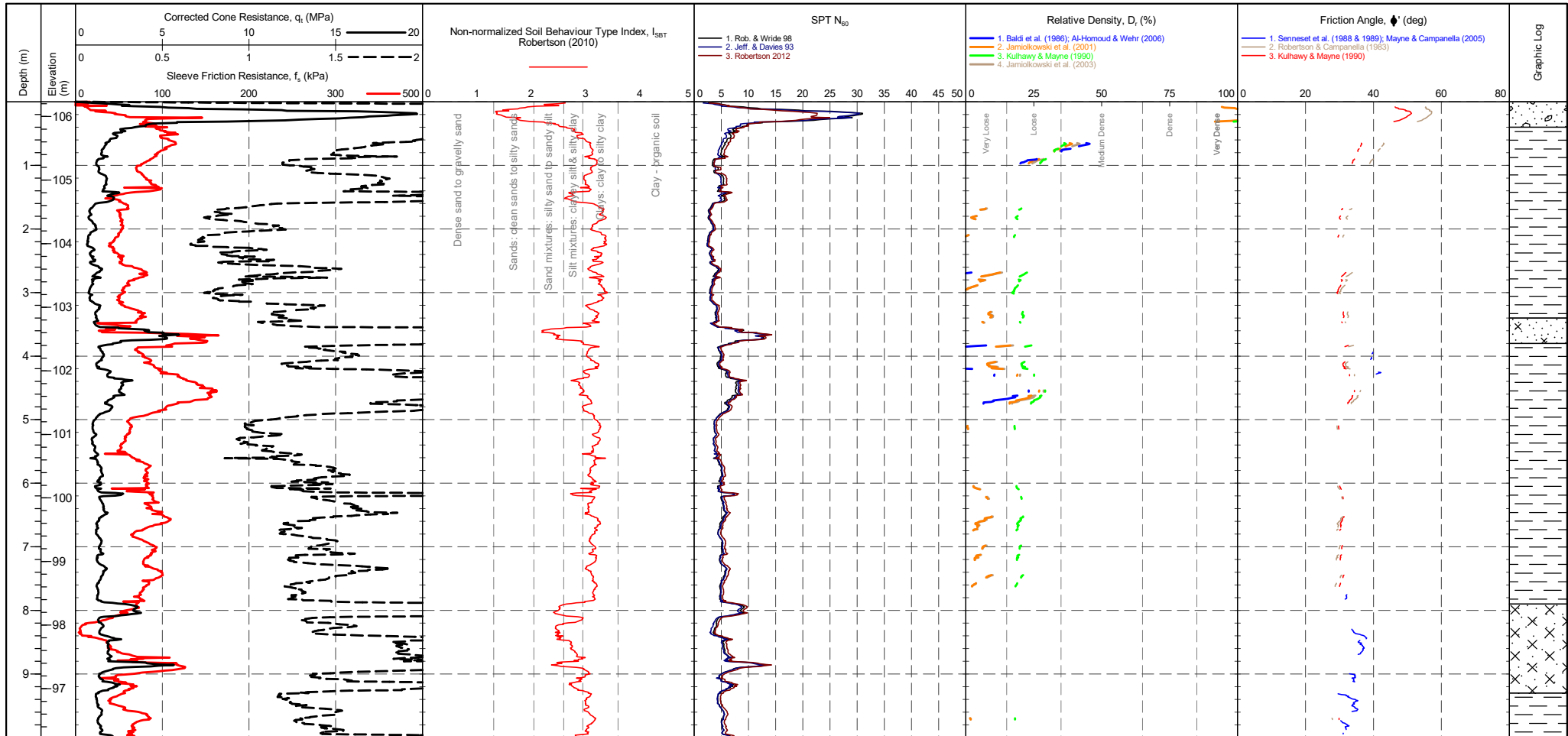
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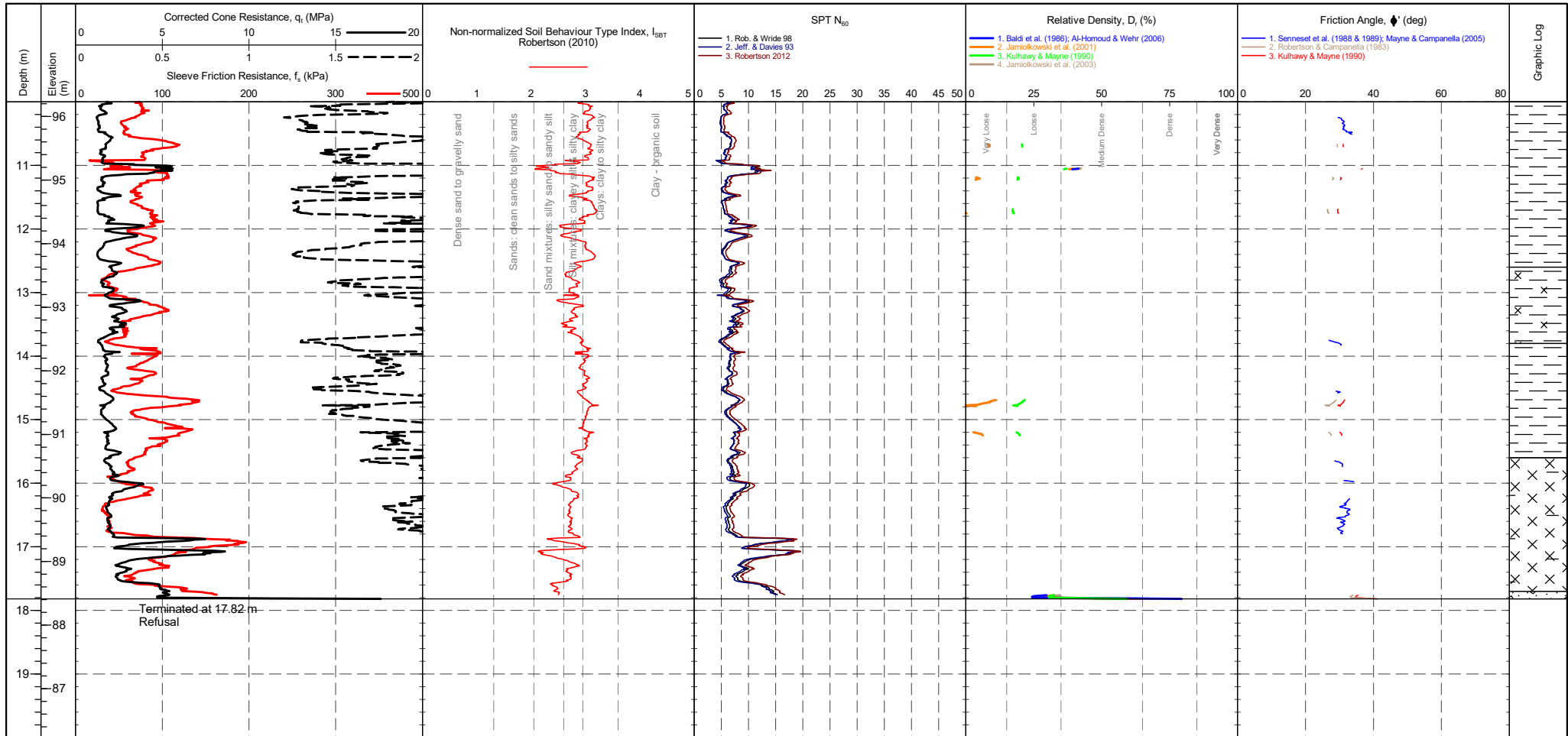


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PointID	<b>CPT08A</b>
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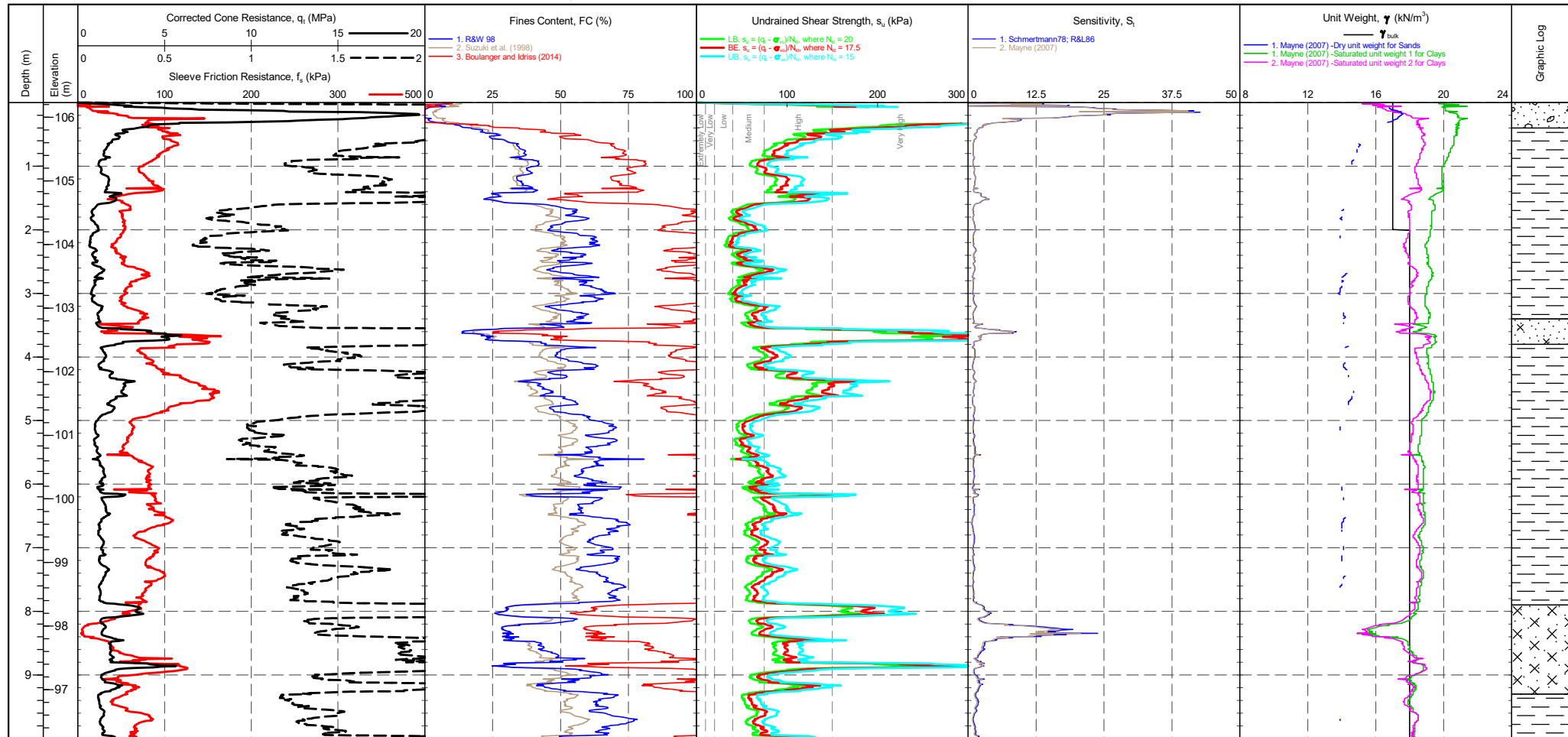
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490892.029 m <b>NORTHING</b> : 290837.383 m <b>ELEVATION</b> : 106.232 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>372 mV</td> <td>363 mV</td> <td>-0.1 MPa</td> </tr> <tr> <td>Sleeve</td> <td>290 mV</td> <td>287 mV</td> <td>-0.002 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>220 mV</td> <td>243 mV</td> <td>0.005 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2593 mV</td> <td>2686 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	372 mV	363 mV	-0.1 MPa	Sleeve	290 mV	287 mV	-0.002 kPa	Pore Pressure 2	220 mV	243 mV	0.005 kPa	X-Y Inclinator	2593 mV	2686 mV		<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, <math>I_c</math></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density <math>D_r</math> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, $I_c$	Description	SPT N value, NSPT	Description	Relative Density $D_r$ (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	▽ Groundwater Level  ▮ Dissipation Test
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PointID	<b>CPT08A</b>
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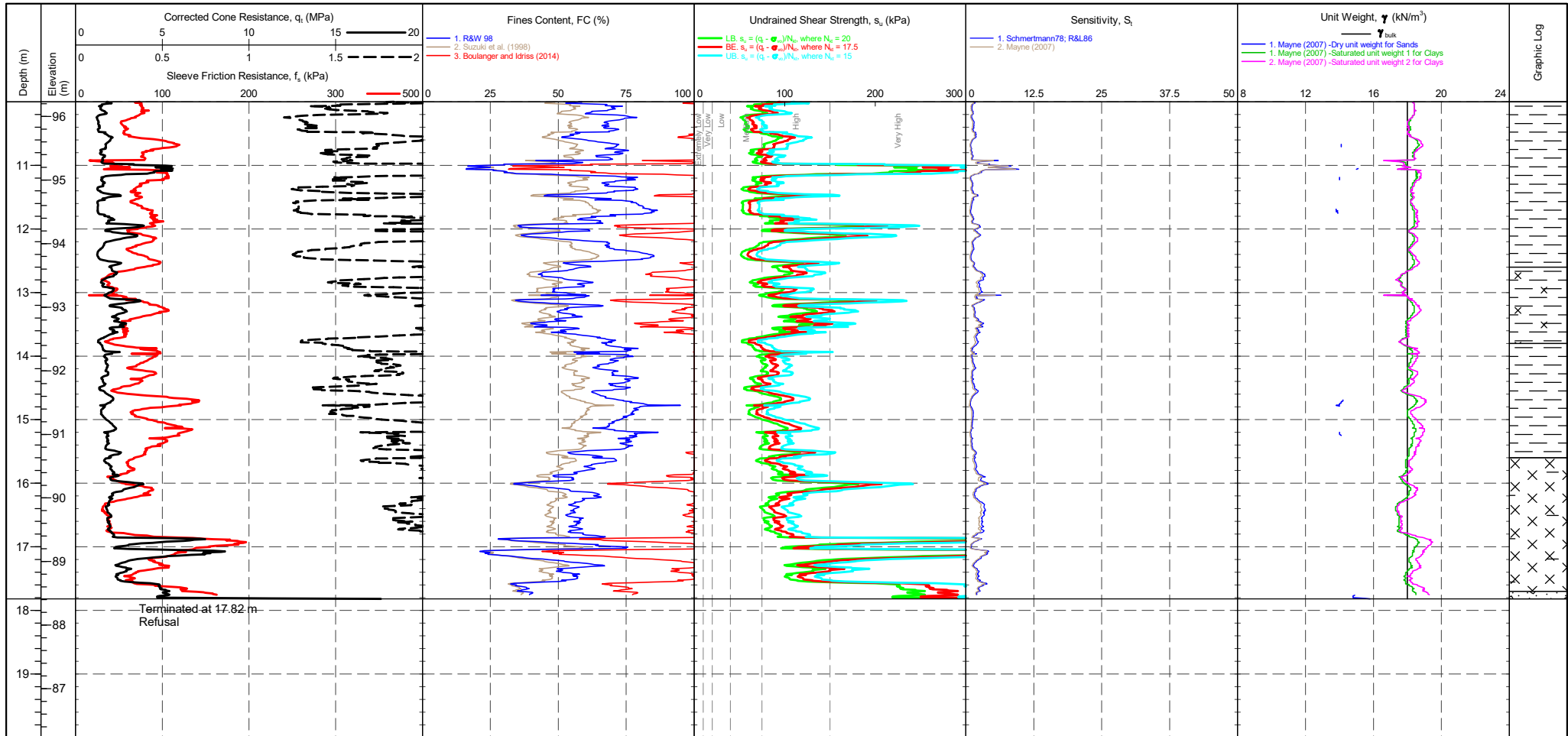
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490892.029 m <b>NORTHING</b> : 290837.383 m <b>ELEVATION</b> : 106.232 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 372 mV / 363 mV / -0.1 MPa Sleeve: 290 mV / 287 mV / -0.002 kPa Pore Pressure 2: 220 mV / 243 mV / 0.005 kPa X-Y Inclinator: 2593 mV / 2686 mV	<b>CPTU ZERO VALUES</b> Pre: 372 mV Post: 363 mV Difference: -0.1 MPa	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> <table border="1"> <tr> <th>Term based on measurement</th> <th>su (kPa)</th> <th>Term based on measurement</th> <th>su (kPa)</th> </tr> <tr> <td>Extremely low strength</td> <td>&lt;10</td> <td>Medium strength</td> <td>40-75</td> </tr> <tr> <td>Very low strength</td> <td>10-20</td> <td>High strength</td> <td>75-150</td> </tr> <tr> <td>Low strength</td> <td>20-40</td> <td>Very high strength</td> <td>150-300</td> </tr> <tr> <td></td> <td></td> <td>Extremely high strength</td> <td>&gt;300</td> </tr> </table>	Term based on measurement	su (kPa)	Term based on measurement	su (kPa)	Extremely low strength	<10	Medium strength	40-75	Very low strength	10-20	High strength	75-150	Low strength	20-40	Very high strength	150-300			Extremely high strength	>300	<b>Groundwater Level</b>  <b>Dissipation Test</b> 
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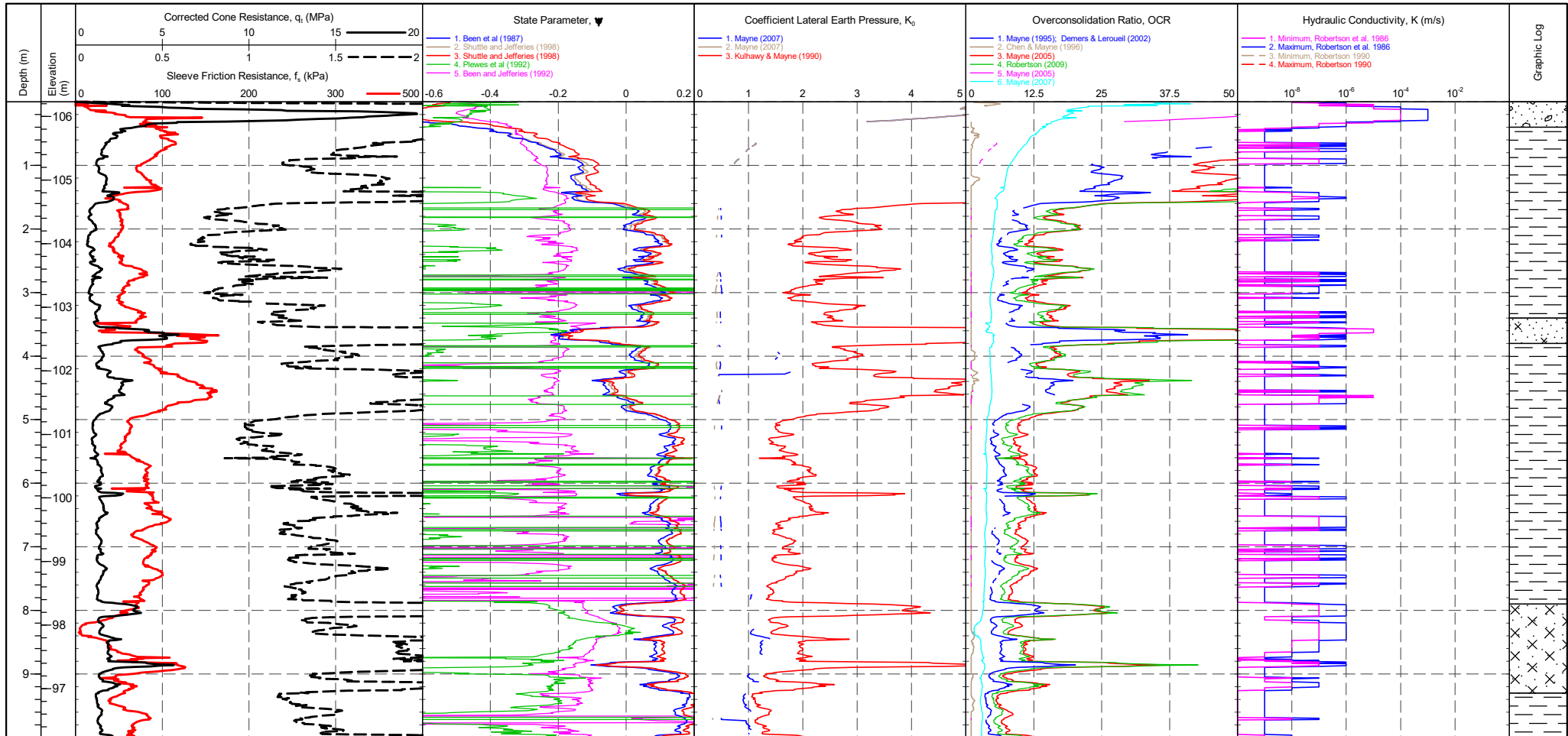
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490892.029 m <b>NORTHING</b> : 290837.383 m <b>ELEVATION</b> : 106.232 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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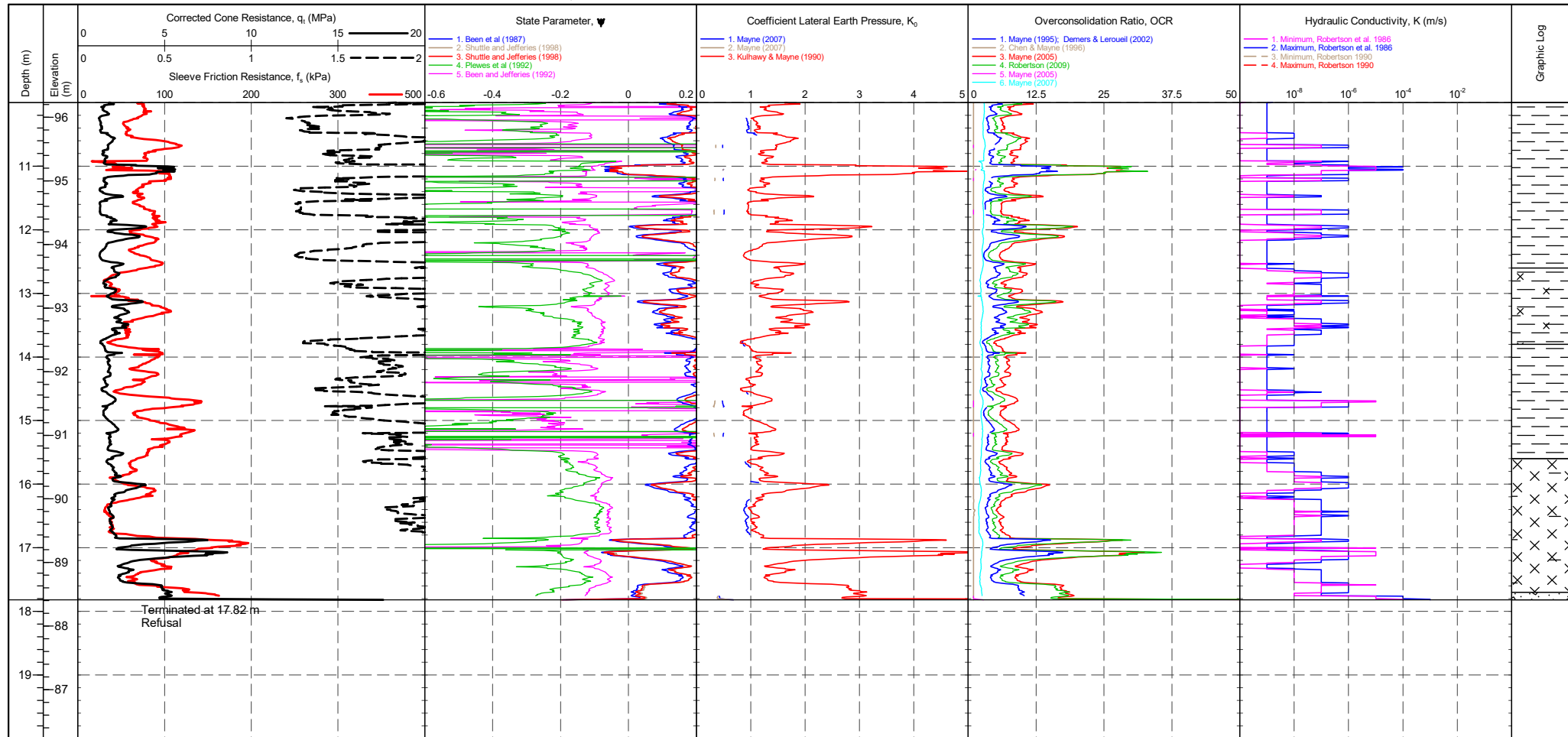
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490892.029 m <b>NORTHING</b> : 290837.383 m <b>ELEVATION</b> : 106.232 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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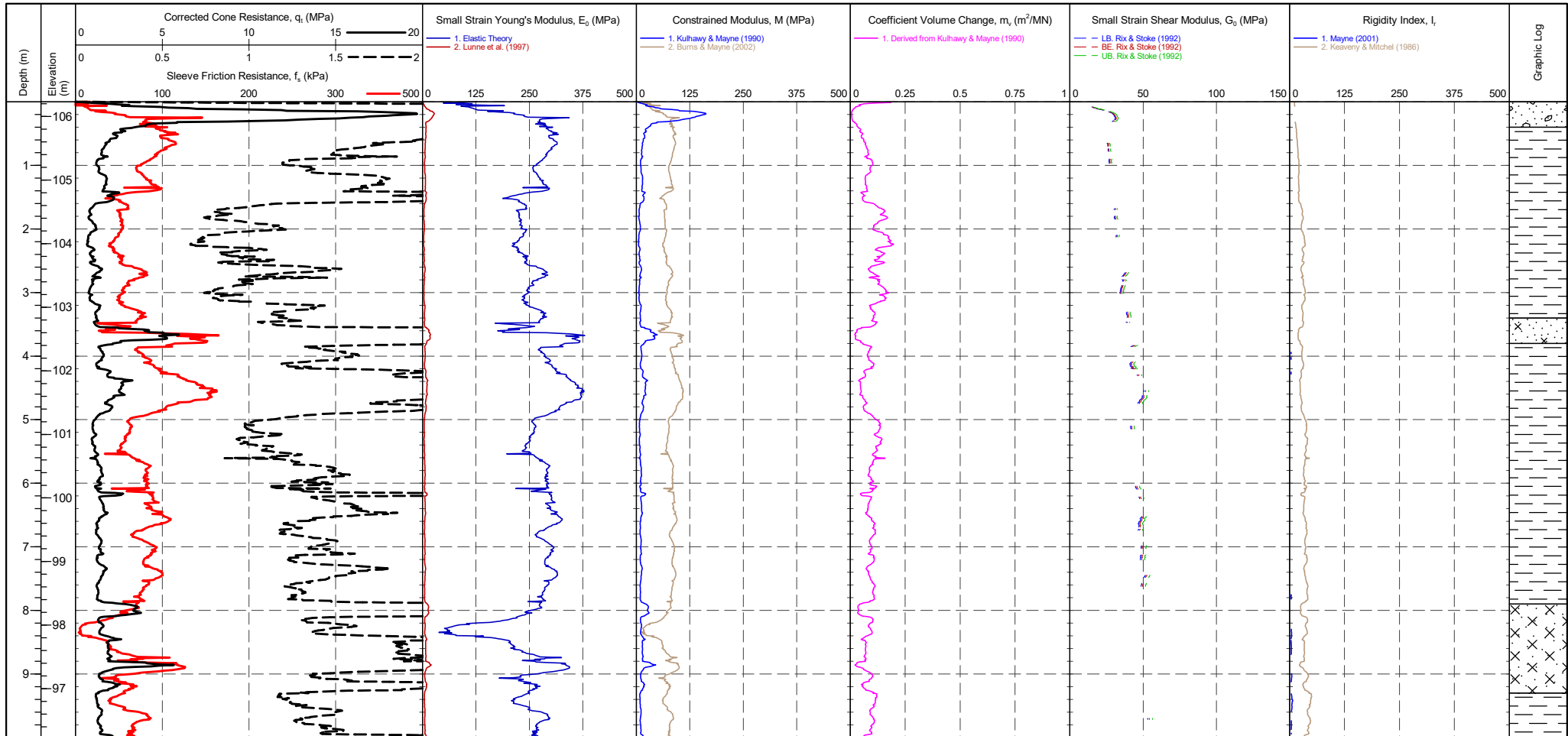
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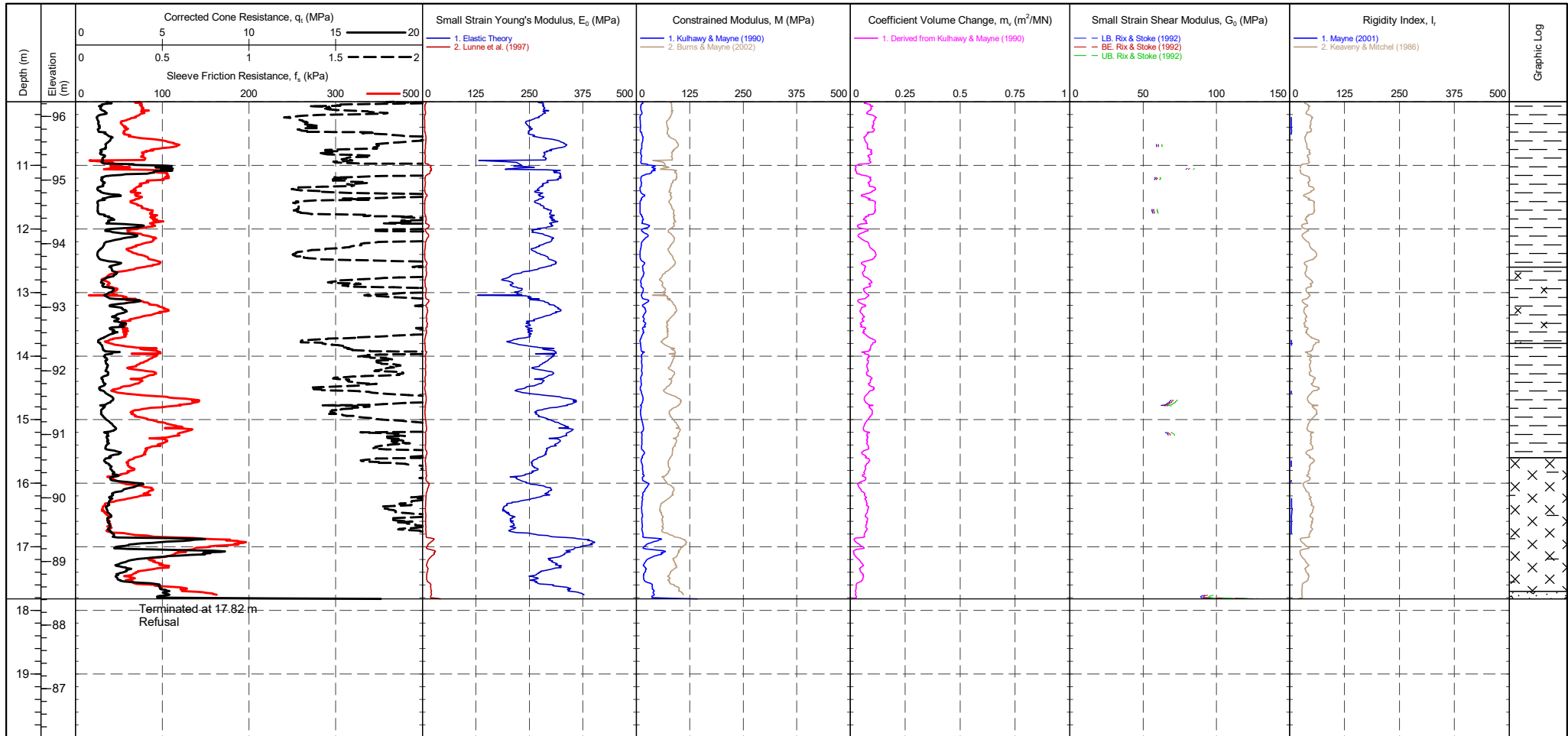
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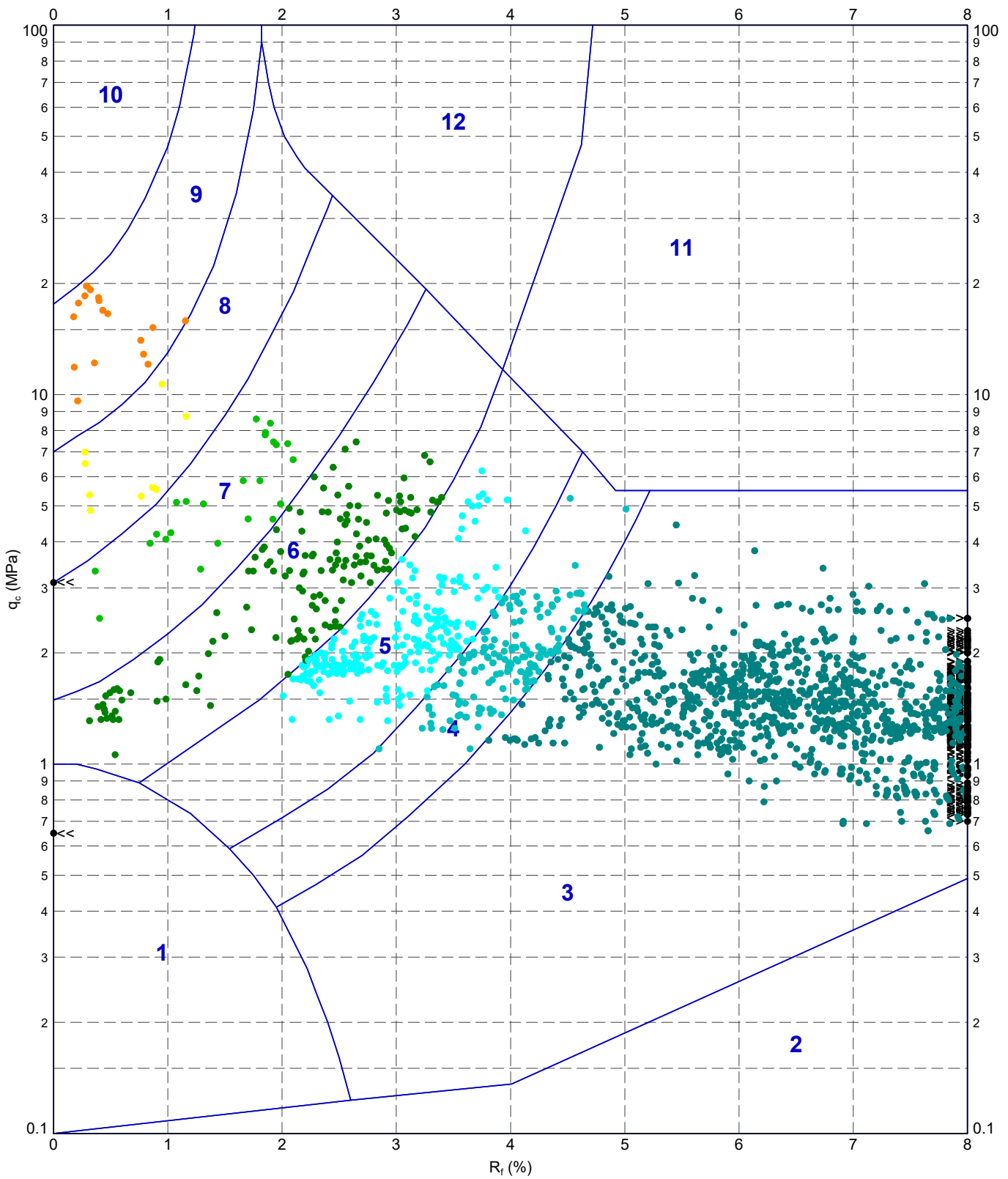
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METHOD: Robertson et al. 1986 qc Rf

- 1 - Sensitive fine grained material
- 4 - Silty CLAY to CLAY
- 7 - Silty SAND to sandy SILT
- 10 - Gravelly SAND to SAND
- 2 - Organic material
- 5 - Clayey SILT to silty CLAY
- 8 - SAND to silty SAND
- 11 - Very stiff fine grained
- 3 - CLAY
- 6 - Sandy SILT to clayey SILT
- 9 - SAND
- 12 - SAND to clayey SAND

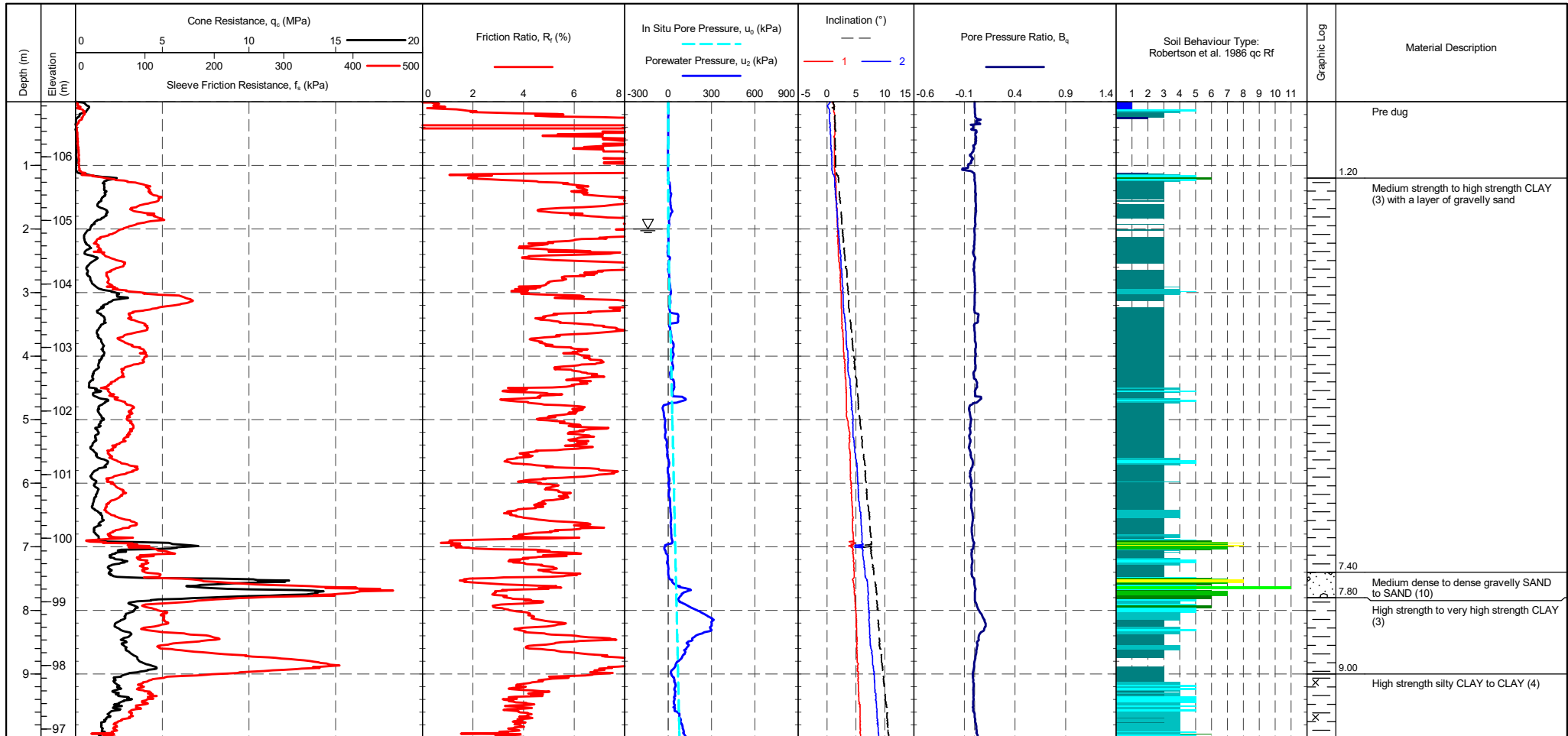


TITLE  
 Delta Simons  
 Cordby  
 Corby  
 Robertson et al. 1986 qc vs. Rf - CPT08A

DRAWN	DATE	04/03/2022
CHECKED	DATE	04/03/2022
SCALE	Not To Scale	
PROJECT No	1220144	
FIGURE No	A4	

PointID  
**CPT09**

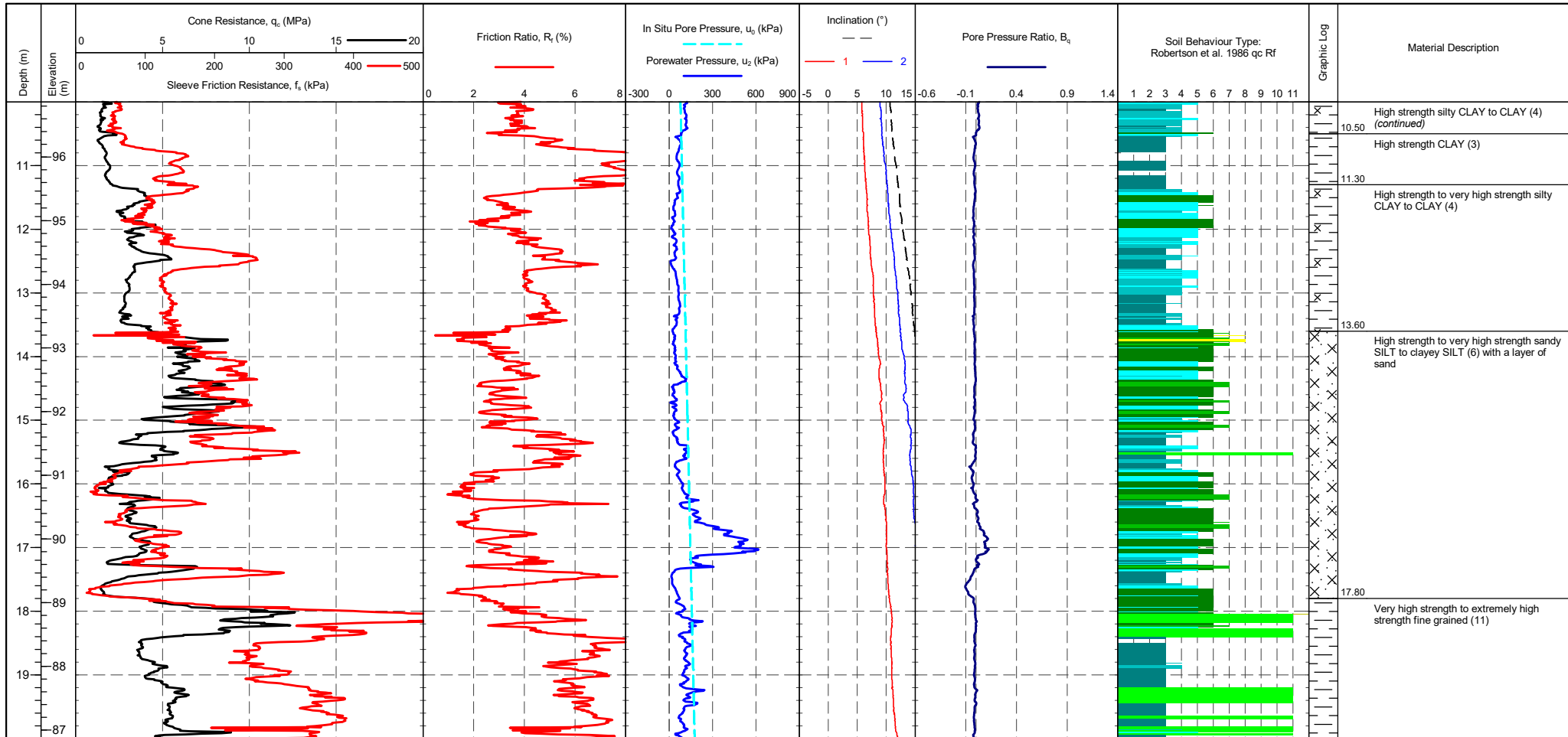
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip: Pre 363 mV, Post 357 mV, Difference -0.066 MPa Sleeve: Pre 288 mV, Post 283 mV, Difference -0.004 kPa Pore Pressure 2: Pre 235 mV, Post 197 mV, Difference -0.009 kPa X-Y Inclinometer: Pre 2618 mV, Post 2599 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravelly SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID	<b>CPT09</b>
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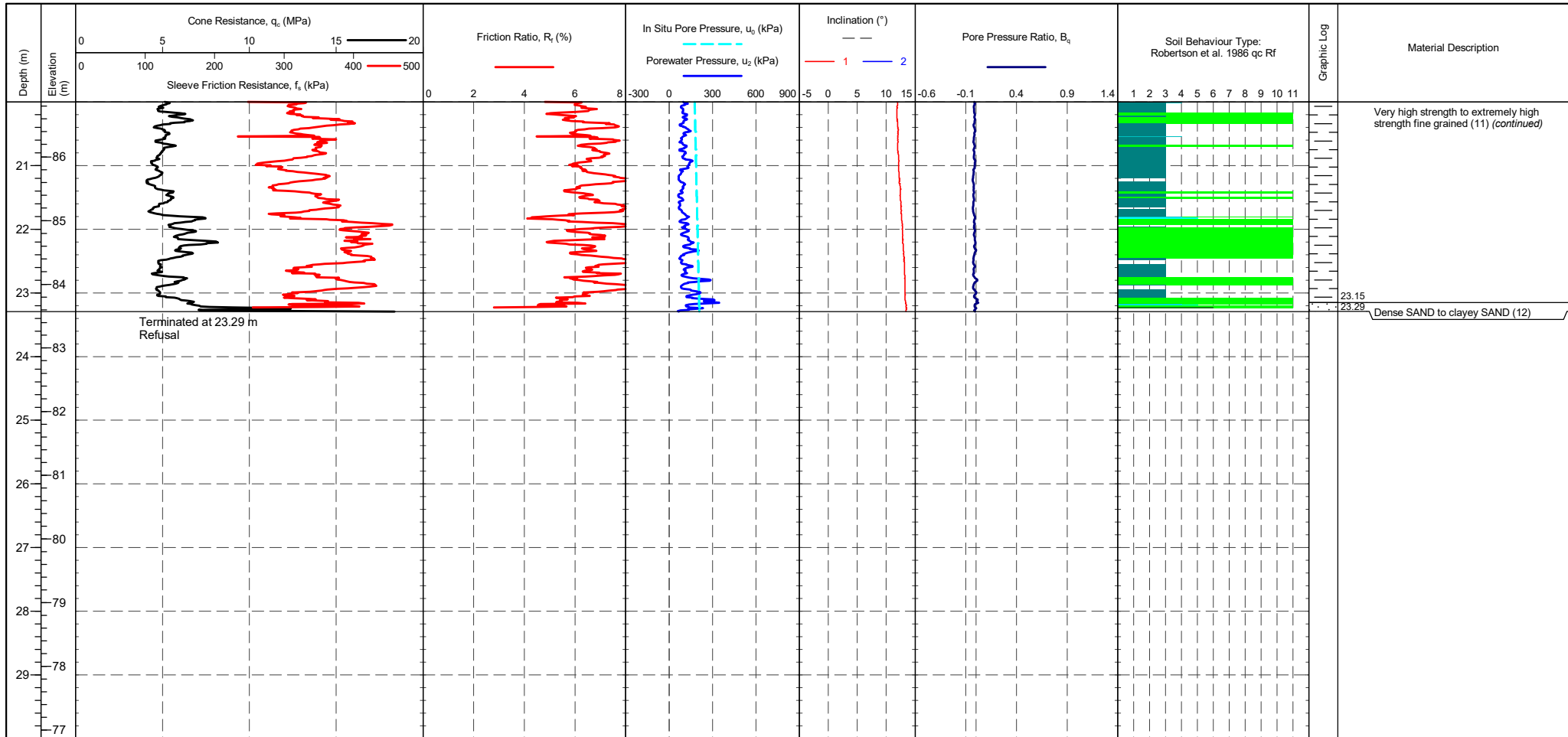
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490918.124 m <b>NORTHING</b> : 290906.184 m <b>ELEVATION</b> : 106.865 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 3 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip : 363 mV / 357 mV / -0.066 MPa Sleeve : 288 mV / 283 mV / -0.004 kPa Pore Pressure 2 : 235 mV / 197 mV / -0.009 kPa X-Y Inclinometer : 2618 mV / 2599 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravely SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID	<b>CPT09</b>
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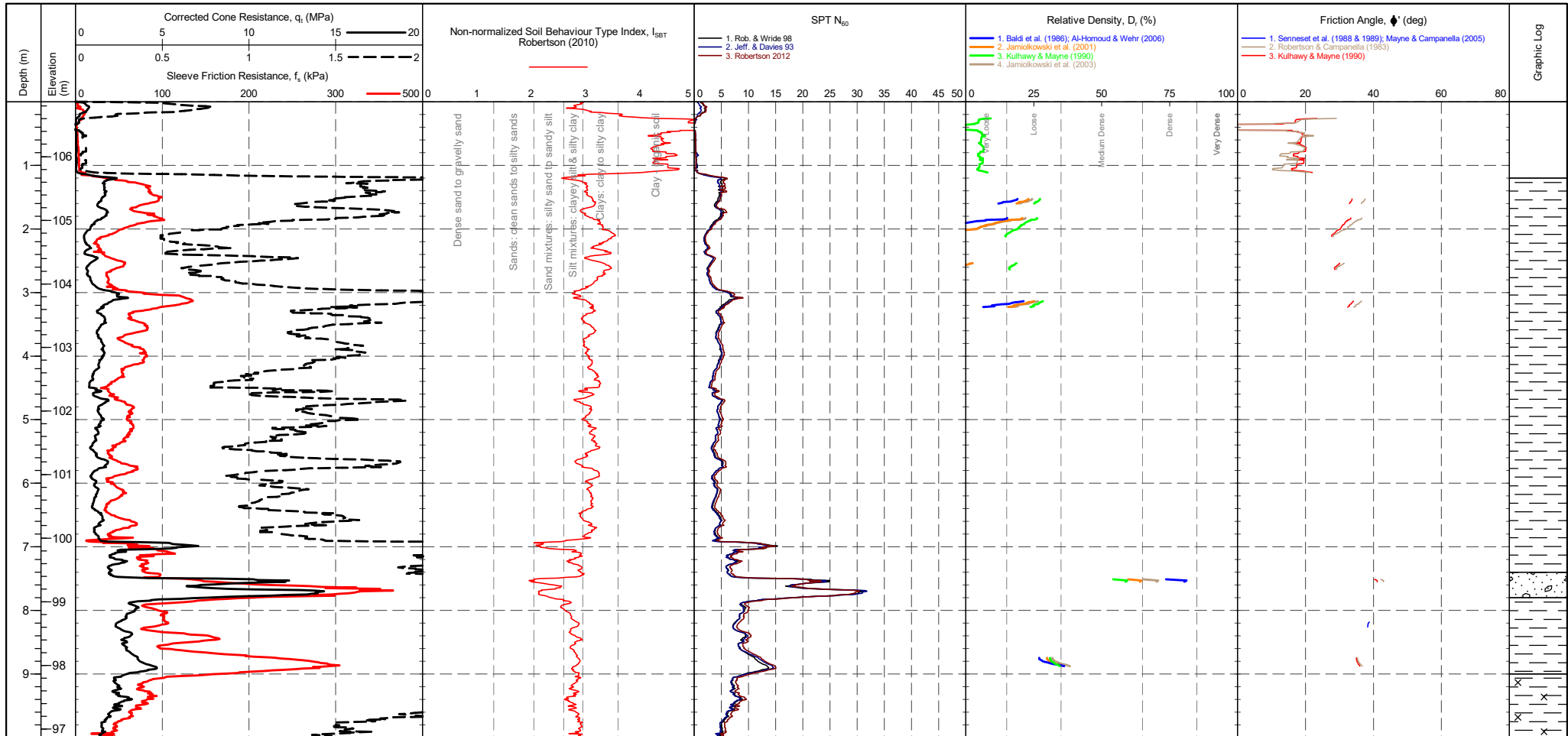
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490918.124 m <b>NORTHING</b> : 290906.184 m <b>ELEVATION</b> : 106.865 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 3 OF 3 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip Pre 363 mV Post 357 mV Difference -0.066 MPa Sleeve 288 mV 283 mV -0.004 kPa Pore Pressure 2 235 mV 197 mV -0.009 kPa X-Y Inclinator 2618 mV 2599 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravely SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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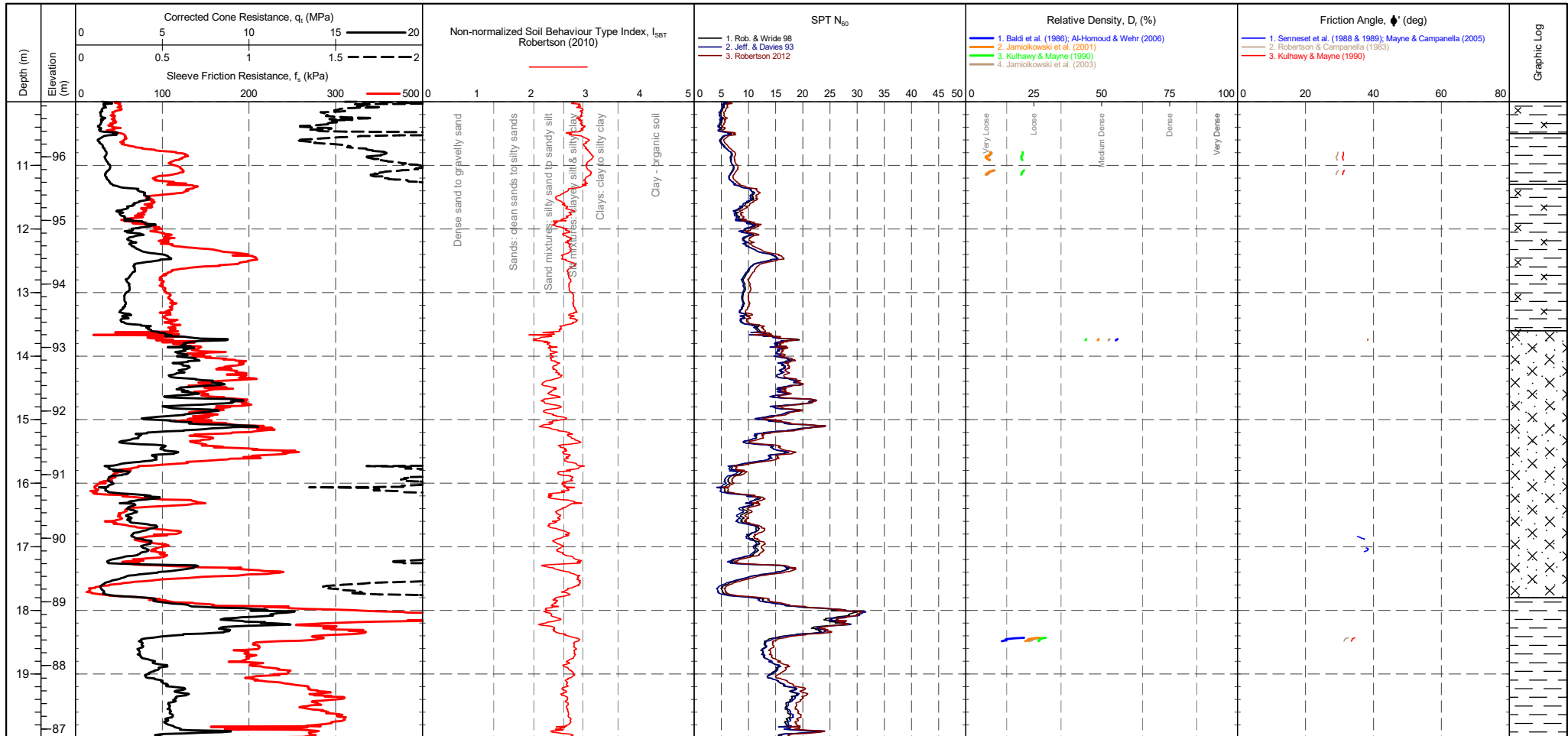
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> Transducer Tip : 363 mV / 357 mV / -0.066 MPa Sleeve : 288 mV / 283 mV / -0.004 kPa Pore Pressure 2 : 235 mV / 197 mV / -0.009 kPa X-Y Inclinator : 2618 mV / 2599 mV	<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, <math>I_c</math></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density <math>D_r</math> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, $I_c$	Description	SPT N value, NSPT	Description	Relative Density $D_r$ (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	▽ Groundwater Level  ▮ Dissipation Test
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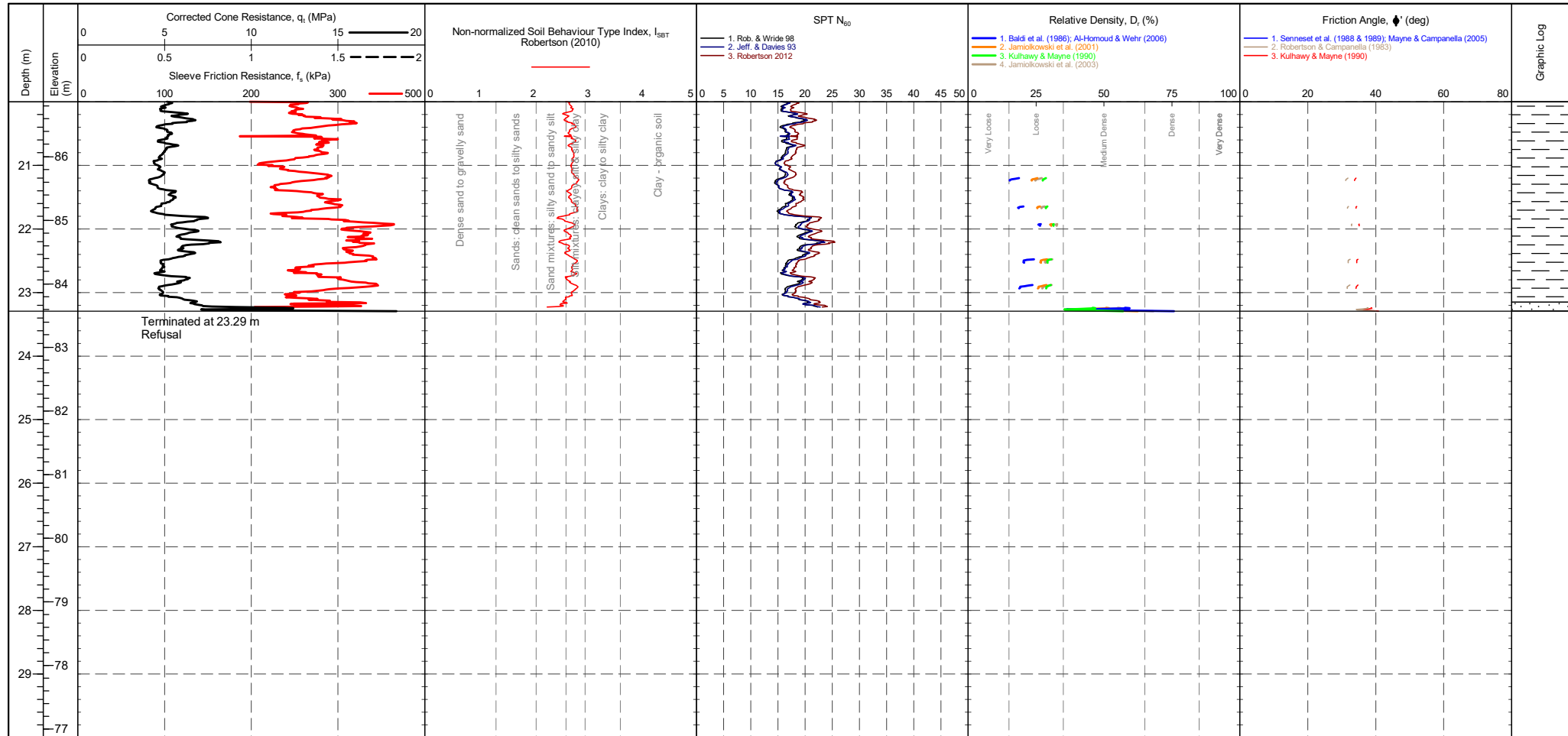
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490918.124 m <b>NORTHING</b> : 290906.184 m <b>ELEVATION</b> : 106.865 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 3 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> Transducer Pre Post Difference Tip 363 mV 357 mV -0.066 MPa Sleeve 288 mV 283 mV -0.004 kPa Pore Pressure 2 235 mV 197 mV -0.009 kPa X-Y Inclinator 2618 mV 2599 mV	<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, <math>I_c</math></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density <math>D_r</math> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, $I_c$	Description	SPT N value, NSPT	Description	Relative Density $D_r$ (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	▽ Groundwater Level  ▮ Dissipation Test
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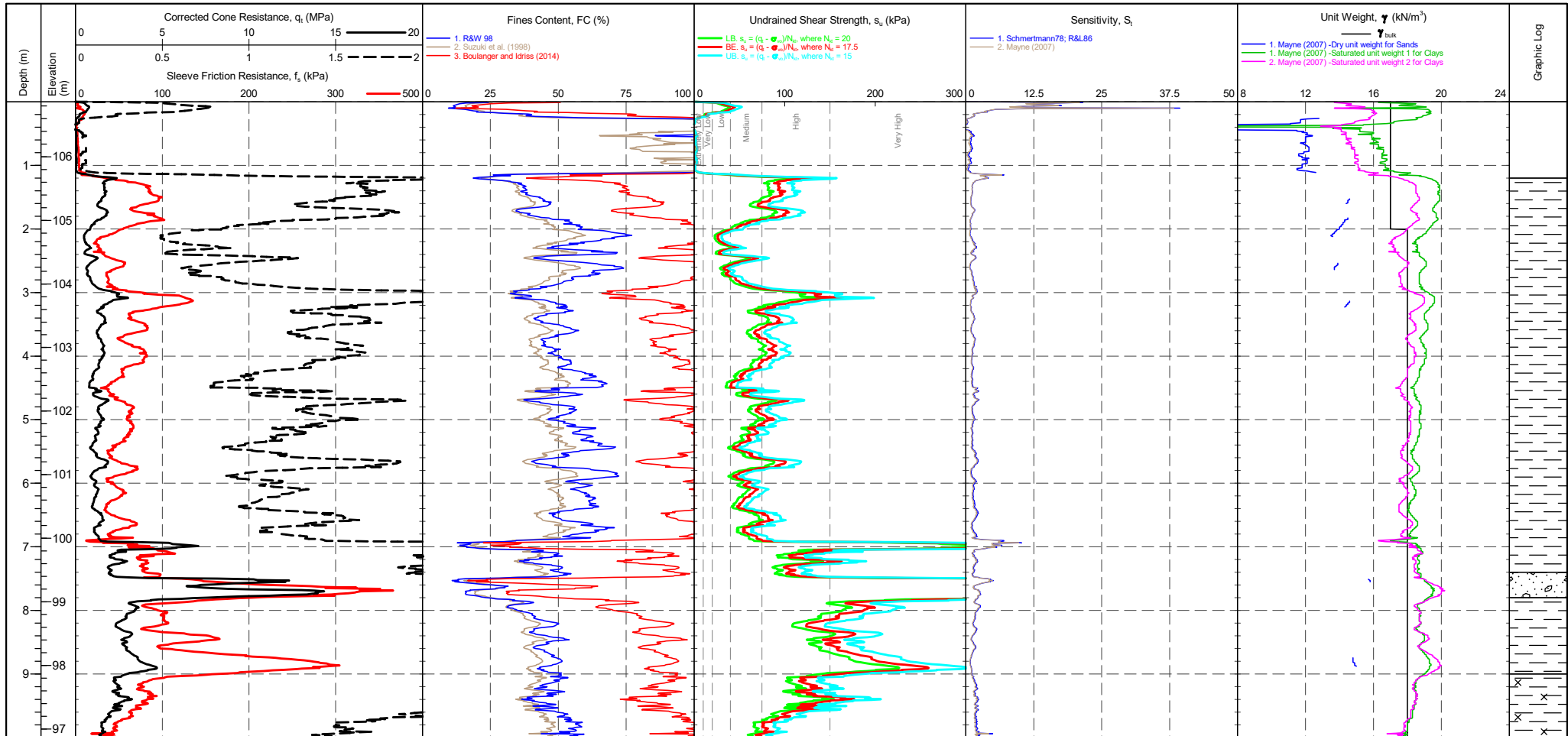


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>363 mV</td> <td>357 mV</td> <td>-0.066 MPa</td> </tr> <tr> <td>Sleeve</td> <td>288 mV</td> <td>283 mV</td> <td>-0.004 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>235 mV</td> <td>197 mV</td> <td>-0.009 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2618 mV</td> <td>2599 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	363 mV	357 mV	-0.066 MPa	Sleeve	288 mV	283 mV	-0.004 kPa	Pore Pressure 2	235 mV	197 mV	-0.009 kPa	X-Y Inclinator	2618 mV	2599 mV		<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, <math>I_c</math></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density <math>D_r</math> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, $I_c$	Description	SPT N value, NSPT	Description	Relative Density $D_r$ (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	▽ Groundwater Level      Dissipation Test
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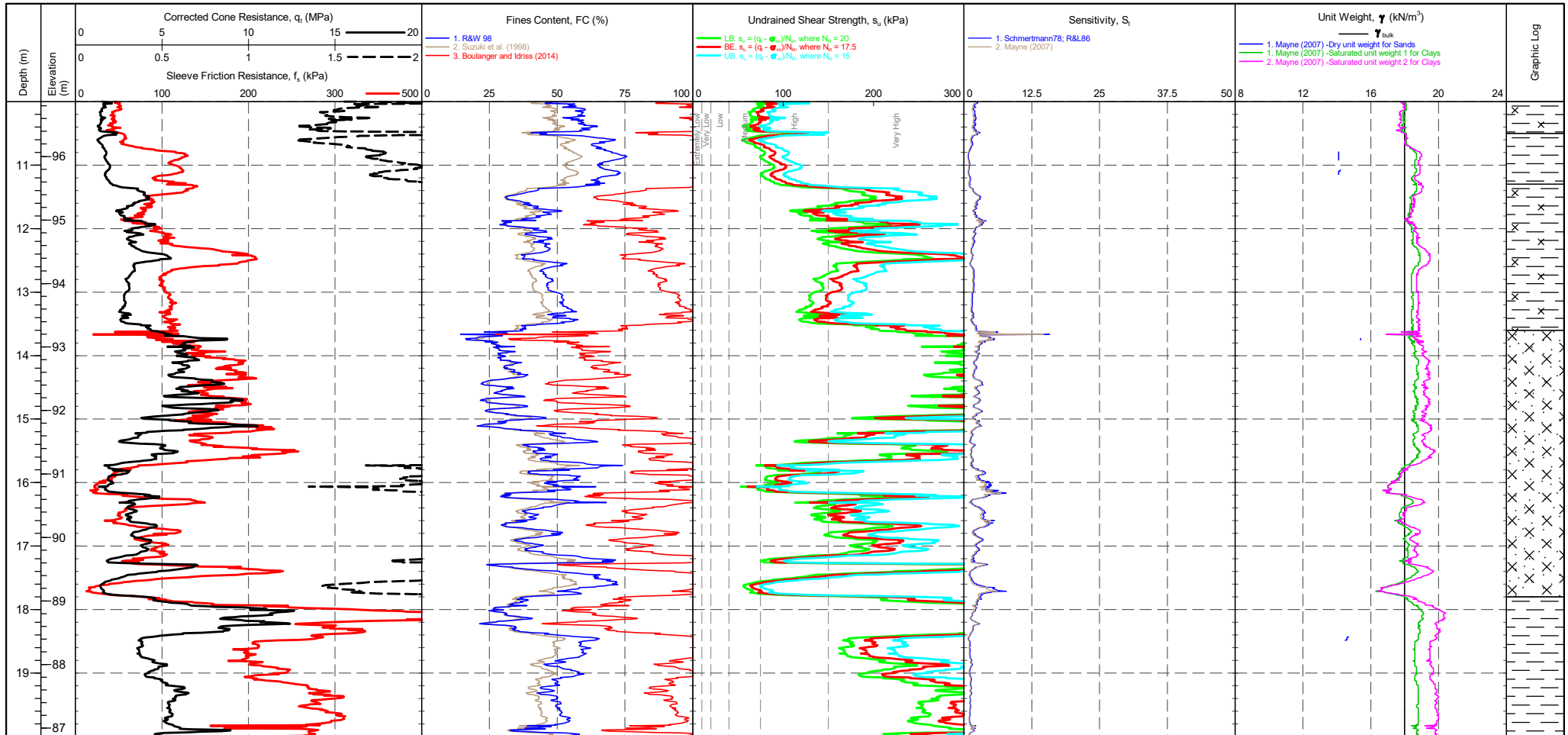


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> Transducer Pre Post Difference Tip 363 mV 357 mV -0.066 MPa Sleeve 288 mV 283 mV -0.004 kPa Pore Pressure 2 235 mV 197 mV -0.009 kPa X-Y Inclinator 2618 mV 2599 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> <table border="1"> <thead> <tr> <th>Term based on measurement</th> <th>su (kPa)</th> <th>Term based on measurement</th> <th>su (kPa)</th> </tr> </thead> <tbody> <tr> <td>Extremely low strength</td> <td>&lt;10</td> <td>Medium strength</td> <td>40-75</td> </tr> <tr> <td>Very low strength</td> <td>10-20</td> <td>High strength</td> <td>75-150</td> </tr> <tr> <td>Low strength</td> <td>20-40</td> <td>Very high strength</td> <td>150-300</td> </tr> <tr> <td></td> <td></td> <td>Extremely high strength</td> <td>&gt;300</td> </tr> </tbody> </table>	Term based on measurement	su (kPa)	Term based on measurement	su (kPa)	Extremely low strength	<10	Medium strength	40-75	Very low strength	10-20	High strength	75-150	Low strength	20-40	Very high strength	150-300			Extremely high strength	>300	▽ Groundwater Level ▩ Dissipation Test
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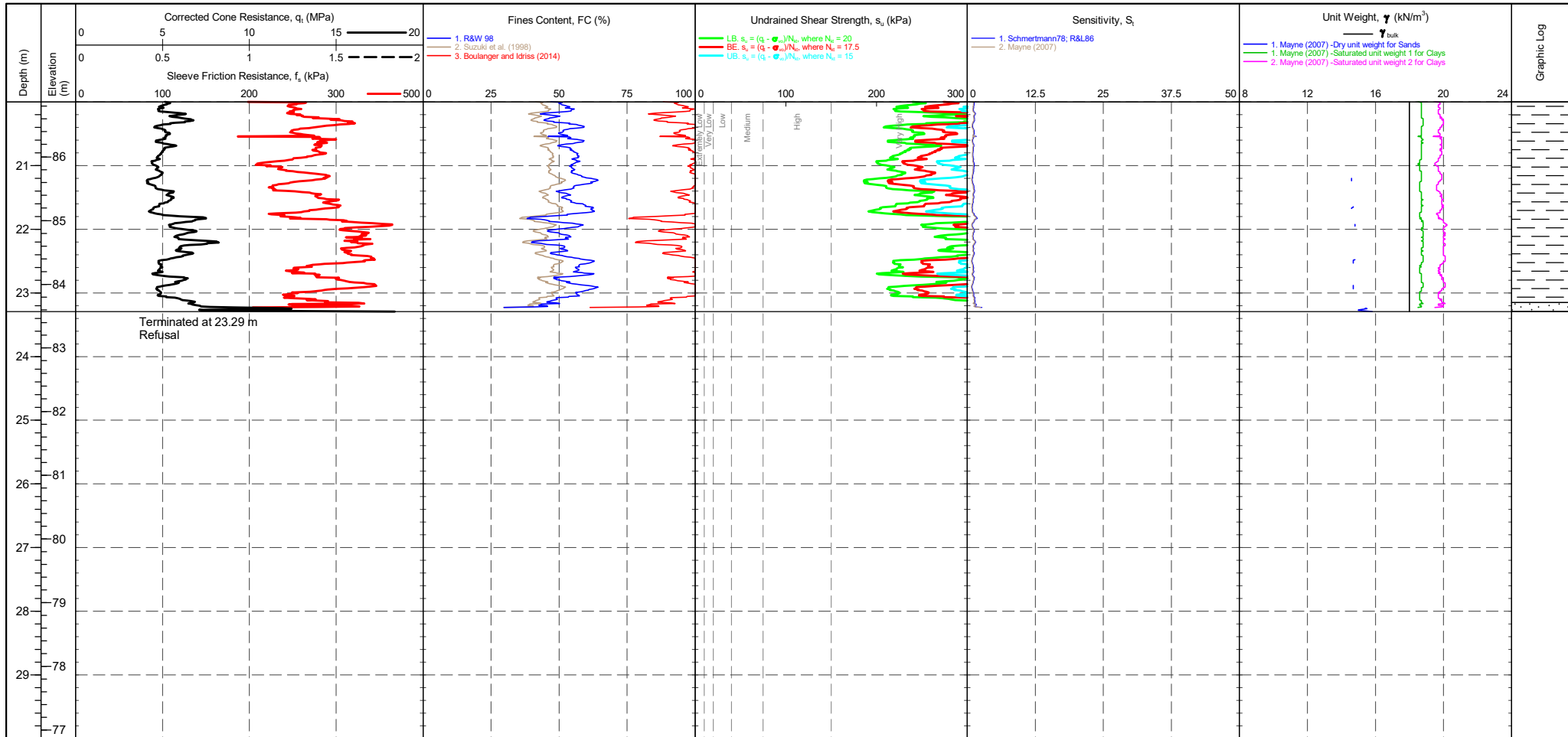
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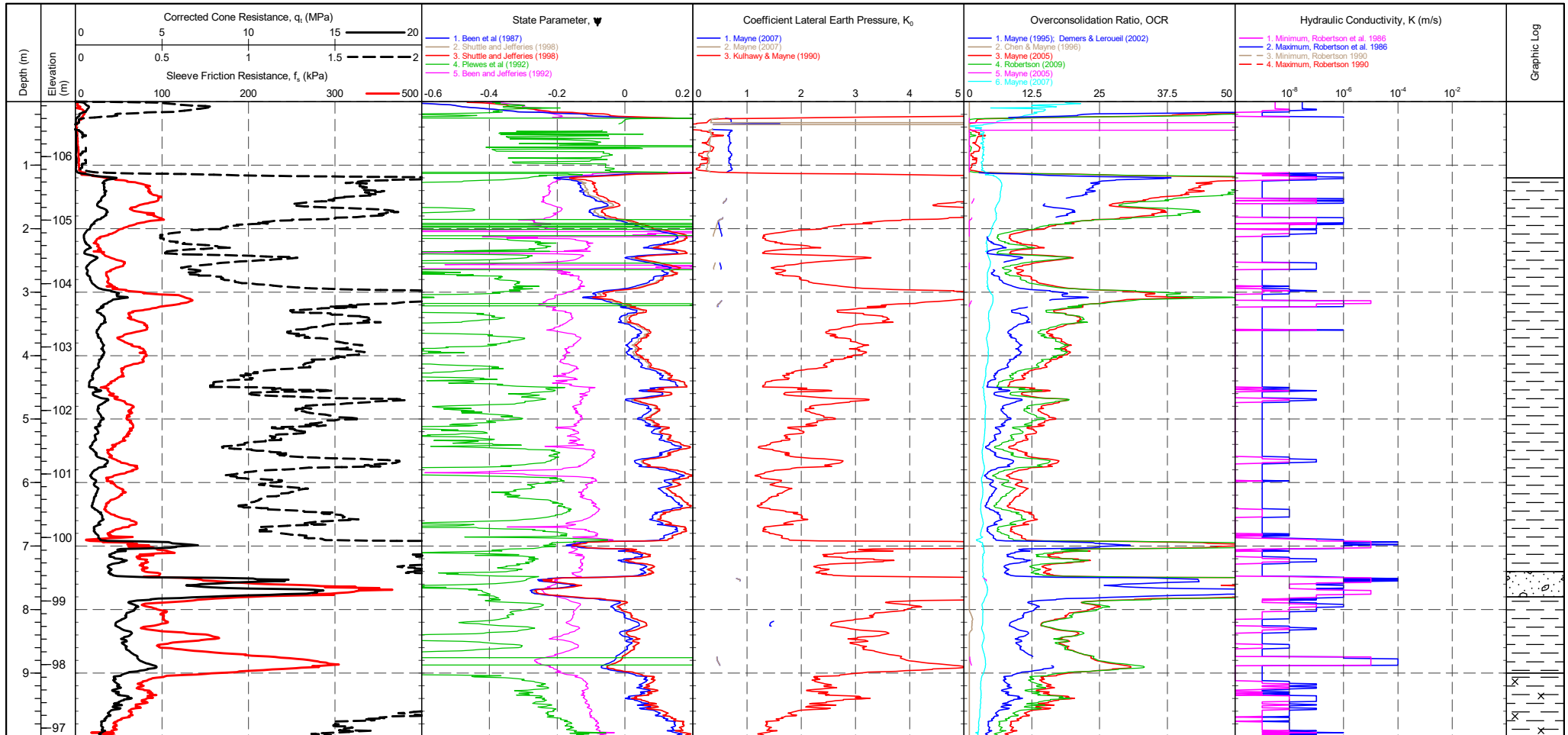


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 363 mV Sleeve: 288 mV Pore Pressure 2: 235 mV X-Y Inclinator: 2618 mV	<b>CPTU ZERO VALUES</b> Post: 357 mV Difference: -0.066 MPa 283 mV -0.004 kPa 197 mV -0.009 kPa 2599 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement su (kPa) Extremely low strength <10 Very low strength 10-20 Low strength 20-40	Term based on measurement su (kPa) Medium strength 40-75 High strength 75-150 Very high strength 150-300 Extremely high strength >300	Groundwater Level Dissipation Test
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PointID

**CPT09**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490918.124 m <b>NORTHING</b> : 290906.184 m <b>ELEVATION</b> : 106.865 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 3 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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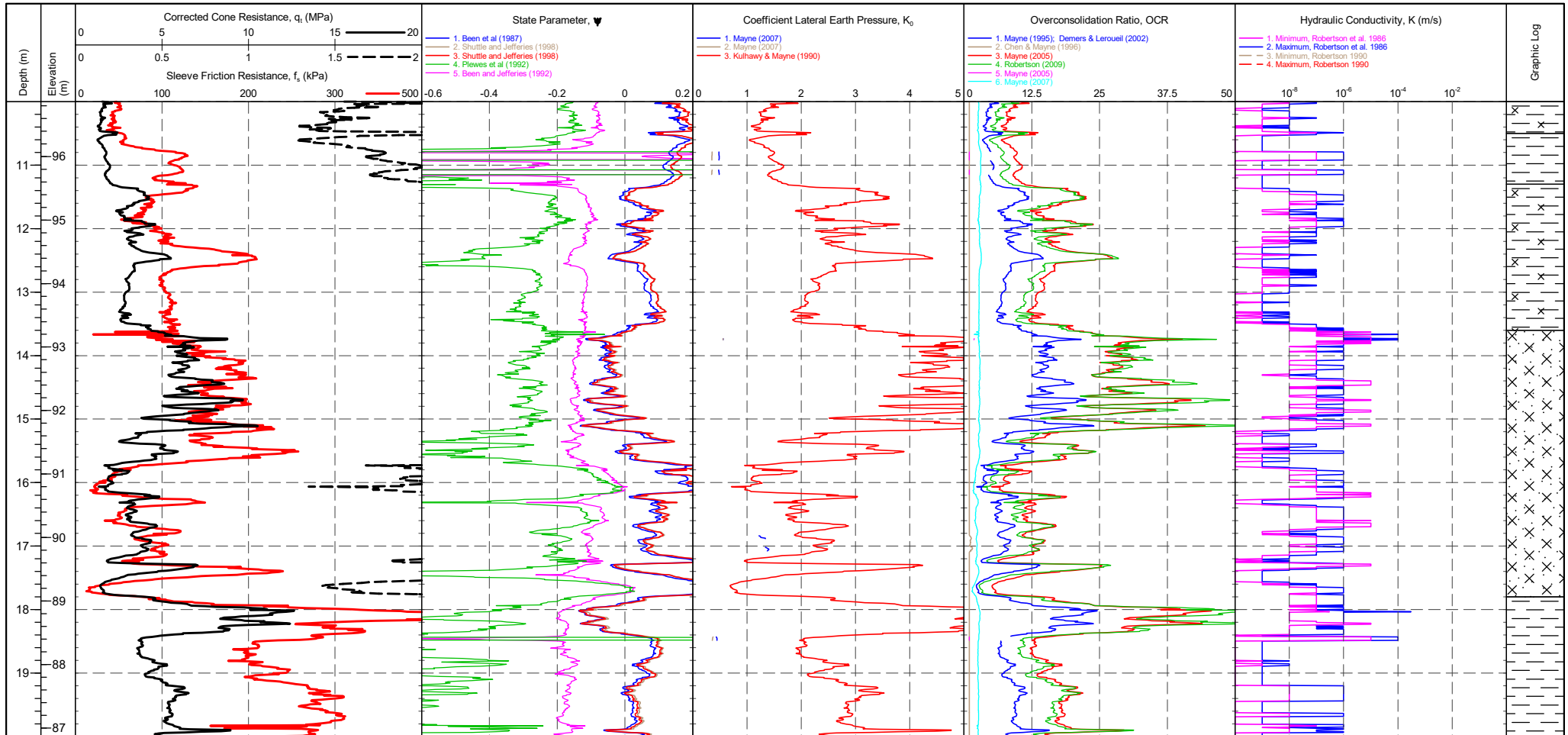


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>363 mV</td> <td>357 mV</td> <td>-0.066 MPa</td> </tr> <tr> <td>Sleeve</td> <td>288 mV</td> <td>283 mV</td> <td>-0.004 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>235 mV</td> <td>197 mV</td> <td>-0.009 kPa</td> </tr> <tr> <td>X-Y inclinometer</td> <td>2618 mV</td> <td>2599 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	363 mV	357 mV	-0.066 MPa	Sleeve	288 mV	283 mV	-0.004 kPa	Pore Pressure 2	235 mV	197 mV	-0.009 kPa	X-Y inclinometer	2618 mV	2599 mV		Groundwater Level Dissipation Test
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490918.124 m <b>NORTHING</b> : 290906.184 m <b>ELEVATION</b> : 106.865 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 3 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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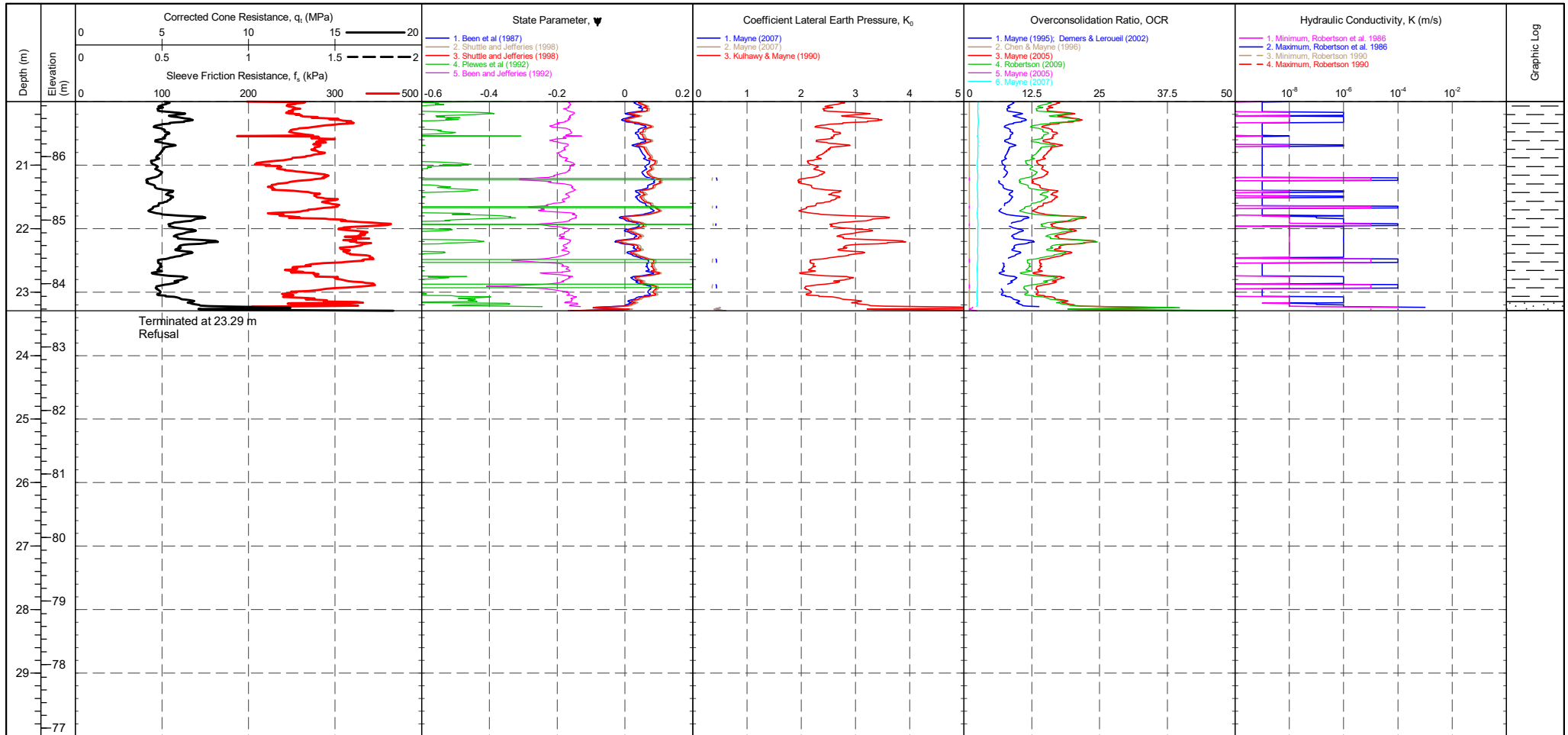


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>363 mV</td> <td>357 mV</td> <td>-0.066 MPa</td> </tr> <tr> <td>Sleeve</td> <td>288 mV</td> <td>283 mV</td> <td>-0.004 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>235 mV</td> <td>197 mV</td> <td>-0.009 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2618 mV</td> <td>2599 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	363 mV	357 mV	-0.066 MPa	Sleeve	288 mV	283 mV	-0.004 kPa	Pore Pressure 2	235 mV	197 mV	-0.009 kPa	X-Y Inclinator	2618 mV	2599 mV		Groundwater Level Dissipation Test
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CPT09

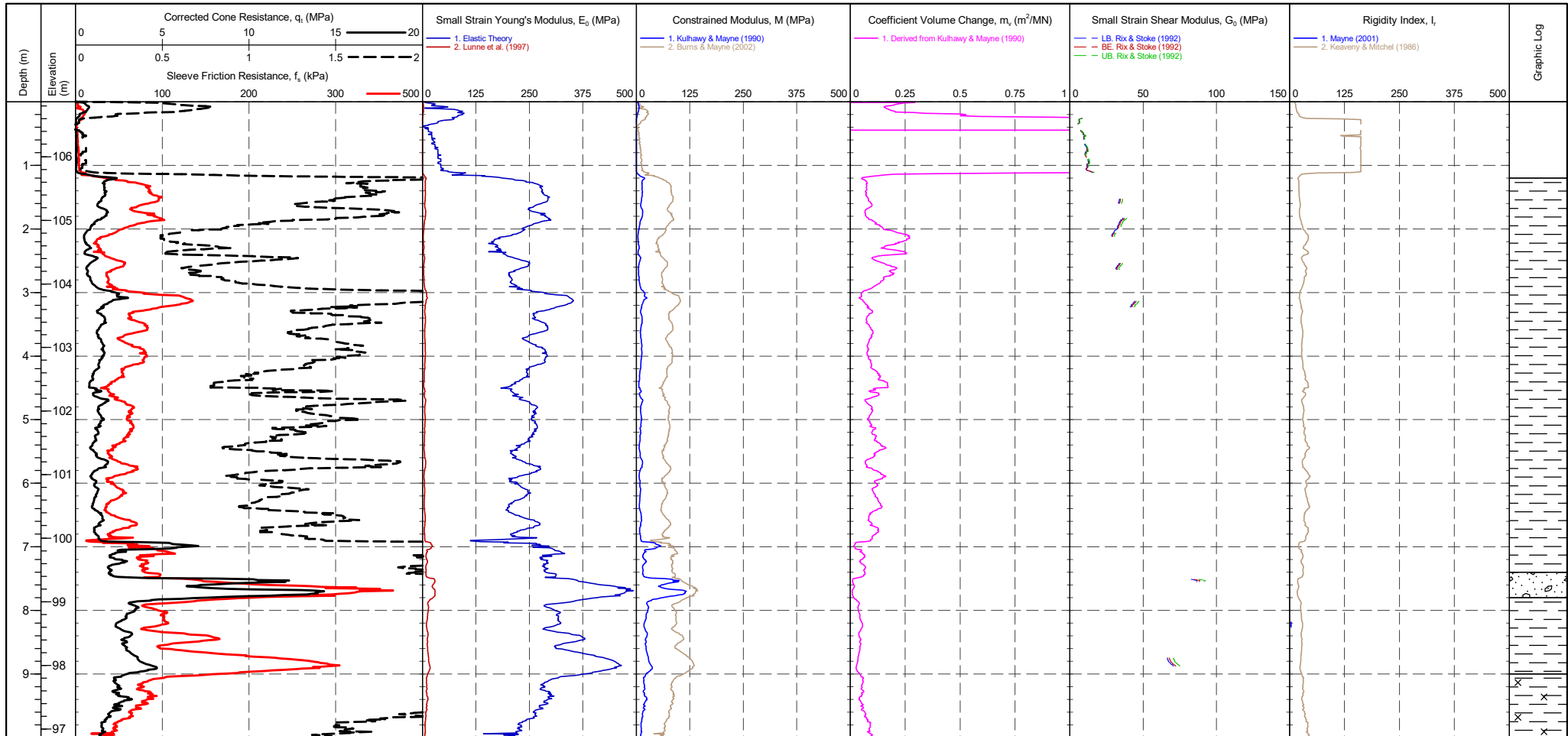
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490918.124 m <b>NORTHING</b> : 290906.184 m <b>ELEVATION</b> : 106.865 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 3 OF 3 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>363 mV</td> <td>357 mV</td> <td>-0.066 MPa</td> </tr> <tr> <td>Sleeve</td> <td>288 mV</td> <td>283 mV</td> <td>-0.004 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>235 mV</td> <td>197 mV</td> <td>-0.009 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2618 mV</td> <td>2599 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	363 mV	357 mV	-0.066 MPa	Sleeve	288 mV	283 mV	-0.004 kPa	Pore Pressure 2	235 mV	197 mV	-0.009 kPa	X-Y Inclinator	2618 mV	2599 mV		Groundwater Level Dissipation Test
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**CPT09**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490918.124 m <b>NORTHING</b> : 290906.184 m <b>ELEVATION</b> : 106.865 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 3 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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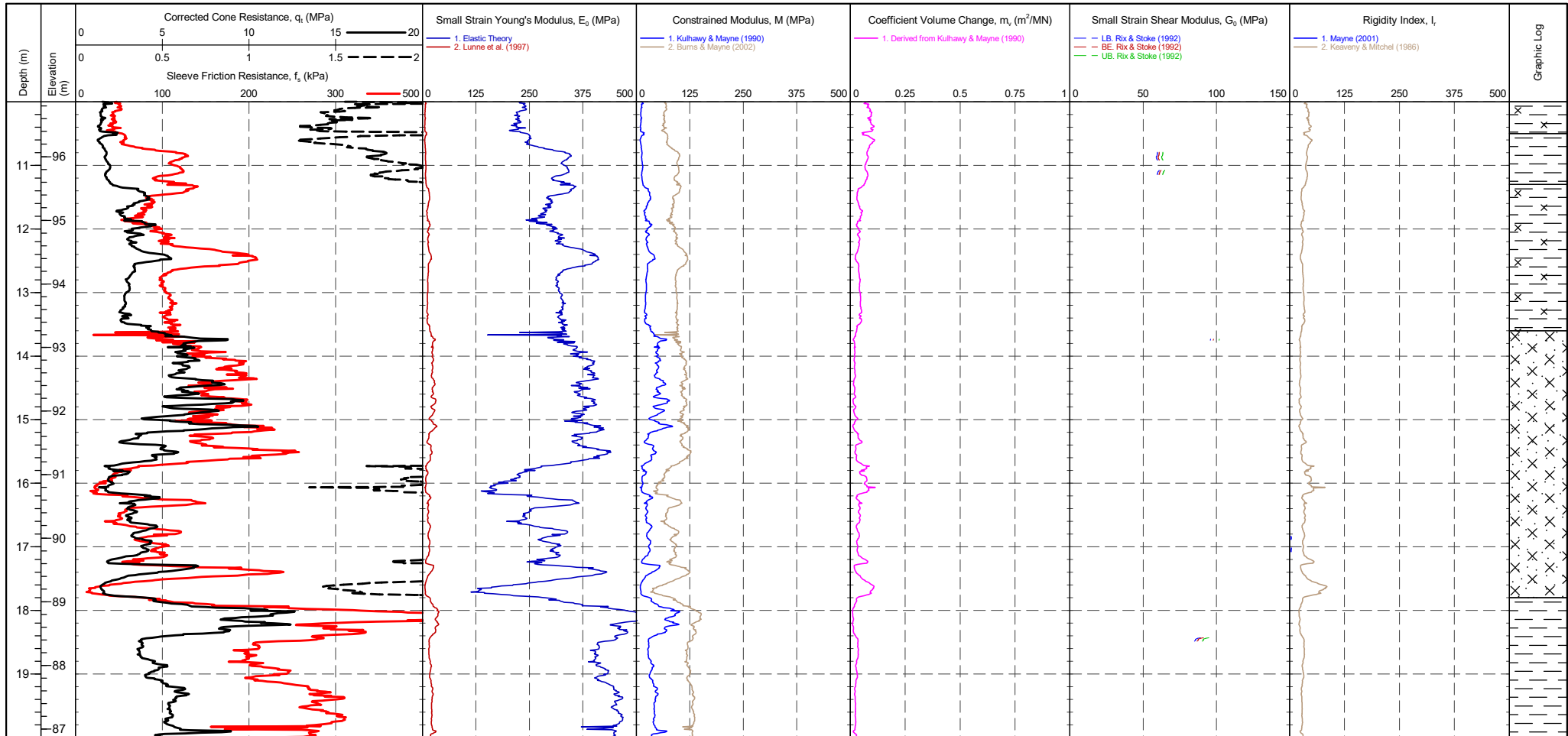


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>363 mV</td> <td>357 mV</td> <td>-0.066 MPa</td> </tr> <tr> <td>Sleeve</td> <td>288 mV</td> <td>283 mV</td> <td>-0.004 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>235 mV</td> <td>197 mV</td> <td>-0.009 kPa</td> </tr> <tr> <td>X-Y Inclinometer</td> <td>2618 mV</td> <td>2599 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	363 mV	357 mV	-0.066 MPa	Sleeve	288 mV	283 mV	-0.004 kPa	Pore Pressure 2	235 mV	197 mV	-0.009 kPa	X-Y Inclinometer	2618 mV	2599 mV		Groundwater Level Dissipation Test
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**CPT09**

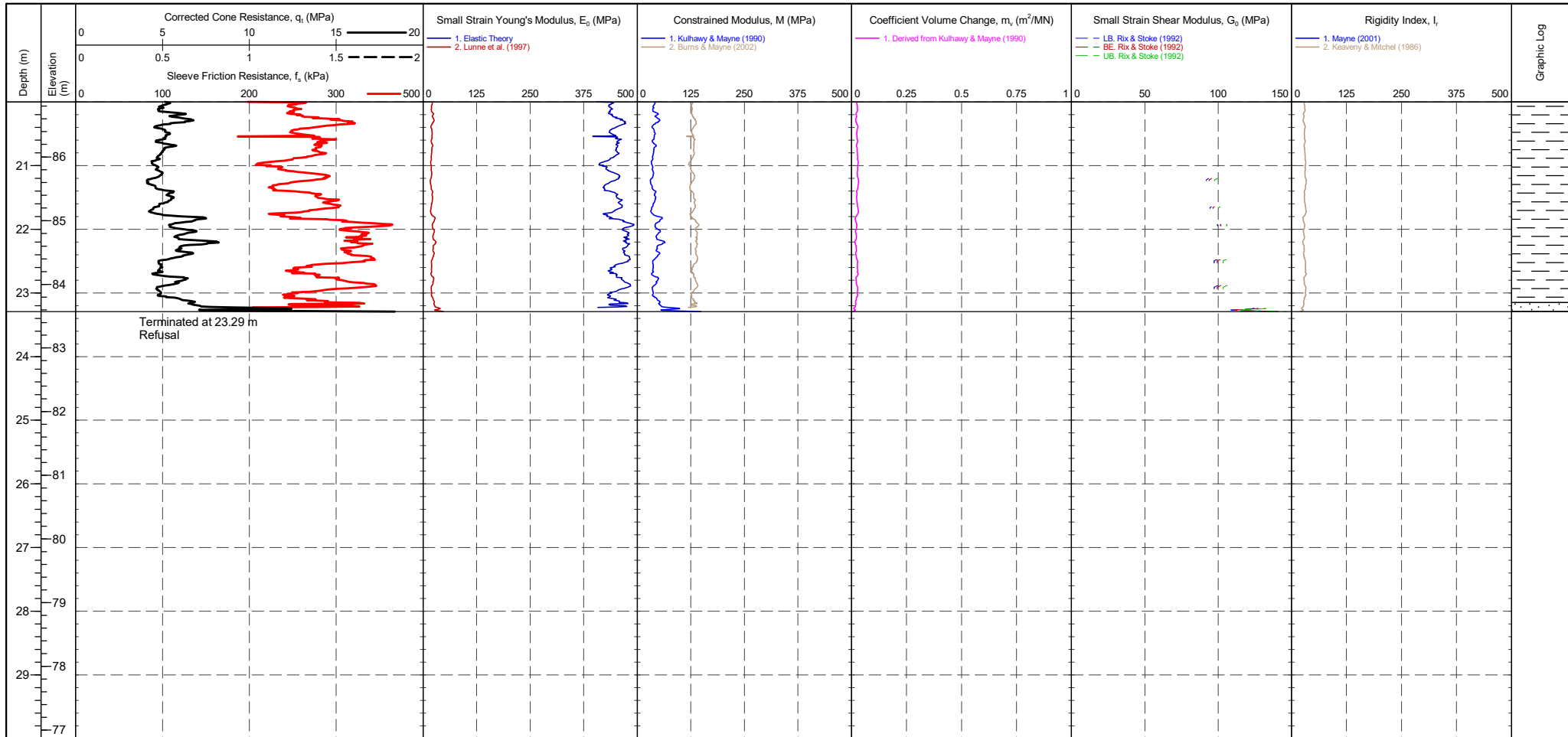
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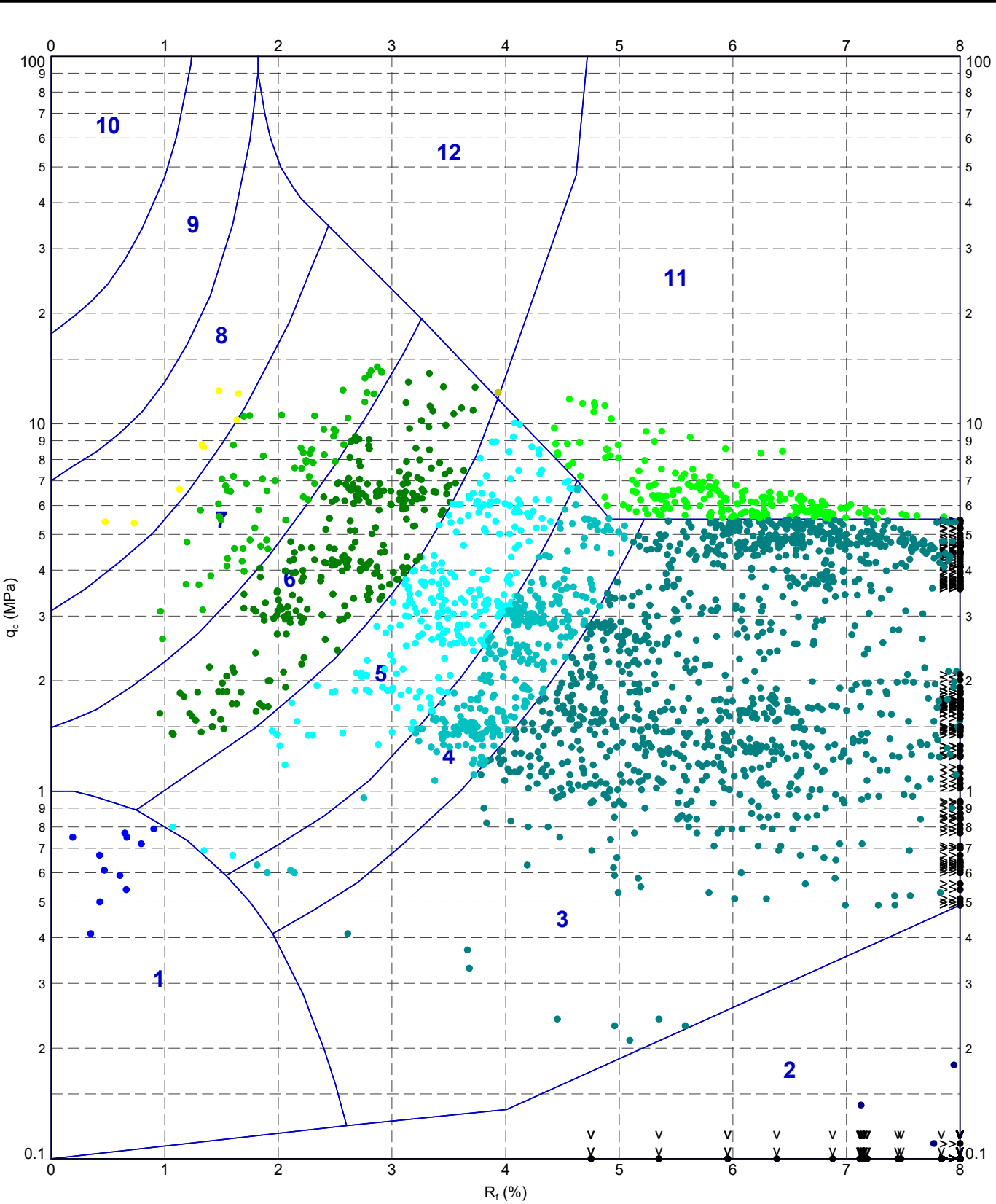
PointID  
**CPT09**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490918.124 m <b>NORTHING</b> : 290906.184 m <b>ELEVATION</b> : 106.865 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 3 OF 3 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>363 mV</td> <td>357 mV</td> <td>-0.066 MPa</td> </tr> <tr> <td>Sleeve</td> <td>288 mV</td> <td>283 mV</td> <td>-0.004 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>235 mV</td> <td>197 mV</td> <td>-0.009 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2618 mV</td> <td>2599 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	363 mV	357 mV	-0.066 MPa	Sleeve	288 mV	283 mV	-0.004 kPa	Pore Pressure 2	235 mV	197 mV	-0.009 kPa	X-Y Inclinator	2618 mV	2599 mV		Groundwater Level Dissipation Test
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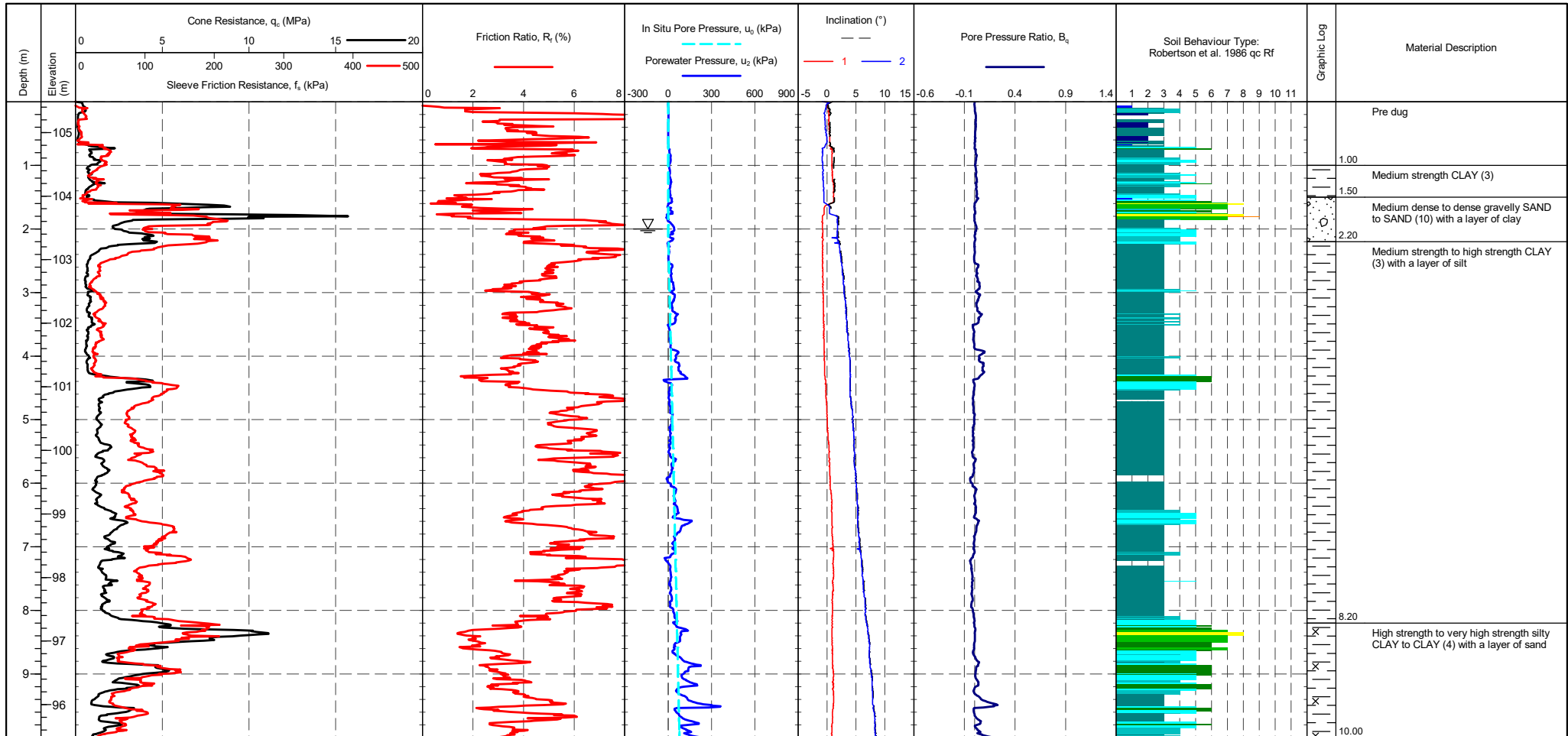
METHOD: Robertson et al. 1986 qc Rf

- 1 - Sensitive fine grained material
- 4 - Silty CLAY to CLAY
- 7 - Silty SAND to sandy SILT
- 10 - Gravelly SAND to SAND
- 2 - Organic material
- 5 - Clayey SILT to silty CLAY
- 8 - SAND to silty SAND
- 11 - Very stiff fine grained
- 3 - CLAY
- 6 - Sandy SILT to clayey SILT
- 9 - SAND
- 12 - SAND to clayey SAND

	TITLE	DRAWN	DATE
	Delta Simons Cordby Corby	CHECKED	DATE
	Robertson et al. 1986 qc vs. Rf - CPT09	SCALE	FIGURE No
		PROJECT No 1220144	A4

PointID	<b>CPT10</b>
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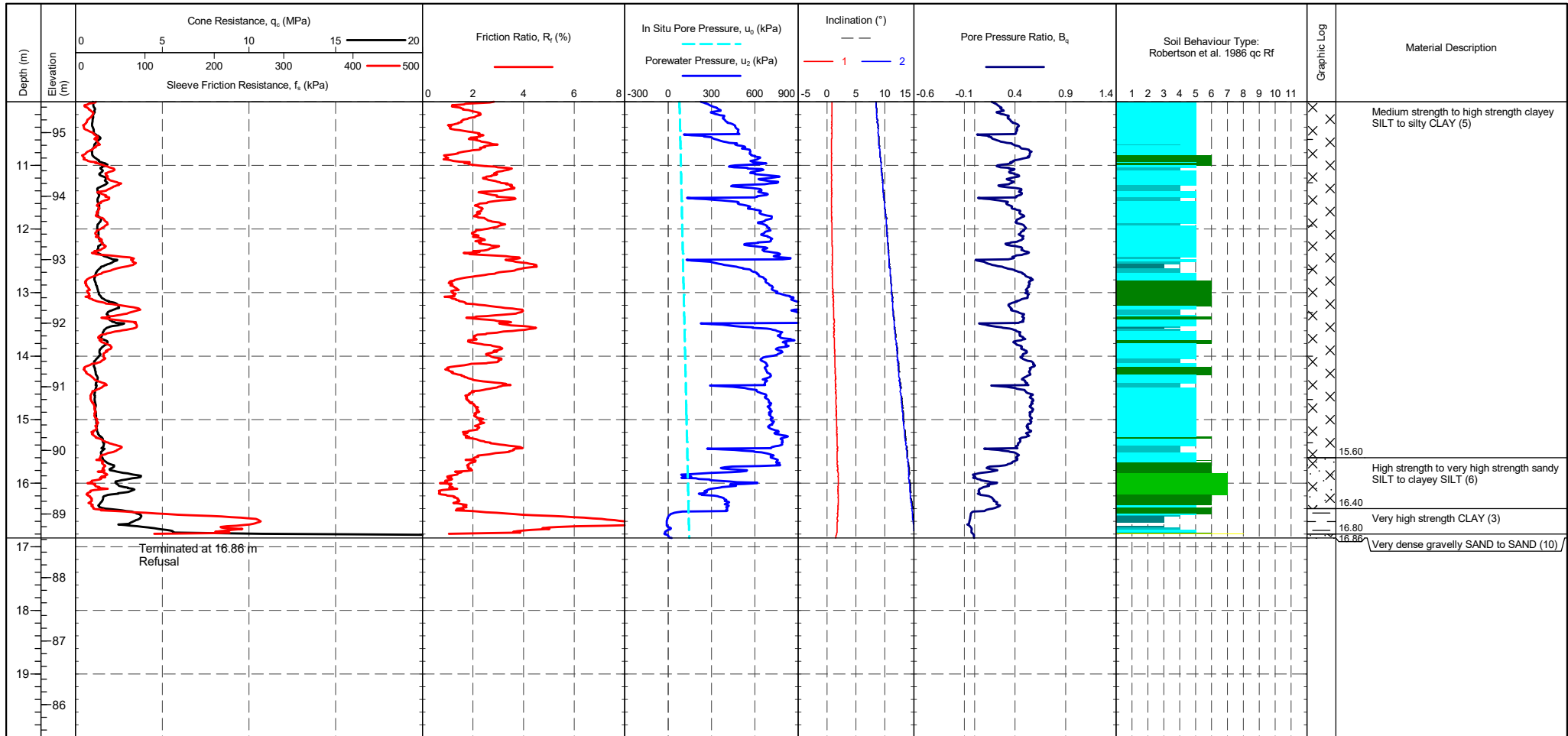
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491027.577 m <b>NORTHING</b> : 290924.637 m <b>ELEVATION</b> : 105.483 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip: Pre 360 mV, Post 362 mV, Difference 0.022 MPa Sleeve: Pre 287 mV, Post 286 mV, Difference -0.001 kPa Pore Pressure 2: Pre 213 mV, Post 255 mV, Difference 0.01 kPa X-Y Inclinometer: Pre 2476 mV, Post 2598 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravelly SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID	<b>CPT10</b>
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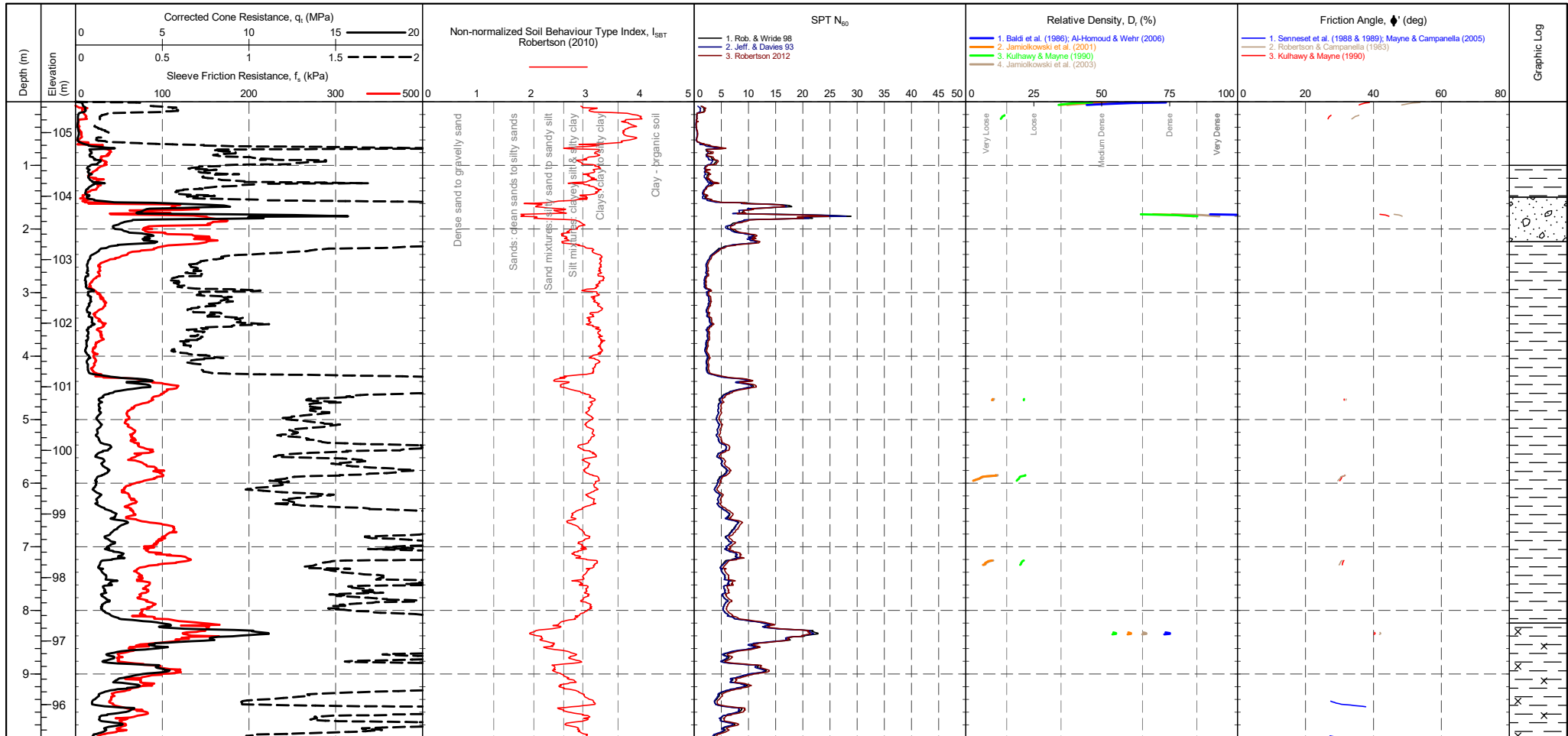
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491027.577 m <b>NORTHING</b> : 290924.637 m <b>ELEVATION</b> : 105.483 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip: Pre 360 mV, Post 362 mV, Difference 0.022 MPa Sleeve: 287 mV, 286 mV, -0.001 kPa Pore Pressure 2: 213 mV, 255 mV, 0.01 kPa X-Y Inclinator: 2476 mV, 2598 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravelly SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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**CPT10**

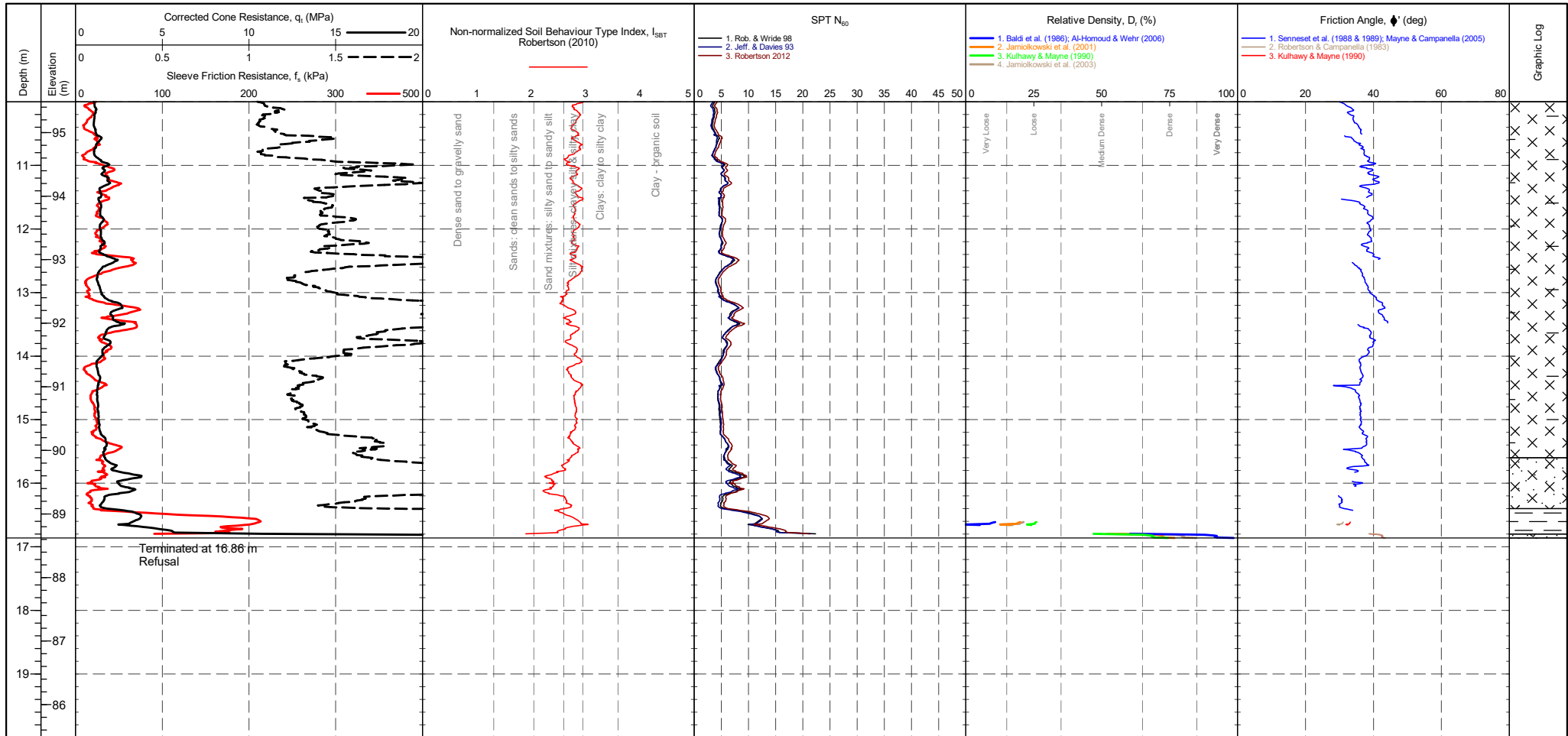
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491027.577 m <b>NORTHING</b> : 290924.637 m <b>ELEVATION</b> : 105.483 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 360 mV Sleeve: 287 mV Pore Pressure 2: 213 mV X-Y Inclinator: 2476 mV	<b>CPTU ZERO VALUES</b> Pre: 362 mV Post: 286 mV Difference: -0.001 kPa 2598 mV	<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, <math>I_c</math></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density <math>D_r</math> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, $I_c$	Description	SPT N value, NSPT	Description	Relative Density $D_r$ (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
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**CPT10**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491027.577 m <b>NORTHING</b> : 290924.637 m <b>ELEVATION</b> : 105.483 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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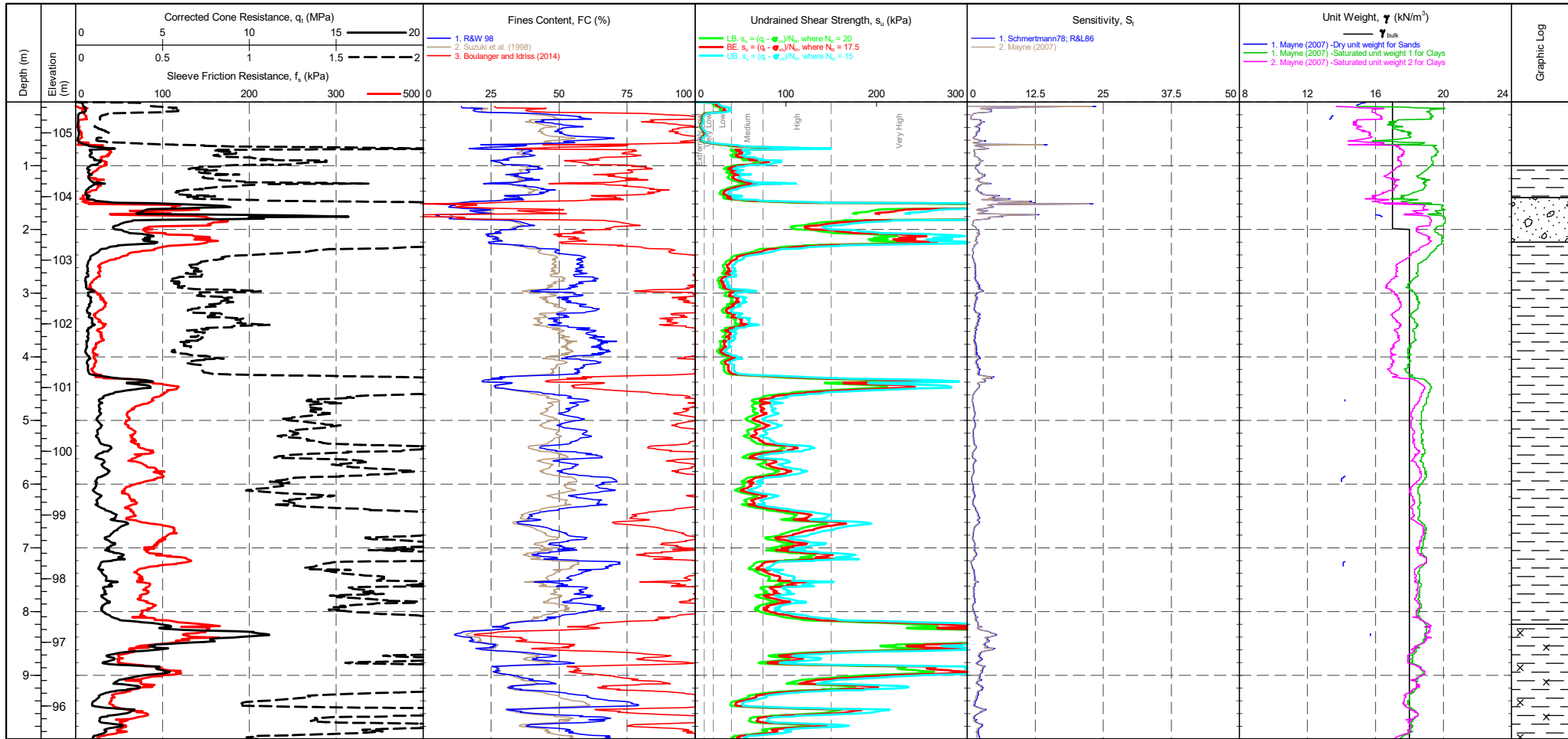




<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>360 mV</td> <td>362 mV</td> <td>0.022 MPa</td> </tr> <tr> <td>Sleeve</td> <td>287 mV</td> <td>286 mV</td> <td>-0.001 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>213 mV</td> <td>255 mV</td> <td>0.01 kPa</td> </tr> <tr> <td>X-Y inclinometer</td> <td>2476 mV</td> <td>2598 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	360 mV	362 mV	0.022 MPa	Sleeve	287 mV	286 mV	-0.001 kPa	Pore Pressure 2	213 mV	255 mV	0.01 kPa	X-Y inclinometer	2476 mV	2598 mV		<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, <math>I_c</math></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density <math>D_r</math> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, $I_c$	Description	SPT N value, NSPT	Description	Relative Density $D_r$ (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
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**CPT10**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491027.577 m <b>NORTHING</b> : 290924.637 m <b>ELEVATION</b> : 105.483 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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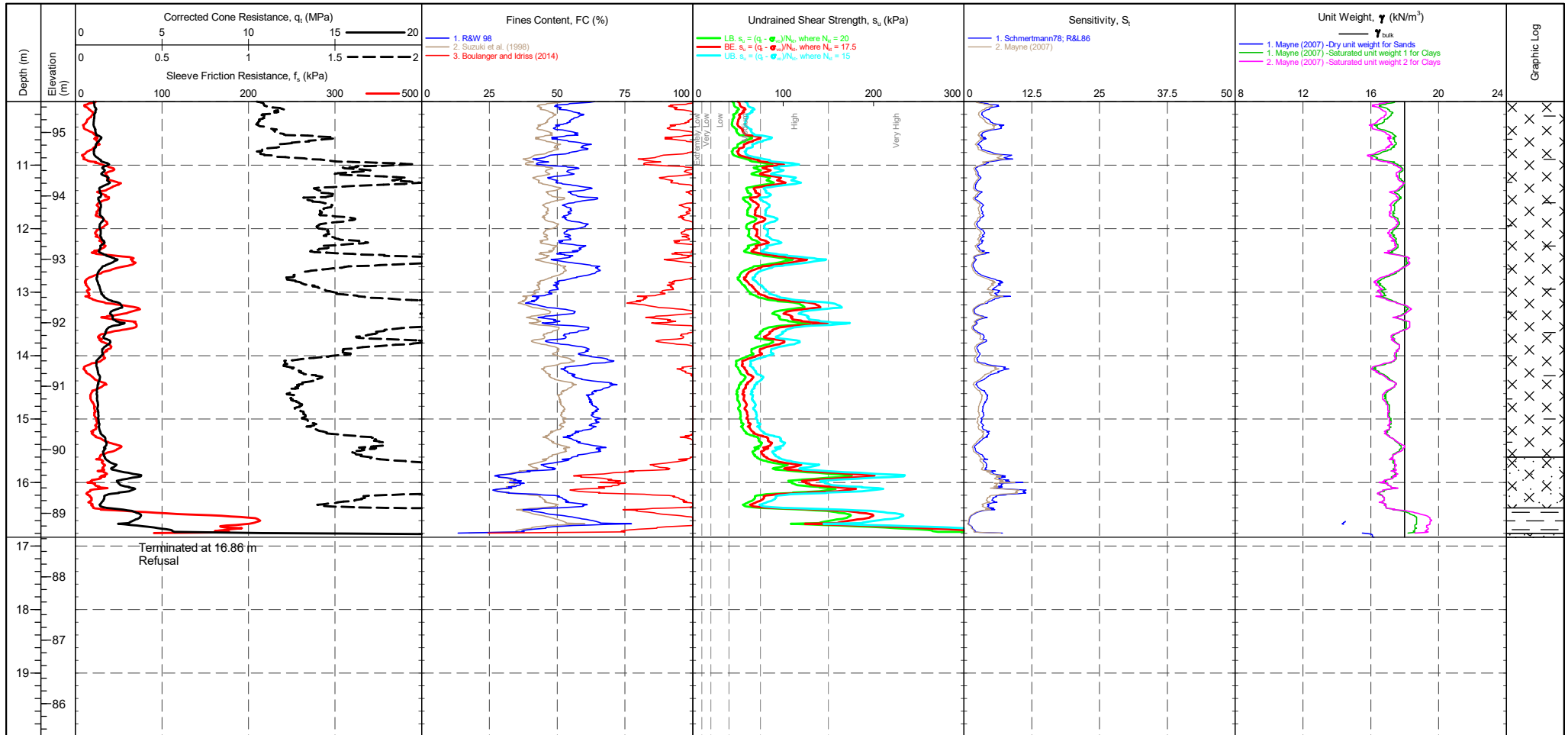


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 360 mV / 362 mV / 0.022 MPa Sleeve: 287 mV / 286 mV / -0.001 kPa Pore Pressure 2: 213 mV / 255 mV / 0.01 kPa X-Y Inclinator: 2476 mV / 2598 mV	<b>CPTU ZERO VALUES</b> Pre: 360 mV Post: 362 mV Difference: 0.022 MPa Sleeve: 287 mV Post: 286 mV Difference: -0.001 kPa Pore Pressure 2: 213 mV Post: 255 mV Difference: 0.01 kPa X-Y Inclinator: 2476 mV Post: 2598 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> <table border="1"> <tr> <th>Term based on measurement</th> <th>su (kPa)</th> <th>Term based on measurement</th> <th>su (kPa)</th> </tr> <tr> <td>Extremely low strength</td> <td>&lt;10</td> <td>Medium strength</td> <td>40-75</td> </tr> <tr> <td>Very low strength</td> <td>10-20</td> <td>High strength</td> <td>75-150</td> </tr> <tr> <td>Low strength</td> <td>20-40</td> <td>Very high strength</td> <td>150-300</td> </tr> <tr> <td></td> <td></td> <td>Extremely high strength</td> <td>&gt;300</td> </tr> </table>	Term based on measurement	su (kPa)	Term based on measurement	su (kPa)	Extremely low strength	<10	Medium strength	40-75	Very low strength	10-20	High strength	75-150	Low strength	20-40	Very high strength	150-300			Extremely high strength	>300	<b>Groundwater Level</b>  <b>Dissipation Test</b> 
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**CPT10**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491027.577 m <b>NORTHING</b> : 290924.637 m <b>ELEVATION</b> : 105.483 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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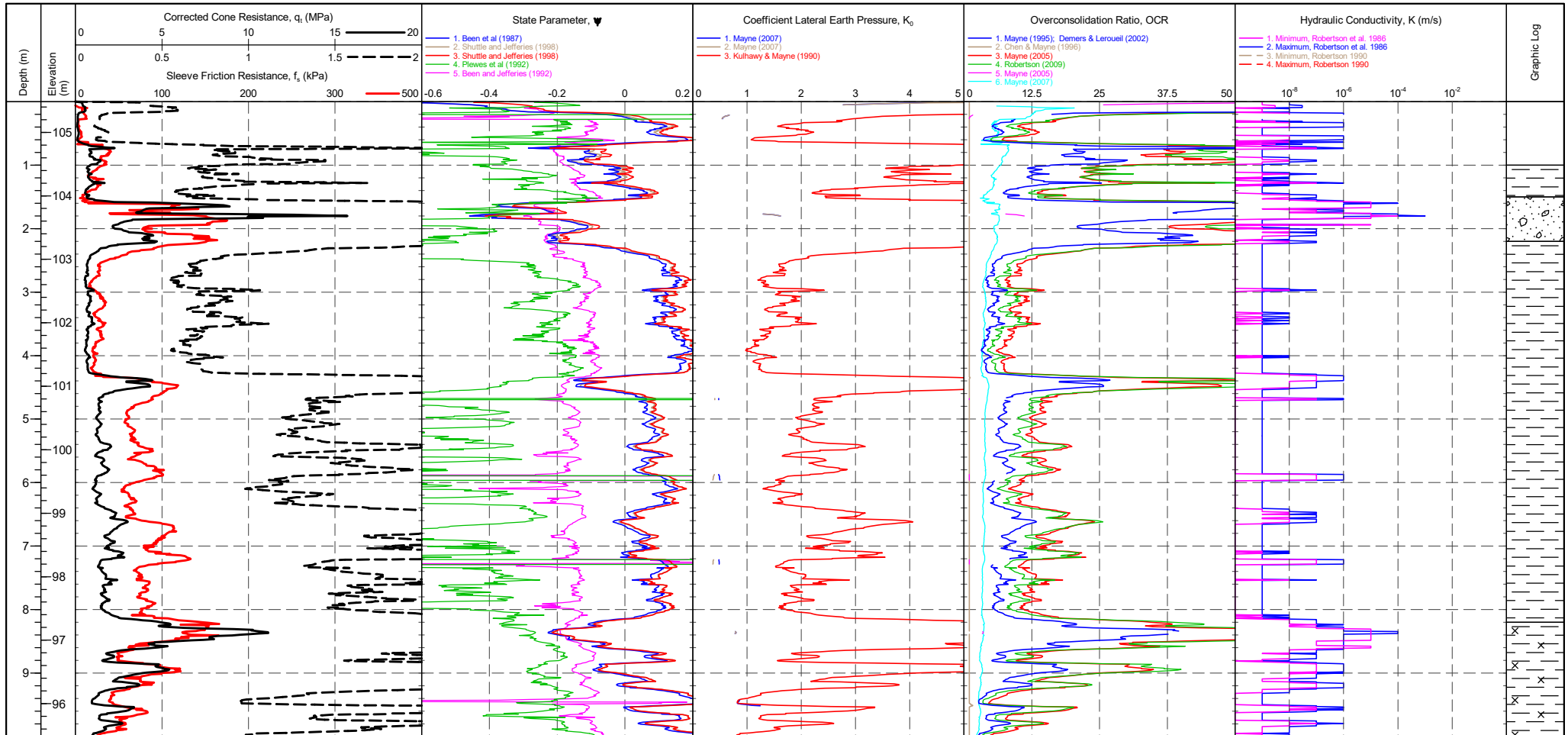


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 360 mV Sleeve: 287 mV Pore Pressure 2: 213 mV X-Y Inclinator: 2476 mV	<b>CPTU ZERO VALUES</b> Post: 362 mV Difference: 0.022 MPa Post: 286 mV Difference: -0.001 kPa Post: 255 mV Difference: 0.01 kPa Post: 2598 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement su (kPa) Extremely low strength <10 Very low strength 10-20 Low strength 20-40	Term based on measurement su (kPa) Medium strength 40-75 High strength 75-150 Very high strength 150-300 Extremely high strength >300	Groundwater Level Dissipation Test
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PointID

**CPT10**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491027.577 m <b>NORTHING</b> : 290924.637 m <b>ELEVATION</b> : 105.483 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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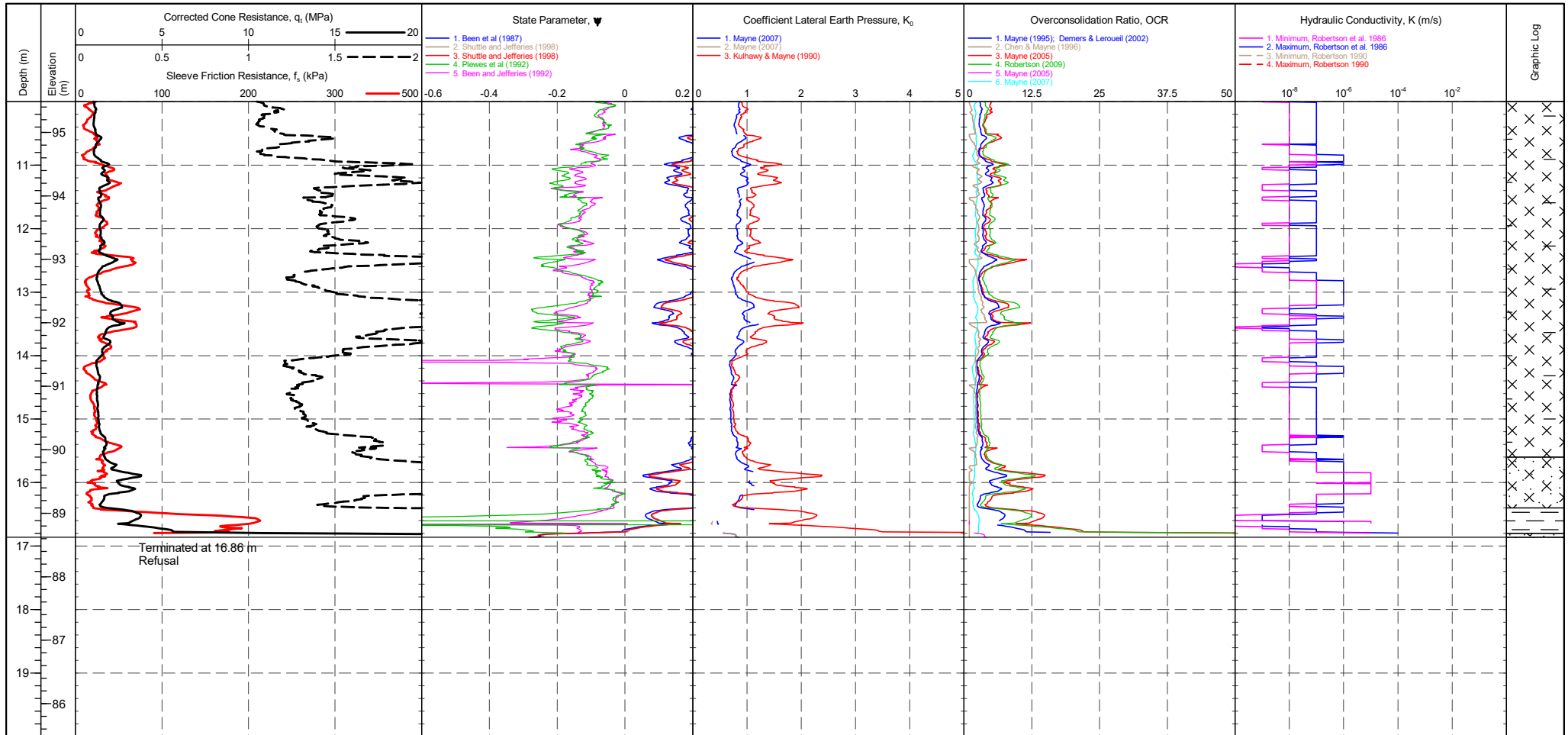


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>360 mV</td> <td>362 mV</td> <td>0.022 MPa</td> </tr> <tr> <td>Sleeve</td> <td>287 mV</td> <td>286 mV</td> <td>-0.001 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>213 mV</td> <td>255 mV</td> <td>0.01 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2476 mV</td> <td>2598 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	360 mV	362 mV	0.022 MPa	Sleeve	287 mV	286 mV	-0.001 kPa	Pore Pressure 2	213 mV	255 mV	0.01 kPa	X-Y Inclinator	2476 mV	2598 mV		Groundwater Level Dissipation Test
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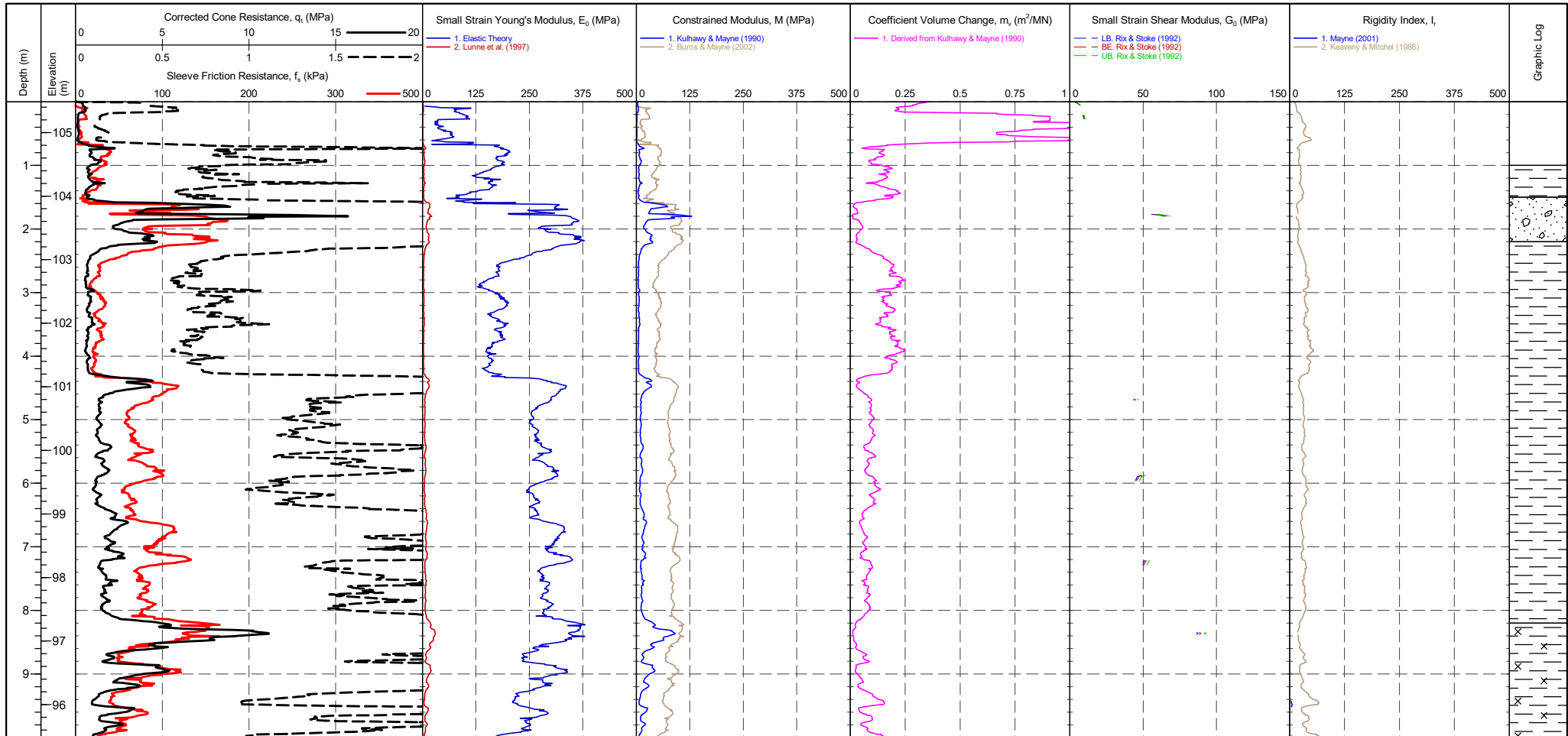
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491027.577 m <b>NORTHING</b> : 290924.637 m <b>ELEVATION</b> : 105.483 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>360 mV</td> <td>362 mV</td> <td>0.022 MPa</td> </tr> <tr> <td>Sleeve</td> <td>287 mV</td> <td>286 mV</td> <td>-0.001 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>213 mV</td> <td>255 mV</td> <td>0.01 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2476 mV</td> <td>2598 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	360 mV	362 mV	0.022 MPa	Sleeve	287 mV	286 mV	-0.001 kPa	Pore Pressure 2	213 mV	255 mV	0.01 kPa	X-Y Inclinator	2476 mV	2598 mV		Groundwater Level Dissipation Test
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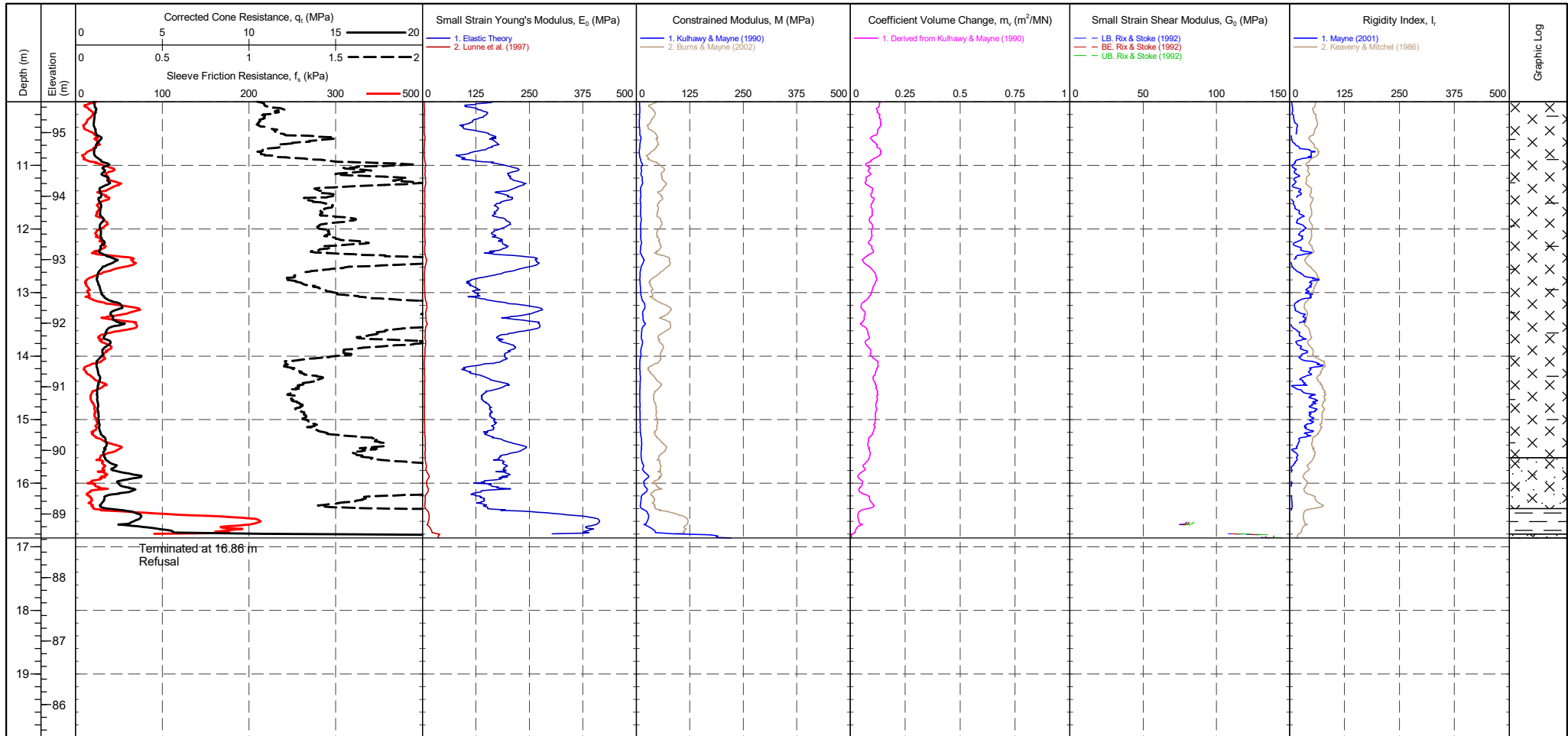
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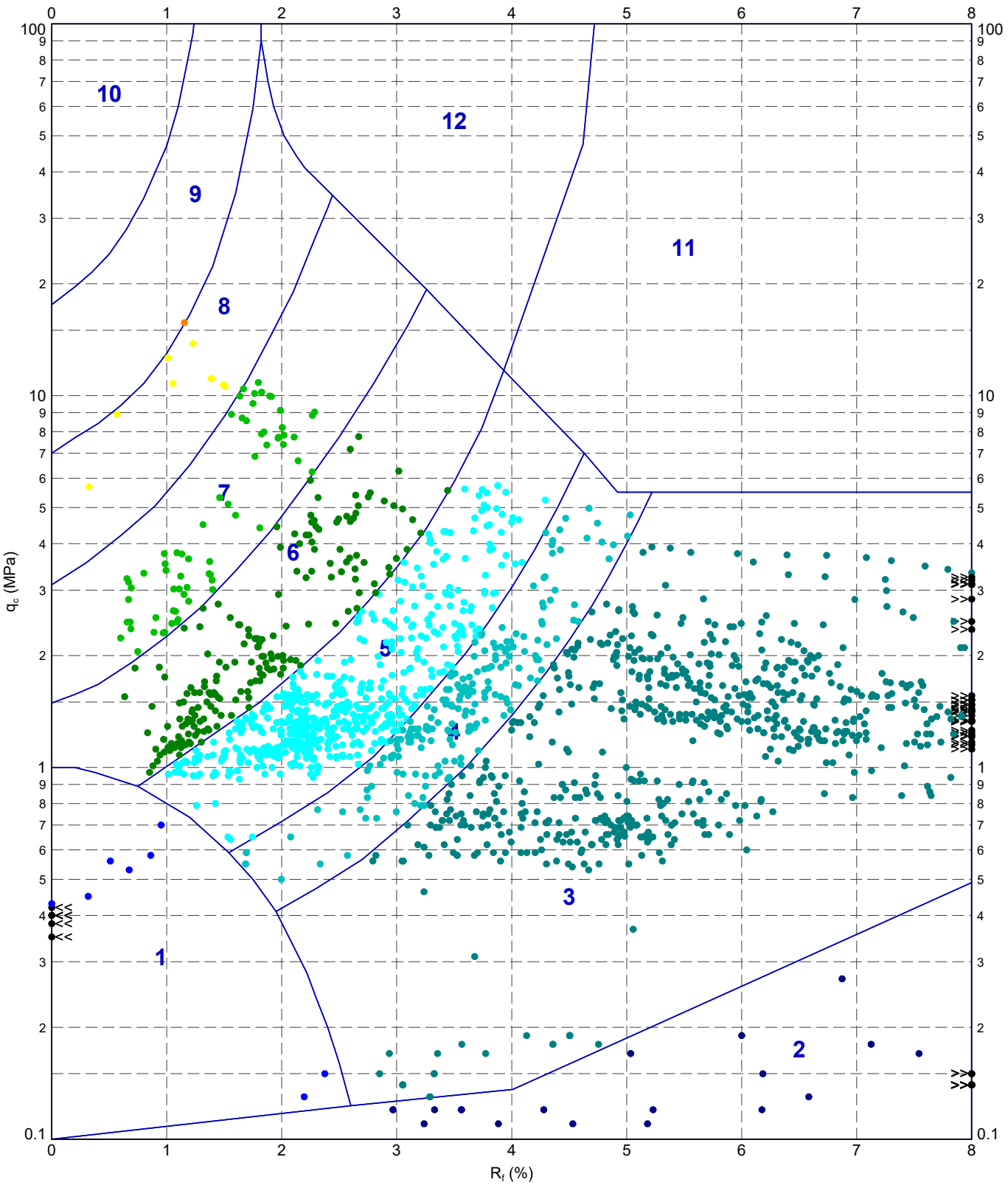
PointID  
**CPT10**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491027.577 m <b>NORTHING</b> : 290924.637 m <b>ELEVATION</b> : 105.483 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>360 mV</td> <td>362 mV</td> <td>0.022 MPa</td> </tr> <tr> <td>Sleeve</td> <td>287 mV</td> <td>286 mV</td> <td>-0.001 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>213 mV</td> <td>255 mV</td> <td>0.01 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2476 mV</td> <td>2598 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	360 mV	362 mV	0.022 MPa	Sleeve	287 mV	286 mV	-0.001 kPa	Pore Pressure 2	213 mV	255 mV	0.01 kPa	X-Y Inclinator	2476 mV	2598 mV		Groundwater Level Dissipation Test
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220228-ADVANCED REPORT INSTITUSI 2.02.1 LIB - CHLOE.GLB Graph CPT ROBERTSON ET AL. 8F QC VS. RF APF 1220144 CORBY DELTA SIMONS G.P.J. <<DrawingFile>> 04/03/2022 17:36 10.01.00.11 Datagel Lab and In Situ Tool - DGD [Lib: In Situ SI 2.02.0 2017-07-10 Proj: In Situ SI 2.02.0 2017-07-10



**METHOD: Robertson et al. 1986 qc Rf**

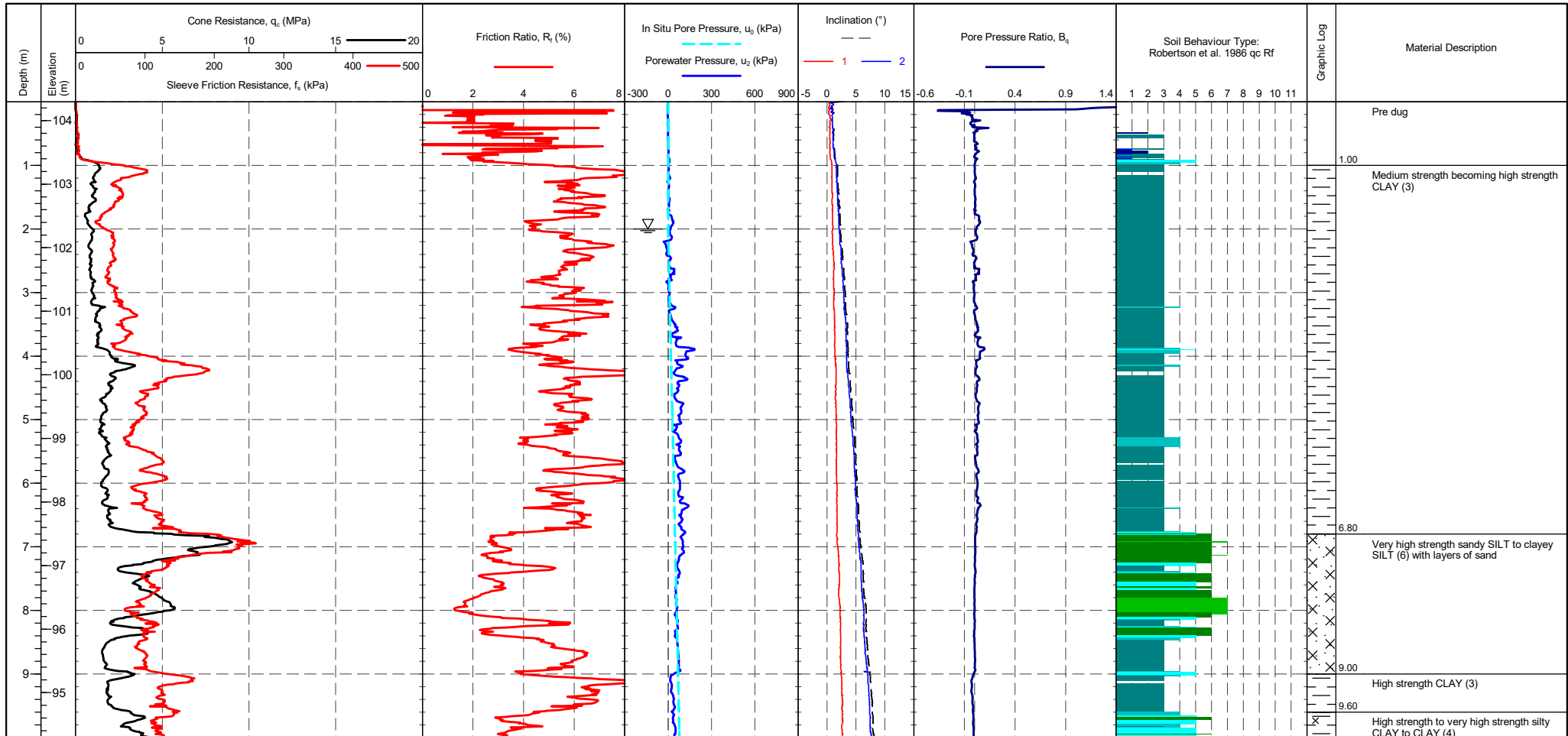
1 - Sensitive fine grained material	4 - Silty CLAY to CLAY	7 - Silty SAND to sandy SILT	10 - Gravelly SAND to SAND
2 - Organic material	5 - Clayey SILT to silty CLAY	8 - SAND to silty SAND	11 - Very stiff fine grained
3 - CLAY	6 - Sandy SILT to clayey SILT	9 - SAND	12 - SAND to clayey SAND

	TITLE	DRAWN	DATE
	Delta Simons Cordby Corby Robertson et al. 1986 qc vs. Rf - CPT10	CHECKED	DATE
		SCALE	FIGURE No
		PROJECT No	
		1220144	A4



PointID	<b>CPT11</b>
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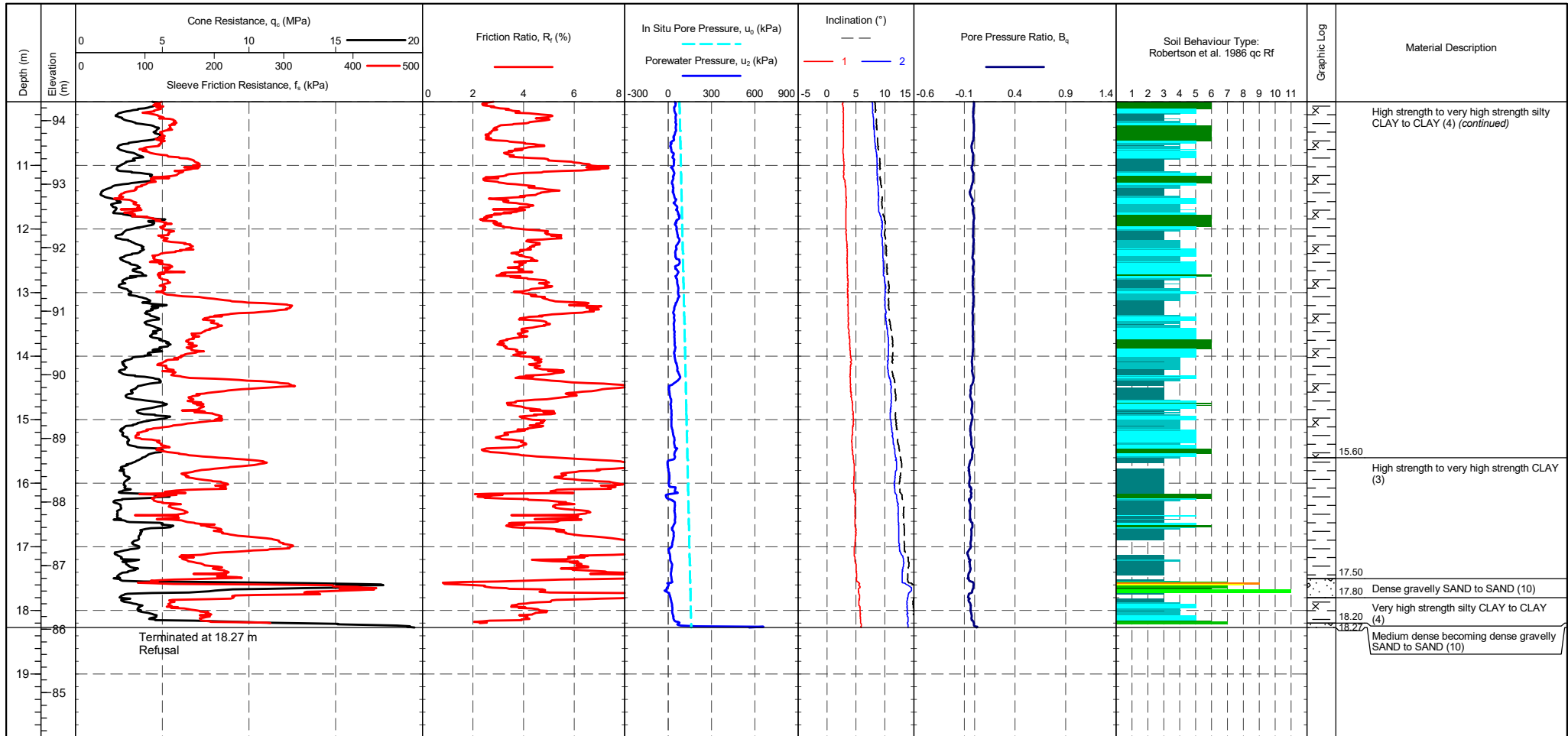
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491050.407 m <b>NORTHING</b> : 290872.435 m <b>ELEVATION</b> : 104.295 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip: Pre 362 mV, Post 361 mV, Difference -0.011 MPa Sleeve: Pre 286 mV, Post 286 mV, Difference 0 kPa Pore Pressure 2: Pre 244 mV, Post 247 mV, Difference 0.001 kPa X-Y Inclinator: Pre 2757 mV, Post 2569 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf Legend: 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravely SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID	<b>CPT11</b>
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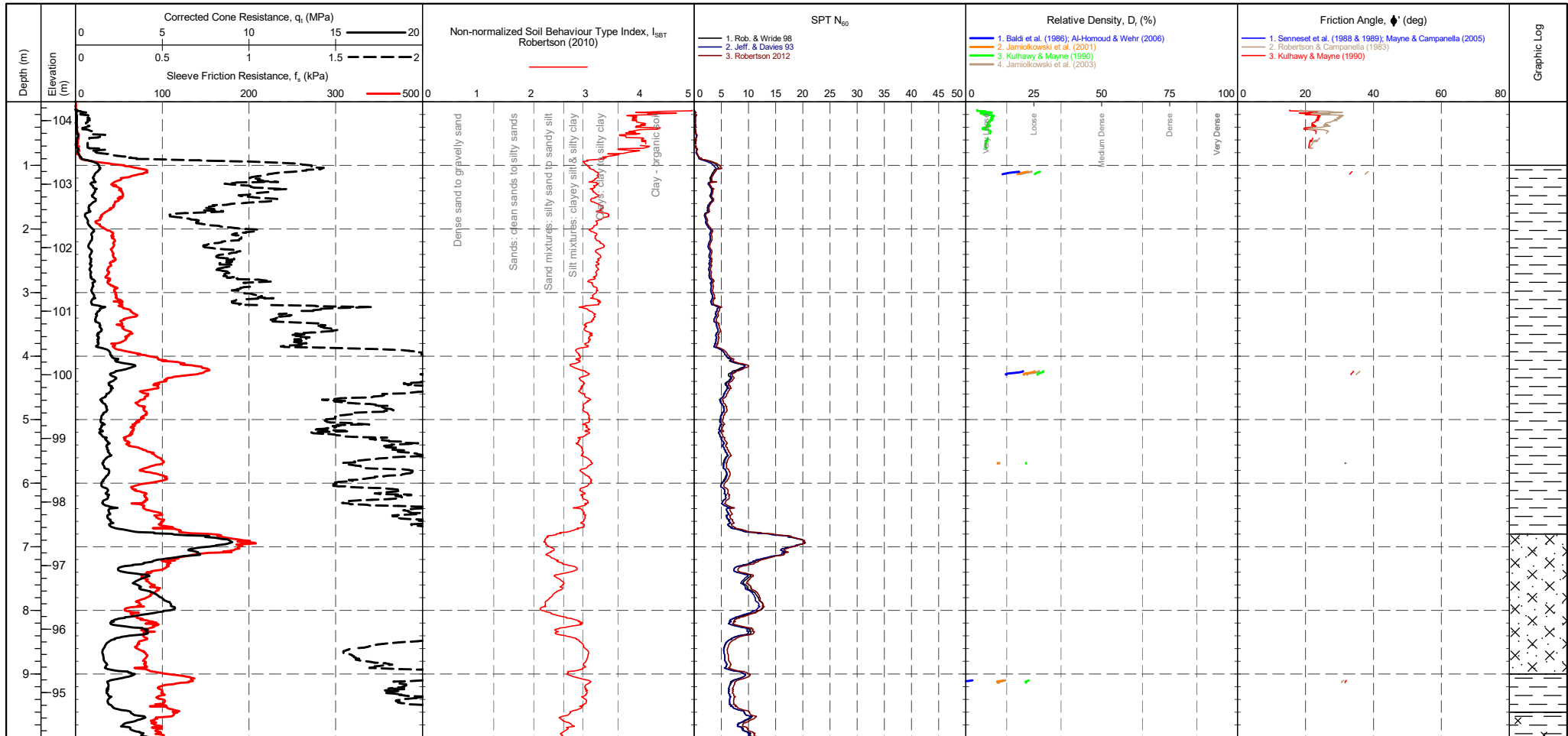
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 491050.407 m <b>NORTHING</b> : 290872.435 m <b>ELEVATION</b> : 104.295 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip : 362 mV / 361 mV / -0.011 MPa Sleeve : 286 mV / 286 mV / 0 kPa Pore Pressure 2 : 244 mV / 247 mV / 0.001 kPa X-Y Inclinometer : 2757 mV / 2569 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravely SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID	<b>CPT11</b>
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491050.407 m <b>NORTHING</b> : 290872.435 m <b>ELEVATION</b> : 104.295 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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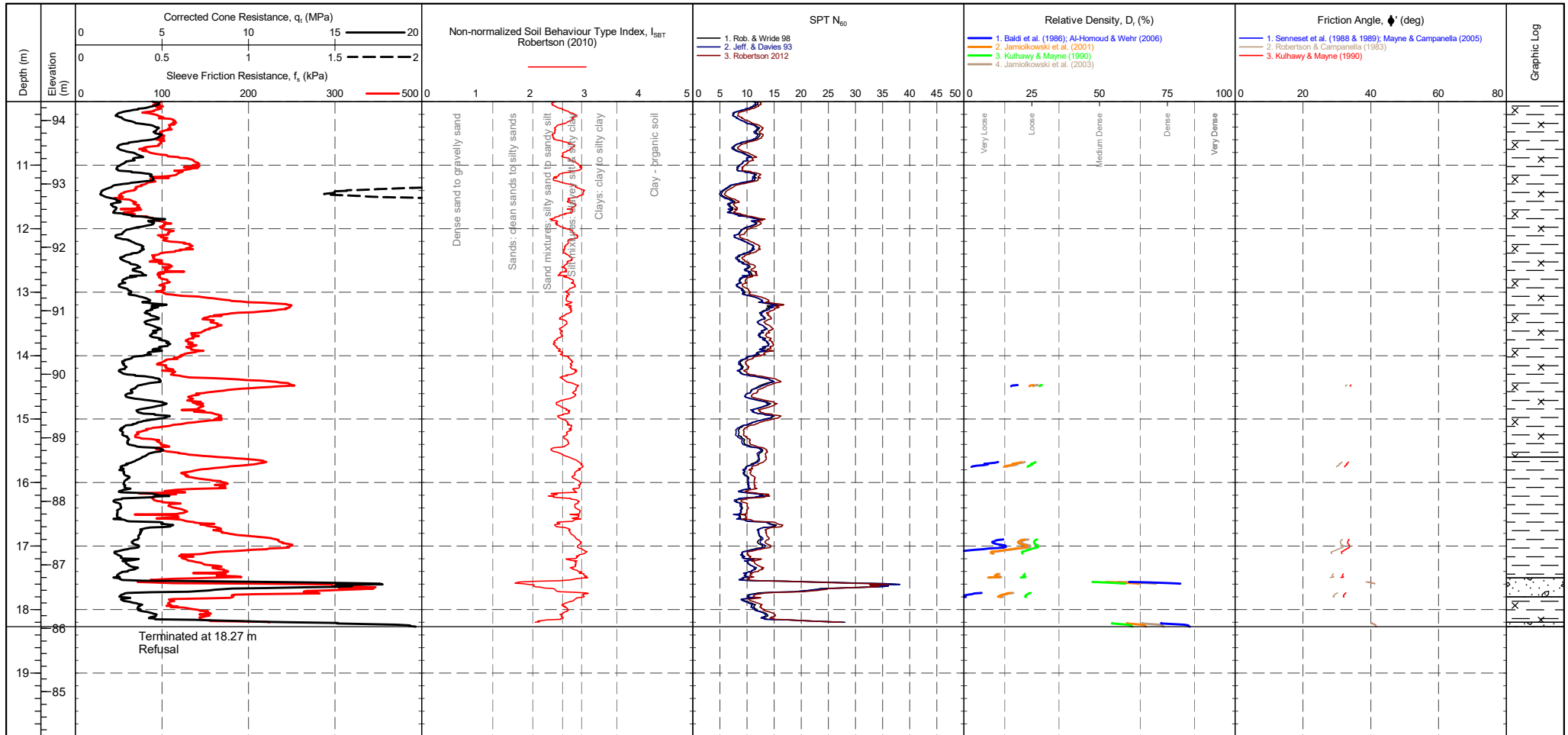


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> <b>Tip</b> : 362 mV <b>Sleeve</b> : 286 mV <b>Pore Pressure 2</b> : 244 mV <b>X-Y Inclinator</b> : 2757 mV	<b>CPTU ZERO VALUES</b> <b>Post</b> : 361 mV <b>Difference</b> : -0.011 MPa <b>0 kPa</b> <b>0.001 kPa</b> <b>2569 mV</b>	<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, I<sub>c</sub></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density D<sub>r</sub> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, I <sub>c</sub>	Description	SPT N value, NSPT	Description	Relative Density D <sub>r</sub> (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
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PointID

**CPT11**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491050.407 m <b>NORTHING</b> : 290872.435 m <b>ELEVATION</b> : 104.295 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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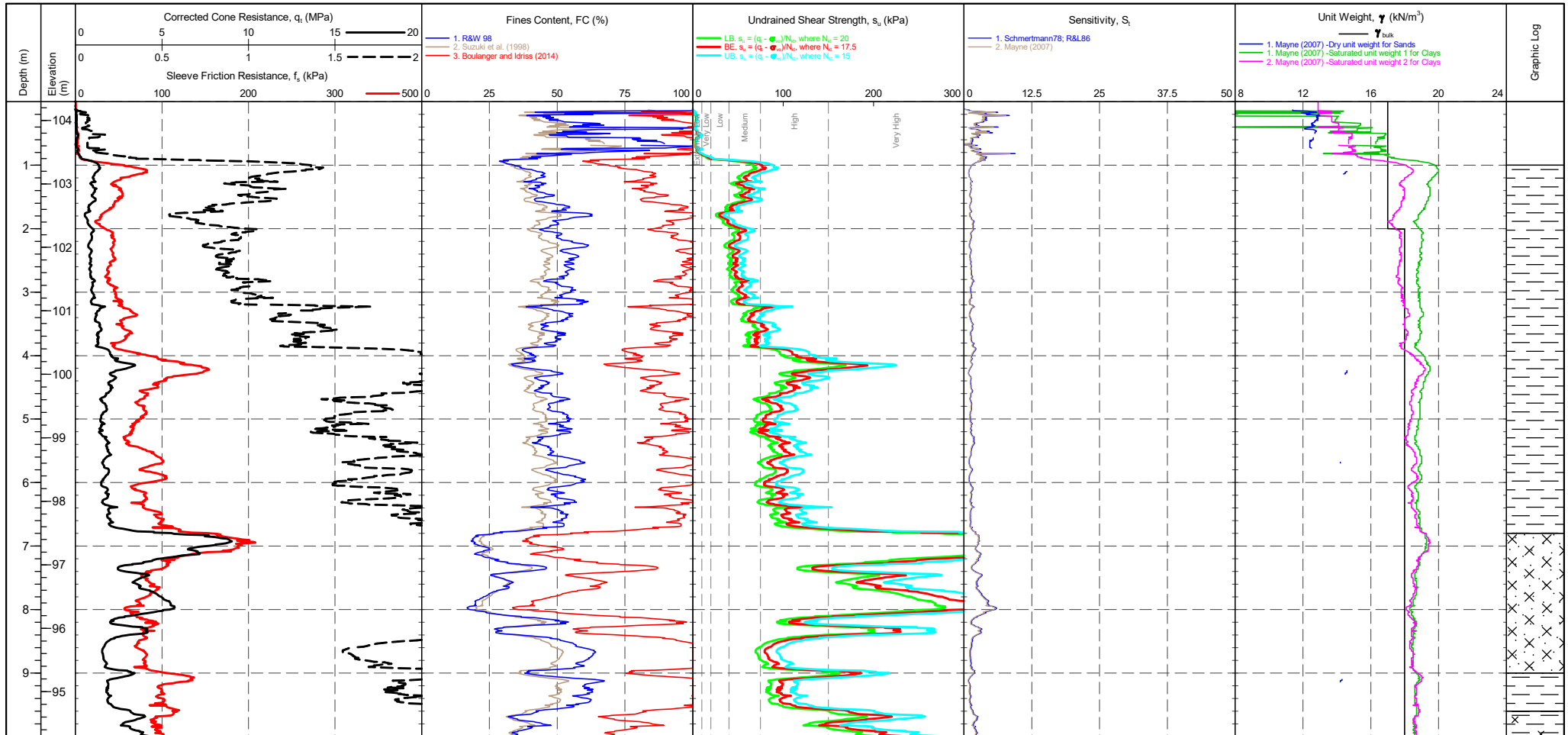


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> <b>Tip</b> : 362 mV <b>Sleeve</b> : 286 mV <b>Pore Pressure 2</b> : 244 mV <b>X-Y inclinometer</b> : 2757 mV	<b>CPTU ZERO VALUES</b> <b>Pre</b> : 361 mV <b>Post</b> : 361 mV <b>Difference</b> : -0.011 MPa <b>0 kPa</b> <b>0.001 kPa</b> <b>2569 mV</b>	<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, I<sub>c</sub></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density D<sub>r</sub> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, I <sub>c</sub>	Description	SPT N value, NSPT	Description	Relative Density D <sub>r</sub> (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
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CPT11

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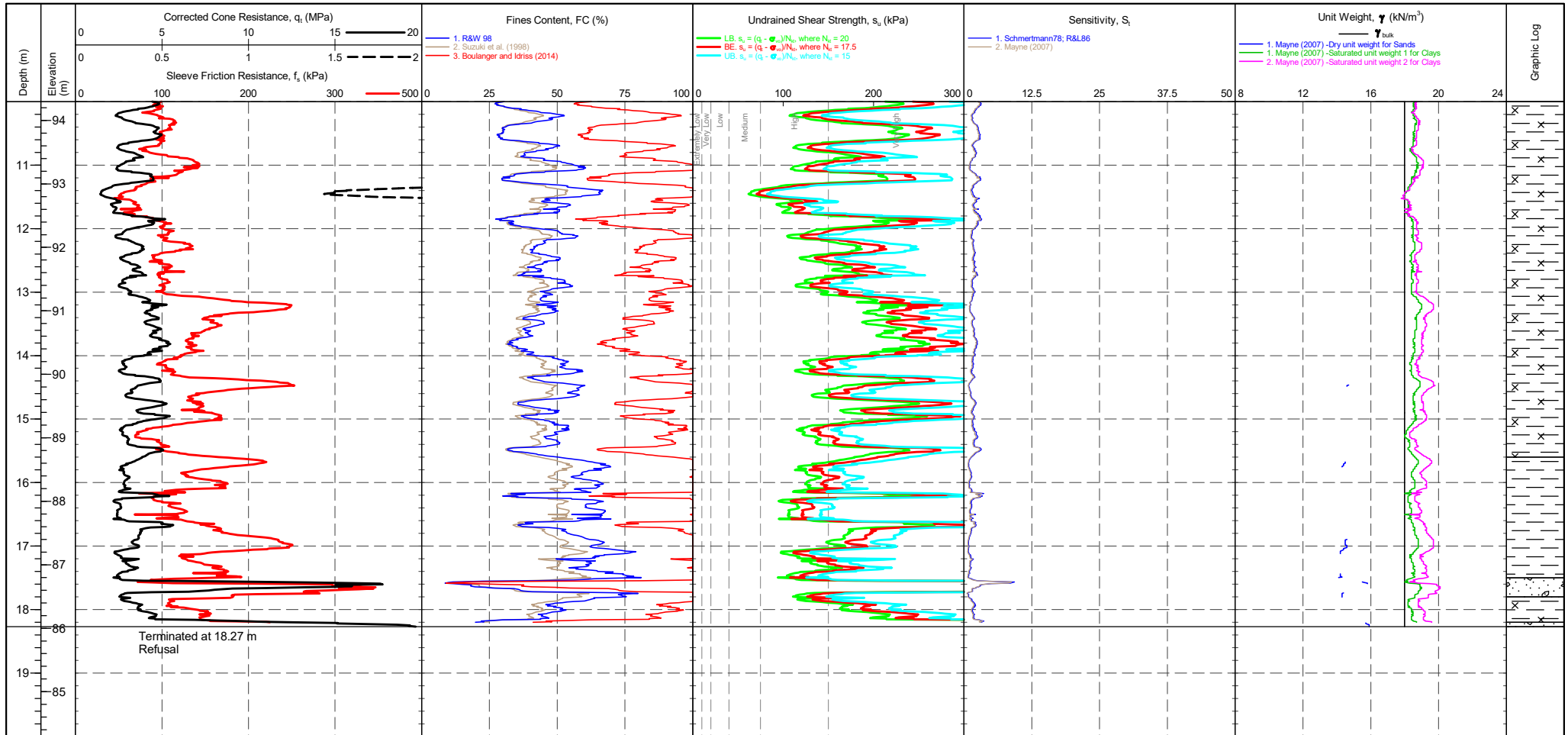


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 362 mV / 361 mV Sleeve: 286 mV / 286 mV Pore Pressure 2: 244 mV / 247 mV X-Y Inclinator: 2757 mV / 2569 mV	<b>CPTU ZERO VALUES</b> Pre: 361 mV Post: 361 mV Difference: -0.011 MPa 0 kPa 0.001 kPa	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement   $s_u$ (kPa)   Term based on measurement   $s_u$ (kPa) Extremely low strength   <10   Medium strength   40-75 Very low strength   10-20   High strength   75-150 Low strength   20-40   Very high strength   150-300     Extremely high strength   >300	▽ Groundwater Level ▮ Dissipation Test
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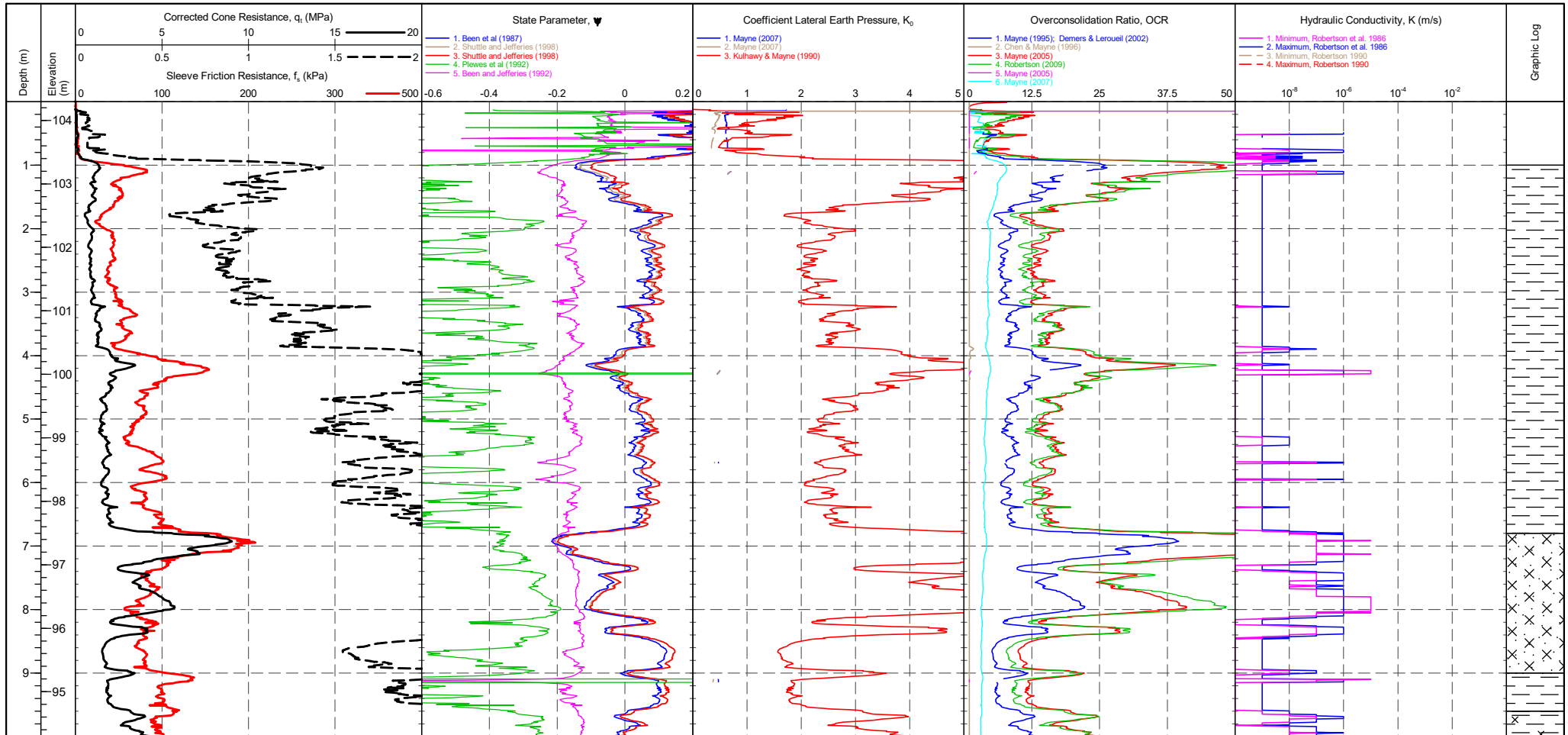


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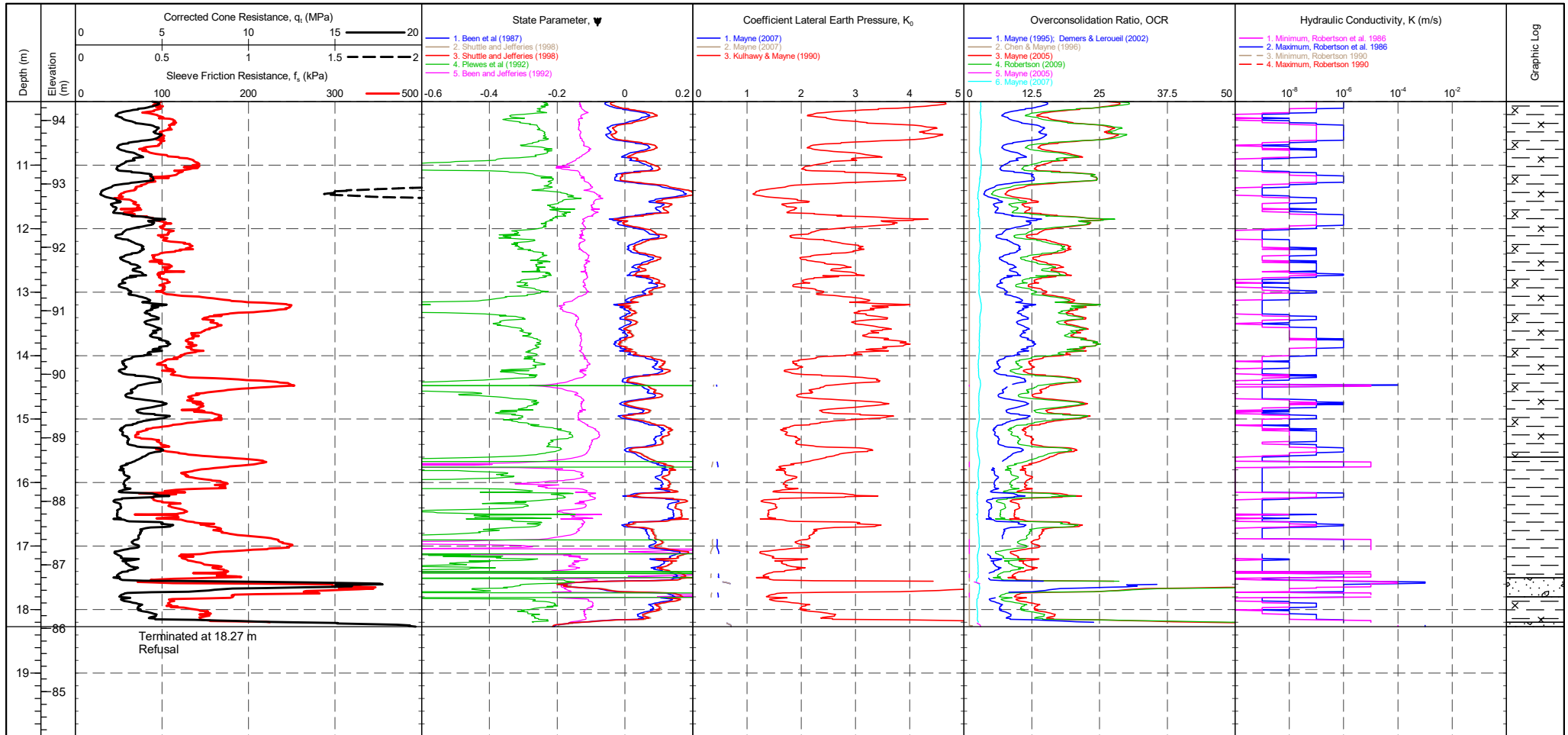
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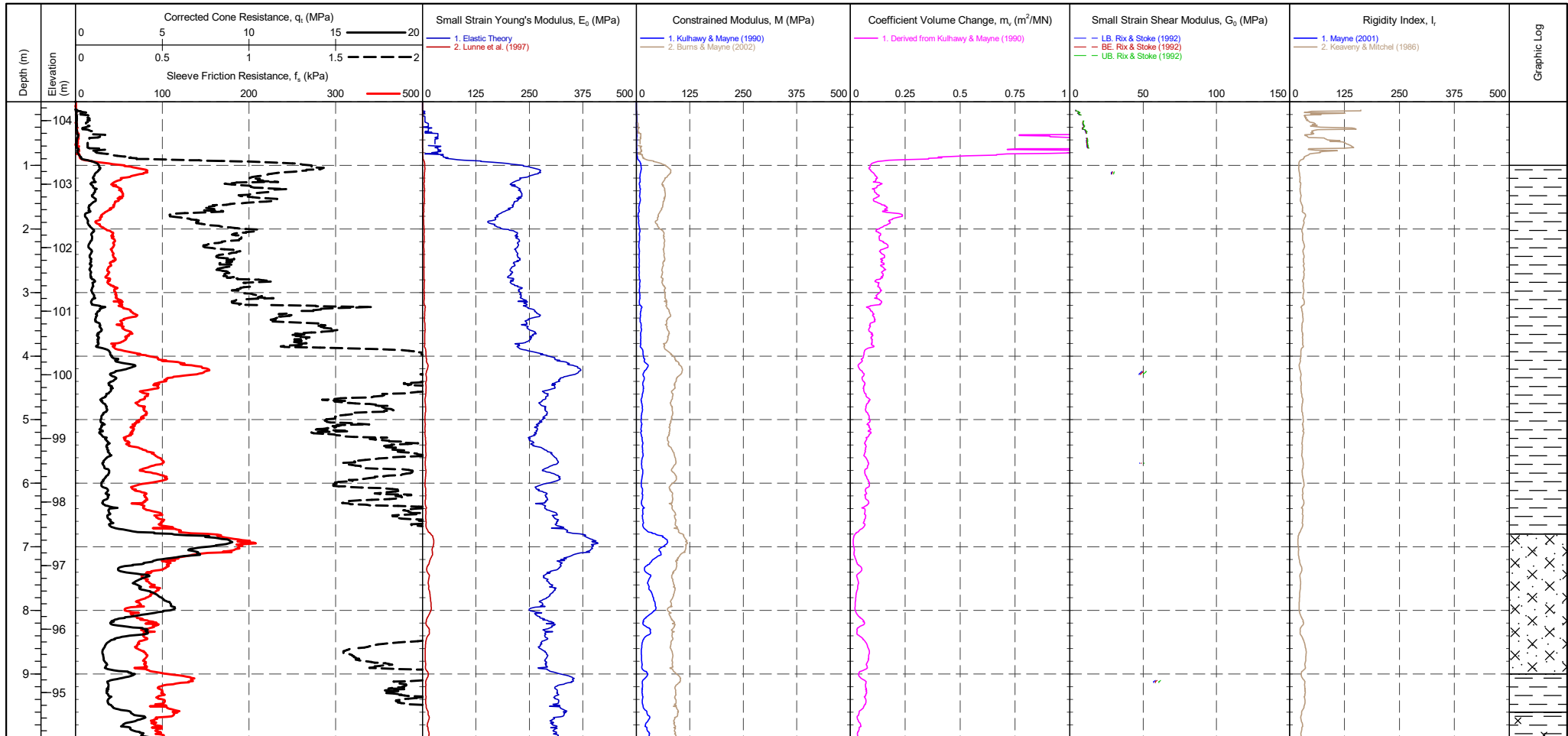
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491050.407 m <b>NORTHING</b> : 290872.435 m <b>ELEVATION</b> : 104.295 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>362 mV</td> <td>361 mV</td> <td>-0.011 MPa</td> </tr> <tr> <td>Sleeve</td> <td>286 mV</td> <td>286 mV</td> <td>0 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>244 mV</td> <td>247 mV</td> <td>0.001 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2757 mV</td> <td>2569 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	362 mV	361 mV	-0.011 MPa	Sleeve	286 mV	286 mV	0 kPa	Pore Pressure 2	244 mV	247 mV	0.001 kPa	X-Y Inclinator	2757 mV	2569 mV		Groundwater Level Dissipation Test
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Pore Pressure 2	244 mV	247 mV	0.001 kPa																				
X-Y Inclinator	2757 mV	2569 mV																					

PointID  
**CPT11**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491050.407 m <b>NORTHING</b> : 290872.435 m <b>ELEVATION</b> : 104.295 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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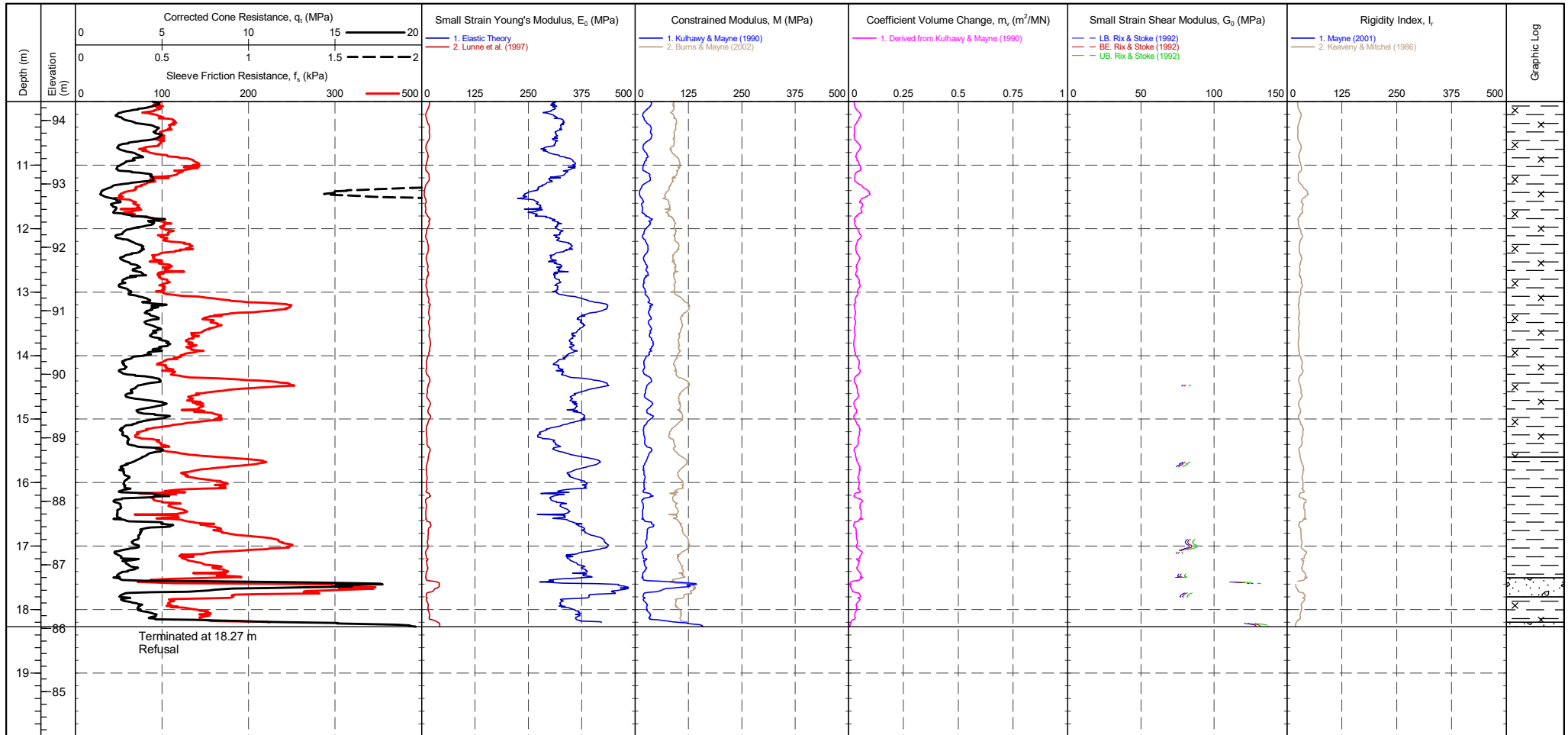


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>362 mV</td> <td>361 mV</td> <td>-0.011 MPa</td> </tr> <tr> <td>Sleeve</td> <td>286 mV</td> <td>286 mV</td> <td>0 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>244 mV</td> <td>247 mV</td> <td>0.001 kPa</td> </tr> <tr> <td>X-Y Inclinometer</td> <td>2757 mV</td> <td>2569 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	362 mV	361 mV	-0.011 MPa	Sleeve	286 mV	286 mV	0 kPa	Pore Pressure 2	244 mV	247 mV	0.001 kPa	X-Y Inclinometer	2757 mV	2569 mV		Groundwater Level Dissipation Test
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PointID

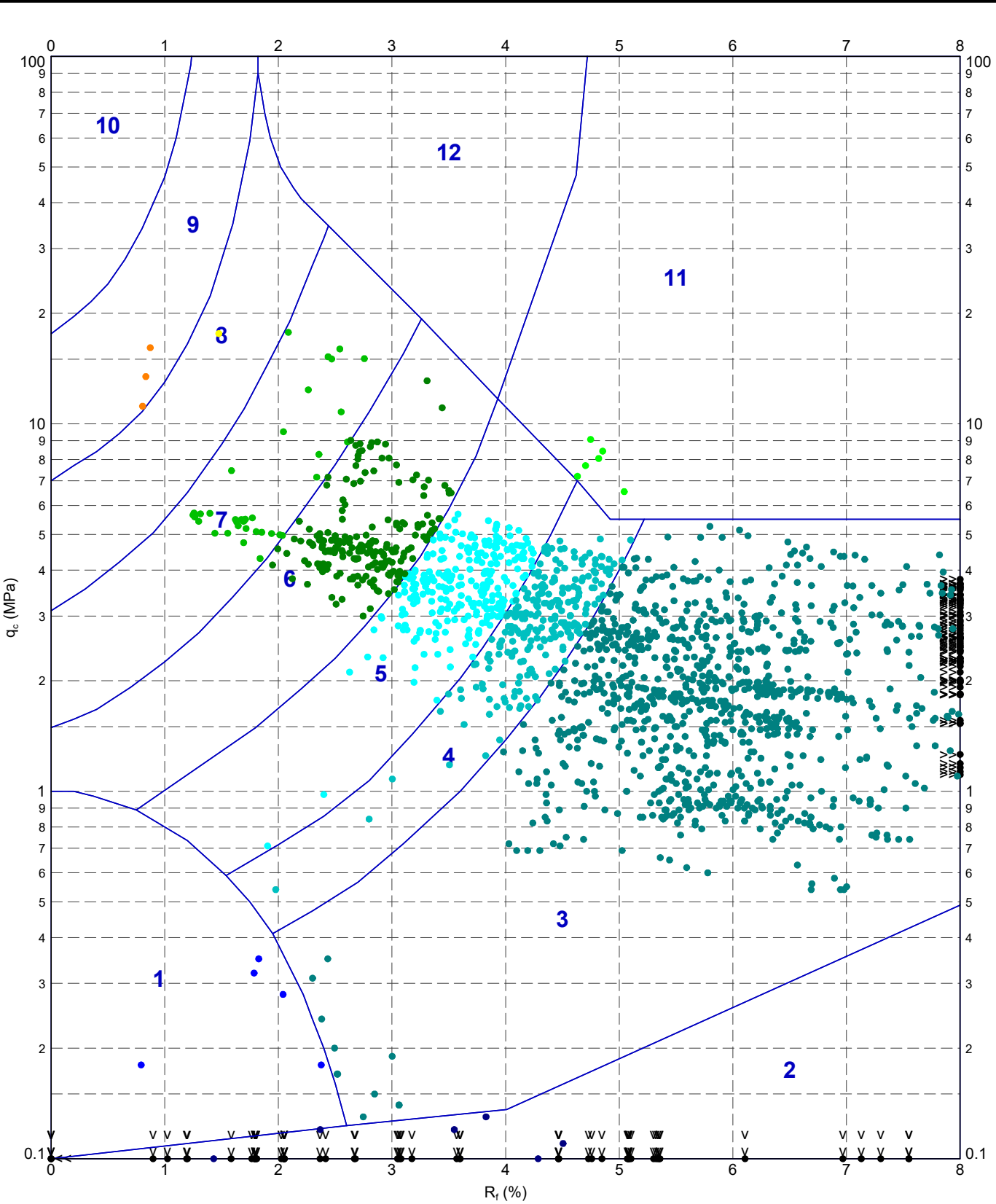
**CPT11**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 491050.407 m <b>NORTHING</b> : 290872.435 m <b>ELEVATION</b> : 104.295 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 10/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>362 mV</td> <td>361 mV</td> <td>-0.011 MPa</td> </tr> <tr> <td>Sleeve</td> <td>286 mV</td> <td>286 mV</td> <td>0 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>244 mV</td> <td>247 mV</td> <td>0.001 kPa</td> </tr> <tr> <td>X-Y Inclinometer</td> <td>2757 mV</td> <td>2569 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	362 mV	361 mV	-0.011 MPa	Sleeve	286 mV	286 mV	0 kPa	Pore Pressure 2	244 mV	247 mV	0.001 kPa	X-Y Inclinometer	2757 mV	2569 mV		Groundwater Level Dissipation Test
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220228-ADVANCED REPORT INSTITUTE 2.02.1 LIB - CHLOE.GLB Graph CPT ROBERTSON ET AL. 8F QC VS. RF APF 1220144 CORBY DELTA SIMONS.GPJ <<DrawingFile>> 04/03/2022 17:43 10.01.00.11 Datagel Lab and In Situ Tool - DGD [Lib: In Situ SI 2.02.0 2017-07-10 Proj: In Situ SI 2.02.0 2017-07-10]



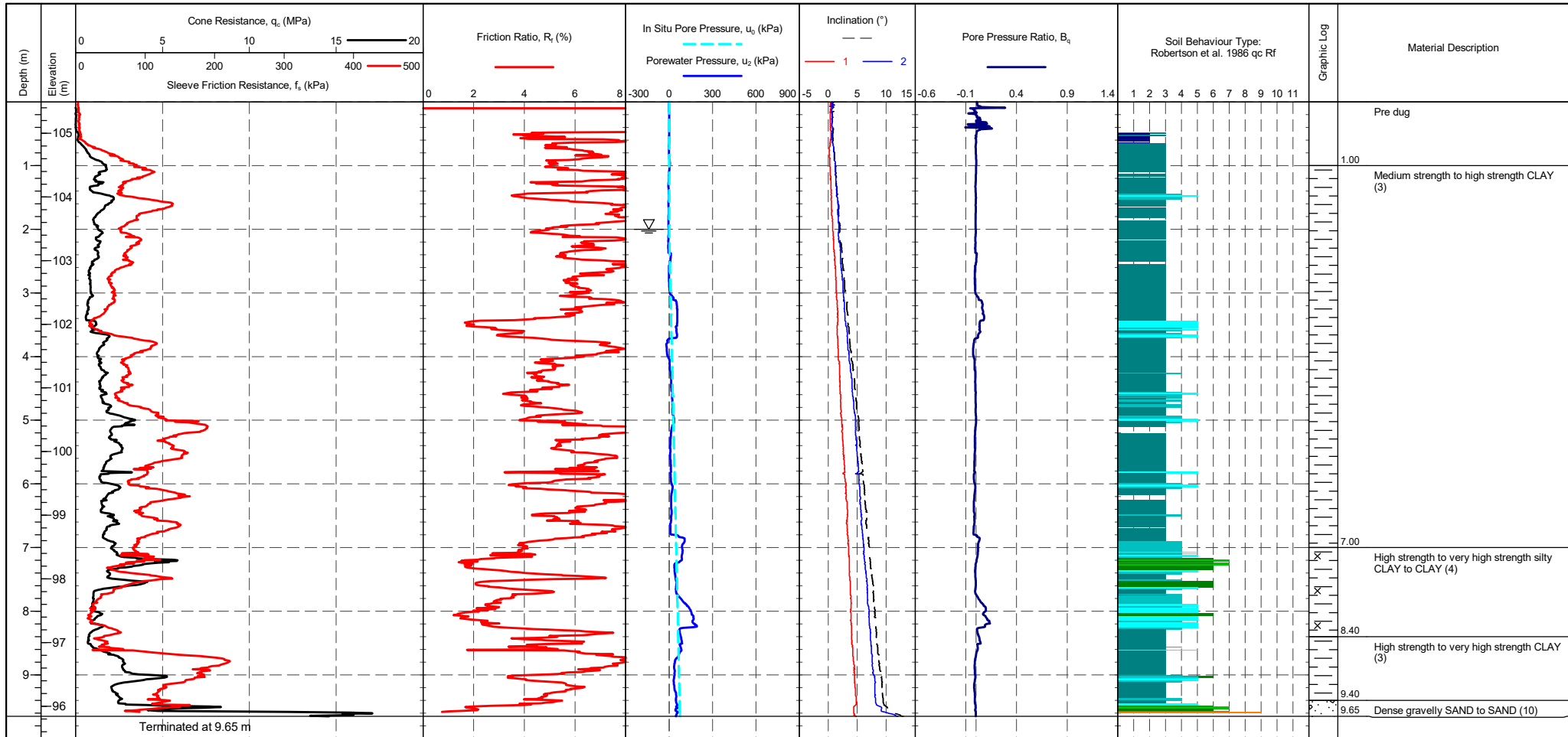
**METHOD: Robertson et al. 1986 qc Rf**

1 - Sensitive fine grained material	4 - Silty CLAY to CLAY	7 - Silty SAND to sandy SILT	10 - Gravelly SAND to SAND
2 - Organic material	5 - Clayey SILT to silty CLAY	8 - SAND to silty SAND	11 - Very stiff fine grained
3 - CLAY	6 - Sandy SILT to clayey SILT	9 - SAND	12 - SAND to clayey SAND

	TITLE	DRAWN	DATE
	Delta Simons Cordby Corby	CHECKED	DATE
	Robertson et al. 1986 qc vs. Rf - CPT11	SCALE	Not To Scale
		PROJECT No 1220144	FIGURE No
		A4	

PointID	<b>CPT12</b>
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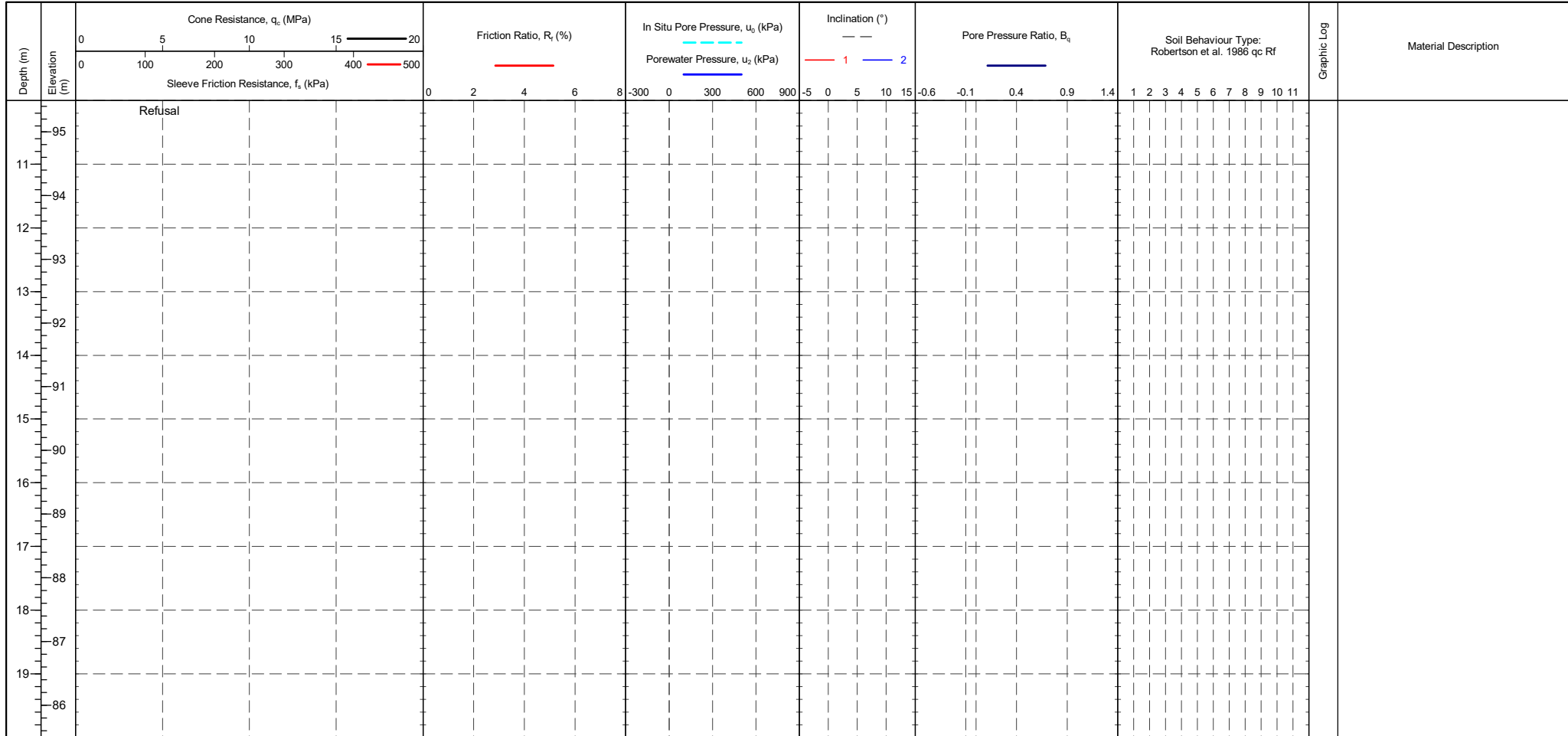
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490922.098 m <b>NORTHING</b> : 290829.929 m <b>ELEVATION</b> : 105.492 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on inclination.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>Transducer</b> Tip : 358 mV / 355 mV / -0.033 MPa Sleeve : 289 mV / 285 mV / -0.003 kPa Pore Pressure 2 : 250 mV / 190 mV / -0.014 kPa X-Y Inclinometer : 2604 mV / 2553 mV	<b>CPTU ZERO VALUES</b> Pre : 358 mV / 289 mV / 250 mV / 2604 mV Post : 355 mV / 285 mV / 190 mV / 2553 mV Difference : -0.033 MPa / -0.003 kPa / -0.014 kPa	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravely SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID  
**CPT12**

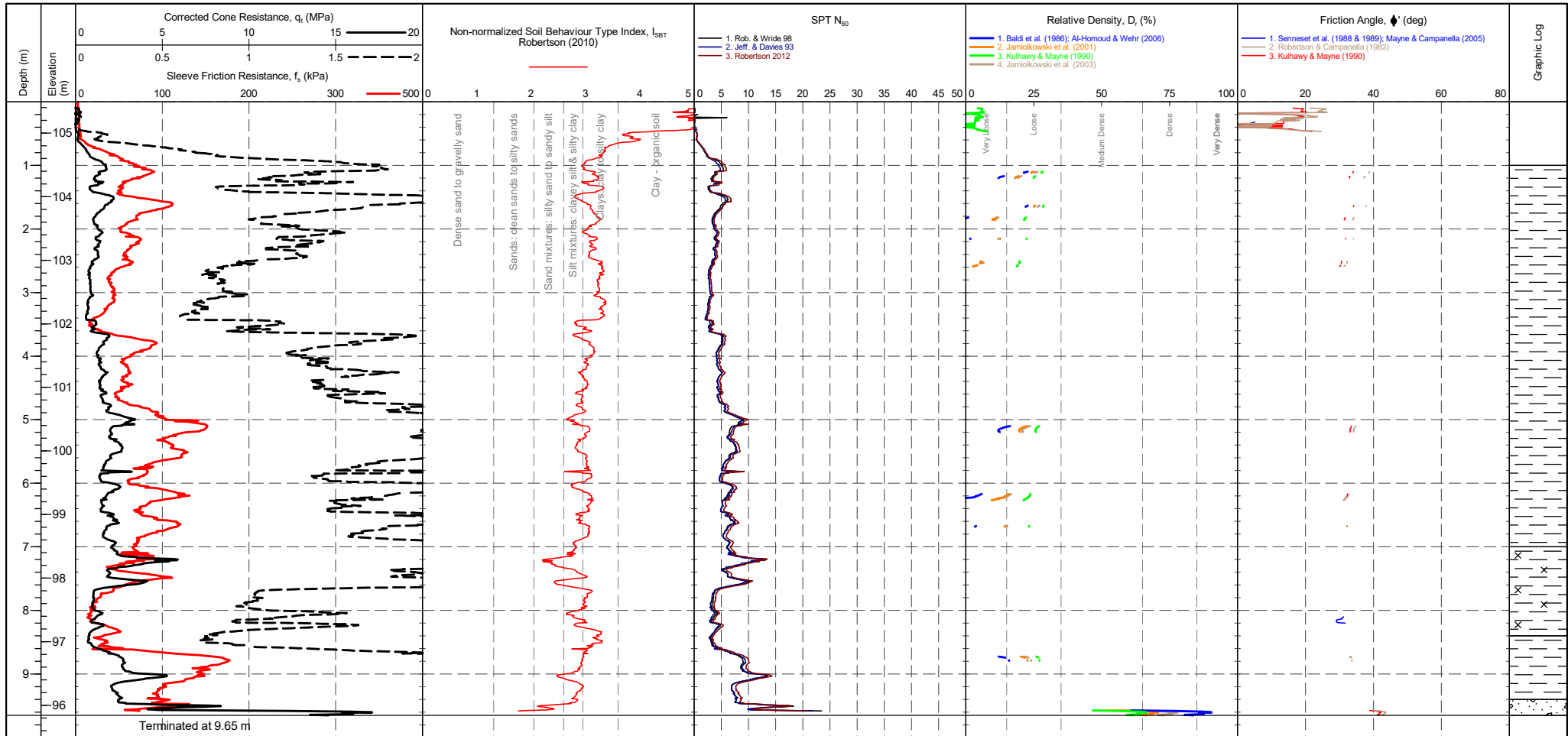
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PointID  
**CPT12**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490922.098 m <b>NORTHING</b> : 290829.929 m <b>ELEVATION</b> : 105.492 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on inclination.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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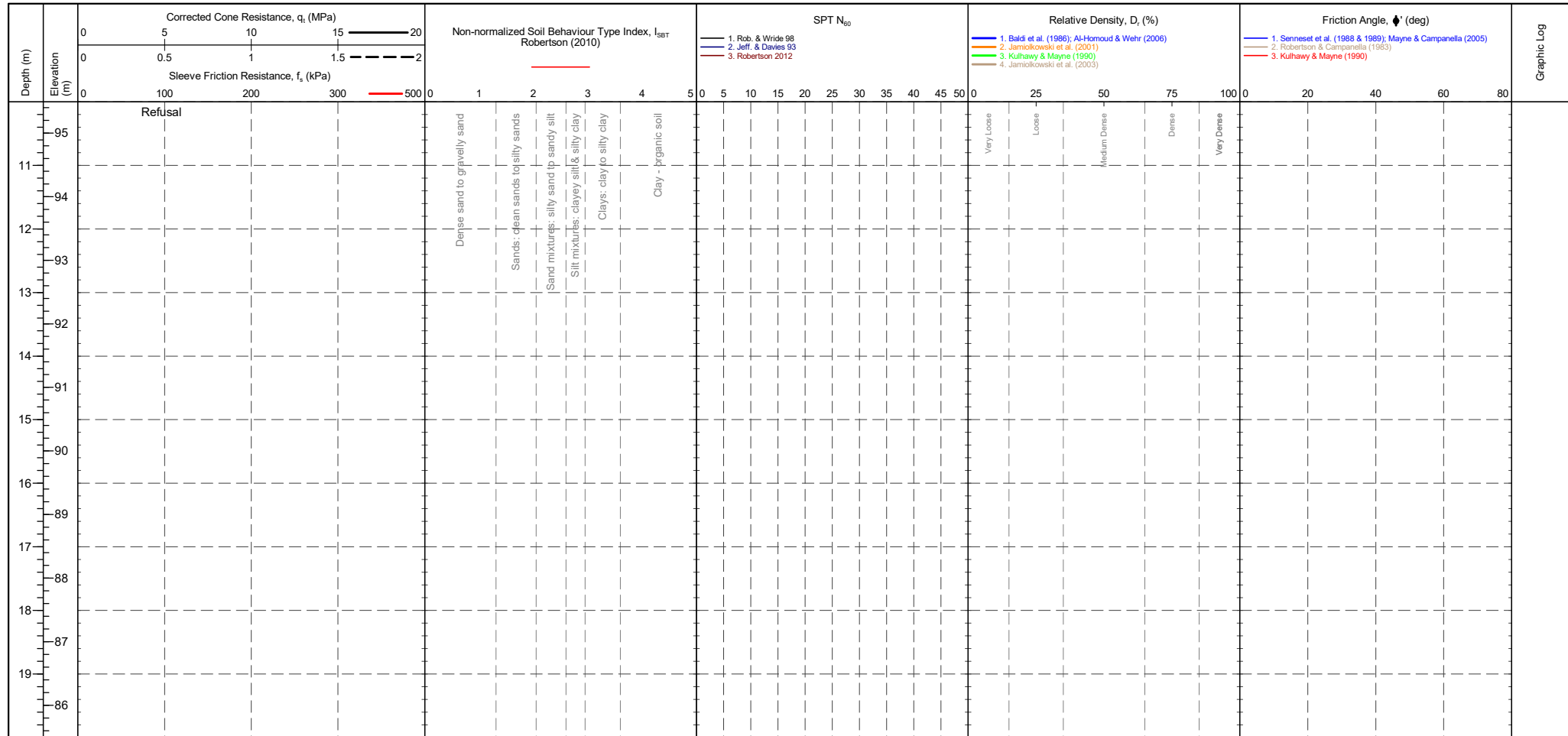




<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip : 358 mV / 355 mV Sleeve : 289 mV / 285 mV Pore Pressure 2 : 250 mV / 190 mV X-Y Inclinator : 2604 mV / 2553 mV	<b>CPTU ZERO VALUES</b> Pre : 358 mV Post : 355 mV Difference : -0.033 MPa Pre : 289 mV Post : 285 mV Difference : -0.003 kPa Pre : 250 mV Post : 190 mV Difference : -0.014 kPa Pre : 2604 mV Post : 2553 mV	<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, I<sub>c</sub></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density D<sub>r</sub> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, I <sub>c</sub>	Description	SPT N value, NSPT	Description	Relative Density D <sub>r</sub> (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
Description	SBT Index, I <sub>c</sub>	Description	SPT N value, NSPT	Description	Relative Density D <sub>r</sub> (%)																																				
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PointID	<b>CPT12</b>
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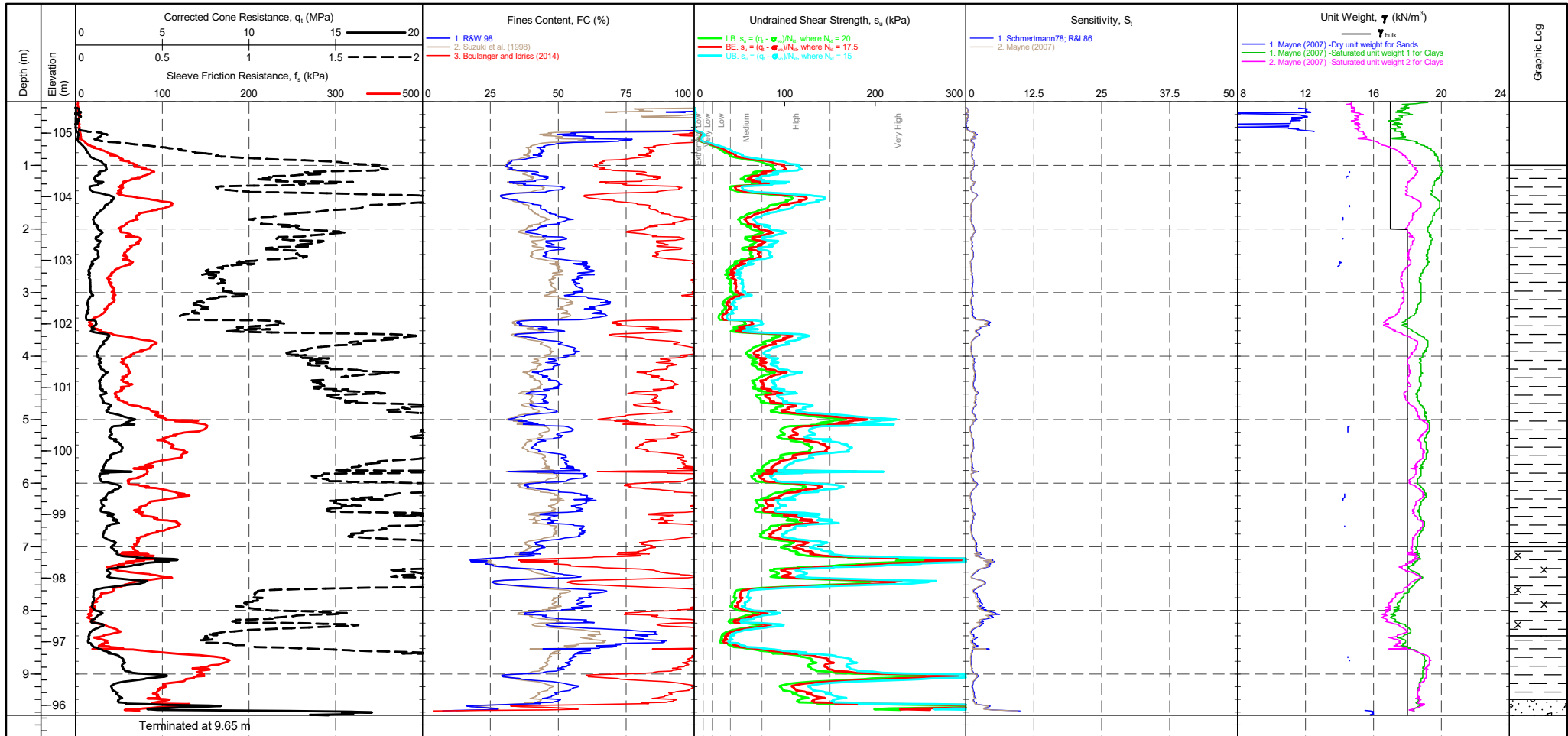
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>358 mV</td> <td>355 mV</td> <td>-0.033 MPa</td> </tr> <tr> <td>Sleeve</td> <td>289 mV</td> <td>285 mV</td> <td>-0.003 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>250 mV</td> <td>190 mV</td> <td>-0.014 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2604 mV</td> <td>2553 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	358 mV	355 mV	-0.033 MPa	Sleeve	289 mV	285 mV	-0.003 kPa	Pore Pressure 2	250 mV	190 mV	-0.014 kPa	X-Y Inclinator	2604 mV	2553 mV		<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, I<sub>c</sub></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density Dr (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, I <sub>c</sub>	Description	SPT N value, NSPT	Description	Relative Density Dr (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	 <b>Groundwater Level</b>   <b>Dissipation Test</b>
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**CPT12**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490922.098 m <b>NORTHING</b> : 290829.929 m <b>ELEVATION</b> : 105.492 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on inclination.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip : 358 mV / 355 mV / -0.033 MPa Sleeve : 289 mV / 285 mV / -0.003 kPa Pore Pressure 2 : 250 mV / 190 mV / -0.014 kPa X-Y Inclinator : 2604 mV / 2553 mV	<b>CPTU ZERO VALUES</b> Pre : 358 mV Post : 355 mV Difference : -0.033 MPa 289 mV / 285 mV / -0.003 kPa 250 mV / 190 mV / -0.014 kPa 2604 mV / 2553 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement su (kPa) Extremely low strength <10 Very low strength 10-20 Low strength 20-40 Term based on measurement su (kPa) Medium strength 40-75 High strength 75-150 Very high strength 150-300 Extremely high strength >300	▽ Groundwater Level ▮ Dissipation Test
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PointID	CPT12
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<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490922.098 m <b>NORTHING</b> : 290829.929 m <b>ELEVATION</b> : 105.492 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on inclination.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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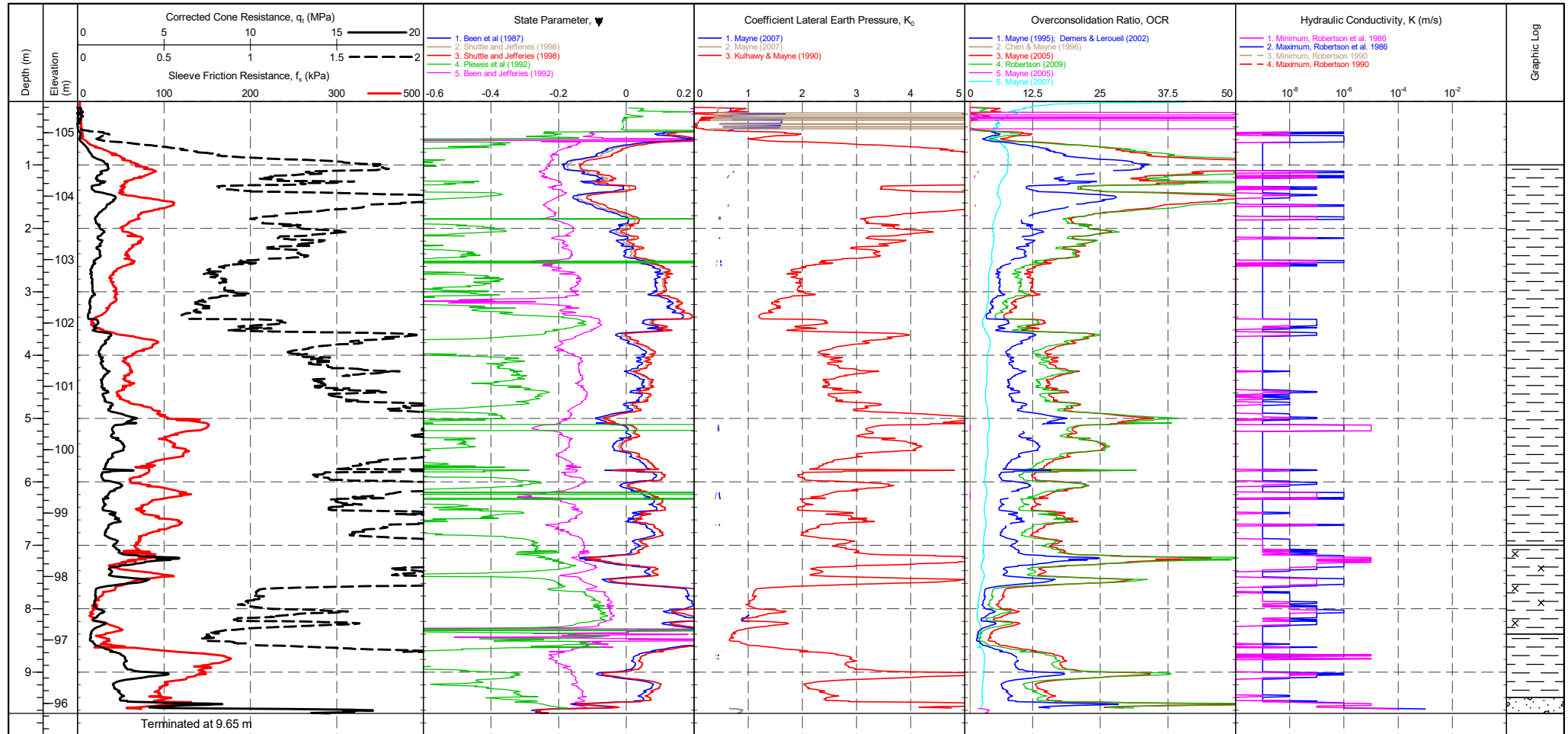


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 358 mV / 355 mV / -0.033 MPa Sleeve: 289 mV / 285 mV / -0.003 kPa Pore Pressure 2: 250 mV / 190 mV / -0.014 kPa X-Y Inclinator: 2604 mV / 2553 mV	<b>CPTU ZERO VALUES</b> Pre Post Difference Tip: 358 mV 355 mV -0.033 MPa Sleeve: 289 mV 285 mV -0.003 kPa Pore Pressure 2: 250 mV 190 mV -0.014 kPa X-Y Inclinator: 2604 mV 2553 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement su (kPa) Term based on measurement su (kPa) Extremely low strength <10 Medium strength 40-75 Very low strength 10-20 High strength 75-150 Low strength 20-40 Very high strength 150-300 Extremely high strength >300	Groundwater Level Dissipation Test
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PointID

**CPT12**

<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490922.098 m <b>NORTHING</b> : 290829.929 m <b>ELEVATION</b> : 105.492 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on inclination.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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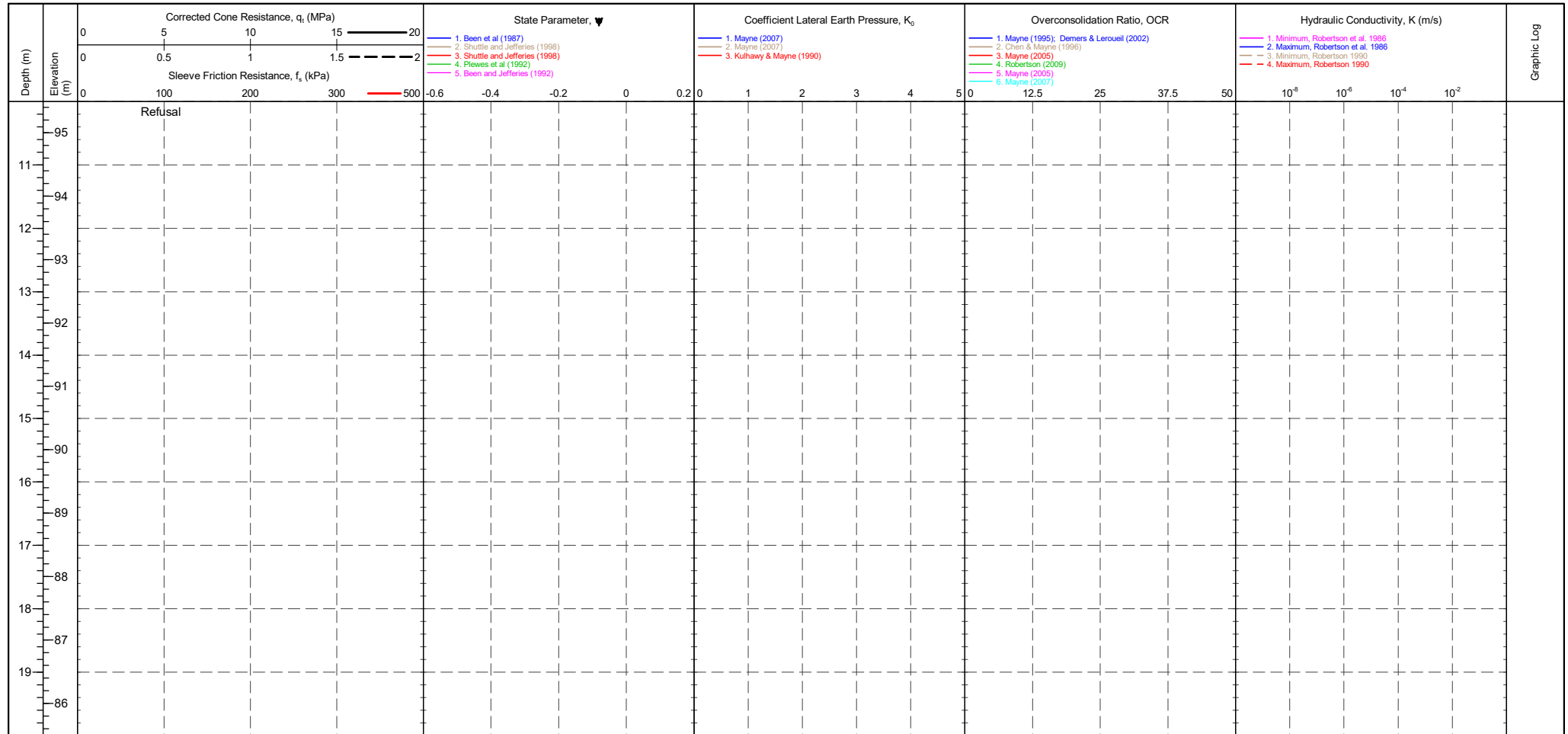


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip: 358 mV / 355 mV / -0.033 MPa Sleeve: 289 mV / 285 mV / -0.003 kPa Pore Pressure 2: 250 mV / 190 mV / -0.014 kPa X-Y Inclinator: 2604 mV / 2553 mV	<b>CPTU ZERO VALUES</b> Pre: 358 mV Post: 355 mV Difference: -0.033 MPa Pre: 289 mV Post: 285 mV Difference: -0.003 kPa Pre: 250 mV Post: 190 mV Difference: -0.014 kPa Pre: 2604 mV Post: 2553 mV	Groundwater Level Dissipation Test
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PointID

CPT12

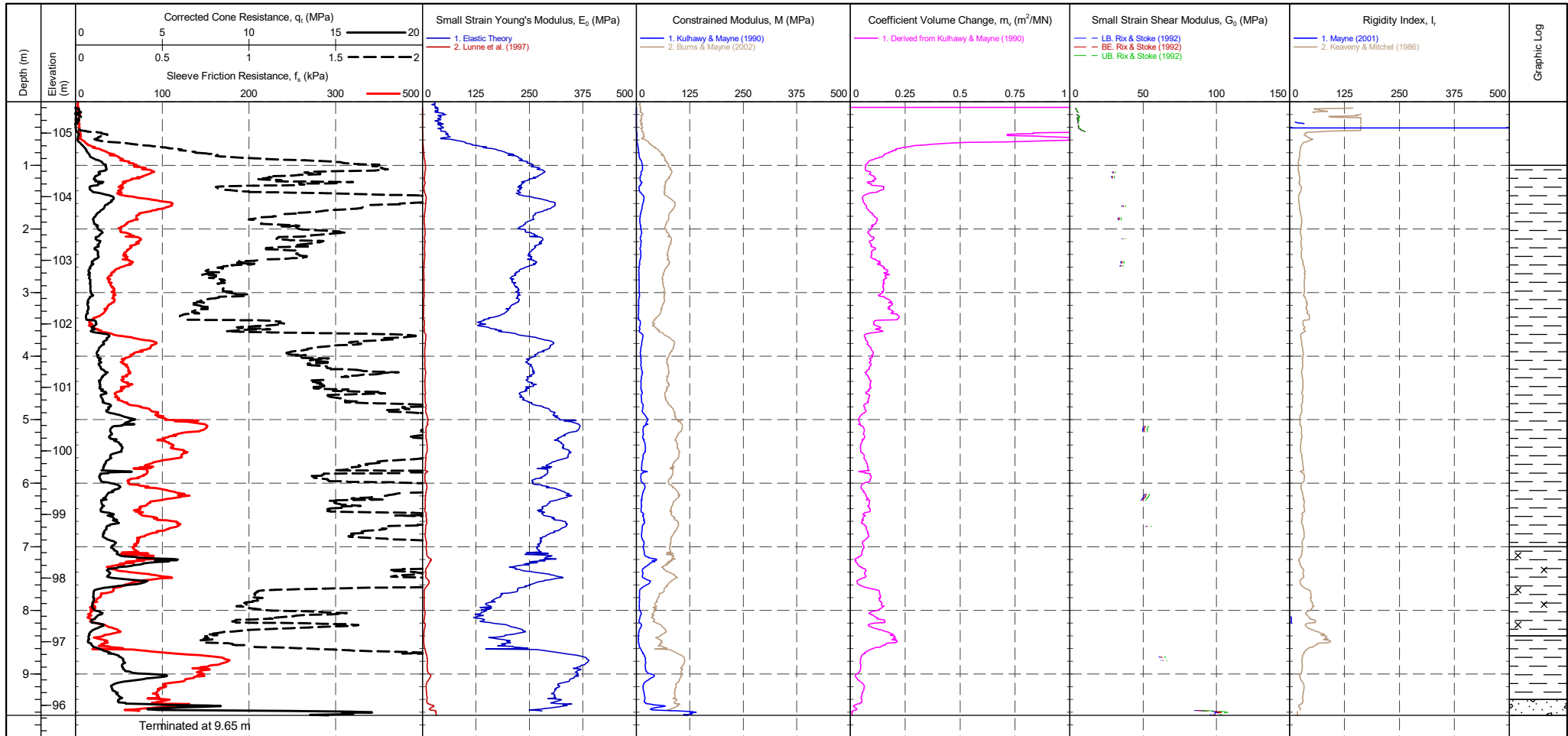
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490922.098 m <b>NORTHING</b> : 290829.929 m <b>ELEVATION</b> : 105.492 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on inclination.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>358 mV</td> <td>355 mV</td> <td>-0.033 MPa</td> </tr> <tr> <td>Sleeve</td> <td>289 mV</td> <td>285 mV</td> <td>-0.003 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>250 mV</td> <td>190 mV</td> <td>-0.014 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2604 mV</td> <td>2553 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	358 mV	355 mV	-0.033 MPa	Sleeve	289 mV	285 mV	-0.003 kPa	Pore Pressure 2	250 mV	190 mV	-0.014 kPa	X-Y Inclinator	2604 mV	2553 mV		Groundwater Level Dissipation Test
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PointID  
**CPT12**

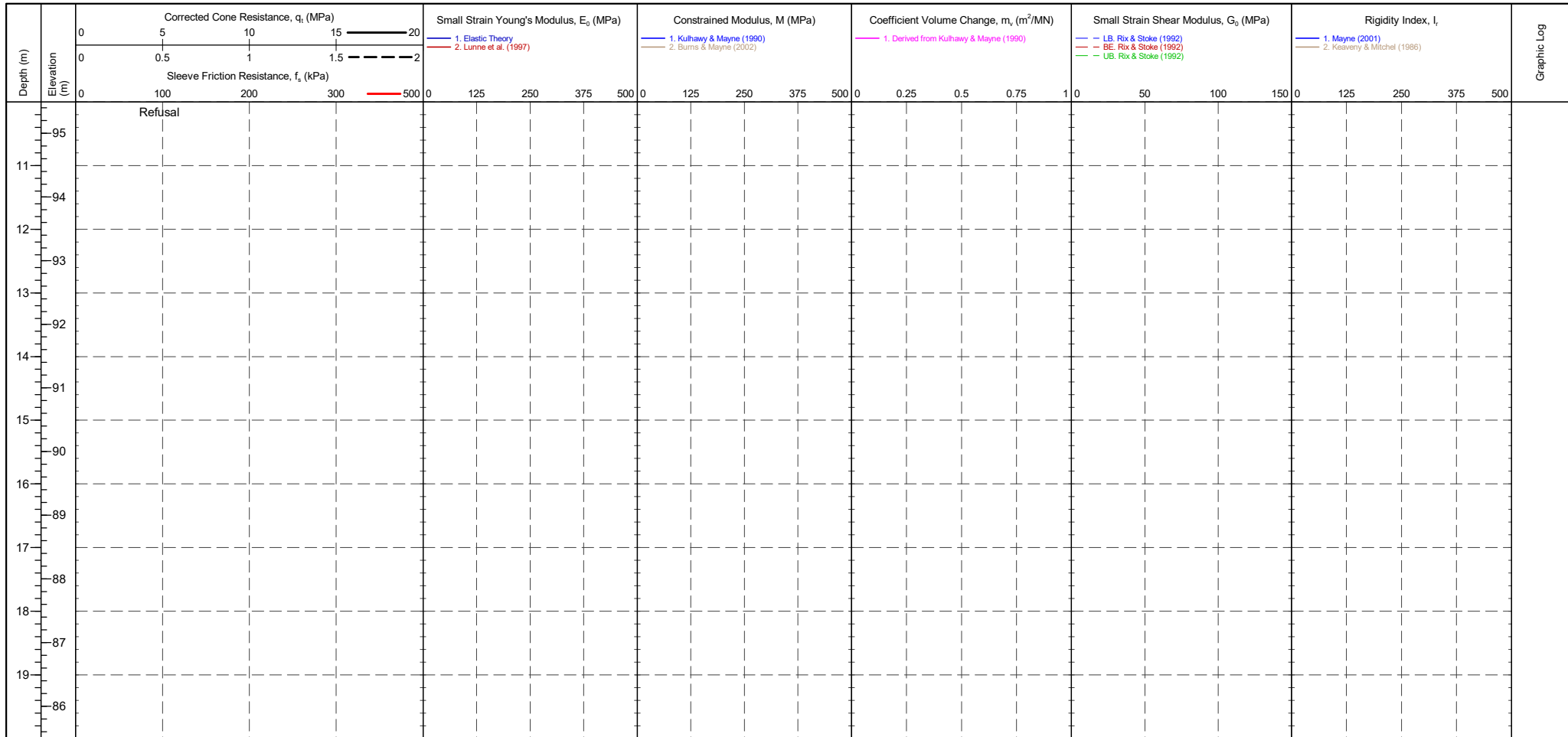
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490922.098 m <b>NORTHING</b> : 290829.929 m <b>ELEVATION</b> : 105.492 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on inclination.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> Transducer Pre Post Difference Tip 358 mV 355 mV -0.033 MPa Sleeve 289 mV 285 mV -0.003 kPa Pore Pressure 2 250 mV 190 mV -0.014 kPa X-Y Inclinator 2604 mV 2553 mV	Groundwater Level Dissipation Test
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PointID	<b>CPT12</b>
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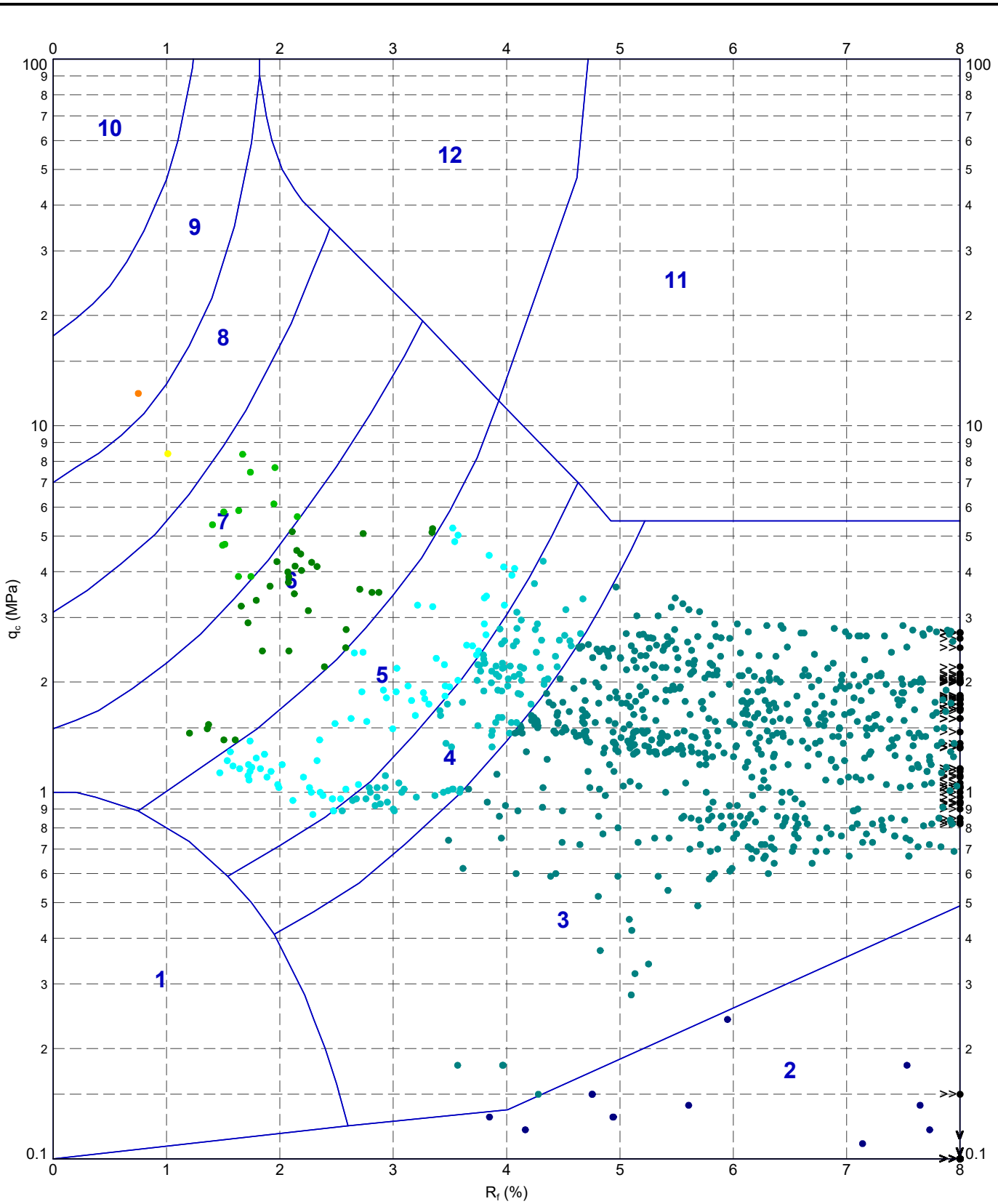
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490922.098 m <b>NORTHING</b> : 290829.929 m <b>ELEVATION</b> : 105.492 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on inclination.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>358 mV</td> <td>355 mV</td> <td>-0.033 MPa</td> </tr> <tr> <td>Sleeve</td> <td>289 mV</td> <td>285 mV</td> <td>-0.003 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>250 mV</td> <td>190 mV</td> <td>-0.014 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2604 mV</td> <td>2553 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	358 mV	355 mV	-0.033 MPa	Sleeve	289 mV	285 mV	-0.003 kPa	Pore Pressure 2	250 mV	190 mV	-0.014 kPa	X-Y Inclinator	2604 mV	2553 mV		Groundwater Level Dissipation Test
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220228-ADVANCED REPORT INSTITUTE 2.02.1 LIB - CHLOE.GLB Graph CPT ROBERTSON ET AL. 8F QC VS. RF APF 1220144 CORBY DELTA SIMONS G.P.J. <<DrawingFile>> 04/03/2022 17:46 10.01.00.11 Datagel Lab and In Situ Tool - DGD [Lib: In Situ SI 2.02.0 2017-07-10 Proj: In Situ SI 2.02.0 2017-07-10]



METHOD: Robertson et al. 1986 qc Rf

- 1 - Sensitive fine grained material
- 4 - Silty CLAY to CLAY
- 7 - Silty SAND to sandy SILT
- 10 - Gravelly SAND to SAND
- 2 - Organic material
- 5 - Clayey SILT to silty CLAY
- 8 - SAND to silty SAND
- 11 - Very stiff fine grained
- 3 - CLAY
- 6 - Sandy SILT to clayey SILT
- 9 - SAND
- 12 - SAND to clayey SAND

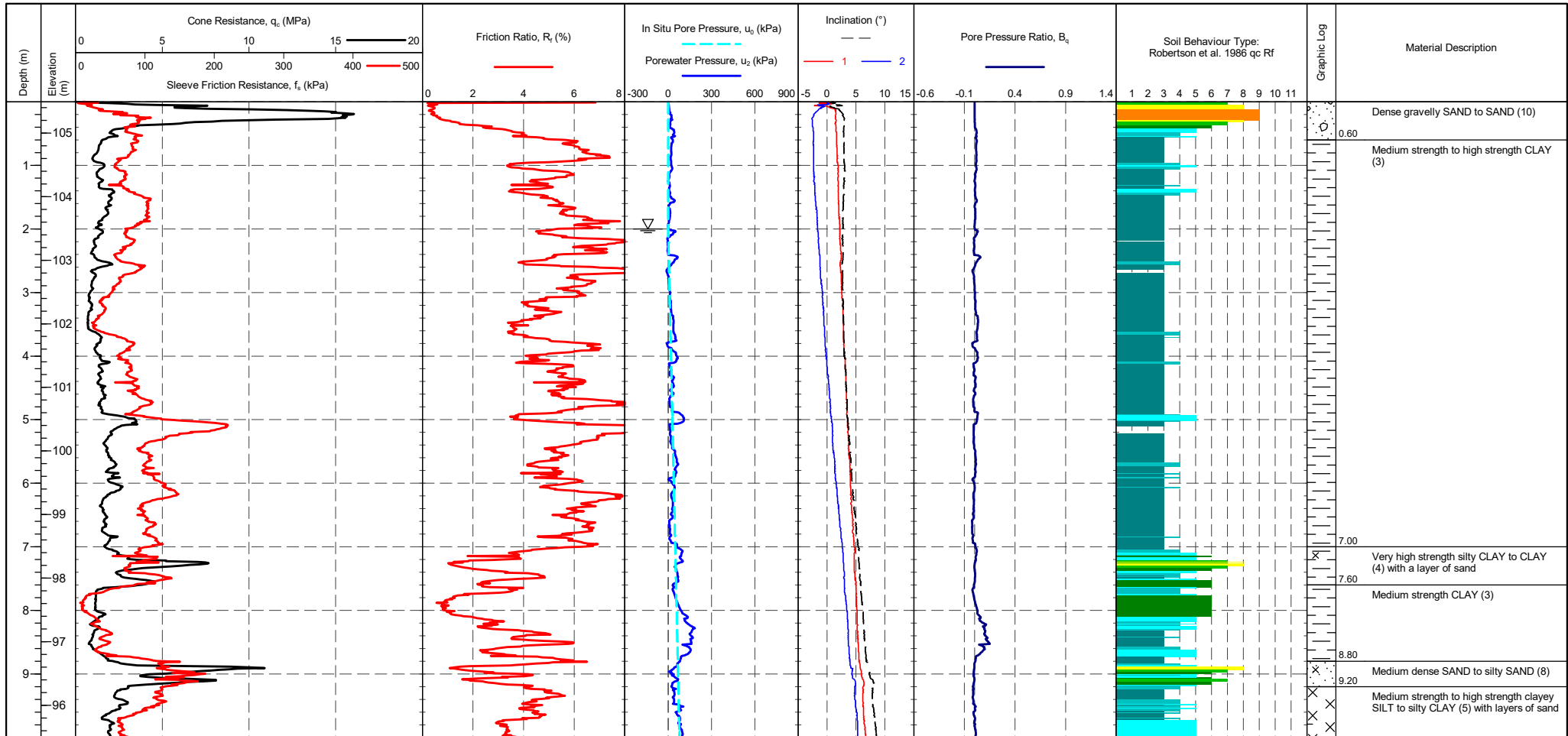


TITLE  
 Delta Simons  
 Cordby  
 Corby  
 Robertson et al. 1986 qc vs. Rf - CPT12

DRAWN	DATE	04/03/2022
CHECKED	DATE	04/03/2022
SCALE	Not To Scale	
PROJECT No	1220144	
FIGURE No	A4	

PointID	<b>CPT12A</b>
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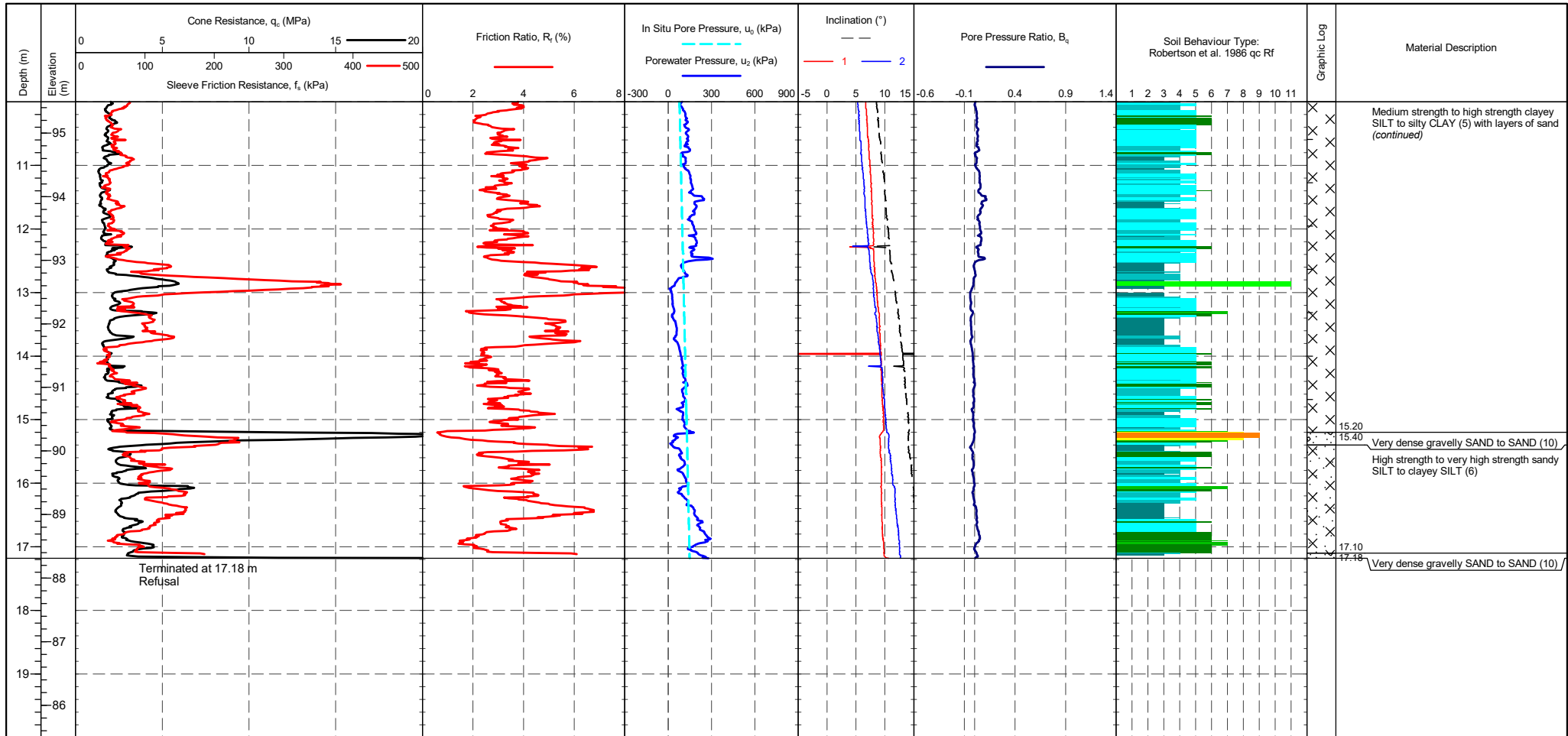
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490922.098 m <b>NORTHING</b> : 290829.929 m <b>ELEVATION</b> : 105.492 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip Pre 359 mV Post 361 mV Difference 0.022 MPa Sleeve Pre 289 mV Post 286 mV Difference -0.002 kPa Pore Pressure 2 Pre 215 mV Post 250 mV Difference 0.008 kPa X-Y Inclinator Pre 2609 mV Post 2630 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravely SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID	<b>CPT12A</b>
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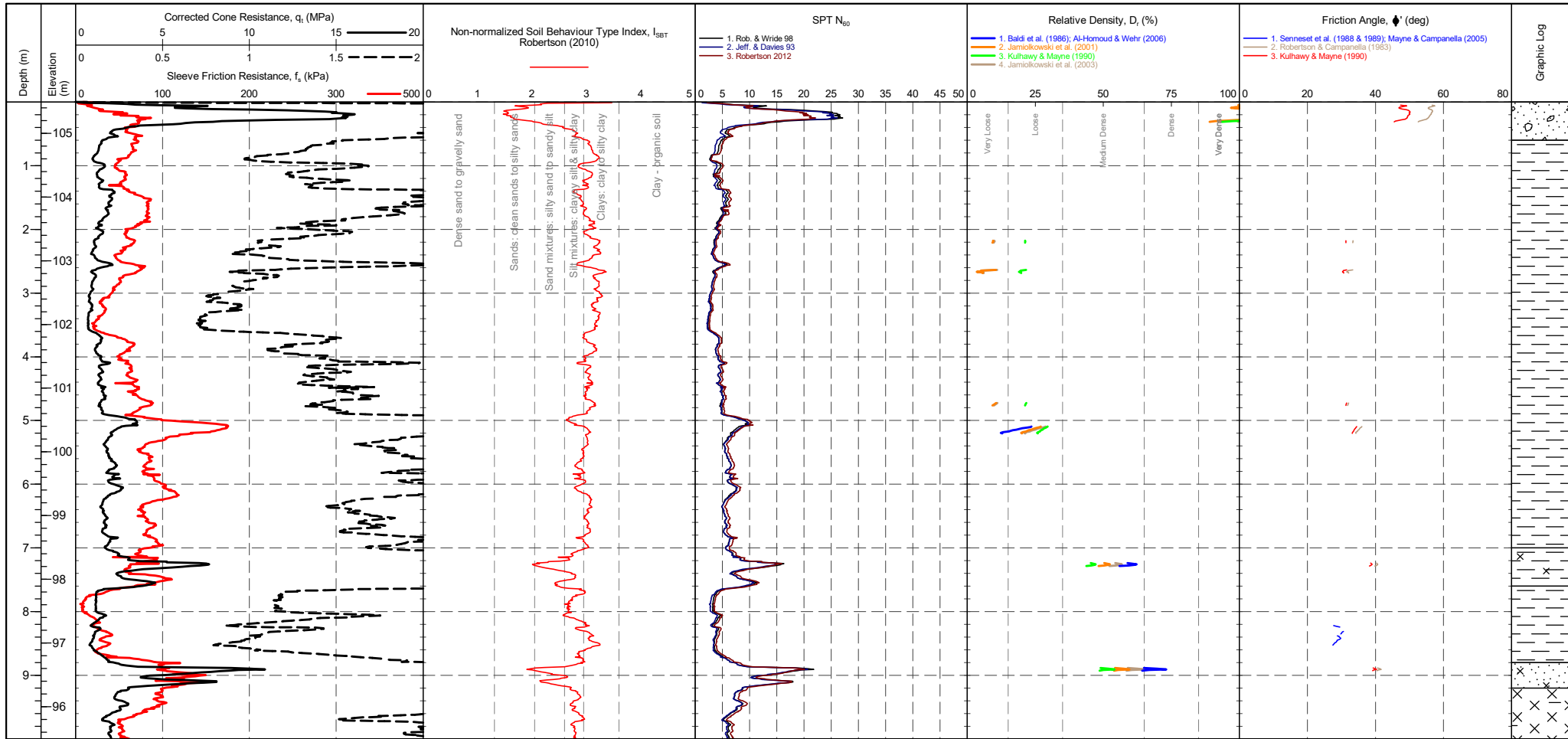
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<b>CONE ID</b> : S15-CFIP.1867 <b>CALIBRATION DATE</b> : 05/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> Transducer Tip : 359 mV / 361 mV / 0.022 MPa Sleeve : 289 mV / 286 mV / -0.002 kPa Pore Pressure 2 : 215 mV / 250 mV / 0.008 kPa X-Y Inclinator : 2609 mV / 2630 mV	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravely SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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PointID	<b>CPT12A</b>
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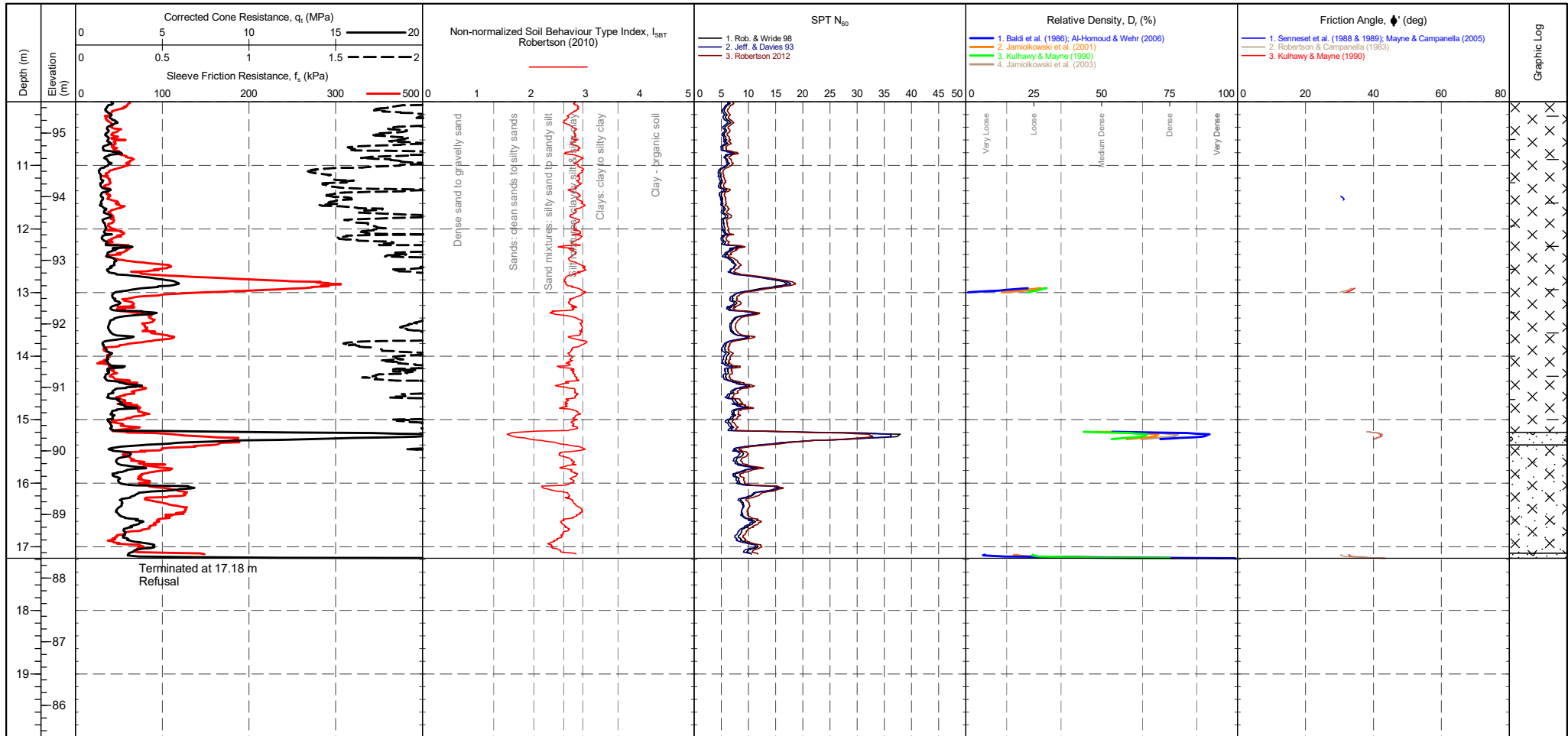
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Description	SBT Index, $I_c$	Description	SPT N value, NSPT	Description	Relative Density $D_r$ (%)																																				
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Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65																																				
Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85																																				
Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85																																				

PointID	<b>CPT12A</b>
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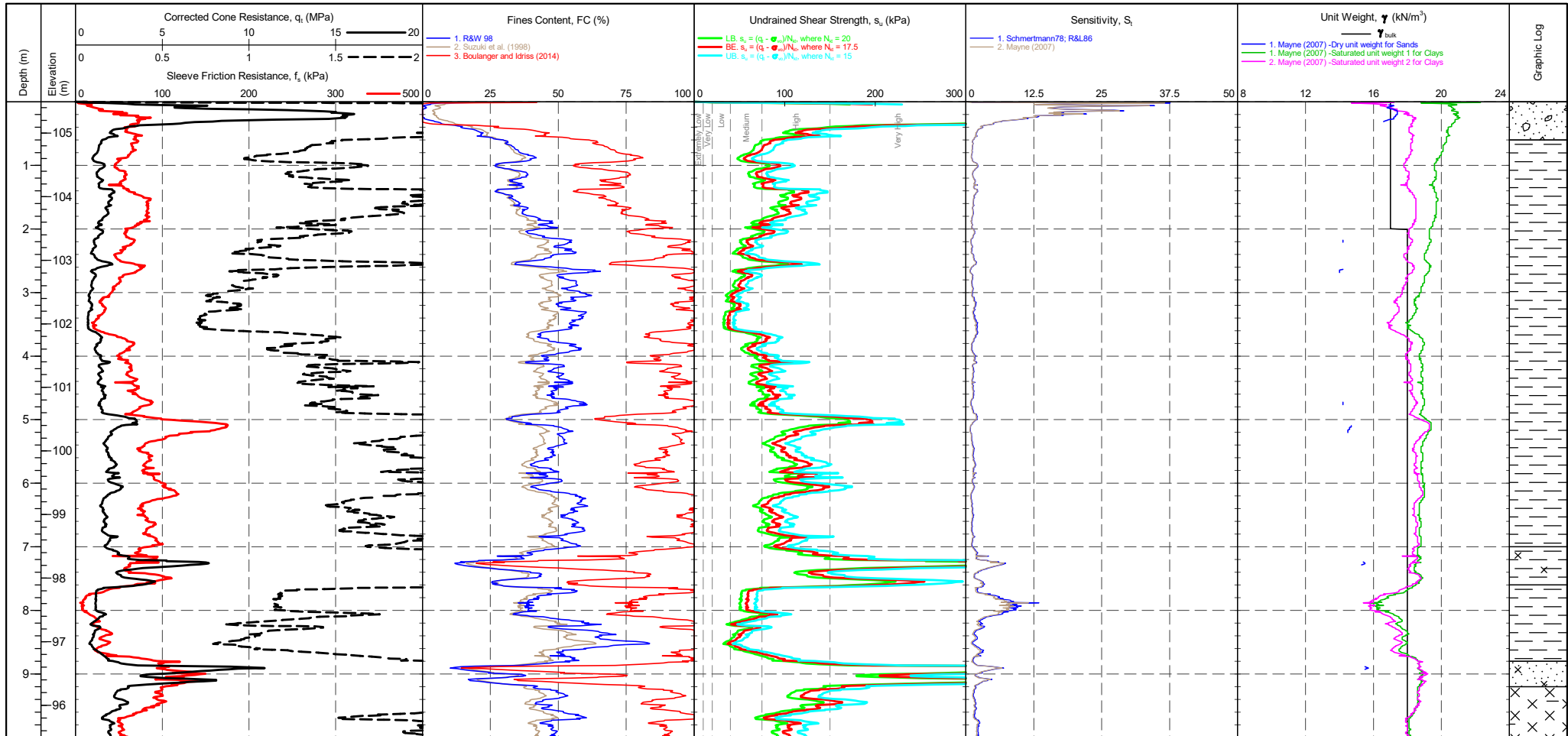
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490922.098 m <b>NORTHING</b> : 290829.929 m <b>ELEVATION</b> : 105.492 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 2 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>359 mV</td> <td>361 mV</td> <td>0.022 MPa</td> </tr> <tr> <td>Sleeve</td> <td>289 mV</td> <td>286 mV</td> <td>-0.002 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>215 mV</td> <td>250 mV</td> <td>0.008 kPa</td> </tr> <tr> <td>X-Y inclinometer</td> <td>2609 mV</td> <td>2630 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	359 mV	361 mV	0.022 MPa	Sleeve	289 mV	286 mV	-0.002 kPa	Pore Pressure 2	215 mV	250 mV	0.008 kPa	X-Y inclinometer	2609 mV	2630 mV		<b>GRANULAR SOILS (Sands &amp; Gravels) Robertson et al. 1986 Zones 7-10 and Zone 12</b> <table border="1"> <thead> <tr> <th>Description</th> <th>SBT Index, <math>I_c</math></th> <th>Description</th> <th>SPT N value, NSPT</th> <th>Description</th> <th>Relative Density <math>D_r</math> (%)</th> </tr> </thead> <tbody> <tr> <td>Clays</td> <td>2.95-3.60</td> <td>Very Loose</td> <td>0 - 4</td> <td>Very Loose</td> <td>0 - 15</td> </tr> <tr> <td>Silt mixtures</td> <td>2.60-2.95</td> <td>Loose</td> <td>4 - 10</td> <td>Loose</td> <td>15 - 35</td> </tr> <tr> <td>Sand mixtures</td> <td>2.05-2.60</td> <td>Medium Dense</td> <td>10 - 30</td> <td>Medium Dense</td> <td>35 - 65</td> </tr> <tr> <td>Sands</td> <td>1.31-2.05</td> <td>Dense</td> <td>30 - 50</td> <td>Dense</td> <td>65 - 85</td> </tr> <tr> <td>Gravelly sand</td> <td>&lt;1.31</td> <td>Very Dense</td> <td>&gt;50</td> <td>Very Dense</td> <td>&gt;85</td> </tr> </tbody> </table>	Description	SBT Index, $I_c$	Description	SPT N value, NSPT	Description	Relative Density $D_r$ (%)	Clays	2.95-3.60	Very Loose	0 - 4	Very Loose	0 - 15	Silt mixtures	2.60-2.95	Loose	4 - 10	Loose	15 - 35	Sand mixtures	2.05-2.60	Medium Dense	10 - 30	Medium Dense	35 - 65	Sands	1.31-2.05	Dense	30 - 50	Dense	65 - 85	Gravelly sand	<1.31	Very Dense	>50	Very Dense	>85	Groundwater Level Dissipation Test
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**CPT12A**

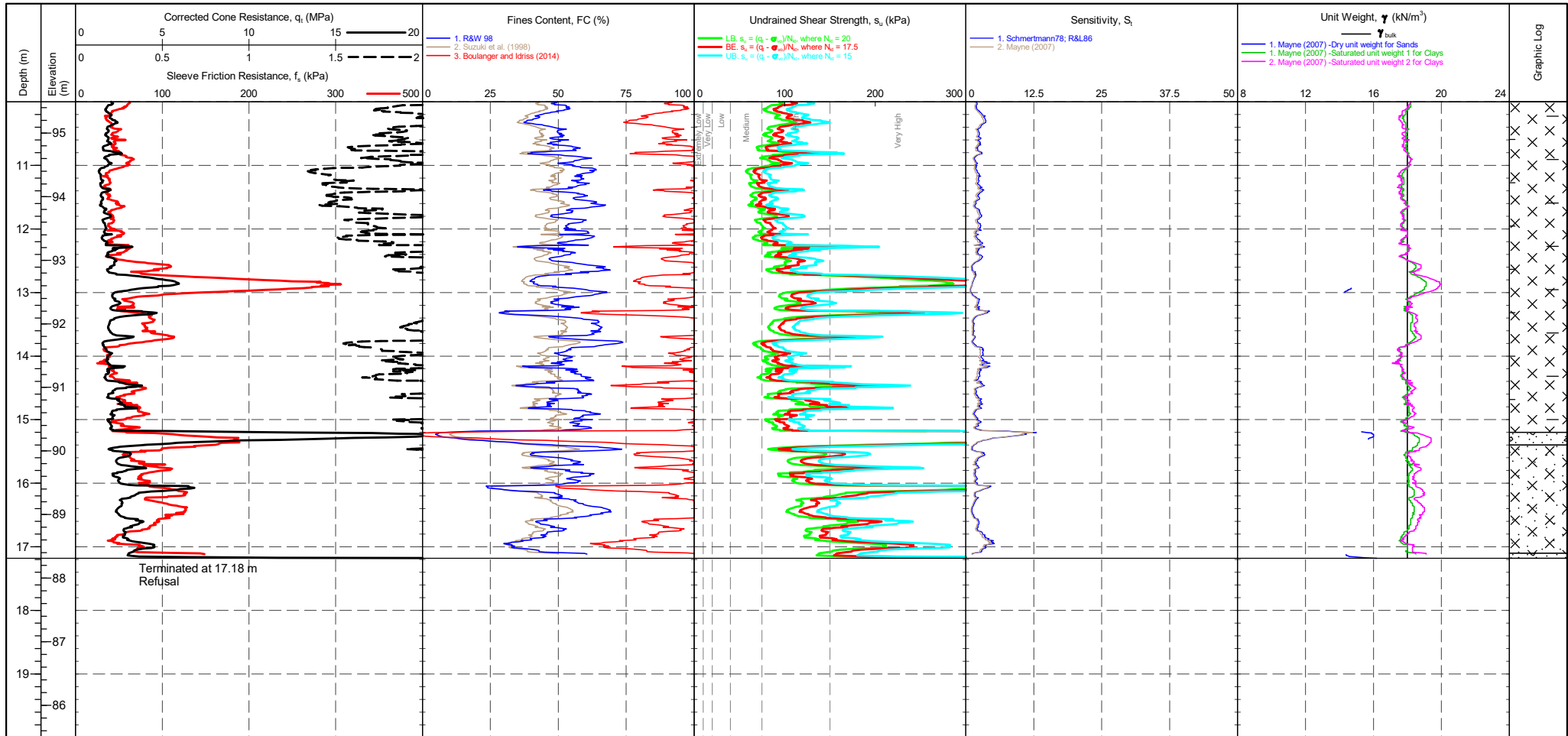
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby <b>LOCATION</b> : Cordby <b>PROJECT No.</b> : 1220144	<b>EASTING</b> : 490922.098 m <b>NORTHING</b> : 290829.929 m <b>ELEVATION</b> : 105.492 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 2 <b>STATUS</b> : Final <b>TEST DATE</b> : 09/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip</td> <td>359 mV</td> <td>361 mV</td> <td>0.022 MPa</td> </tr> <tr> <td>Sleeve</td> <td>289 mV</td> <td>286 mV</td> <td>-0.002 kPa</td> </tr> <tr> <td>Pore Pressure 2</td> <td>215 mV</td> <td>250 mV</td> <td>0.008 kPa</td> </tr> <tr> <td>X-Y Inclinator</td> <td>2609 mV</td> <td>2630 mV</td> <td></td> </tr> </table>	Transducer	Pre	Post	Difference	Tip	359 mV	361 mV	0.022 MPa	Sleeve	289 mV	286 mV	-0.002 kPa	Pore Pressure 2	215 mV	250 mV	0.008 kPa	X-Y Inclinator	2609 mV	2630 mV		<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> <table border="1"> <tr> <th>Term based on measurement</th> <th>su (kPa)</th> <th>Term based on measurement</th> <th>su (kPa)</th> </tr> <tr> <td>Extremely low strength</td> <td>&lt;10</td> <td>Medium strength</td> <td>40-75</td> </tr> <tr> <td>Very low strength</td> <td>10-20</td> <td>High strength</td> <td>75-150</td> </tr> <tr> <td>Low strength</td> <td>20-40</td> <td>Very high strength</td> <td>150-300</td> </tr> <tr> <td></td> <td></td> <td>Extremely high strength</td> <td>&gt;300</td> </tr> </table>	Term based on measurement	su (kPa)	Term based on measurement	su (kPa)	Extremely low strength	<10	Medium strength	40-75	Very low strength	10-20	High strength	75-150	Low strength	20-40	Very high strength	150-300			Extremely high strength	>300	Groundwater Level Dissipation Test
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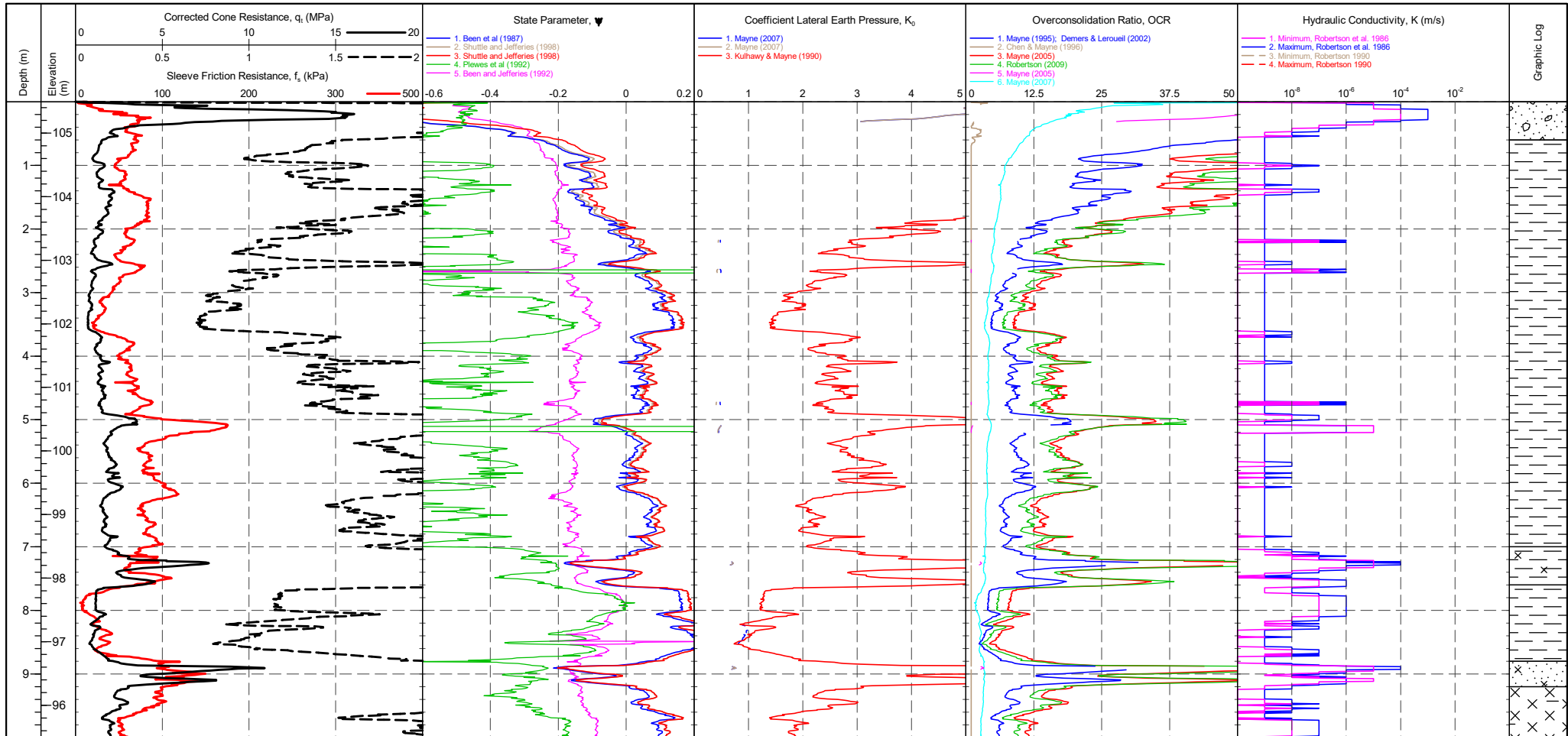


<b>CONE ID</b> : S15-CFIP.1867 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 15cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.79 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> Tip : 359 mV Sleeve : 289 mV Pore Pressure 2 : 215 mV X-Y Inclinator : 2609 mV	<b>CPTU ZERO VALUES</b> Post : 361 mV Difference : 0.022 MPa -0.002 kPa 250 mV 2630 mV	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> Term based on measurement su (kPa) Extremely low strength <10 Very low strength 10-20 Low strength 20-40	Term based on measurement su (kPa) Medium strength 40-75 High strength 75-150 Very high strength 150-300 Extremely high strength >300	Groundwater Level Dissipation Test
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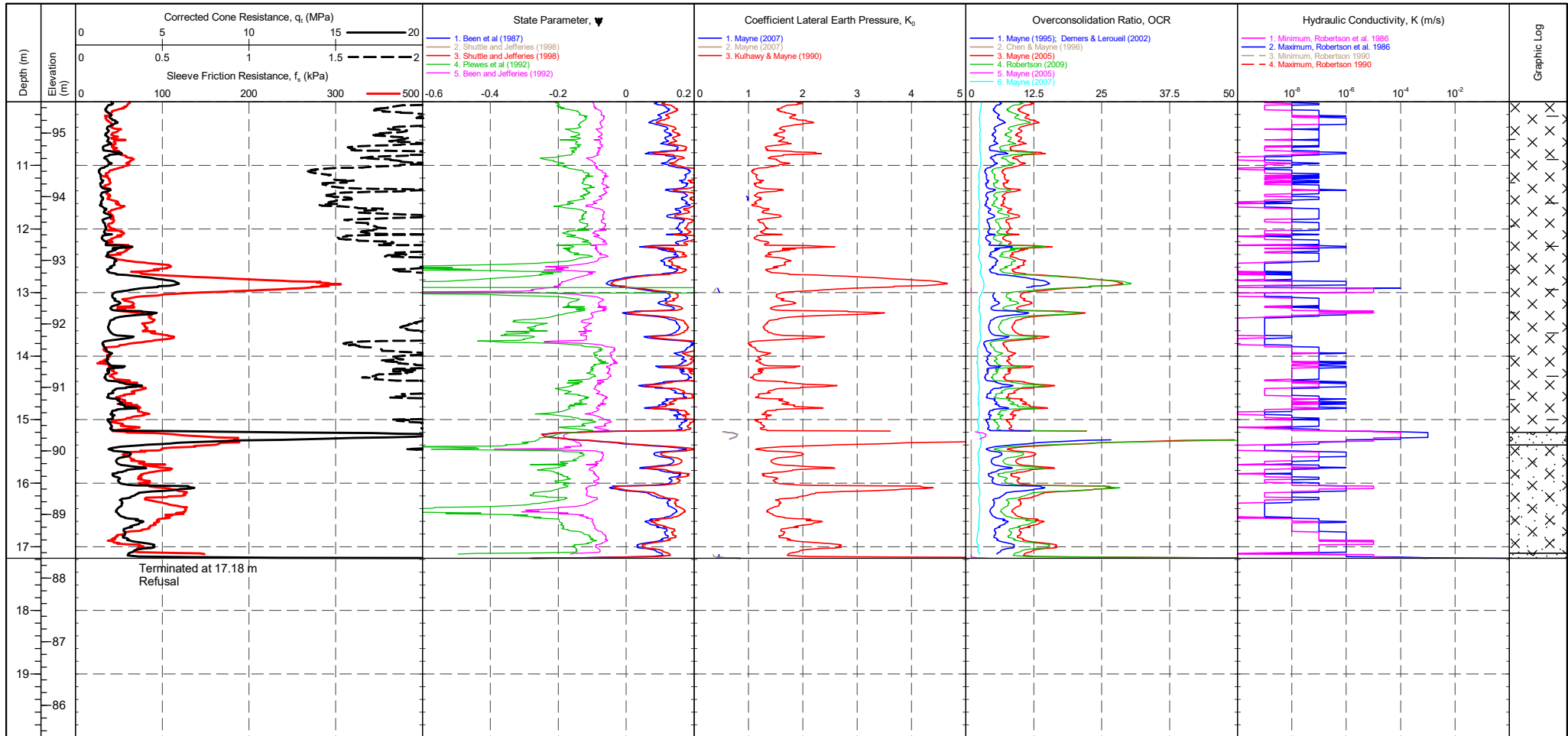
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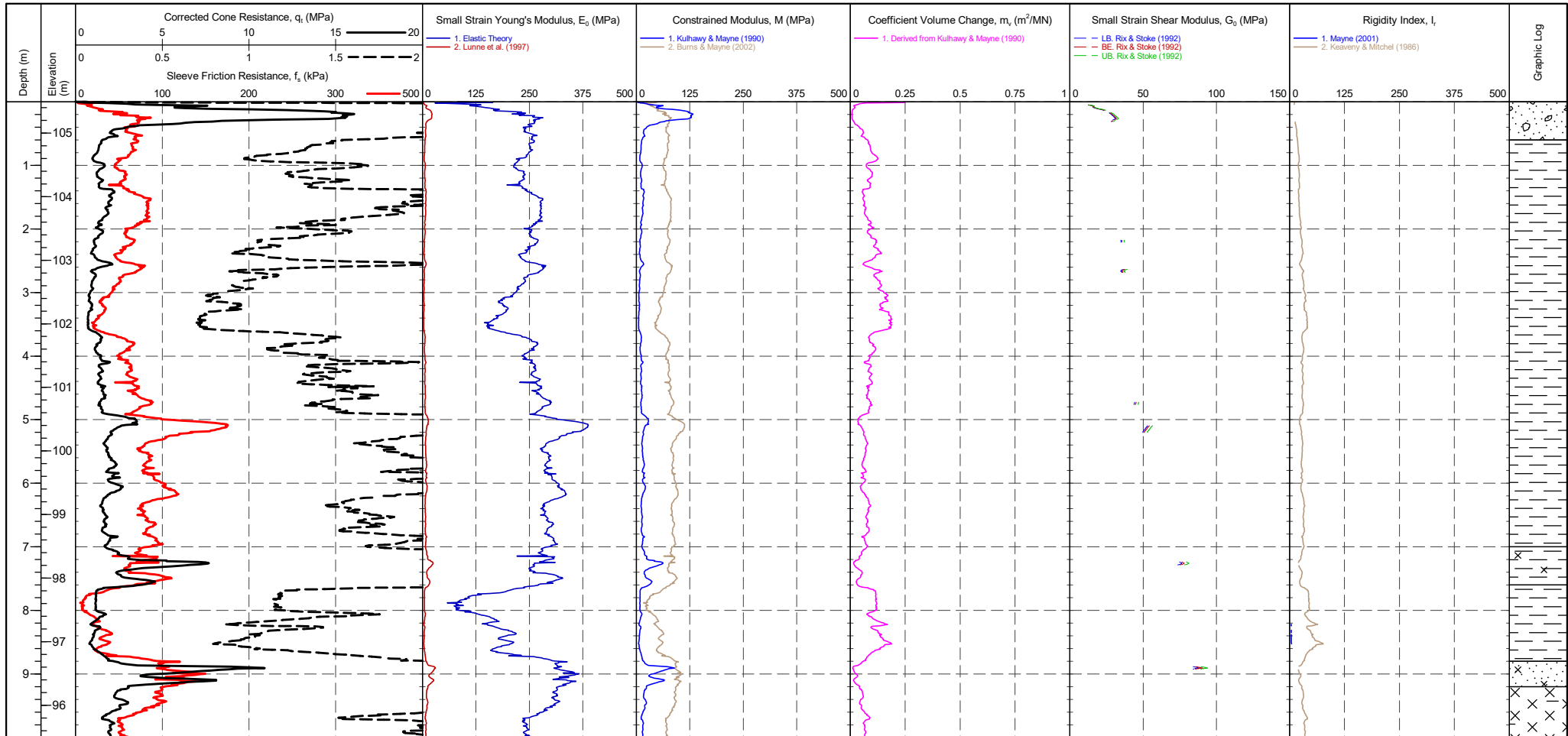
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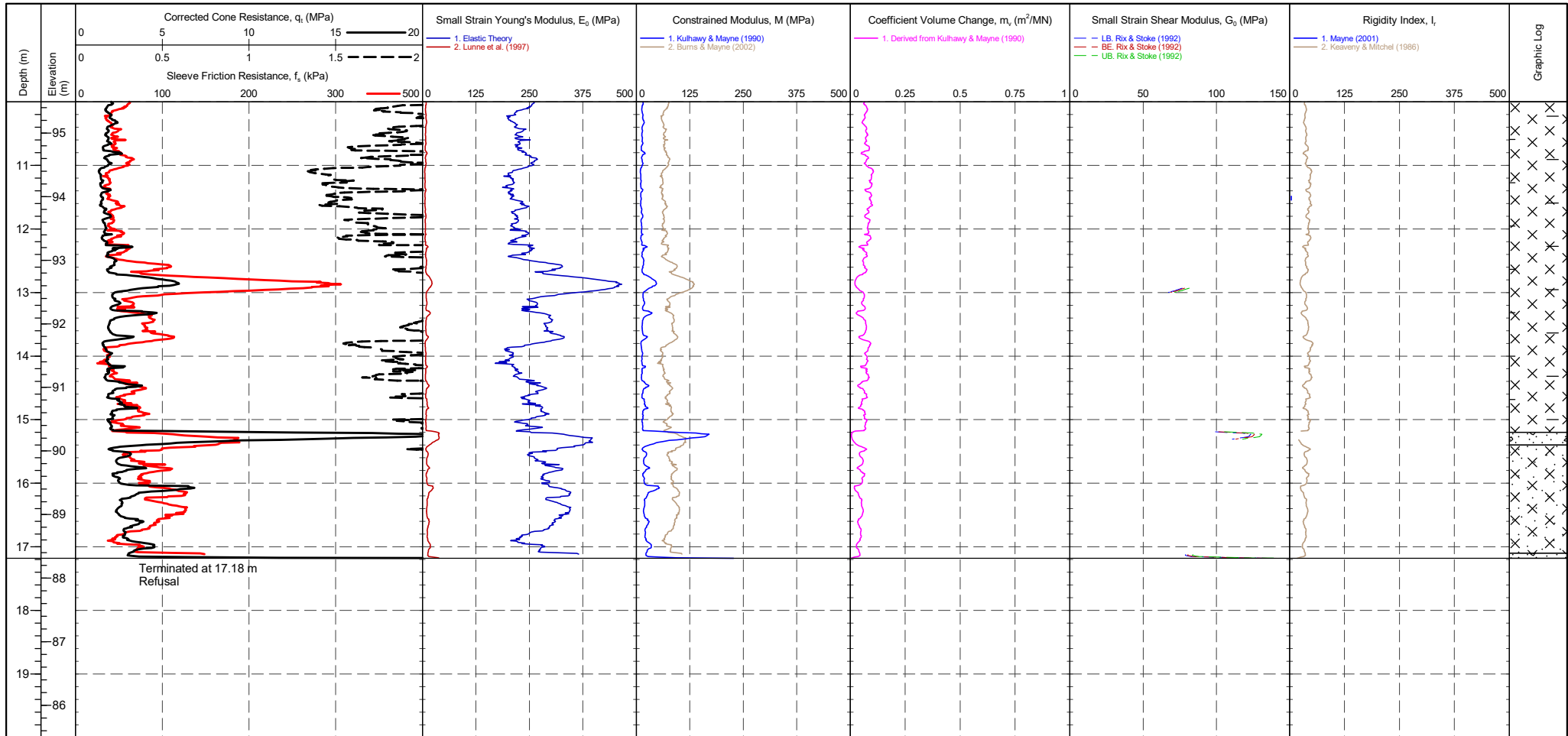
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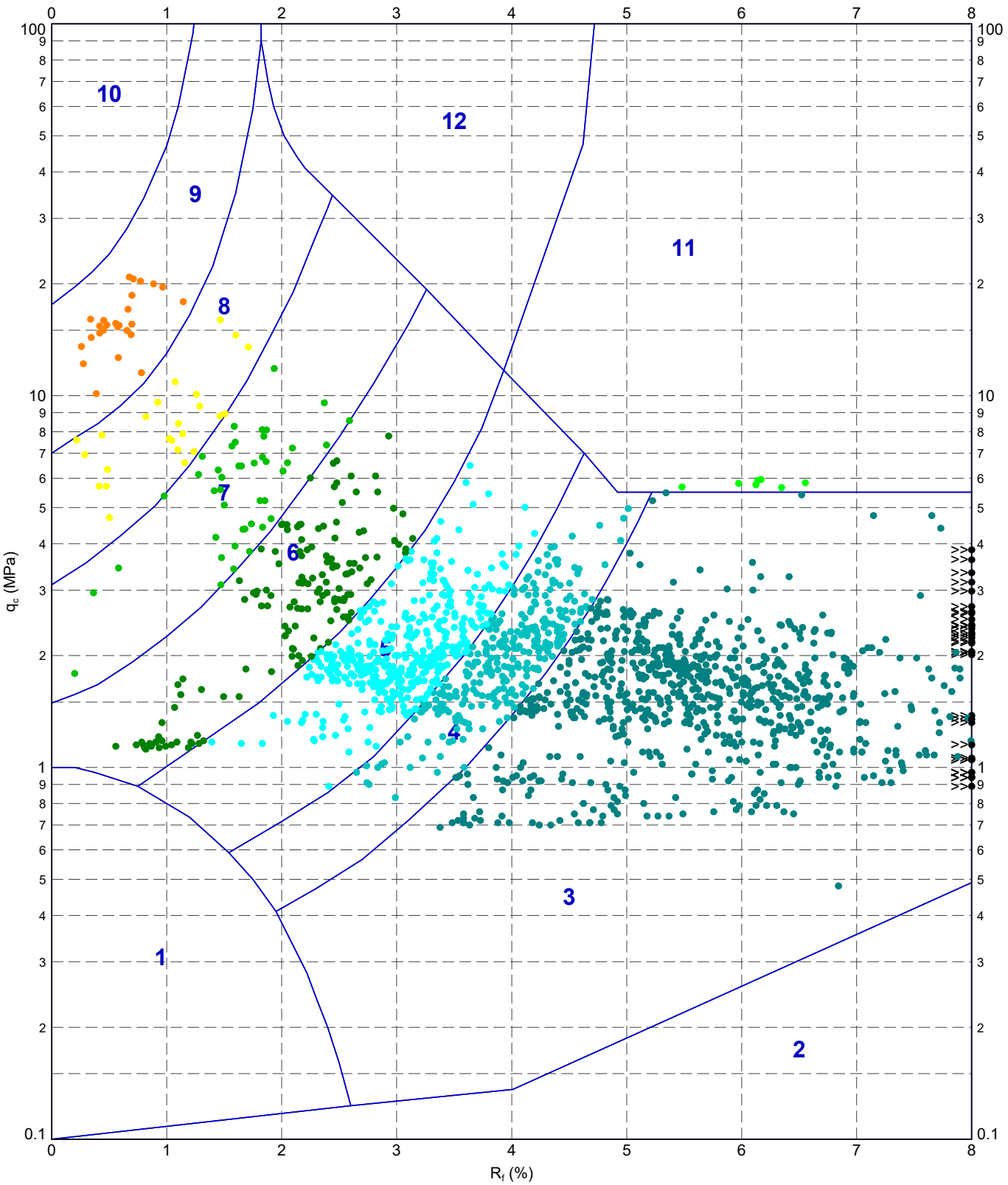
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**CPT12A**

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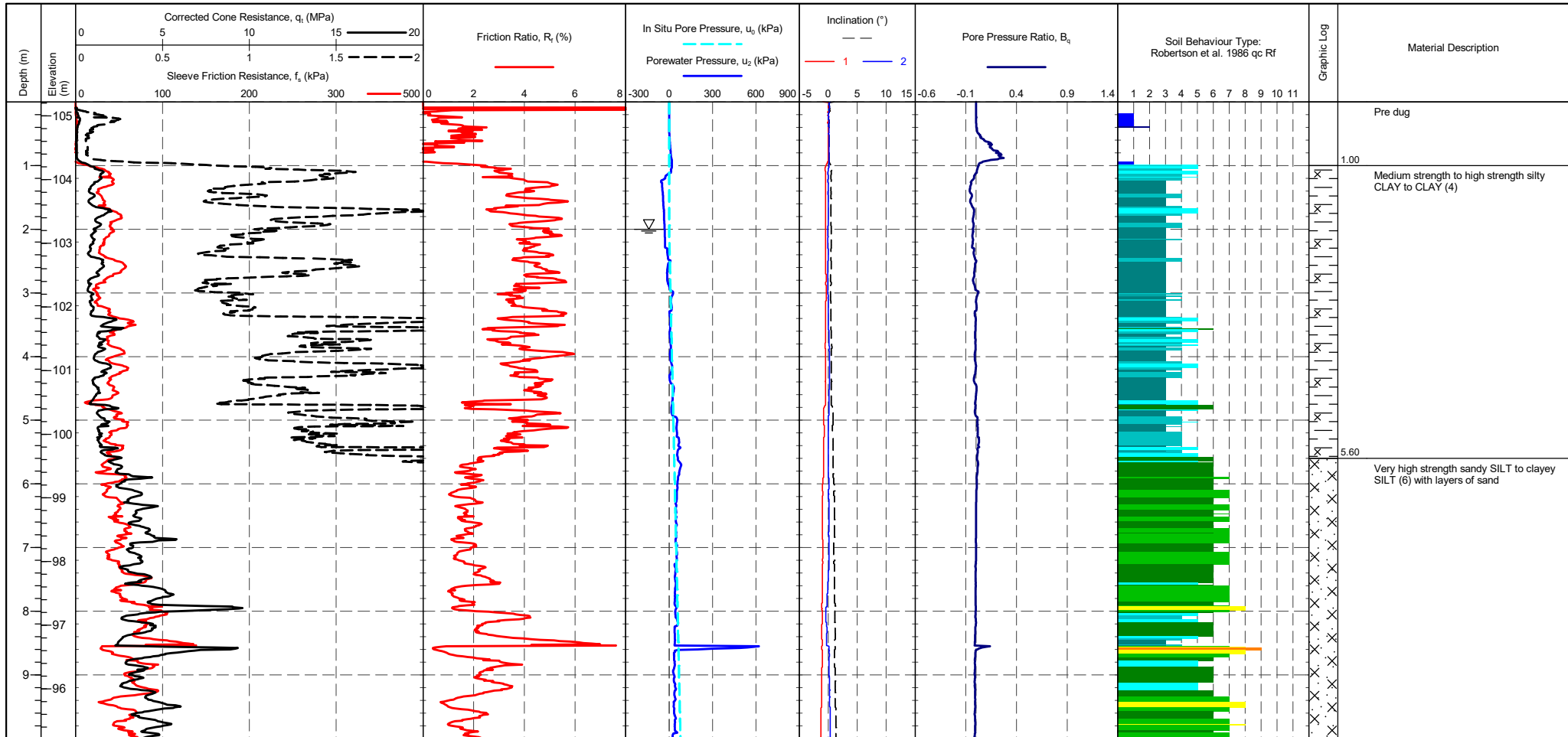
**METHOD: Robertson et al. 1986 qc Rf**

1 - Sensitive fine grained material	4 - Silty CLAY to CLAY	7 - Silty SAND to sandy SILT	10 - Gravelly SAND to SAND
2 - Organic material	5 - Clayey SILT to silty CLAY	8 - SAND to silty SAND	11 - Very stiff fine grained
3 - CLAY	6 - Sandy SILT to clayey SILT	9 - SAND	12 - SAND to clayey SAND

	TITLE	DRAWN	DATE
	Delta Simons Cordby Corby	CHECKED	DATE
	Robertson et al. 1986 qc vs. Rf - CPT12A	SCALE	Not To Scale
		PROJECT No 1220144	FIGURE No
			A4

PointID	<b>SCPT</b>
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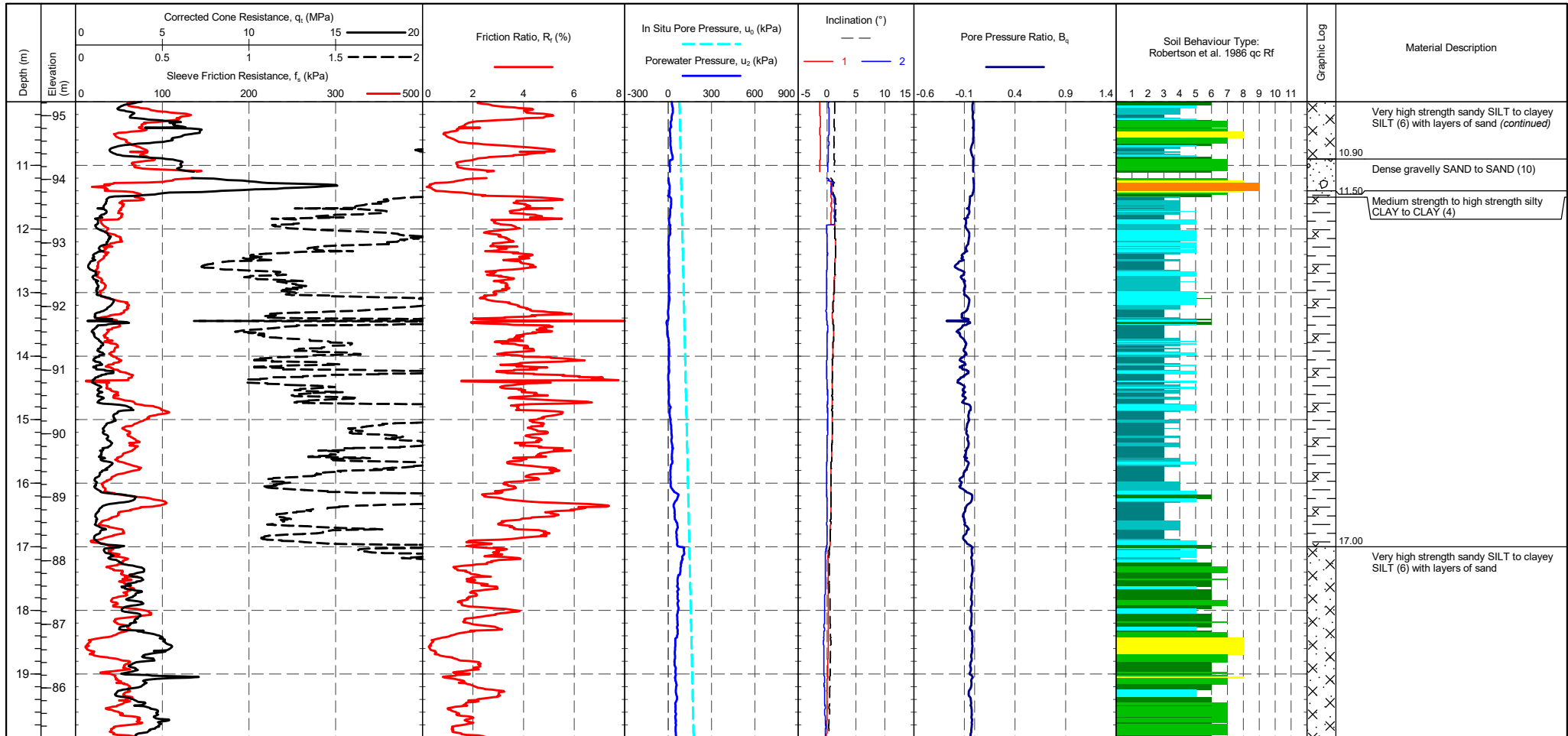
<b>CLIENT</b> : Delta Simons <b>PROJECT</b> : Corby LOCATION : Cordby PROJECT No. : 1220144	<b>EASTING</b> : 490984.811 m <b>NORTHING</b> : 290849.714 m <b>ELEVATION</b> : 105.220 m OD <b>CHECKED BY</b> : LD <b>TERMINATION REASON</b> : Refusal	<b>Remark:</b> Test refused on tip resistance.	<b>SHEET</b> : 1 OF 3 <b>STATUS</b> : Final <b>TEST DATE</b> : 11/02/2022 <b>PLOT DATE</b> : 04/03/2022 <b>METHOD</b> : ISO 22476-1:2012
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<b>CONE ID</b> : DP10-CFPTxy.60154 <b>CALIBRATION DATE</b> : 30/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 10cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.71 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Transducer</th> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>Tip (MPa)</td> <td>0.305</td> <td>0.321</td> <td>-0.016485</td> </tr> <tr> <td>Sleeve (kPa)</td> <td>0.0173</td> <td>0.0168</td> <td>0.000551</td> </tr> <tr> <td><math>u_2</math> (kPa)</td> <td>-0.00254</td> <td>0.0127</td> <td>-0.015223</td> </tr> <tr> <td>Inclinometer 1 (<math>^\circ</math>)</td> <td>-0.927</td> <td>0.440</td> <td>-1.366902</td> </tr> <tr> <td>Inclinometer 2 (<math>^\circ</math>)</td> <td>0.455</td> <td>-0.326</td> <td>0.781173</td> </tr> </table>	Transducer	Pre	Post	Difference	Tip (MPa)	0.305	0.321	-0.016485	Sleeve (kPa)	0.0173	0.0168	0.000551	$u_2$ (kPa)	-0.00254	0.0127	-0.015223	Inclinometer 1 ( $^\circ$ )	-0.927	0.440	-1.366902	Inclinometer 2 ( $^\circ$ )	0.455	-0.326	0.781173	<b>METHOD</b> : Robertson et al. 1986 qc Rf <table border="1"> <tr> <td>1 - Sensitive fine grained material</td> <td>5 - Clayey SILT to silty CLAY</td> <td>9 - SAND</td> </tr> <tr> <td>2 - Organic material</td> <td>6 - Sandy SILT to clayey SILT</td> <td>10 - Gravelly SAND to SAND</td> </tr> <tr> <td>3 - CLAY</td> <td>7 - Silty SAND to sandy SILT</td> <td>11 - Very stiff fine grained</td> </tr> <tr> <td>4 - Silty CLAY to CLAY</td> <td>8 - SAND to silty SAND</td> <td>12 - SAND to clayey SAND</td> </tr> </table>	1 - Sensitive fine grained material	5 - Clayey SILT to silty CLAY	9 - SAND	2 - Organic material	6 - Sandy SILT to clayey SILT	10 - Gravelly SAND to SAND	3 - CLAY	7 - Silty SAND to sandy SILT	11 - Very stiff fine grained	4 - Silty CLAY to CLAY	8 - SAND to silty SAND	12 - SAND to clayey SAND	Groundwater Level  Dissipation Test
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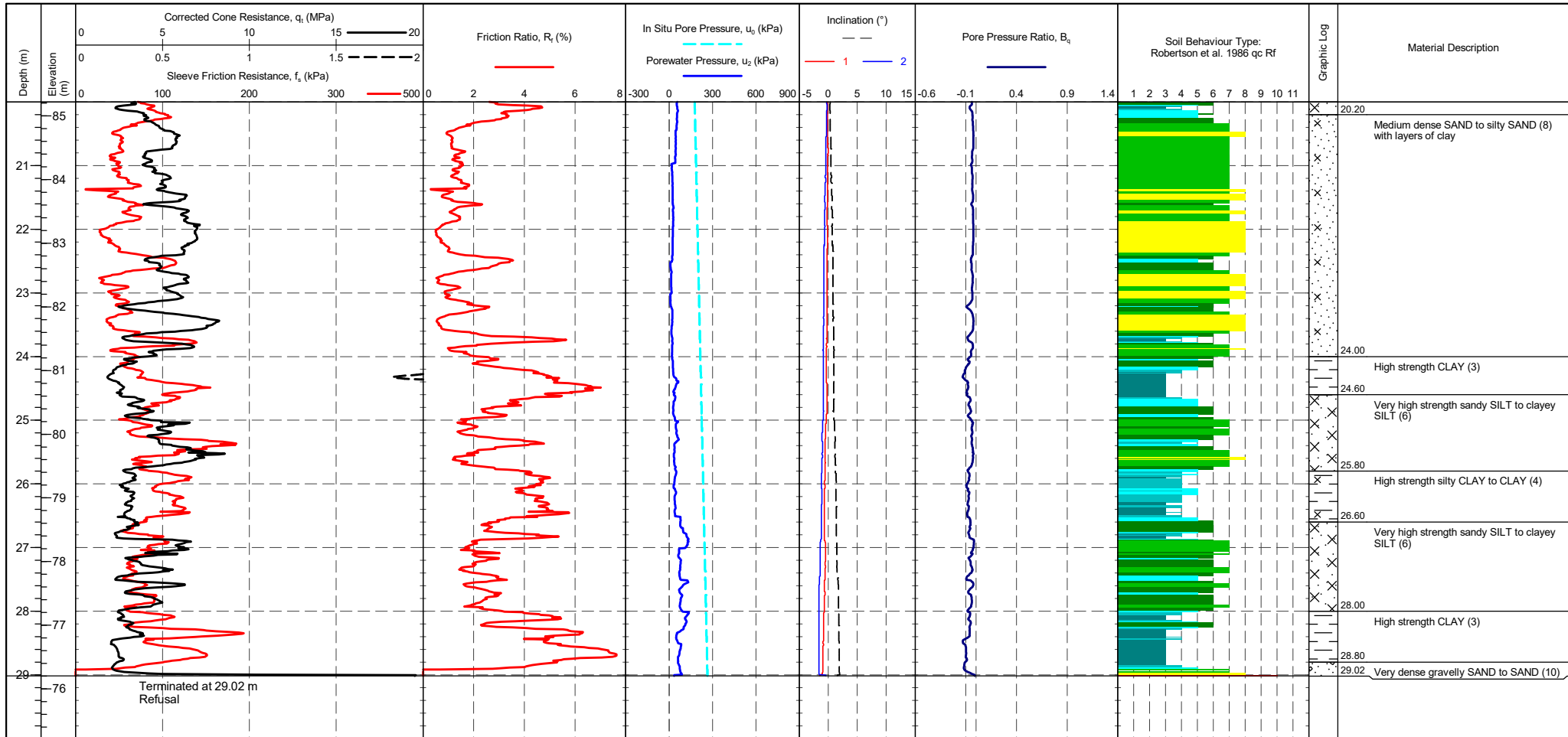


<b>CONE ID</b> : DP10-CFPTxy.60154 <b>CALIBRATION DATE</b> : 30/03/2021 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 10cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.71 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICITION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot <b>GROUNDWATER DEPTH</b> : Assumed for calculation purposes	<b>CPT ZERO VALUES</b> Transducer Pre Post Difference Tip (MPa) 0.305 0.321 -0.016485 Sleeve (kPa) 0.0173 0.0168 0.000551 u2 (kPa) -0.00254 0.0127 -0.015223 Inclinator 1 ( $^\circ$ ) -0.927 0.440 -1.366902 Inclinator 2 ( $^\circ$ ) 0.455 -0.326 0.781173	<b>METHOD</b> : Robertson et al. 1986 qc Rf 1 - Sensitive fine grained material 2 - Organic material 3 - CLAY 4 - Silty CLAY to CLAY 5 - Clayey SILT to silty CLAY 6 - Sandy SILT to clayey SILT 7 - Silty SAND to sandy SILT 8 - SAND to silty SAND 9 - SAND 10 - Gravelly SAND to SAND 11 - Very stiff fine grained 12 - SAND to clayey SAND	Groundwater Level Dissipation Test
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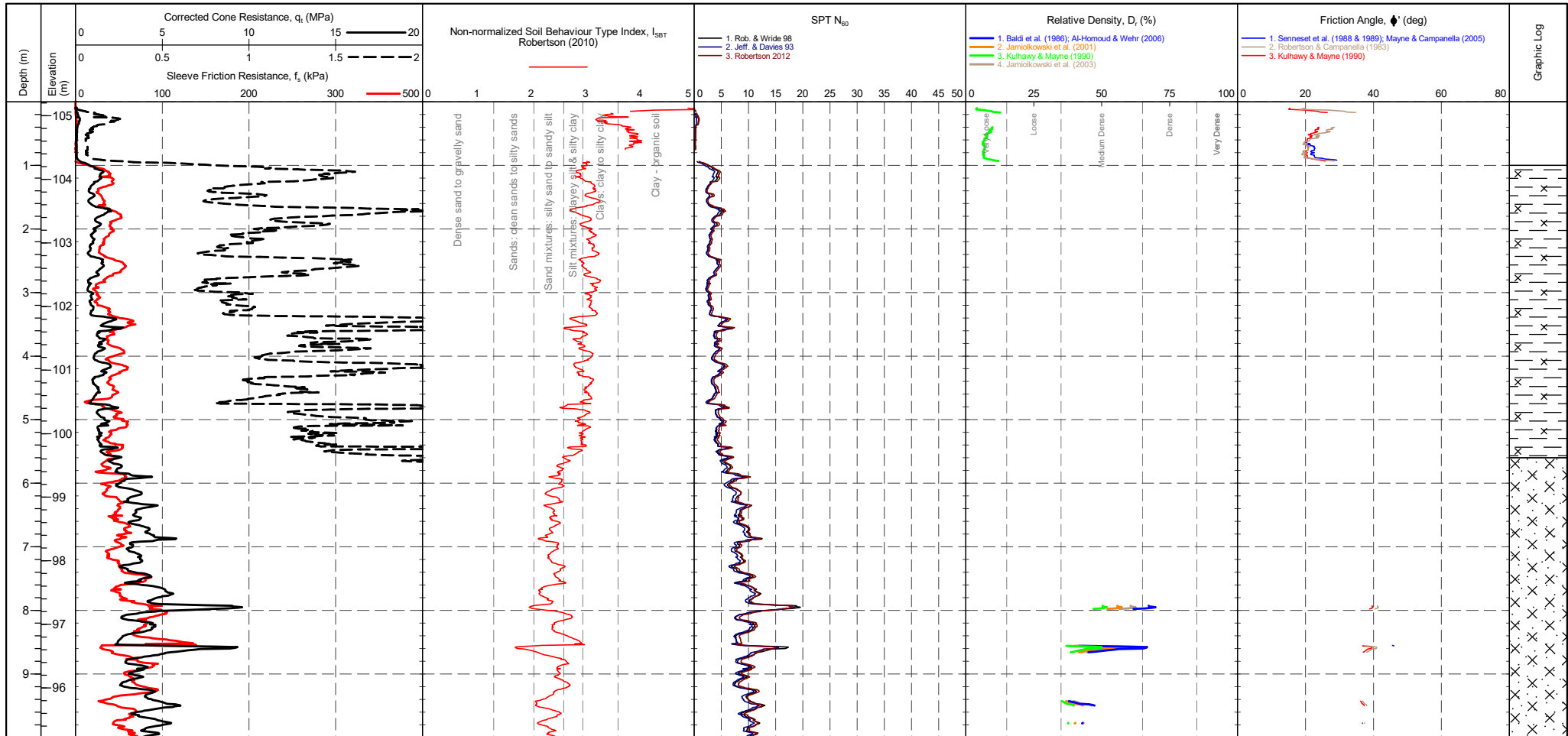
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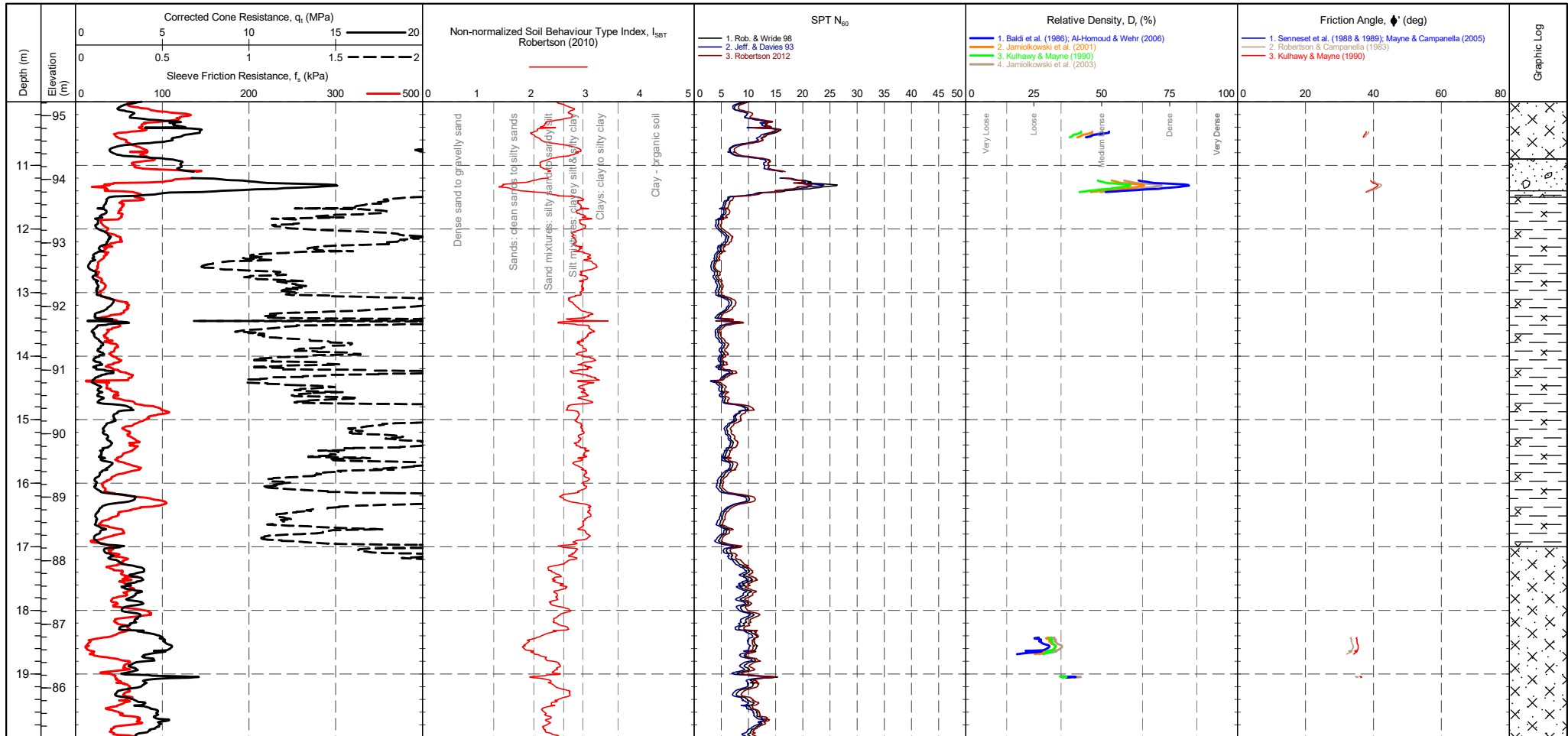
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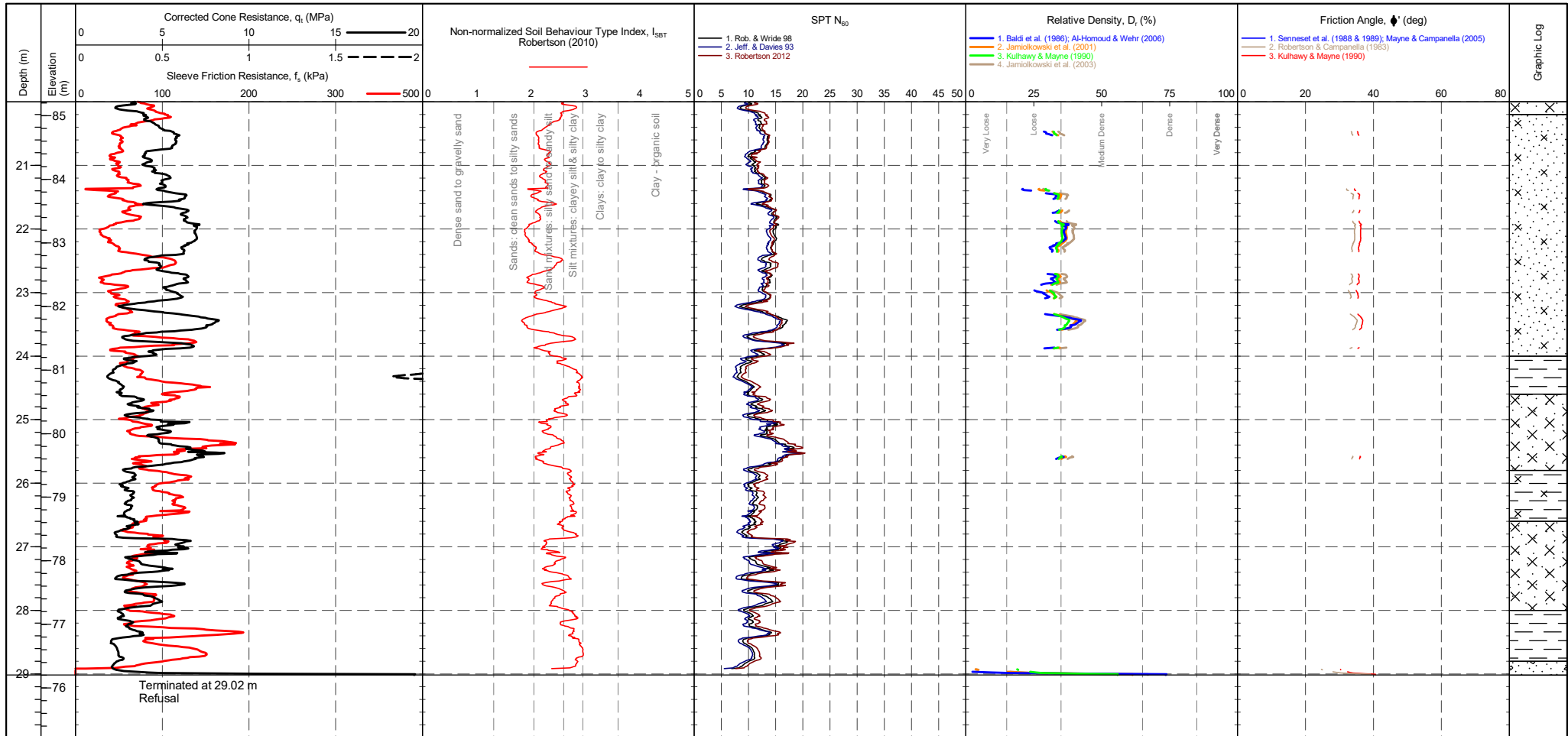
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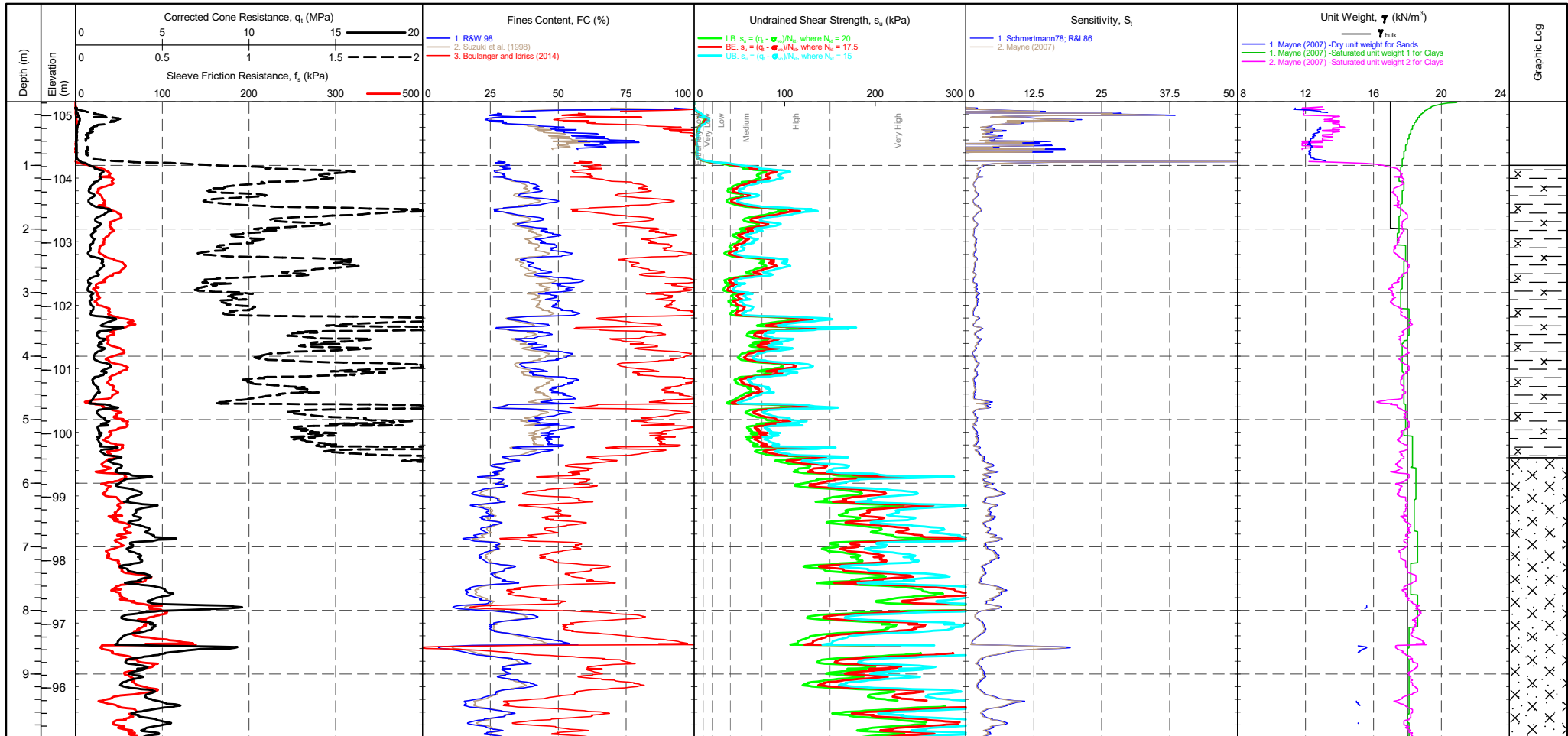
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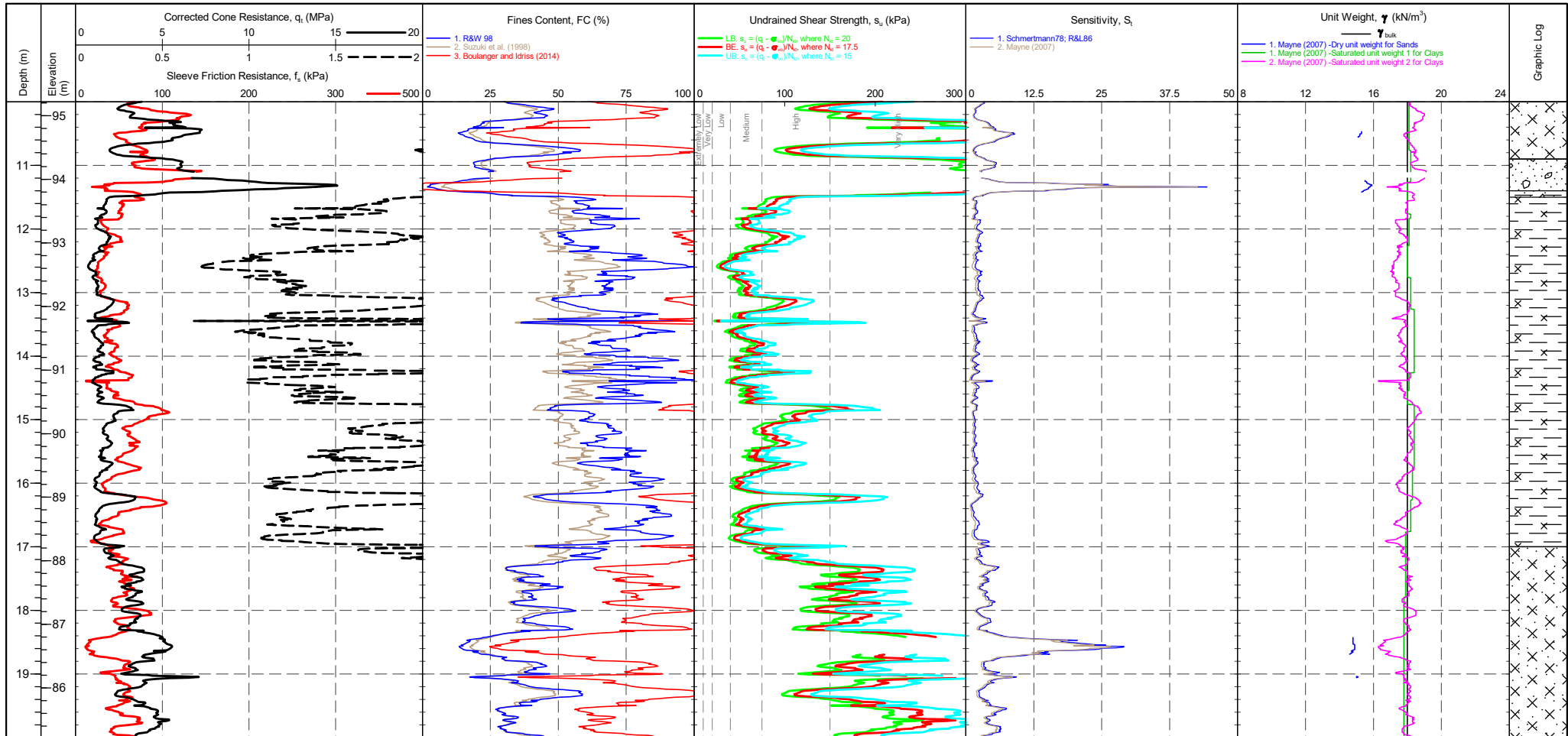
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<b>CONE ID</b> : DP10-CFPTxy.60154 <b>CONE MODEL</b> : Subtraction <b>CONE AREA</b> : 10cm <sup>2</sup> <b>CONE AREA RATIO</b> : 0.71 <b>FILTER POSITION</b> : u2 <b>FILTER TYPE</b> : HDPE	<b>TEST TYPE</b> : TE2 <b>APPLICATION CLASS</b> : 2 <b>RIG</b> : CPT 016 - Broomhall <b>OPERATOR</b> : TR <b>FRICION REDUCER</b> : None <b>WEATHER</b> : Sunny & Hot	<b>Transducer</b> <b>Tip (MPa)</b> <b>Sleeve (kPa)</b> <b>u2 (kPa)</b> <b>Inclinometer 1 (°)</b> <b>Inclinometer 2 (°)</b>	<b>CPTU ZERO VALUES</b> <table border="1"> <tr> <th>Pre</th> <th>Post</th> <th>Difference</th> </tr> <tr> <td>0.305</td> <td>0.321</td> <td>-0.016485</td> </tr> <tr> <td>0.0173</td> <td>0.0168</td> <td>0.000551</td> </tr> <tr> <td>-0.00254</td> <td>0.0127</td> <td>-0.015223</td> </tr> <tr> <td>-0.927</td> <td>0.440</td> <td>-1.366902</td> </tr> <tr> <td>0.455</td> <td>-0.326</td> <td>0.781173</td> </tr> </table>	Pre	Post	Difference	0.305	0.321	-0.016485	0.0173	0.0168	0.000551	-0.00254	0.0127	-0.015223	-0.927	0.440	-1.366902	0.455	-0.326	0.781173	<b>COHESIVE SOILS (Clays &amp; Silts) Robertson et al. 1986 Zones 1-6 and Zone 11</b> <table border="1"> <tr> <th>Term based on measurement</th> <th>su (kPa)</th> <th>Term based on measurement</th> <th>su (kPa)</th> </tr> <tr> <td>Extremely low strength</td> <td>&lt;10</td> <td>Medium strength</td> <td>40-75</td> </tr> <tr> <td>Very low strength</td> <td>10-20</td> <td>High strength</td> <td>75-150</td> </tr> <tr> <td>Low strength</td> <td>20-40</td> <td>Very high strength</td> <td>150-300</td> </tr> <tr> <td></td> <td></td> <td>Extremely high strength</td> <td>&gt;300</td> </tr> </table>	Term based on measurement	su (kPa)	Term based on measurement	su (kPa)	Extremely low strength	<10	Medium strength	40-75	Very low strength	10-20	High strength	75-150	Low strength	20-40	Very high strength	150-300			Extremely high strength	>300	<b>Groundwater Level</b>  <b>Dissipation Test</b> 
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PointID	<b>SCPT</b>
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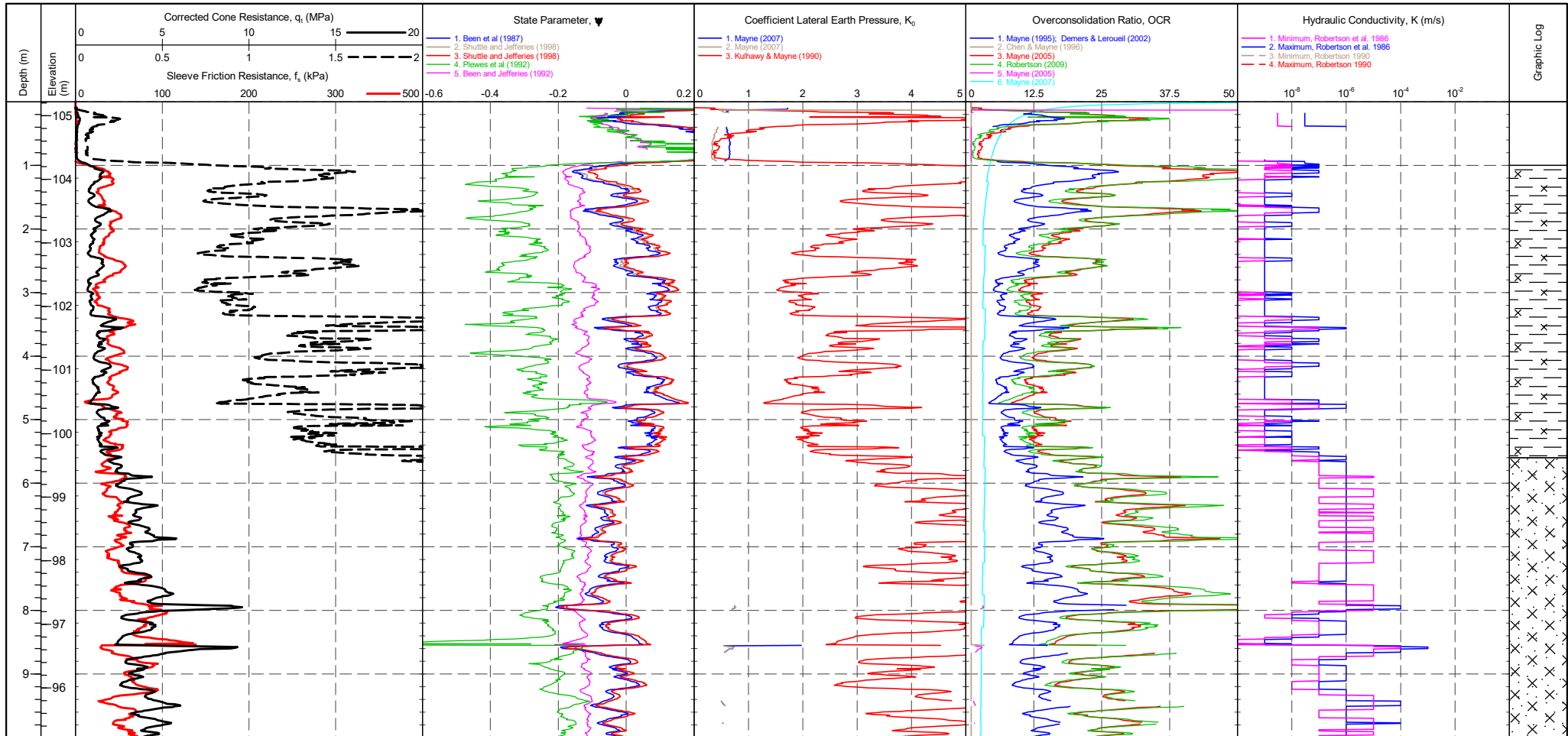






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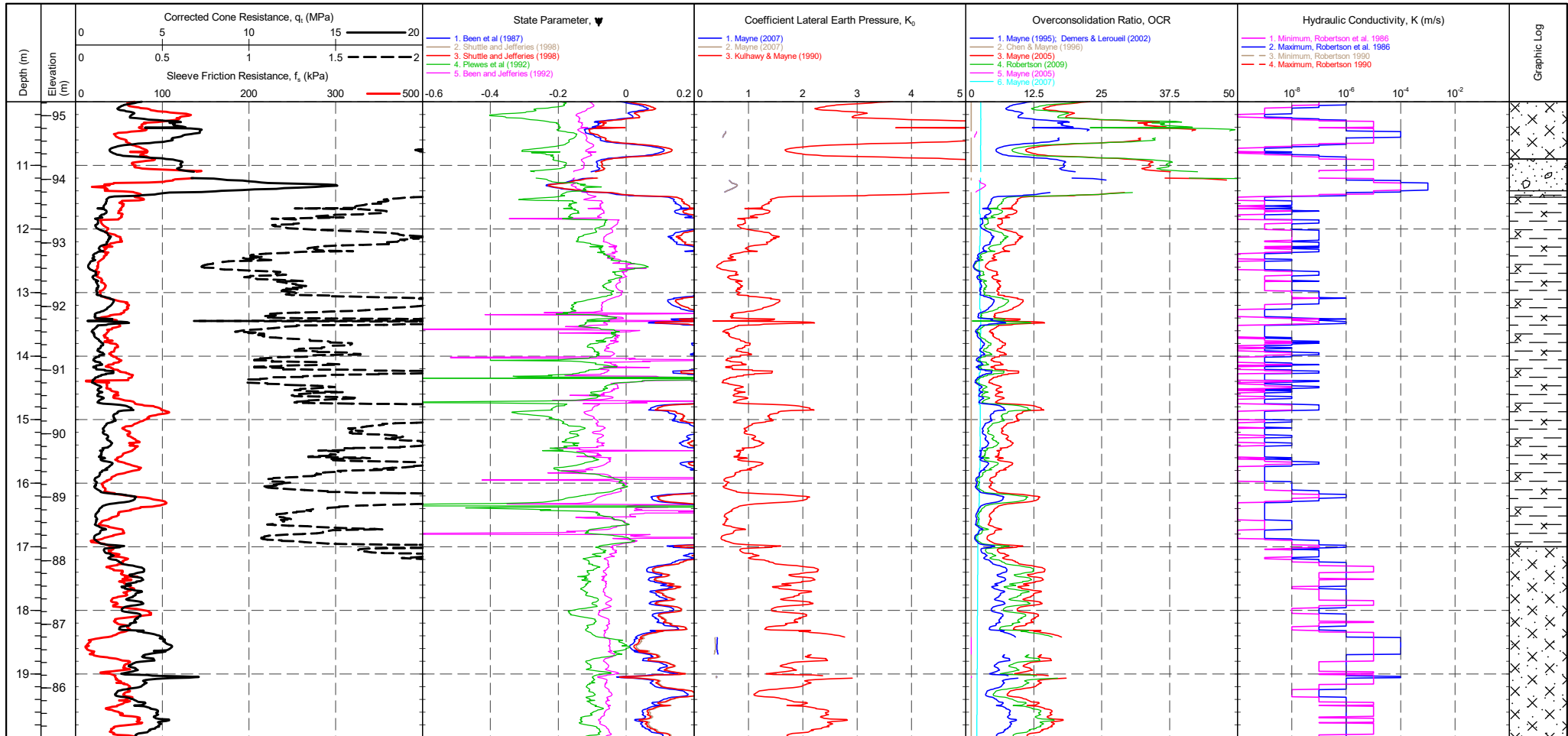
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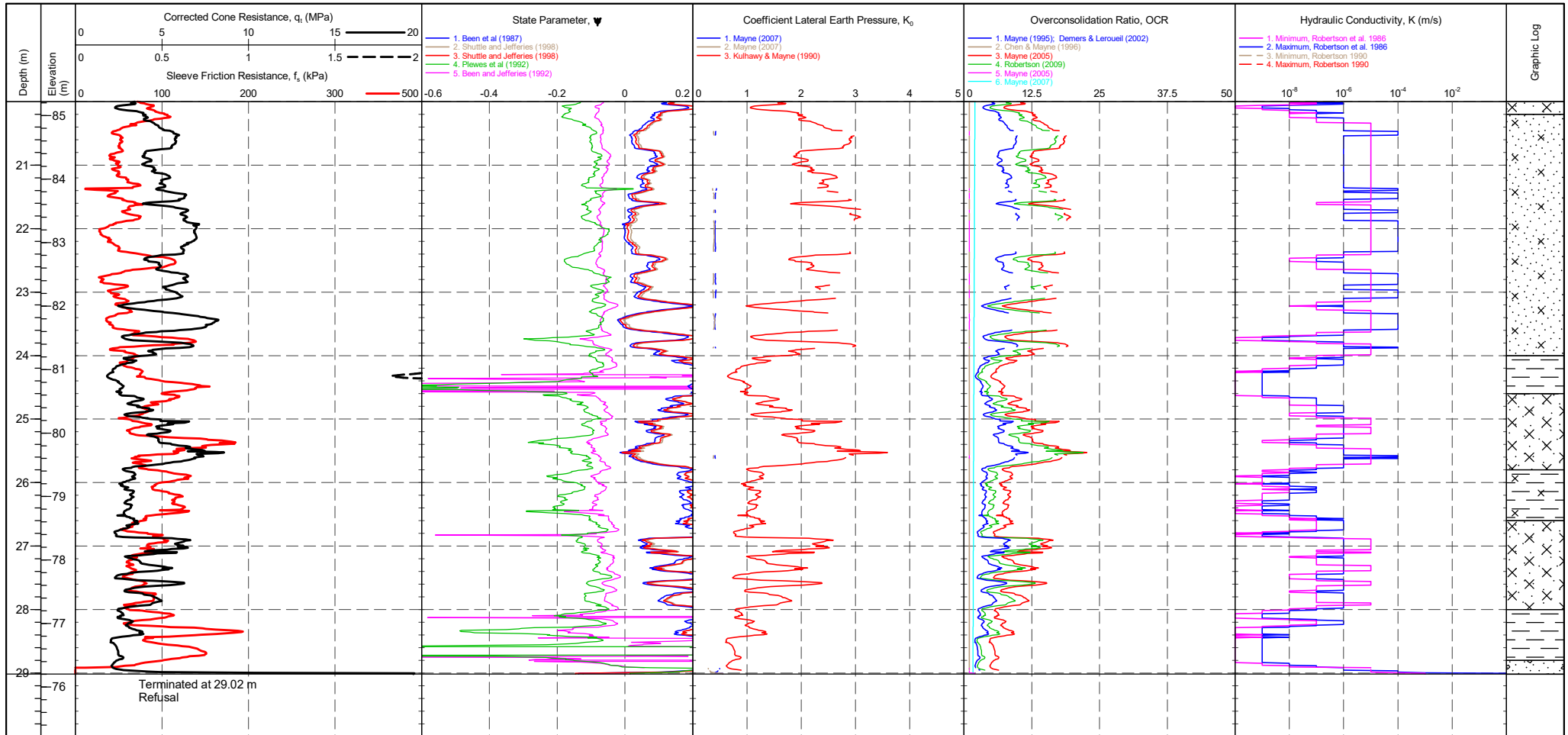


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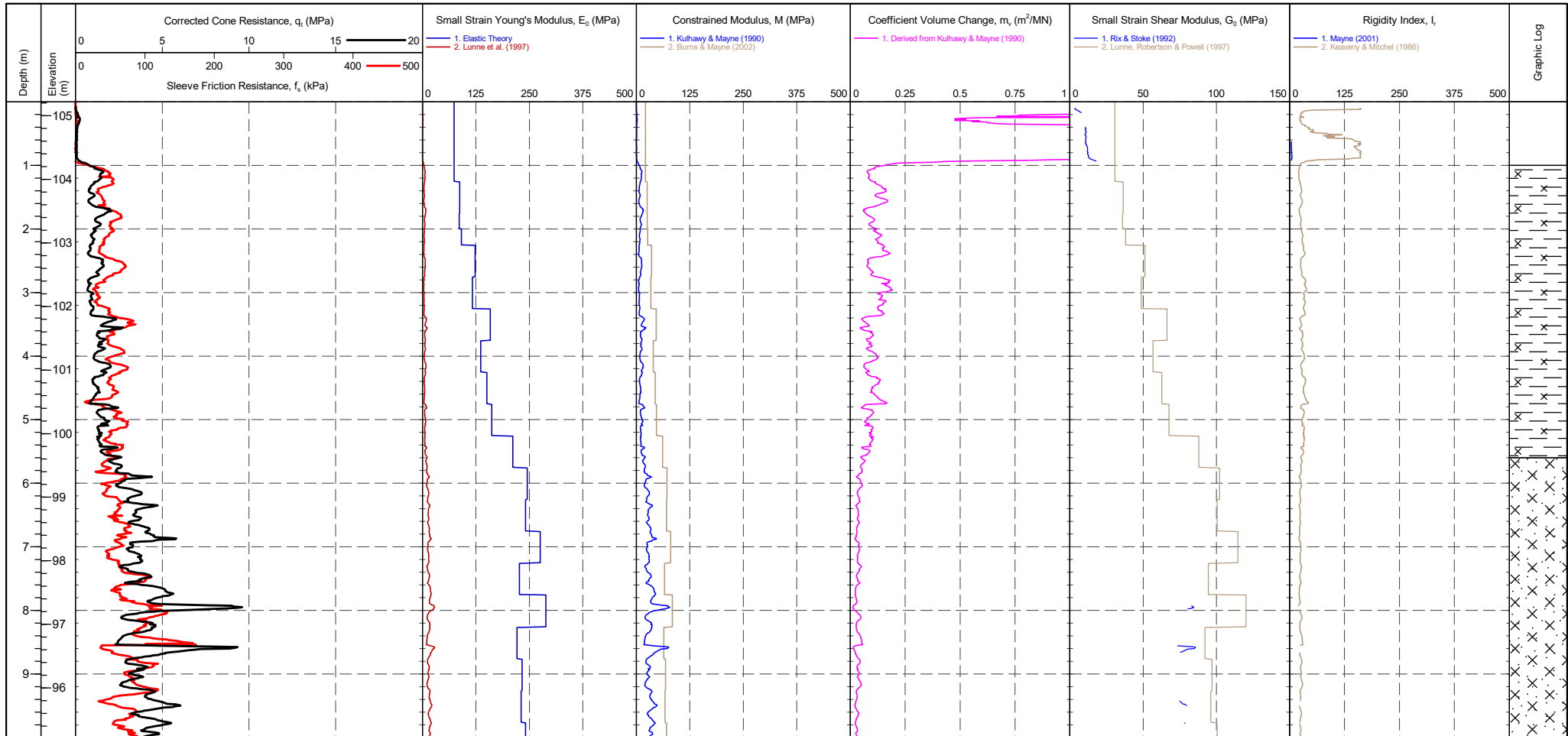
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**SCPT**

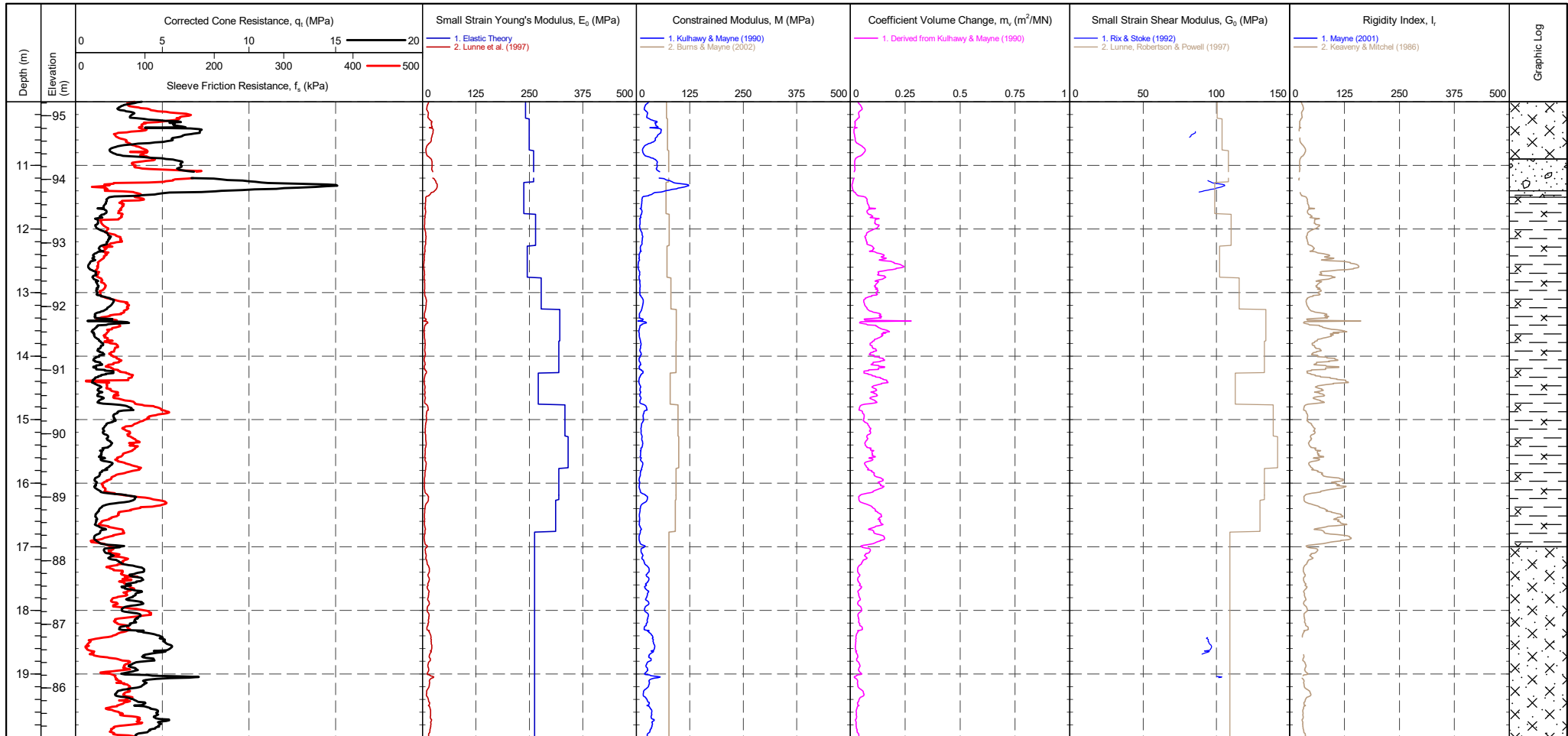
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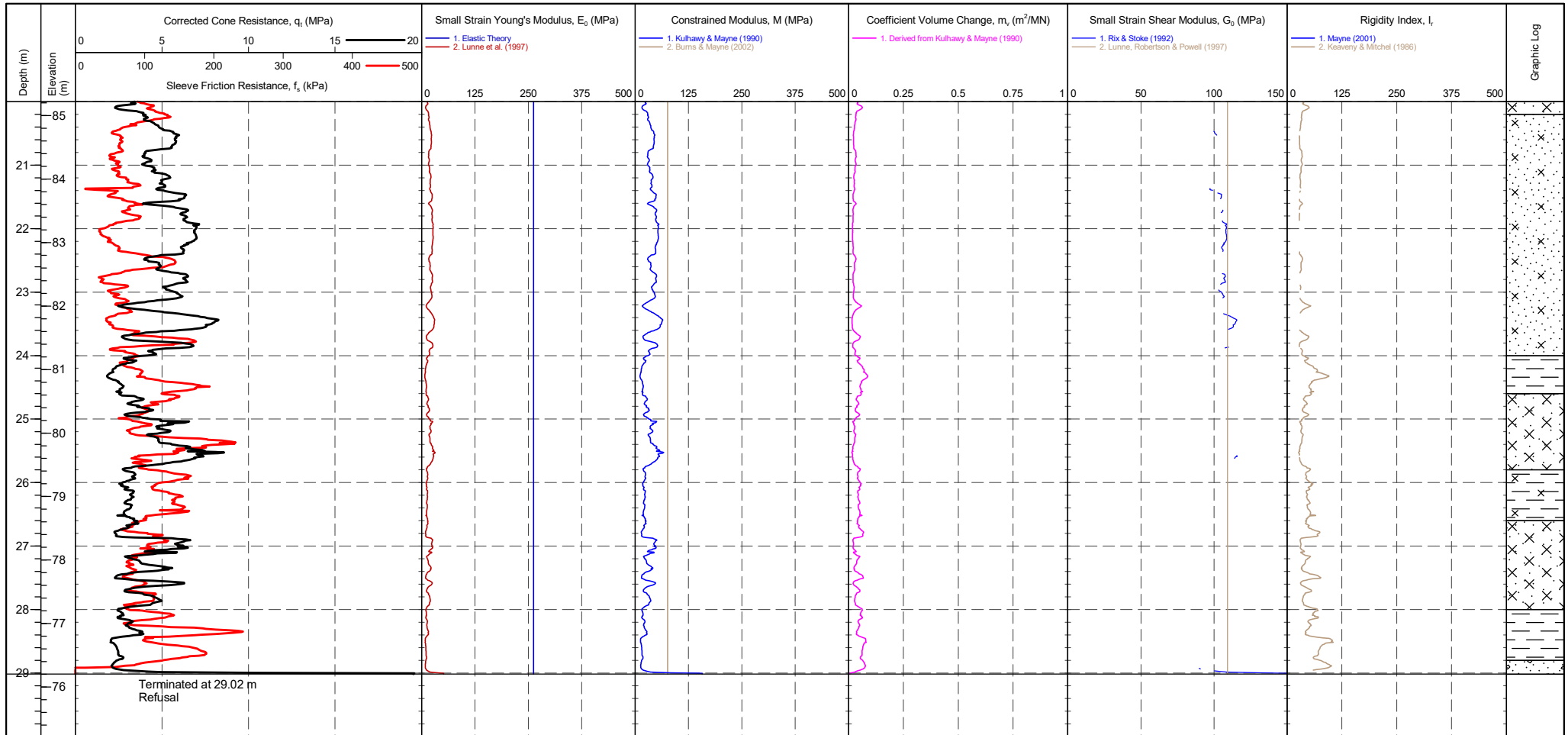


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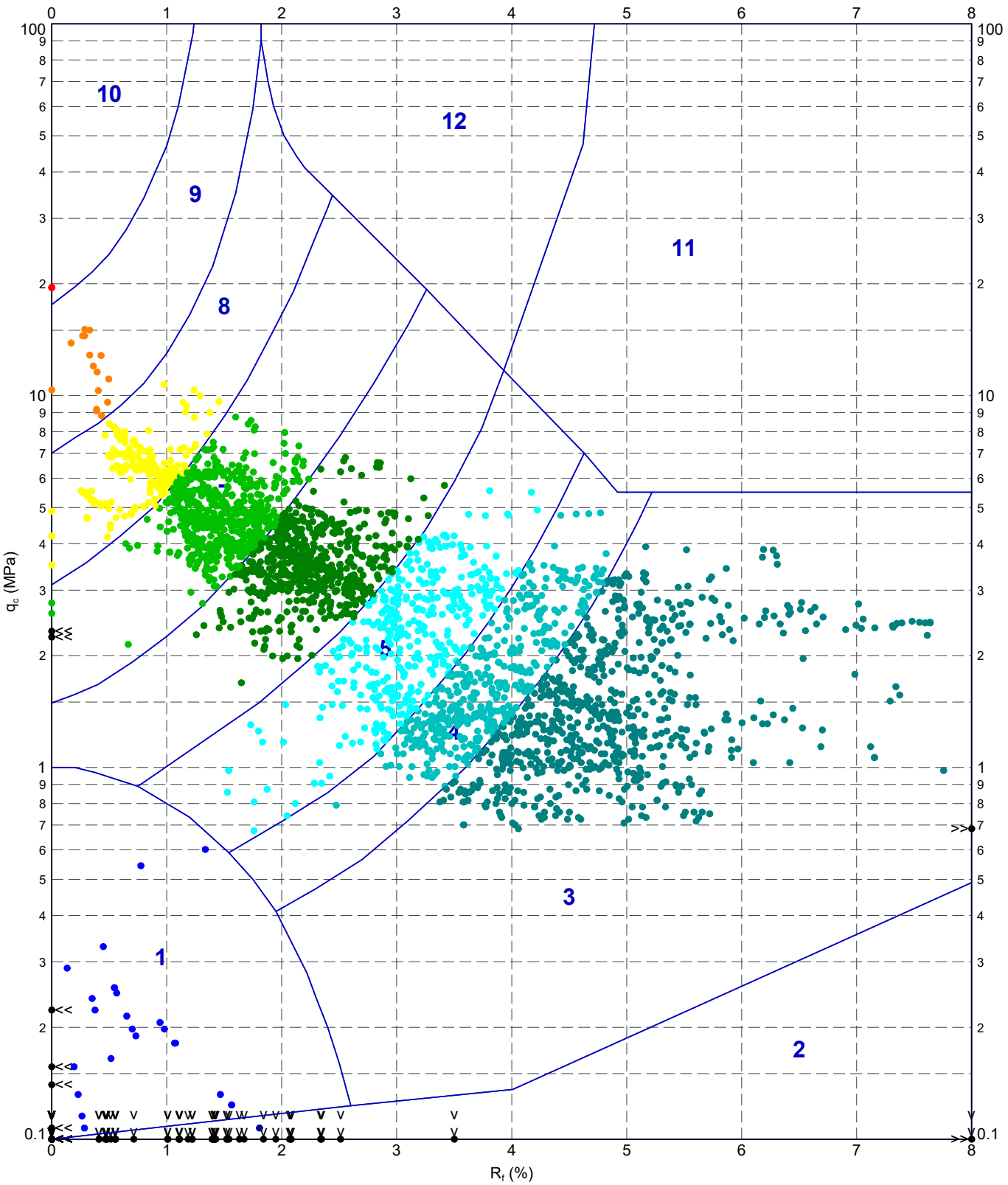
SCPT

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220228-ADVANCED REPORT INSTITUSI 2.02.1 LUB - CHLOE.GLB Graph CPT ROBERTSON ET AL. 8F QC VS. RF APF 1220144 CORBY DELTA SIMONS.GPJ -<<DrawingFile>> 04/03/2022 19:59 10.01.00.11 Datagel Lab and In Situ Tool - DGD [Lib: In Situ SI 2.02.0 2017-07-10 Proj: In Situ SI 2.02.0 2017-07-10



METHOD: Robertson et al. 1986 qc Rf

- 1 - Sensitive fine grained material
- 4 - Silty CLAY to CLAY
- 7 - Silty SAND to sandy SILT
- 10 - Gravelly SAND to SAND
- 2 - Organic material
- 5 - Clayey SILT to silty CLAY
- 8 - SAND to silty SAND
- 11 - Very stiff fine grained
- 3 - CLAY
- 6 - Sandy SILT to clayey SILT
- 9 - SAND
- 12 - SAND to clayey SAND

	TITLE	DRAWN	DATE
	Delta Simons Cordby Corby		04/03/2022
	Robertson et al. 1986 qc vs. Rf - SCPT	CHECKED	DATE
			04/03/2022
		SCALE	FIGURE No
		Not To Scale	A4
		PROJECT No	FIGURE No
		1220144	



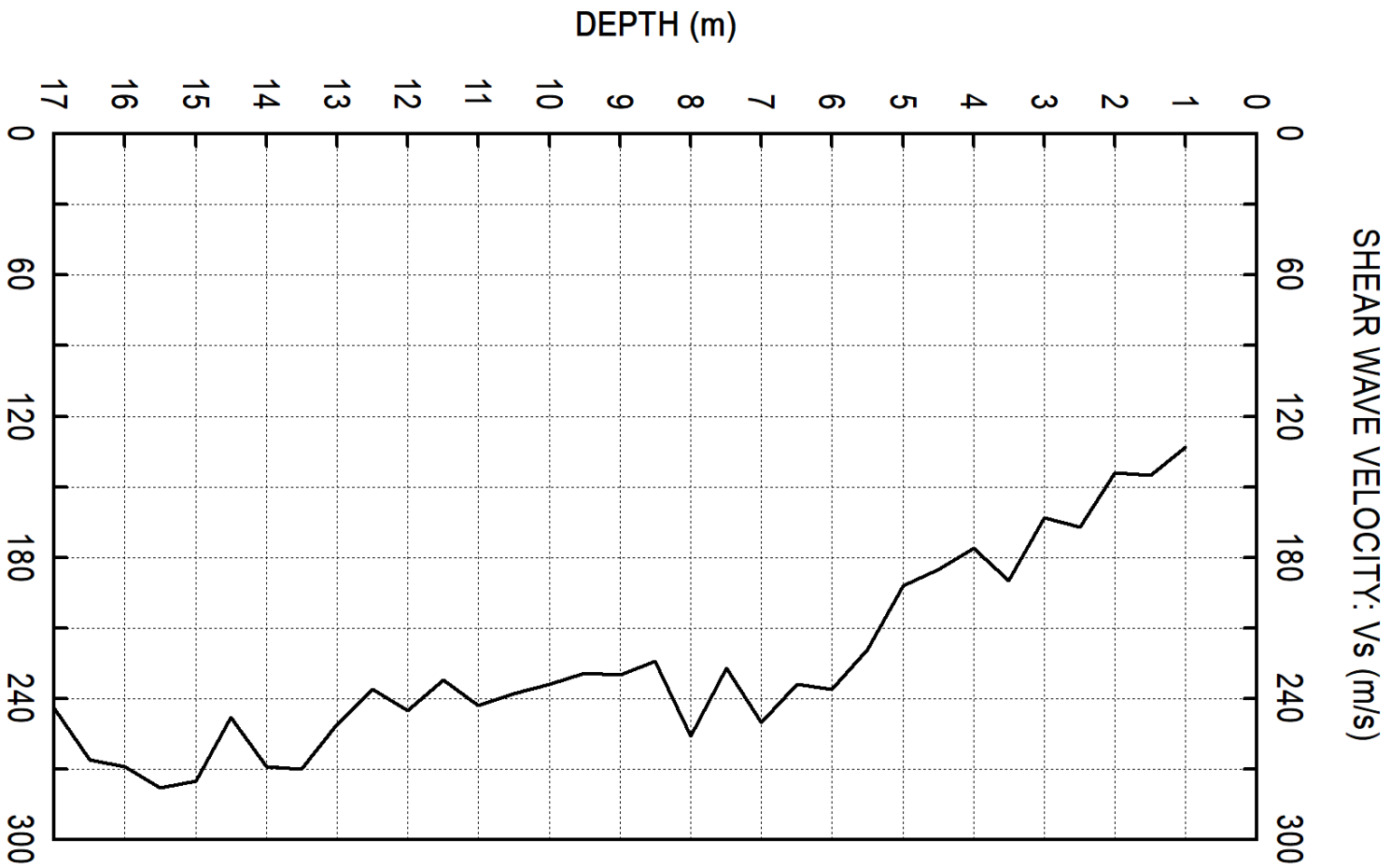
## APPENDIX C

### Seismic Dilatometer Marchetti (SDMT) Measurements

In Situ SI  
1220144-Corby

Delta Simons  
Corby

TEST  
**SCPT 01**  
11 FEB 2022



SCPT 01 - Tabular data: Vs, Go, Vs Repeatability

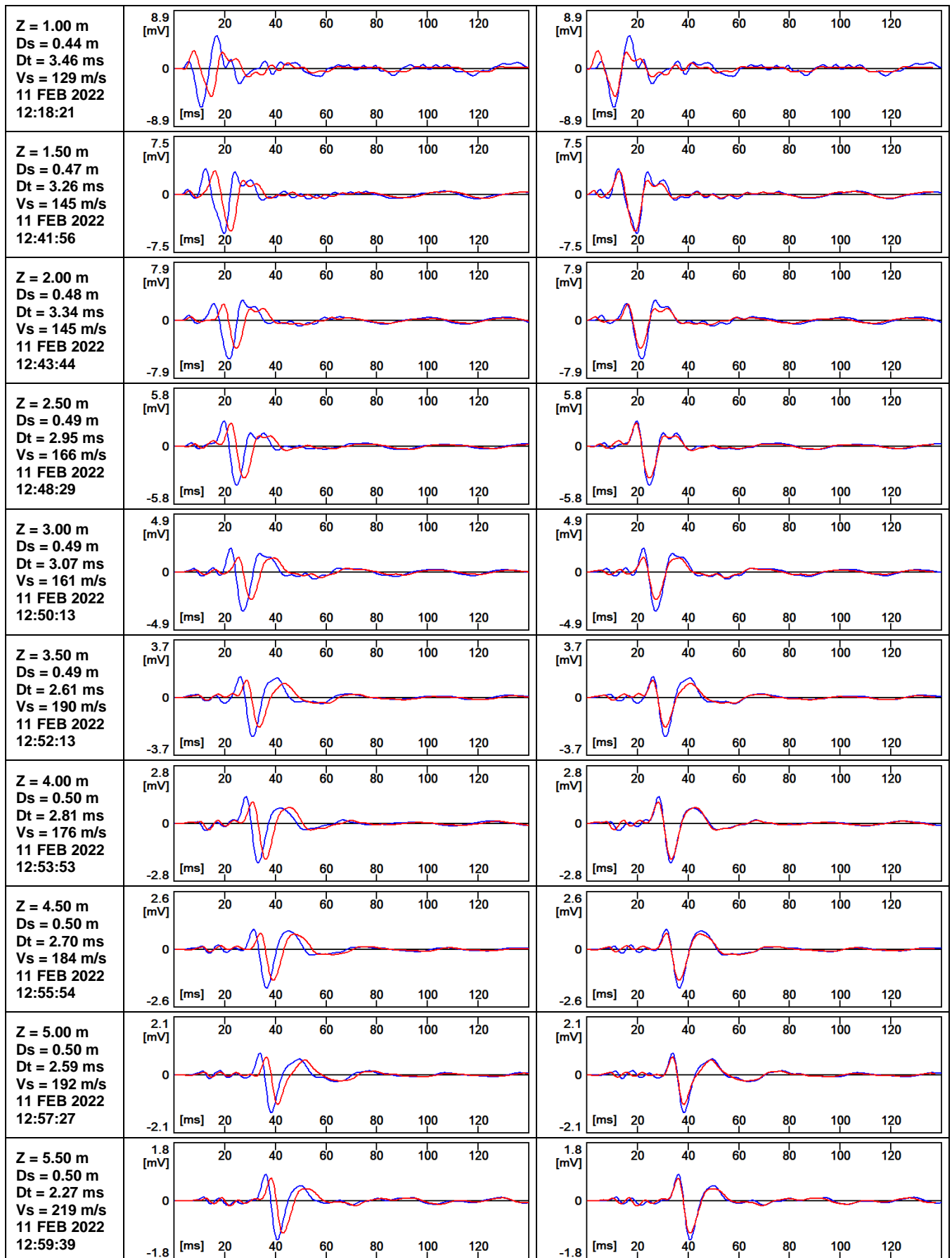
Each Vs value in the 'Vs Repeatability' column corresponds to a distinct energization.

Z	Vs	Go	Rho	Vs Repeatability	Var Coeff.
[m]	[m/s]	[MPa]	[kg/m <sup>3</sup> ]	[m/s]	[%]
1.00	133	30.7	1733	129,130,139	4.15
1.50	145	36.4	1733	145,144,147	1.09
2.00	144	35.9	1733	145,143,144	0.69
2.50	167	48.3	1733	166,169,166	1.04
3.00	163	46.0	1733	161,162,166	1.62
3.50	190	62.6	1733	190,187,192	1.34
4.00	176	53.7	1733	176,175	0.57
4.50	185	59.3	1733	184,185,187	0.85
5.00	192	63.9	1733	192,190,193	0.82
5.50	219	83.1	1733	219,216,222	1.37
6.00	236	96.5	1733	238,236,233	1.08
6.50	234	94.9	1733	234,234,233	0.30
7.00	250	108	1733	250,248,251	0.63
7.50	227	89.3	1733	229,226,225	0.93
8.00	256	114	1733	255,255,257	0.48
8.50	224	87.0	1733	223,226,223	0.77
9.00	230	91.7	1733	228,233,228	1.27
9.50	229	90.9	1733	230,229,228	0.44
10.00	234	94.9	1733	237,234,230	1.51
10.50	238	98.2	1733	236,239,239	0.73
11.00	243	102	1733	243,246,241	1.05
11.50	232	93.3	1733	233,229,234	1.14
12.00	245	104	1733	246,243,247	0.87
12.50	236	96.5	1733	236,237,234	0.67
13.00	251	109	1733	252,252,250	0.49
13.50	270	126	1733	268,271,270	0.59
14.00	269	125	1733	273,264,271	1.76
14.50	248	107	1733	250,246,249	0.86
15.00	275	131	1733	281,272,273	1.80
15.50	278	134	1733	278,283,272	1.99
16.00	269	125	1733	265,277,266	2.48
16.50	266	123	1733	263,262,273	2.29
17.00	244	103	1733	246,246,241	1.19

# SCPT 01 - Vs

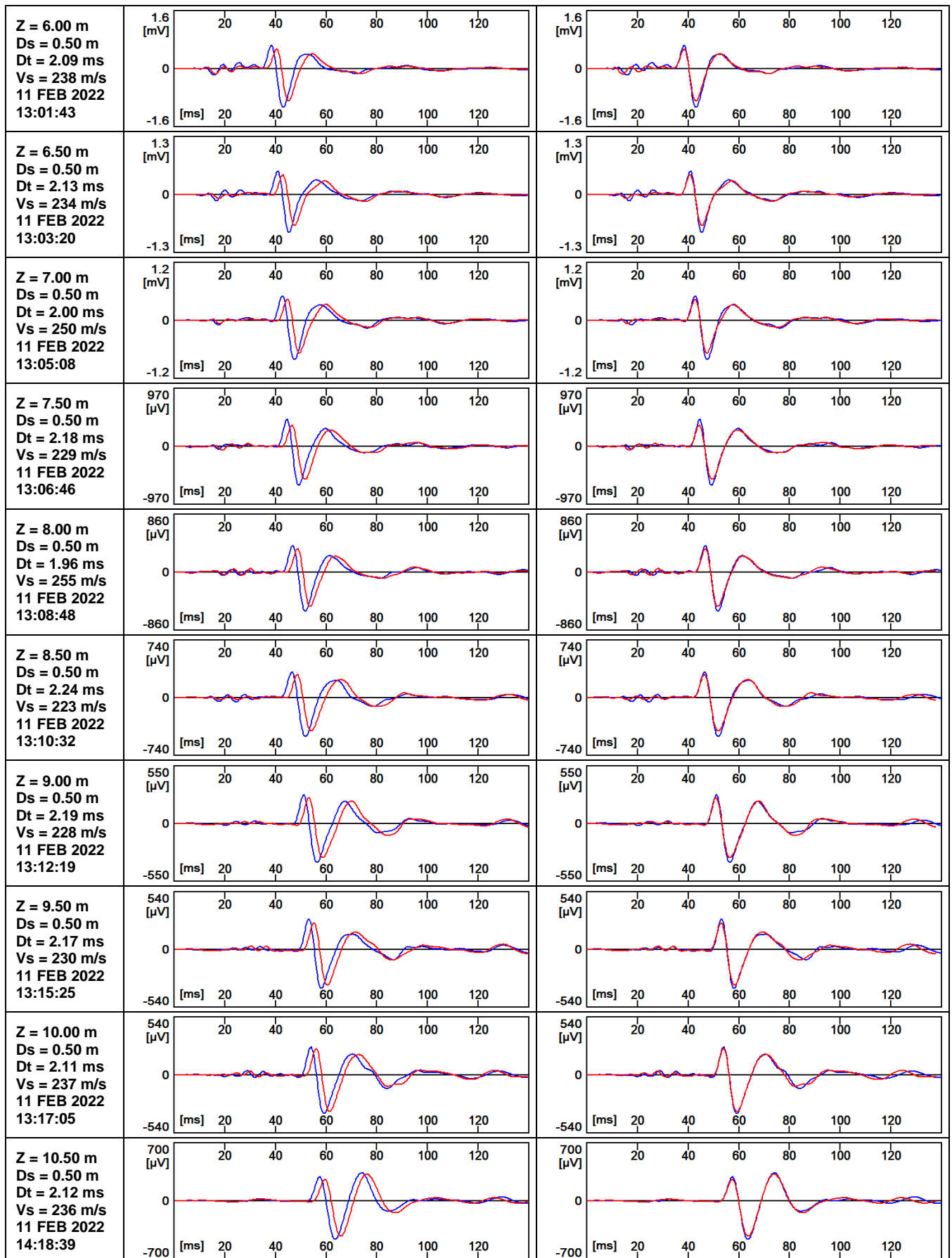
## RECORDED

## RE-PHASED



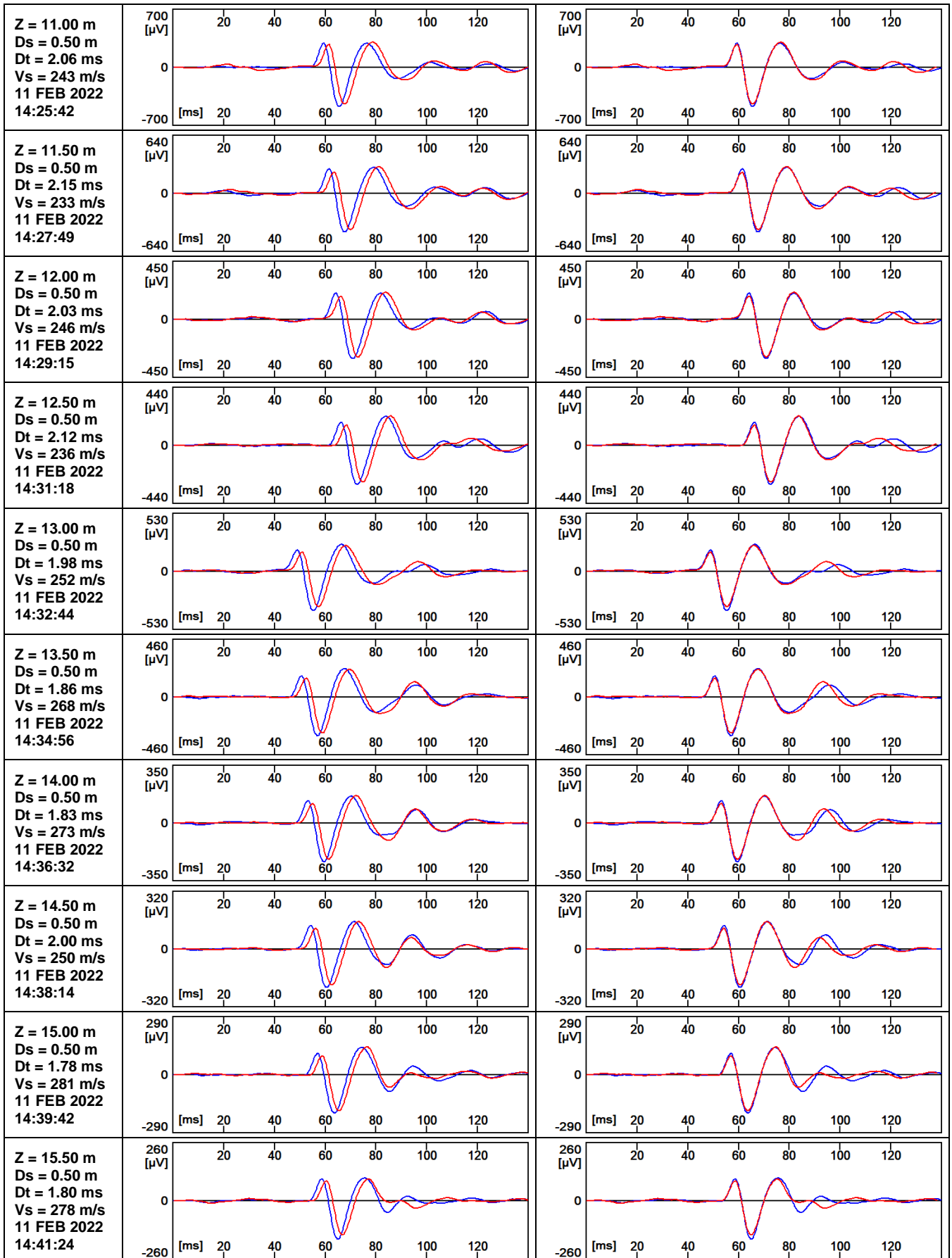
RECORDED

RE-PHASED



RECORDED

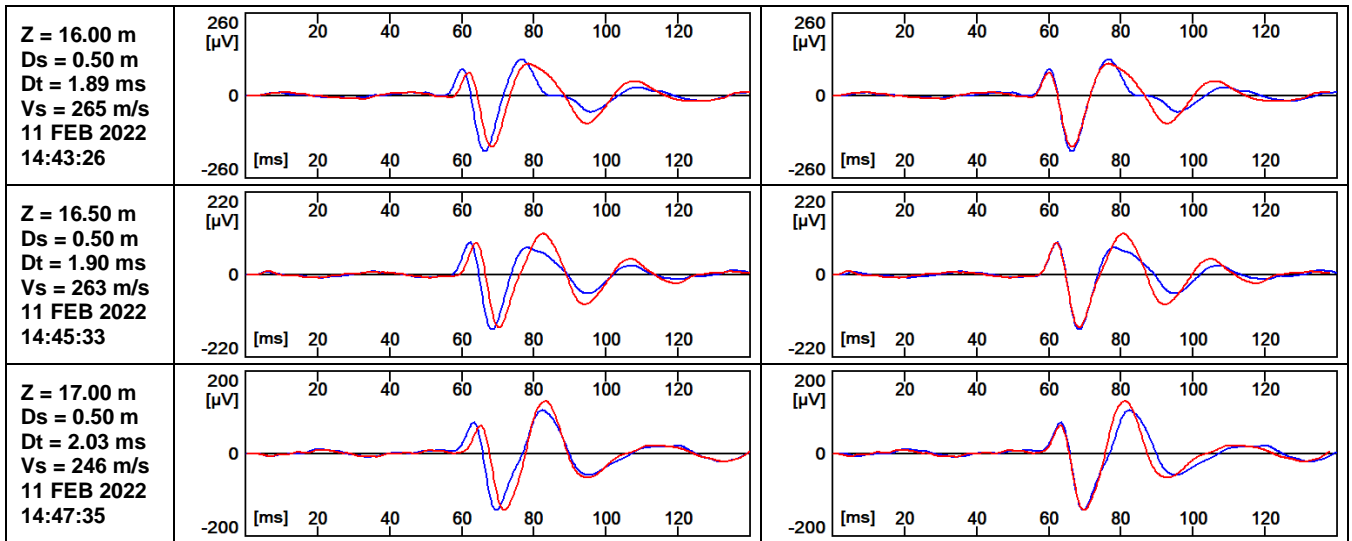
RE-PHASED



# SCPT 01 - Vs

## RECORDED

## RE-PHASED







*IN SITU SITE INVESTIGATION*

Unit 23 Hastings Innovation  
Centre,  
Highfield Drive  
St. Leonards on Sea, East Sussex,  
TN38 9UH, U.K.

Company No.: 6339499  
VAT No.: 922 3561 41

## Appendix D - Geophysical Survey Report

---

# GEOPHYSICAL SURVEY REPORT

Project

## Soil Resistivity Survey

Location

## Corby

Client

## DeltaSimons

---

Head Office  
Unit 1  
Link Trade Park  
Penarth Road  
Cardiff CF11 8TQ  
United Kingdom



down to earth **geophysics**

Telephone: +44 (0)2920 700127  
[www.terradat.co.uk](http://www.terradat.co.uk)

---

Job reference: 7823  
Date: February 2022  
Version: 1

---

# GEOPHYSICAL SURVEY REPORT

Project

## Soil Resistivity Survey

Location

## Corby

Client

## DeltaSimons

**Project Geophysicist:** R Stevens MEdSci (Int) FGS



**Reviewer:** S Hughes PhD BSc FGS



**Job Reference:** 7823

**Date:** February 2022

## CONTENTS

1	EXECUTIVE SUMMARY	3
2	INTRODUCTION	4
	2.2 Site Description	4
	2.3 Geological setting	5
3	Survey objectives	5
	3.1 Survey design	5
	3.1 Quality control	5
4	SURVEY DESCRIPTION	6
	4.1 Survey layout and topographic survey	6
	4.2 Survey design – vertical electrical soundings	6
5	RESULTS	9

### Figure

Figure 1: Location plan

### Appendices

Appendix A: Corby\_VES\_soundings\_TD7823.xlsx

Appendix B: Iris Syscal Jr SN#242 calibration certificate

## 1 EXECUTIVE SUMMARY

This report describes five soil resistivity tests performed as part of a ground investigation at Corby. The survey work was commissioned by DeltaSimons (the Client) and took place on the 8<sup>th</sup> and 9<sup>th</sup> of February 2022.

The electrode “a” spacings utilised during this survey were (in meters) 0.3, 0.9, 1.5, 3, 4.5, 6.1, 9.1, 15.2, 21.3, 27.4, 33.5, 39.6 and 45.7. The specification followed was IEEE Std 81-2012. The data is tabulated and plotted will be used in the design of a proposed energy-from-waste facility.

## 2 INTRODUCTION

This report describes five soil resistivity tests performed as part of a ground investigation at Corby. The survey work was commissioned by DeltaSimons (the Client) and took place on the 8<sup>th</sup> and 9<sup>th</sup> of February 2022.

### 2.2 Site Description

Five tests were performed at the location of a proposed energy-from-waste Facility (Figure 1). Each test was positioned using GPS coordinates provided by the Client. The site covers a 2.3 Ha area that comprises a predominantly gravel surface with some tarmacadam surfaces roadways that run across the site (Plate 1).

At present, the site is utilized as an additional car park area, but historically it was an ironstone quarry from 1951 to 1980, after being decommissioned the quarry was subsequently backfilled with waste material from the quarry.



**Plate 1:** Survey area at RH-1, looking north



### **2.3 Geological setting**

The underlying bedrock strata are the Northampton Sand Formation which has been noted to be up to 21 m thick and is described by the British Geological Survey (BGS) as “*Sandy, berthierine-oidal and sideritic ironstone, greenish-grey where fresh, weathering to brown limonitic sandstone... The unit includes lenses of mudstone and limestone in places...*”.

Historical borehole data suggests the rockhead is around 21.20 m deep (BGS reference: SP99SW1330), with the overlying material being backfill from the decommissioning of the quarry. The fill is dominated by firm to stiff silty clays with regular occurrences of gravel and “bands of fine orange-brown sand”.

## **3 Survey objectives**

The objective of the survey is as follows:

- Produce apparent resistivity data from vertical electrical soundings at five specified locations.

### **3.1 Survey design**

The Client specified vertical electrical soundings from 4-pin testing to aid earthing design. The 4-pin testing was carried out at the five specified locations.

### **3.1 Quality control**

The geophysical data were collected in line with normal operating procedures as outlined by the instrument manufacturer and TerraDat company policy. On completion of the survey, the data sets were downloaded from the survey instrument to a computer and backed up appropriately. The acquired datasets were checked initially for errors that may be caused by instrument noise, weak batteries, and positional discrepancies. Any field notes are subsequently written up or incorporated in the data processing stage. The data sets are then processed using standard processing routines, and once completed, the resulting plots are subject to peer review to

ensure the integrity of the interpretation. The quality control standards are BS EN ISO 9001:2015 certified.

## 4 SURVEY DESCRIPTION

The survey was carried out using the following geophysical method:

- **Vertical electrical sounding (4-pin testing):** These measurements are used to aid the design of earthing installation design.

### 4.1 Survey layout and topographic survey

For the vertical electrical soundings, two approximately orthogonal soundings were acquired at each position provided by the Client (Table 1). The locations were positioned on-site using a Topcon Hiper-SR network-corrected RTK GPS. As it was not possible to acquire positions outside the site, several of the larger “a” spacings were excluded from the survey.

### 4.2 Survey design – vertical electrical soundings

The electrode “a” spacings utilised during this survey were (in meters) 0.3, 0.9, 1.5, 3, 4.5, 6.1, 9.1, 15.2, 21.3, 27.4, 33.5, 39.6 and 45.7. The specification followed was IEEE Std 81-2012.

These spacings measure the apparent resistivity (R) of the ground at depths of investigation approximately equivalent to  $\frac{3}{4}$  of the “a” spacing. Assuming a depth of  $\frac{3}{4}$  of the electrode spacings, this provides resistivity readings between 0.23 and 34.26 m BGL. The resistivity is calculated as  $V / I$  where  $V$  = measured voltage (volts) and  $I$  = injected current (Amps).

Due to the ‘electrical’ insulating properties of the tarmacadam, the Client was required to drill a 38 mm deep hole through the tarmacadam to allow the electrodes to be inserted into the sub-base material.

These positions have been noted in the results.

Each resistivity reading was stacked three times and then repeated twice at each electrode spacing. Therefore, the final values presented in the table are an average of six individual readings.

The instrument used for the testing was an *IRIS SYSCAL Junior Switch 72* resistivity meter (Serial number 242). The calibration certificate for this meter is included in the Appendix.

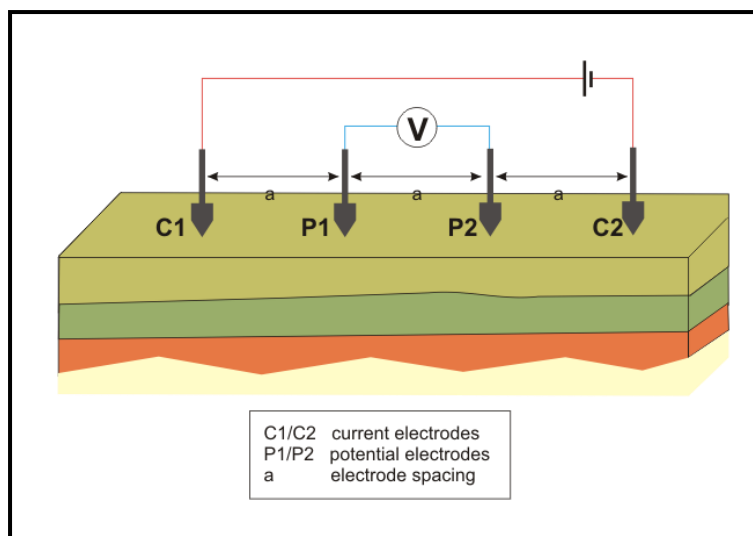
The coordinates of the test locations are presented in Table 1.

<u>Location</u>	<u>Eastings</u>	<u>Northings</u>	<u>Elevation (m aOD)</u>
RH-1	491071.20	290890.88	104.49
RH-2	491019.56	290905.95	104.42
RH-3	491008.07	290865.93	104.56
RH-4	490957.69	290862.88	105.43
RH-5	490896.28	290852.64	106.16

**Table 1:** Test locations in OSGB36 coordinates.

**Vertical electrical sounding – background information**

Resistivity measurements are made by passing a DC electrical current through the ground using a pair of electrodes and measuring the resulting potential gradient within the subsurface using a second electrode pair. There are several different electrode configurations; the most common type used is the Wenner array, which uses equal spaced electrodes (Plate 2).



**Plate 2: Resistivity testing setup (Wenner array)**

For a given electrode spacing 'a', the resistivity calculation is based on

$$\rho_a = 2\pi aR$$

where

$\rho_a$  Apparent resistivity

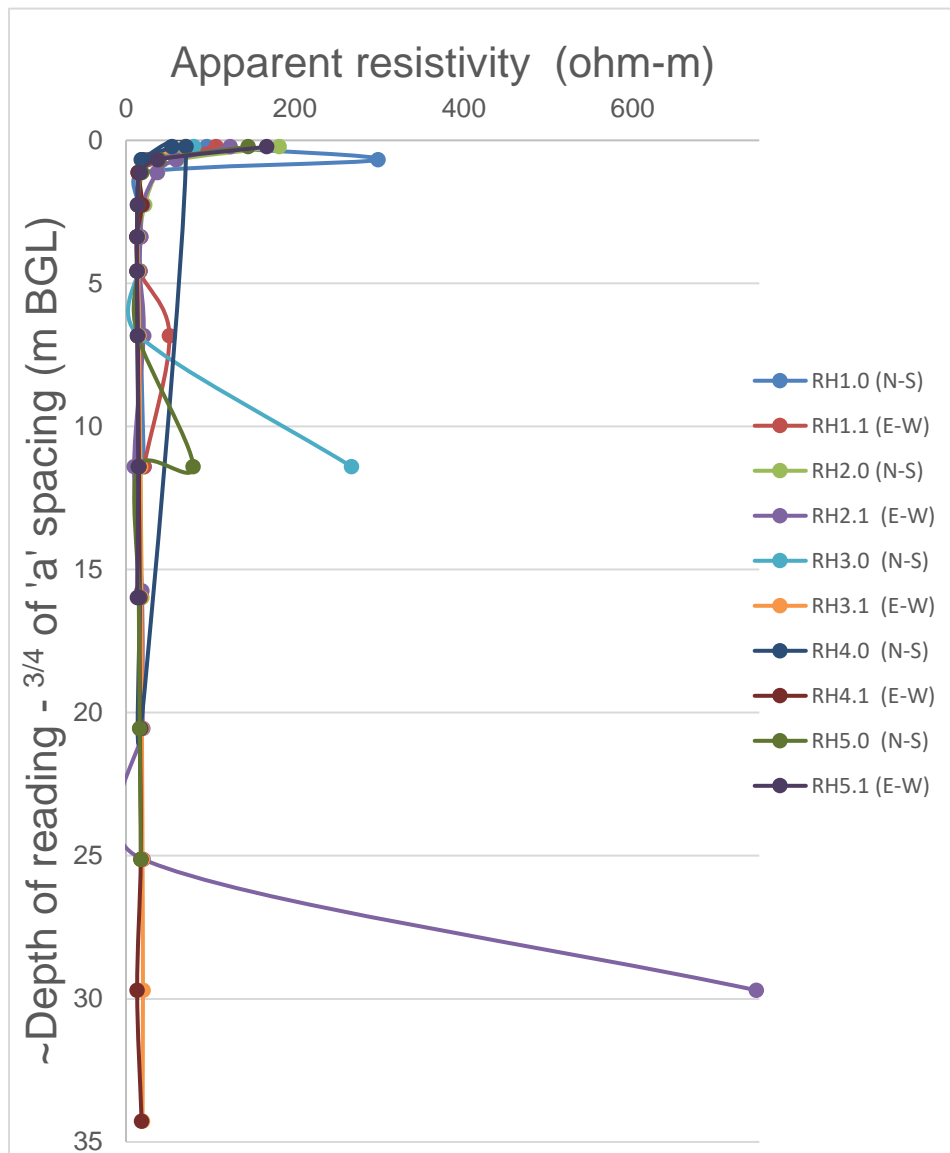
a electrode spacing

R voltage/current (V/I)

By gradually increasing the spacing between the current/potential electrodes, the depth of investigation is increased.

## 5 RESULTS

The results of the vertical electrical soundings are given in appendix 1 (*Corby\_VES\_soundings\_TD7823.xlsx*). Potential (V) and current (I) measurements are provided, and Resistivity values (Rho) are shown in Ohm meters as calculated by the resistivity meter. Resistivity ( $\rho$ ) for the Wenner array is calculated using the formula ( $\rho=2\pi aR$ ), where resistance is derived from the current and potential readings as ( $R=V/I$ ). The results for the apparent resistivity have been plotted in Plate 3 for comparison.



**Plate 3:** Summary apparent resistivity v depth plot of each resistivity sounding

**Field notes:**

Weather conditions –

08/02/2022: Cloudy overcast temperature 8 °c pressure 1027 mbar, readings taken between 8:30 and 16:20 (RH-1, RH-2, RH-3, RH-4)

09/02/2022: Cloudy overcast temperature 10 °c pressure 1022 mbar readings taken between 8:10 and 10:00 (RH-5)

### **General observations:**

There is a general trend showing resistivity values decreasing with depth; the moderate resistivity values for all the subsurface are within a range of 9.6 to 298.51 ohm.m (excluding the anomalous 746.51 ohm.m reading), which is indicative of a clay-rich lithology.

There are two anomalous results; the first is RH-2 line 2 (E-W), which has an anomalous result for “a” spacing 39.6. This is probably a result of the easternmost current electrode being inserted into a bank of very loose material. All possible actions were taken to decrease the resistance between the ground and electrode. Even though the resulting resistance check was within the acceptable range (6 Kohm), it was relatively higher than the others. RH-3 line 1 also has an anomalous reading at “a” spacing 15.2; this is potentially a result of interference from the service that is 2 m south of the southernmost current electrode.

### **Disclaimer**

*This report represents an opinionated interpretation of the geophysical data. It is intended for guidance with an invasive follow-up investigation. Features that do not produce measurable geophysical anomalies or are hidden by other features may remain undetected. Geophysical surveys complement invasive/destructive methods and provide a tool for investigating the subsurface; they do not produce data that can be taken to represent all of the ground conditions found within the surveyed area. Areas that have not been surveyed due to obstructed access or any other reason are excluded from the interpretation.*



# FIGURES

---



A) Location of sections through specified point



Insert map (NTS)



Survey area

KEY

- Resistivity sounding line
- Centre point of sounding location
- Site boundary

Notes

Source: Map data ©2022 Google.

Contains client basemap: 112101-00-YTC-CDA-MET-101-Locations of In Situ Geotechnical Tests.dwg

**TERRA DAT** Tel: +44 (0) 2920 700127  
 down to earth geophysics Web: www.terradat.co.uk  
 Email: web@terradat.co.uk

Title: **LOCATION PLAN**

Project: **Soil resistivity survey, Coby**

Scale: 1:1000 at A3  
 Drawn by/Ref: RS/7823/1  
 Date: 21 February 2022

**FIGURE 1**

B) Coordinates of sounding location

<u>Location</u>	<u>Eastings</u>	<u>Northings</u>	<u>Elevation (m aOD)</u>
RH-1	491071.20	290890.88	104.49
RH-2	491019.56	290905.95	104.42
RH-3	491008.07	290865.93	104.56
RH-4	490957.69	290862.88	105.43
RH-5	490896.28	290852.64	106.16



# APPENDICES

---

Serial Number: 242	<b>SYSCAL JUNIOR switch 72</b>	<b>Test report &amp; Certificate of calibration</b>	
Tested by: SA			
Date: 10/24/19			
Page 1 / 1			

Test equipment used		
Multimeter : FLUKE 189	Serial Number : PM02	Calibration due date : 10/01/20
Multimeter : FLUKE 189	Serial Number : PM03	Calibration due date : 10/01/20
Battery tester	Serial Number : PTB01	Calibration due date : 08/03/20
SWITCH Tester	Model with Extension Link connector	
COMSYS Module	Model with COMSYS SP option	

Detailed Test Report				
Nature of the test	Test conditions, reference data (ammeter, voltmeter, ohmmeter, battery tester...)	Expected Specifications	Unit under test	Pass / Fail
<b>Software</b>				
Software	Version 12.0a			
<b>Measures</b>				
Vmn measure	From Save Energy to Vp max	< 0.2 % typ	0.17%	ok
Precision of the current measure	Deviation from I = 805.8 mA	< 0.2 % typ	0.02%	ok
Input voltage saturation	Injection of voltage > 5 V	5 V	5.0V	ok
<b>Functional tests</b>				
Test of the full output power	For Vab maximum and Rab ≈ 1700 Ω	100 W ± 2.5%	94.78 W	ok
Test of the short circuit output current	For Vab = 50 V and Rab = 20 Ω	1.15 A min	1.195 A	ok
Test of the maximum output voltage	Pointed out during the full output power test	≈ 400 V	400 V	ok
Electrodes switching tested	Check with Prosys II			ok
Leakage Test	Rmn = 33 kΩ, In ≈ 14 mA, 250 ms	Vp < 2 mV	0.100 mV	ok
Isolation test with the front panel	Performed during injection			ok
<b>Batteries</b>				
Type of internal batteries	Sealed lead acid battery type			
Tx battery : Ref & values from the battery tester	Batch ref. number: 181205AB JK01MA	12V / 7.2 Ah	13.1V / 8.7 Ah	ok
Rx battery : Ref & values from the battery tester	Batch ref. number: 181107B JK01MA	12V / 7.2 Ah	13.1V / 8.3 Ah	ok
Internal and external Tx battery operation	Tests performed in both settings			ok
Visual indication of very low Tx battery	Voltage below which the LED lights red		9.63 V	ok
Visual indication of good Tx battery	Voltage below which the LED lights green		11.32 V	ok
Lithium backup battery	Level voltage	3.6 V	3.67 V	ok
<b>Data</b>				
Check internal data storage and copy to PC	With USB cable and Prosys II software			ok
Download data to the IRIS SD Card reader	Reading data with Prosys II software			ok
Load a sequence from ELECTRE Pro software	Check file in Syscal memory			ok
<b>Options</b>				
Check "Extension link" connector	Connector not available on this device			NA
COMSYS SP Option	Option not available on this device			NA
<b>In the field test of endurance</b>				
Electrical survey	Wenner - Schlumberger, 15 different spacing			ok
Multi-electrode survey	To Vp max and external battery: Dipôle-Dipôle, Pôle-Dipôle, Pôle-Pôle, Wenner-Schlumberger et Dipôle-Dipôle multi spacing			ok

Made at IRIS Instruments in Orleans, France,  
October 30th, 2019

L. Cabaret,	Production manager
	

## Appendix E - Geotechnical Analysis Results



# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

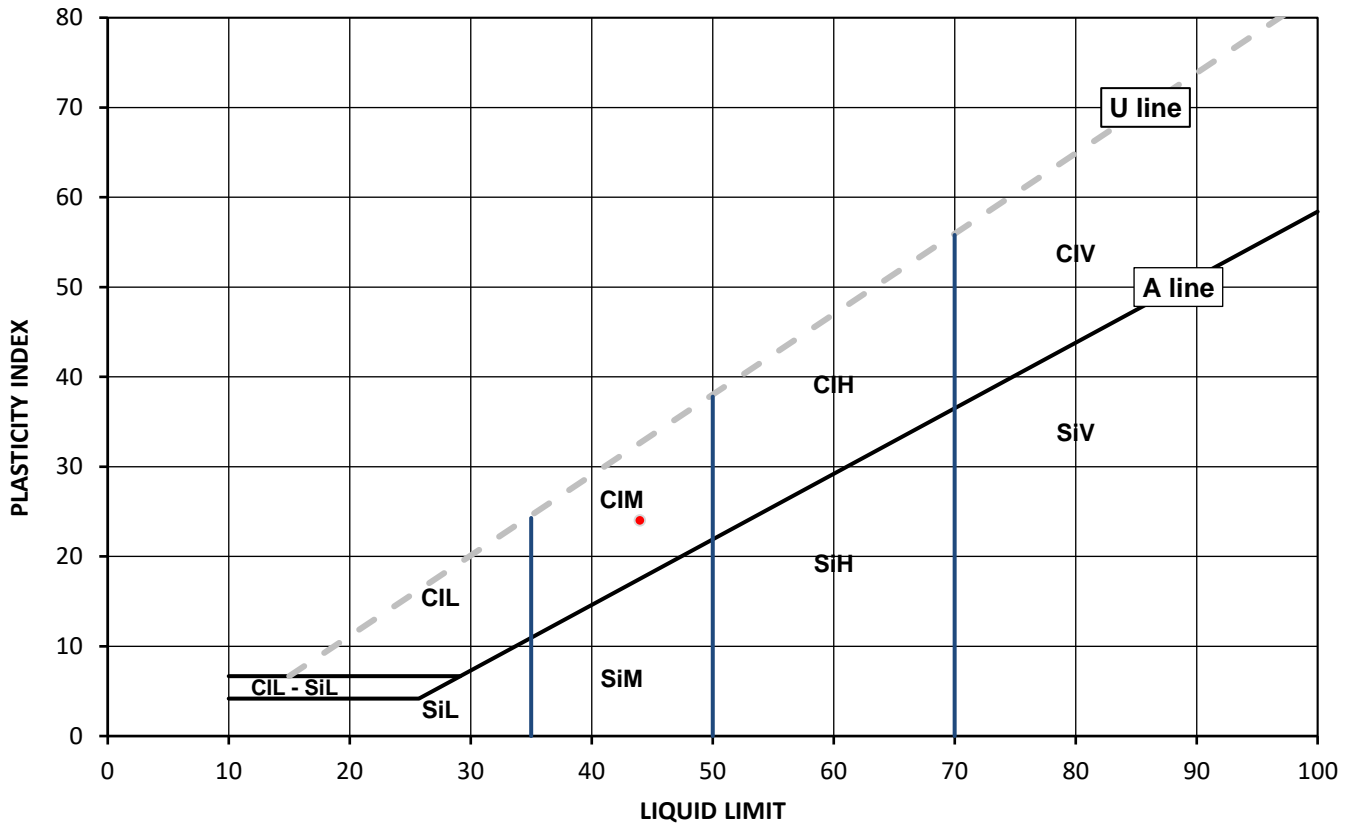
## Test Results:

Laboratory Reference: 2178519  
Hole No.: BH3  
Sample Reference: 1  
Sample Description: Greyish brown slightly gravelly sandy very clayey SILT with fragments of chalk

Depth Top [m]: 2.00  
Depth Base [m]: 2.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
22	44	20	24	90



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	L	Low	Liquid Limit	below 35
Si	Silt		M	Medium		35 to 50
			H	High		50 to 70
			V	Very high		exceeding 70
			O	Organic		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

Opinions and interpretations expressed herein are outside of the scope of the UKAS Accreditation. This report may not be reproduced other than in full without the prior written approval of the issuing laboratory. The results included within the report relate only to the sample(s) submitted for testing.

*Katarzyna Koziel*



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i2 Analytical Ltd  
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Sampled By: Not Given

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Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

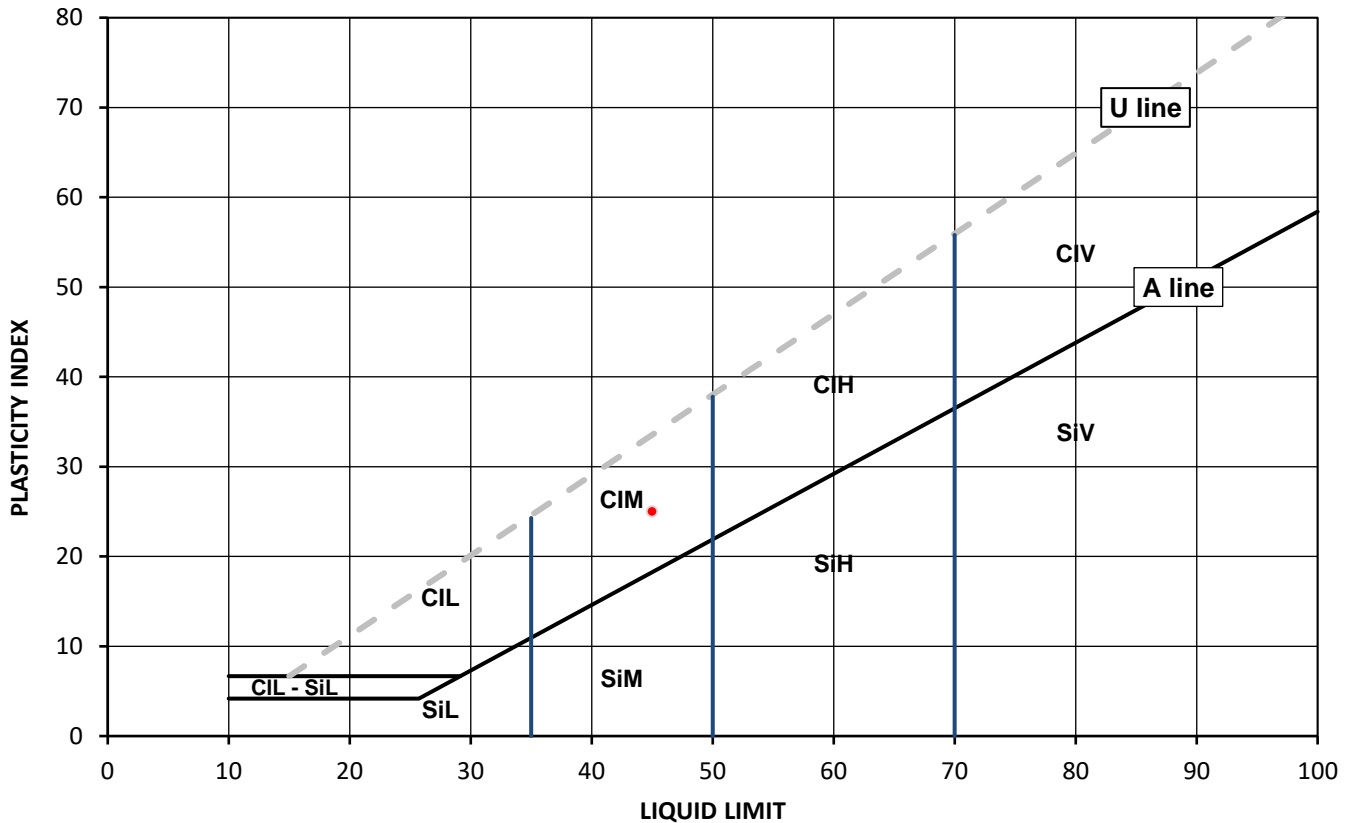
### Test Results:

Laboratory Reference: 2178520  
Hole No.: BH3  
Sample Reference: 2  
Sample Description: Grey gravelly sandy very silty CLAY with fragments of chalk

Depth Top [m]: 4.00  
Depth Base [m]: 4.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
18	45	20	25	76



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	Liquid Limit
Si	Silt	L	Low
		M	Medium
		H	High
		V	Very high
		O	Organic
			append to classification for organic material ( eg CIHO )
			below 35
			35 to 50
			50 to 70
			exceeding 70

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

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Date Tested: 24/02/2022  
Sampled By: Not Given

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

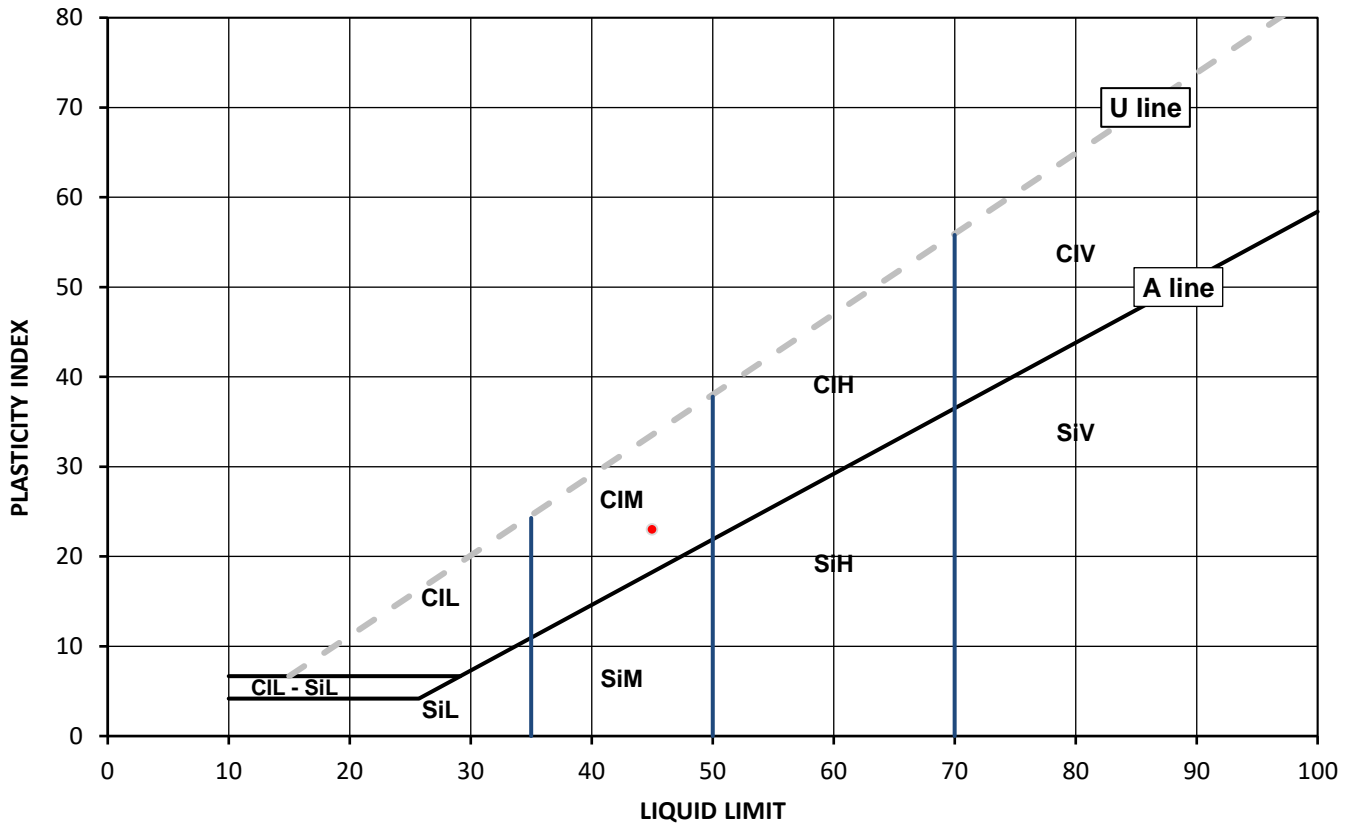
### Test Results:

Laboratory Reference: 2178521  
Hole No.: BH3  
Sample Reference: 3  
Sample Description: Brownish grey slightly gravelly sandy very silty CLAY with fragments of chalk

Depth Top [m]: 6.50  
Depth Base [m]: 6.95  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
21	45	22	23	89



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	L	Low	Liquid Limit	below 35
Si	Silt		M	Medium		35 to 50
			H	High		50 to 70
			V	Very high		exceeding 70
			O	Organic		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

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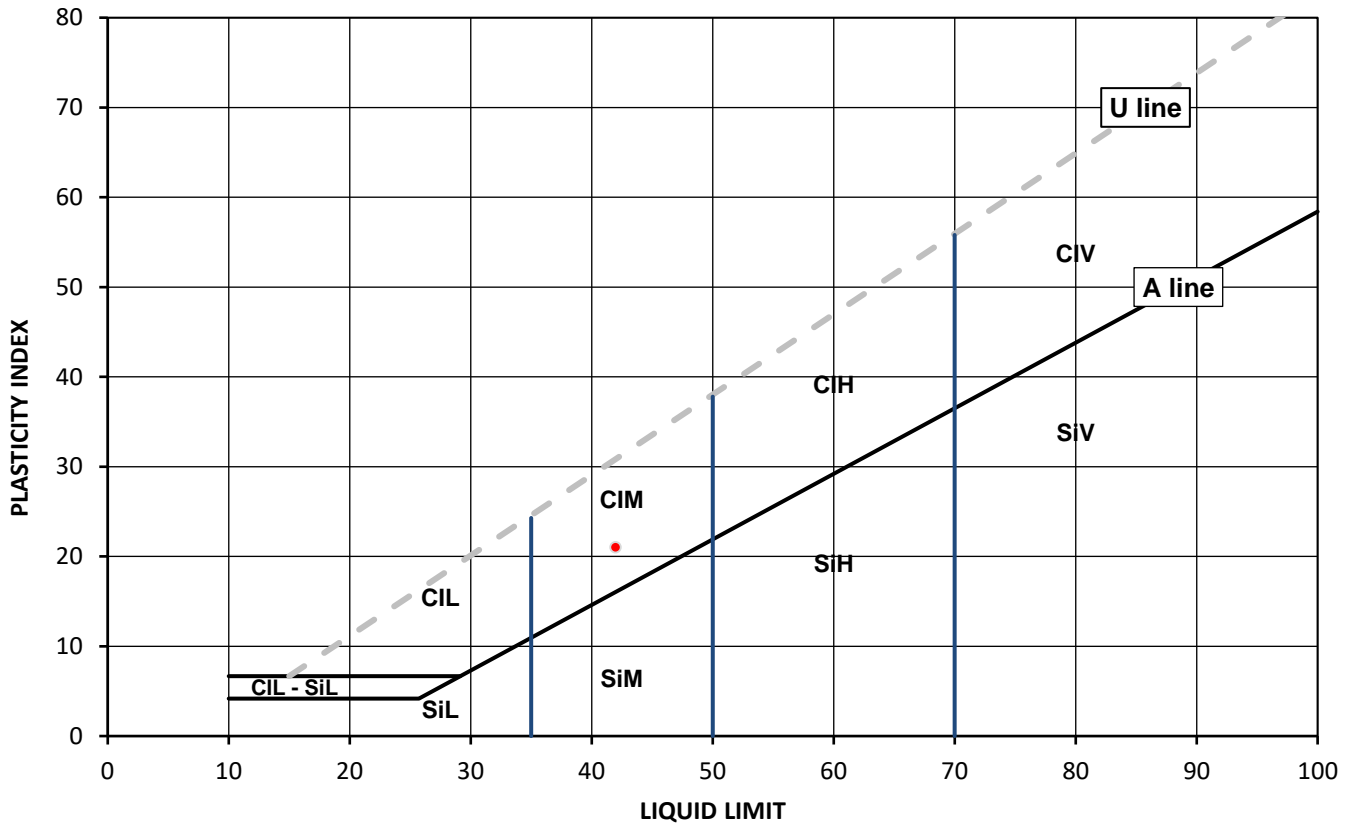
## Test Results:

Laboratory Reference: 2178522  
Hole No.: BH11  
Sample Reference: 1  
Sample Description: Grey slightly gravelly sandy very clayey SILT

Depth Top [m]: 2.00  
Depth Base [m]: 2.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
19	42	21	21	86



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

	Plasticity	Liquid Limit
Cl	Clay	below 35
Si	Silt	35 to 50
	L	Low
	M	Medium
	H	High
	V	Very high
	O	Organic
		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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*Katarzyna Koziel*



# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EFW

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

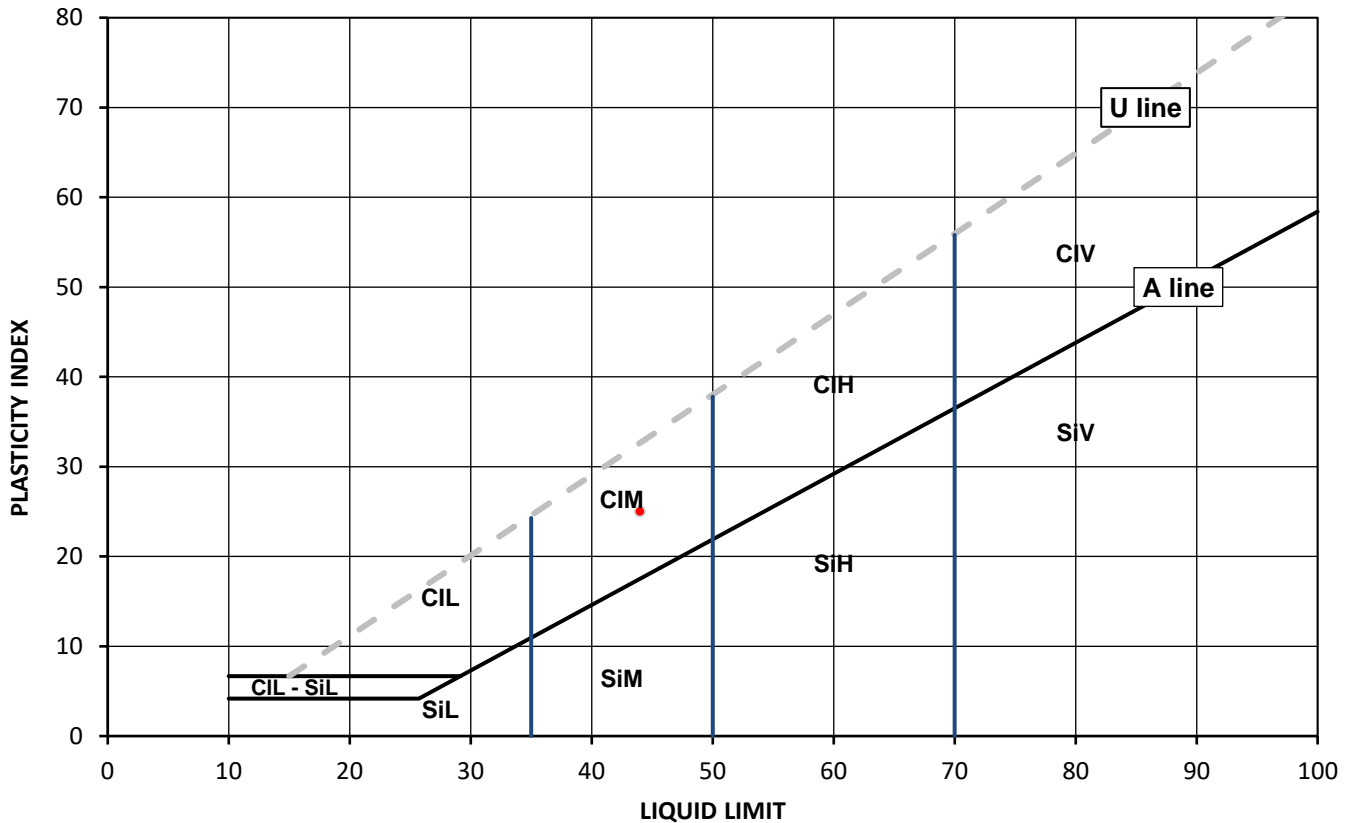
## Test Results:

Laboratory Reference: 2178523  
Hole No.: BH11  
Sample Reference: 2  
Sample Description: Greyish brown gravelly sandy very clayey SILT with fragments of chalk

Depth Top [m]: 4.00  
Depth Base [m]: 4.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
20	44	19	25	90



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	L	Low	Liquid Limit	below 35
Si	Silt		M	Medium		35 to 50
			H	High		50 to 70
			V	Very high		exceeding 70
			O	Organic		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

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Technical Reviewer  
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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
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Environmental Science

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Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

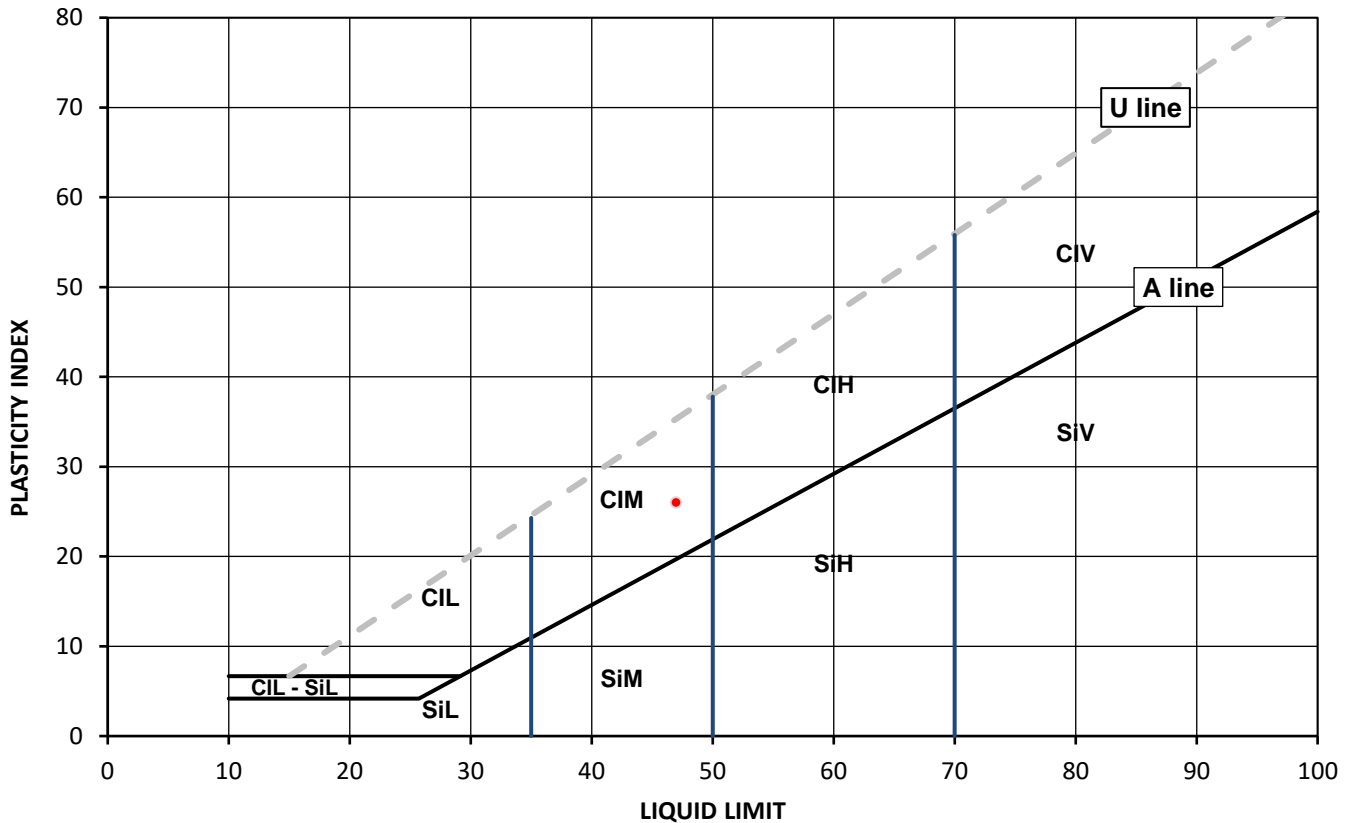
## Test Results:

Laboratory Reference: 2178524  
Hole No.: BH11  
Sample Reference: 3  
Sample Description: Grey to yellowish brown gravelly sandy very silty CLAY

Depth Top [m]: 11.00  
Depth Base [m]: 11.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
16	47	21	26	88



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

	Plasticity	Liquid Limit
Cl Clay	L Low	below 35
Si Silt	M Medium	35 to 50
	H High	50 to 70
	V Very high	exceeding 70
	O Organic	append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

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*Katarzyna Koziel*



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Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

# SUMMARY REPORT

## SUMMARY OF CLASSIFICATION TEST RESULTS

Tested in Accordance with:

Water Content by BS 1377-2:1990: Clause 3.2; Atterberg by BS 1377-2: 1990:  
Clause 4.3 (4 Point Test), Clause 4.4 (1 Point Test) and 5; PD by BS 1377-2:  
1990: Clause 8.2

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

### Test results

Laboratory Reference	Hole No.	Sample				Description	Remarks	Water Content BS 1377-2 [ W ] %	Water Content BS EN ISO 17892-2 [ W ] %	Atterberg				Density			Total Porosity# %		
		Reference	Depth Top m	Depth Base m	Type					% Passing 425um	WL %	Wp %	Ip %	bulk Mg/m3	dry Mg/m3	PD Mg/m3			
2178522	BH11	1	2.00	2.45	U	Grey slightly gravelly sandy very clayey SILT	Atterberg 4 Point	19		86	42	21	21			2.70			
2178523	BH11	2	4.00	4.45	U	Greyish brown gravelly sandy very clayey SILT with fragments of chalk	Atterberg 4 Point	20		90	44	19	25			2.69			
2178524	BH11	3	11.00	11.45	U	Grey to yellowish brown gravelly sandy very silty CLAY	Atterberg 4 Point	16		88	47	21	26						
2178519	BH3	1	2.00	2.45	U	Greyish brown slightly gravelly sandy very clayey SILT with fragments of chalk	Atterberg 4 Point	22		90	44	20	24						
2178520	BH3	2	4.00	4.45	U	Grey gravelly sandy very silty CLAY with fragments of chalk	Atterberg 4 Point	18		76	45	20	25						
2178521	BH3	3	6.50	6.95	U	Brownish grey slightly gravelly sandy very silty CLAY with fragments of chalk	Atterberg 4 Point	21		89	45	22	23						

Note: # Non accredited; NP - Non plastic

Comments: Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# SUMMARY REPORT

## DETERMINATION OF WATER CONTENT

Tested in Accordance with: BS 1377-2: 1990: Clause 3.2

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

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Contact: Harry Whittle  
Site Address: Corby EFW

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test results

Laboratory Reference	Hole No.	Sample				Description	Remarks	WC %	Sample preparation / Oven temperature at the time of testing			
		Reference	Depth Top m	Depth Base m	Type							
2178522	BH11	1	2.00	2.45	U	Grey slightly gravelly sandy very clayey SILT		19	Sample was quartered, oven dried at 106.4 °C			
2178523	BH11	2	4.00	4.45	U	Greyish brown gravelly sandy very clayey SILT with fragments of chalk		20	Sample was quartered, oven dried at 106.4 °C			
2178524	BH11	3	11.00	11.45	U	Grey to yellowish brown gravelly sandy very silty CLAY		16	Sample was quartered, oven dried at 106.4 °C			
2178519	BH3	1	2.00	2.45	U	Greyish brown slightly gravelly sandy very clayey SILT with fragments of chalk		22	Sample was quartered, oven dried at 106.4 °C			
2178520	BH3	2	4.00	4.45	U	Grey gravelly sandy very silty CLAY with fragments of chalk		18	Sample was quartered, oven dried at 106.4 °C			
2178521	BH3	3	6.50	6.95	U	Brownish grey slightly gravelly sandy very silty CLAY with fragments of chalk		21	Sample was quartered, oven dried at 106.4 °C			

Comments: Preliminary report

Signed:

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Technical Reviewer  
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4041

# TEST CERTIFICATE

## DETERMINATION OF PARTICLE SIZE DISTRIBUTION

Tested in Accordance with: BS 1377-2: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 04/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

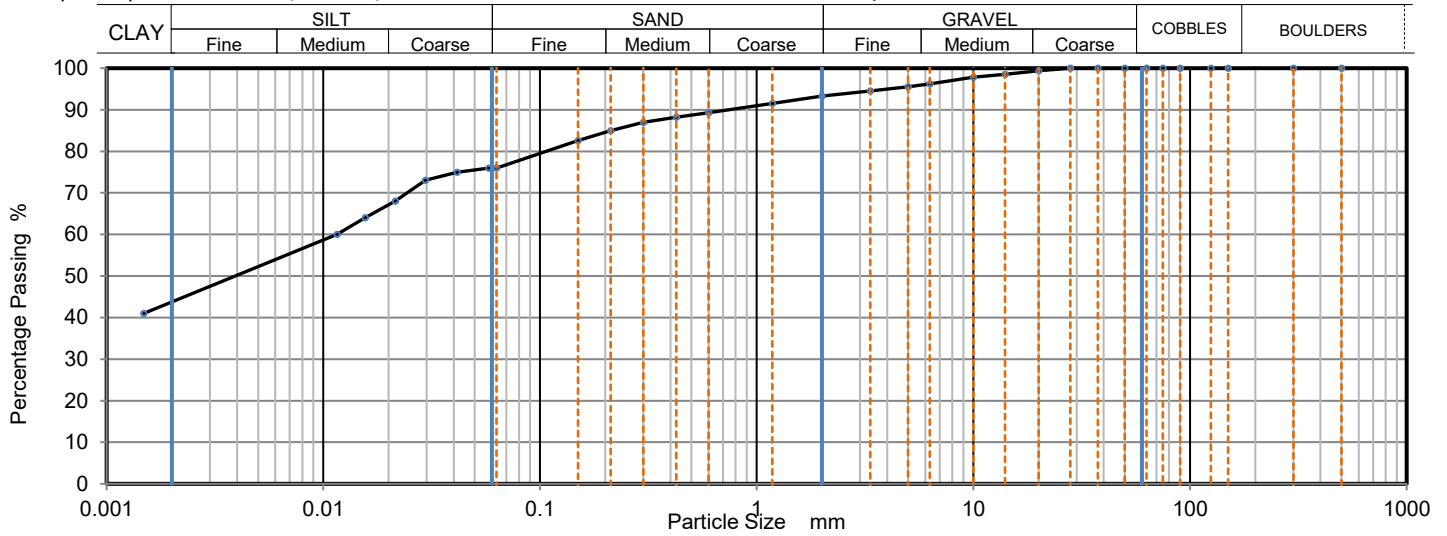
Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178514  
Hole No.: TR-1  
Sample Reference: 1  
Sample Description: Brownish grey slightly gravelly sandy very silty CLAY  
Sample Preparation: Sample was quartered, oven dried at 108.5 °C and broken down by hand.

Depth Top [m]: 1.30  
Depth Base [m]: Not Given  
Sample Type: B



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0580	76
300	100	0.0414	75
150	100	0.0296	73
125	100	0.0215	68
90	100	0.0156	64
75	100	0.0116	60
63	100	0.0015	41
50	100		
37.5	100		
28	100		
20	99		
14	99		
10	98		
6.3	96		
5	96		
3.35	95		
2	93	Particle density (assumed) 2.65 Mg/m3	
1.18	92		
0.6	89		
0.425	88		
0.3	87		
0.212	85		
0.15	83		
0.063	76		

Sample Proportions	% dry mass
Very coarse	0
Gravel	7
Sand	17
Silt	32
Clay	44

Grading Analysis		
D100	mm	28
D60	mm	0.011
D30	mm	
D10	mm	
Uniformity Coefficient		> 7.4
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
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# TEST CERTIFICATE

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Brackmills Industrial Estate  
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Environmental Science

4041

Client: Delta-Simons  
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Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 04/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

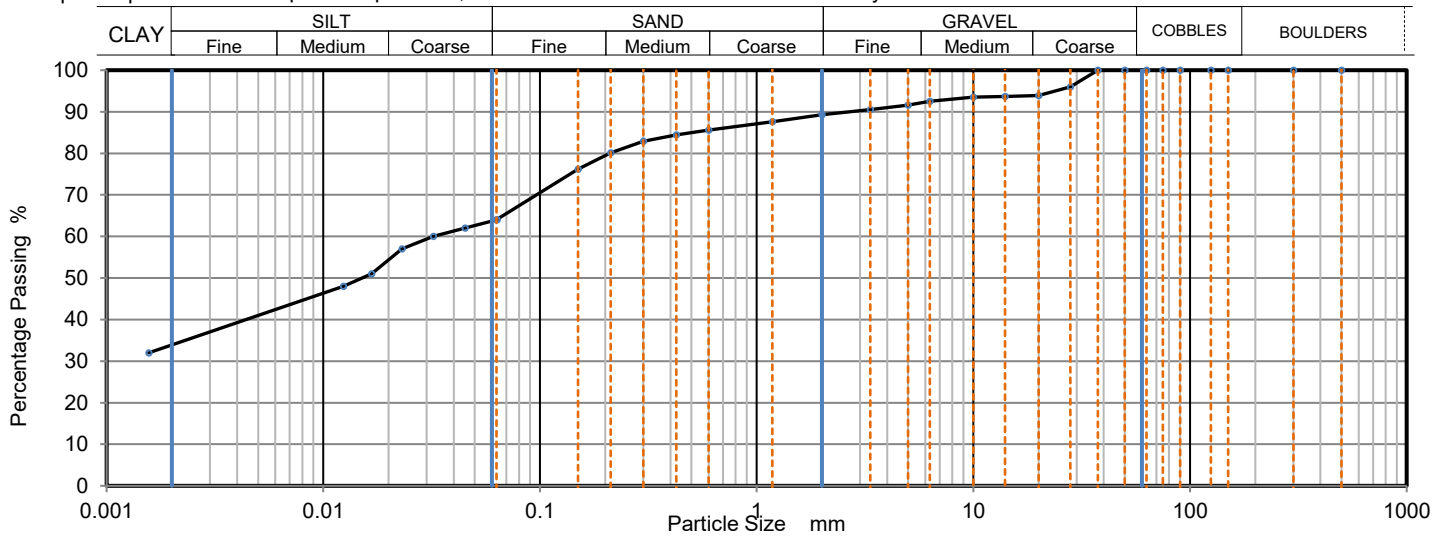
Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178515  
Hole No.: TR-2  
Sample Reference: 1  
Sample Description: Brownish grey gravelly sandy very silty CLAY  
Sample Preparation: Sample was quartered, oven dried at 106.4 °C and broken down by hand.

Depth Top [m]: 0.40  
Depth Base [m]: Not Given  
Sample Type: B



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0633	64
300	100	0.0451	62
150	100	0.0322	60
125	100	0.0231	57
90	100	0.0167	51
75	100	0.0124	48
63	100	0.0016	32
50	100		
37.5	100		
28	96		
20	94		
14	94		
10	94		
6.3	93		
5	92		
3.35	91		
2	89	Particle density (assumed) 2.65 Mg/m <sup>3</sup>	
1.18	88		
0.6	86		
0.425	84		
0.3	83		
0.212	80		
0.15	76		
0.063	64		

Sample Proportions	% dry mass
Very coarse	0
Gravel	11
Sand	25
Silt	30
Clay	34

Grading Analysis		
D100	mm	37.5
D60	mm	0.0311
D30	mm	
D10	mm	
Uniformity Coefficient		> 20
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
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# TEST CERTIFICATE

## DETERMINATION OF PARTICLE SIZE DISTRIBUTION

Tested in Accordance with: BS 1377-2: 1990

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Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

Client: Delta-Simons  
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Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 04/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178516

Hole No.: TR-3

Sample Reference: 1

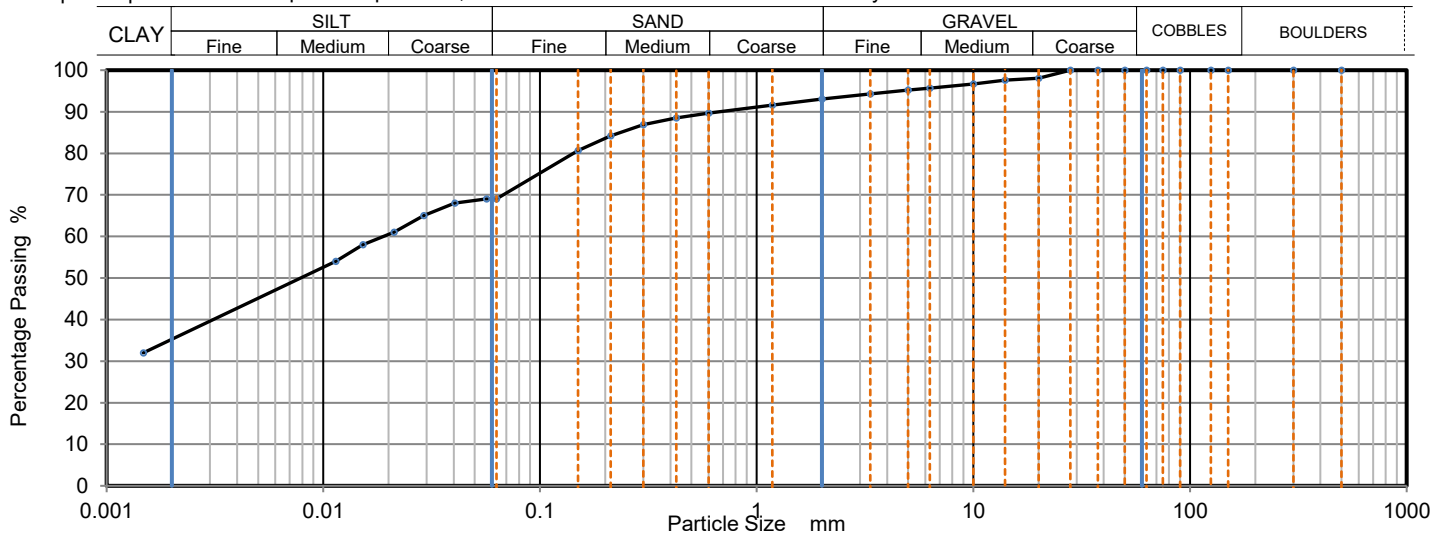
Sample Description: Grey gravelly sandy very silty CLAY

Sample Preparation: Sample was quartered, oven dried at 106.1 °C and broken down by hand.

Depth Top [m]: 1.00

Depth Base [m]: Not Given

Sample Type: B



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0566	69
300	100	0.0404	68
150	100	0.0291	65
125	100	0.0212	61
90	100	0.0152	58
75	100	0.0114	54
63	100	0.0015	32
50	100		
37.5	100		
28	100		
20	98		
14	98		
10	97		
6.3	96		
5	95		
3.35	94		
2	93	Particle density (assumed) 2.65 Mg/m <sup>3</sup>	
1.18	92		
0.6	90		
0.425	89		
0.3	87		
0.212	84		
0.15	81		
0.063	69		

Sample Proportions	% dry mass
Very coarse	0
Gravel	7
Sand	24
Silt	34
Clay	35

Grading Analysis		
D100	mm	28
D60	mm	0.019
D30	mm	
D10	mm	
Uniformity Coefficient		> 13
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

*Katarzyna Koziel*

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF PARTICLE SIZE DISTRIBUTION

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Environmental Science

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Job Number: 22-40679  
Date Sampled: 04/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

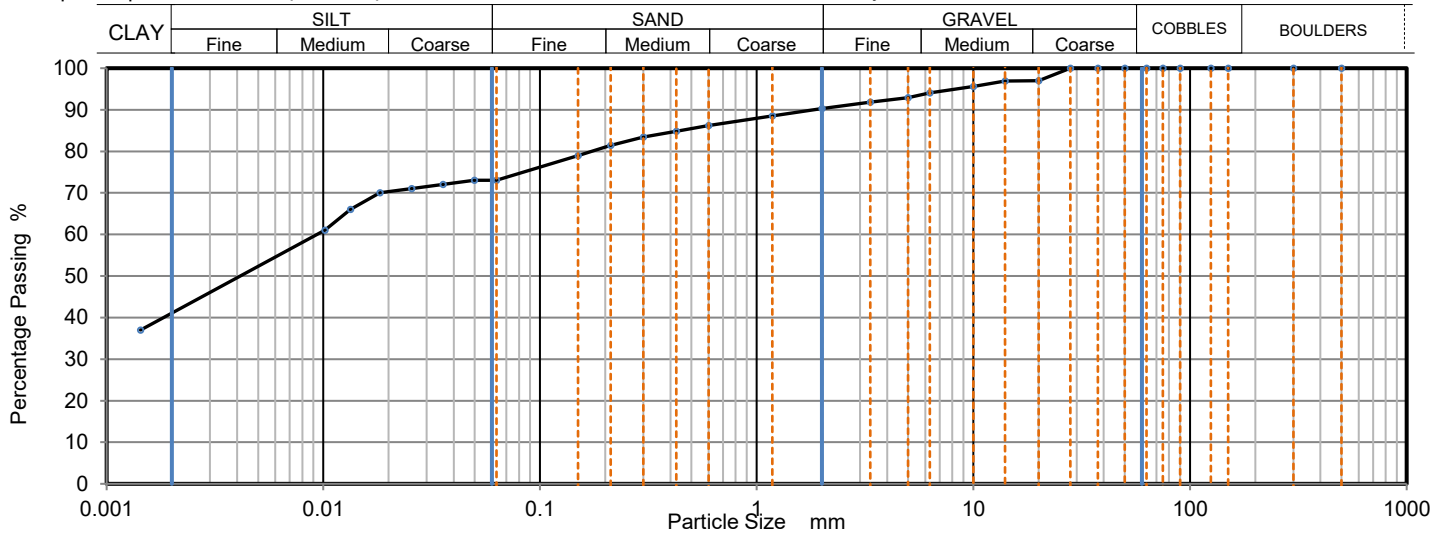
Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178517  
Hole No.: TR-4A  
Sample Reference: 1  
Sample Description: Grey gravelly sandy very silty CLAY  
Sample Preparation: Sample was quartered, oven dried at 108.5 °C and broken down by hand.

Depth Top [m]: 0.60  
Depth Base [m]: Not Given  
Sample Type: B



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0498	73
300	100	0.0356	72
150	100	0.0255	71
125	100	0.0183	70
90	100	0.0134	66
75	100	0.0102	61
63	100	0.0075	57
50	100	0.0050	50
37.5	100	0.0035	43
28	100	0.0025	37
20	97		
14	97		
10	96		
6.3	94		
5	93		
3.35	92		
2	90	Particle density (measured) 2.69 Mg/m <sup>3</sup>	
1.18	89		
0.6	86		
0.425	85		
0.3	83		
0.212	81		
0.15	79		
0.063	73		

Sample Proportions	% dry mass
Very coarse	0
Gravel	10
Sand	17
Silt	32
Clay	41

Grading Analysis		
D100	mm	28
D60	mm	0.00933
D30	mm	
D10	mm	
Uniformity Coefficient		> 6.5
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

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Technical Reviewer  
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# TEST CERTIFICATE

## DETERMINATION OF PARTICLE SIZE DISTRIBUTION

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Environmental Science

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Client Address: 3 Henley Office Park, Doddington Road,  
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Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 04/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

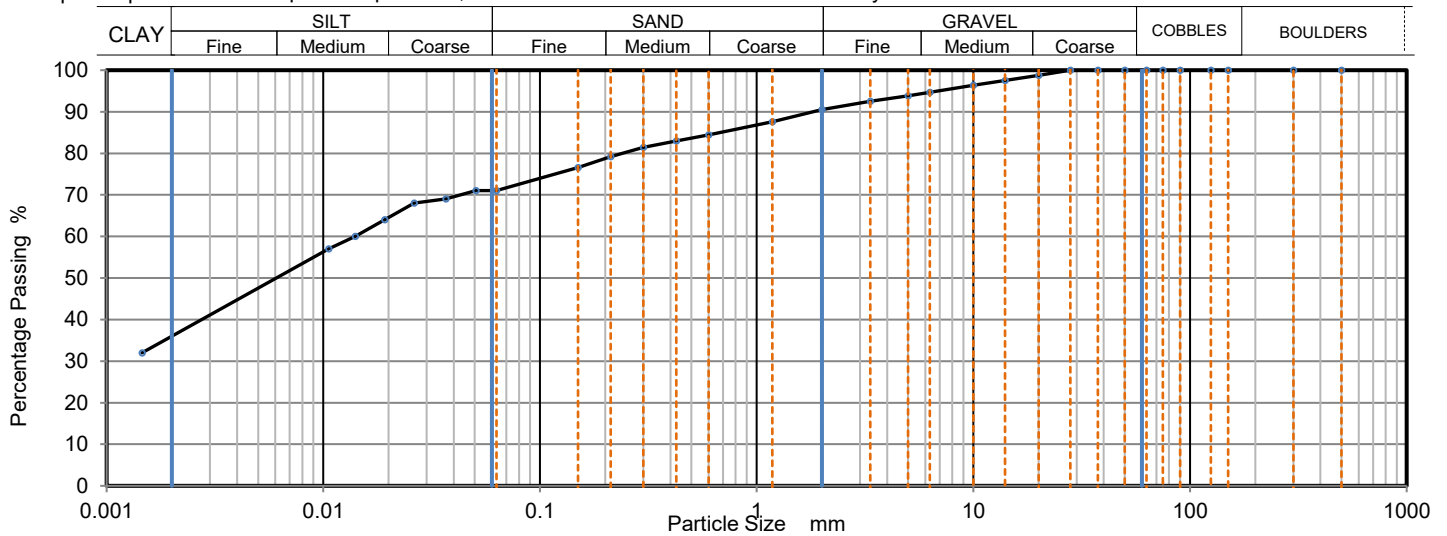
Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178518  
Hole No.: TR-5  
Sample Reference: 2  
Sample Description: Greyish brown gravelly sandy very silty CLAY  
Sample Preparation: Sample was quartered, oven dried at 106.2 °C and broken down by hand.

Depth Top [m]: 0.50  
Depth Base [m]: Not Given  
Sample Type: B



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0506	71
300	100	0.0367	69
150	100	0.0263	68
125	100	0.0192	64
90	100	0.0140	60
75	100	0.0106	57
63	100	0.0075	55
50	100	0.0050	50
37.5	100		
28	100		
20	99		
14	98		
10	96		
6.3	95		
5	94		
3.35	93		
2	91	Particle density (assumed)	
1.18	88	2.65	Mg/m <sup>3</sup>
0.6	84		
0.425	83		
0.3	81		
0.212	79		
0.15	77		
0.063	71		

Sample Proportions	% dry mass
Very coarse	0
Gravel	9
Sand	19
Silt	36
Clay	36

Grading Analysis		
D100	mm	28
D60	mm	0.0138
D30	mm	
D10	mm	
Uniformity Coefficient		> 9.5
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF PARTICLE SIZE DISTRIBUTION

Tested in Accordance with: BS 1377-2: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178519

Hole No.: BH3

Sample Reference: 1

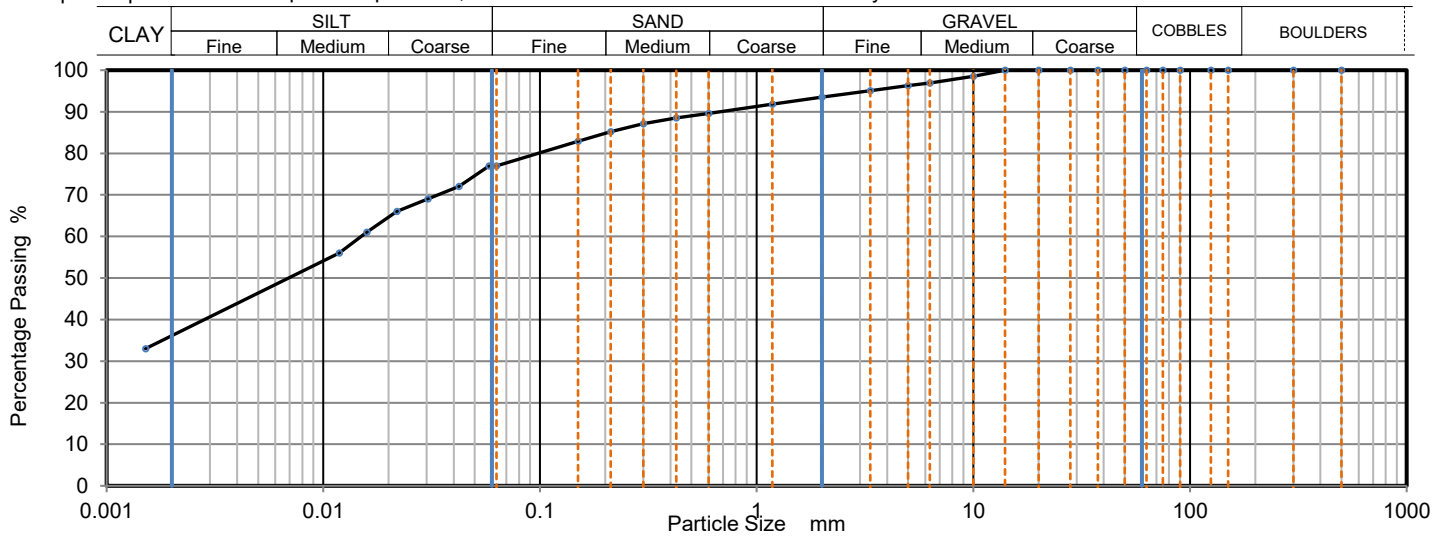
Sample Description: Greyish brown slightly gravelly sandy very clayey SILT with fragments of chalk

Sample Preparation: Sample was quartered, oven dried at 106.4 °C and broken down by hand.

Depth Top [m]: 2.00

Depth Base [m]: 2.45

Sample Type: U



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0581	77
300	100	0.0422	72
150	100	0.0304	69
125	100	0.0219	66
90	100	0.0158	61
75	100	0.0118	56
63	100	0.0015	33
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	99		
6.3	97		
5	96		
3.35	95		
2	94	Particle density (assumed) 2.65 Mg/m <sup>3</sup>	
1.18	92		
0.6	90		
0.425	89		
0.3	87		
0.212	85		
0.15	83		
0.063	77		

Sample Proportions	% dry mass
Very coarse	0
Gravel	6
Sand	17
Silt	41
Clay	36

Grading Analysis		
D100	mm	14
D60	mm	0.0153
D30	mm	
D10	mm	
Uniformity Coefficient		> 10
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

*Katarzyna Koziel*

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF PARTICLE SIZE DISTRIBUTION

Tested in Accordance with: BS 1377-2: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

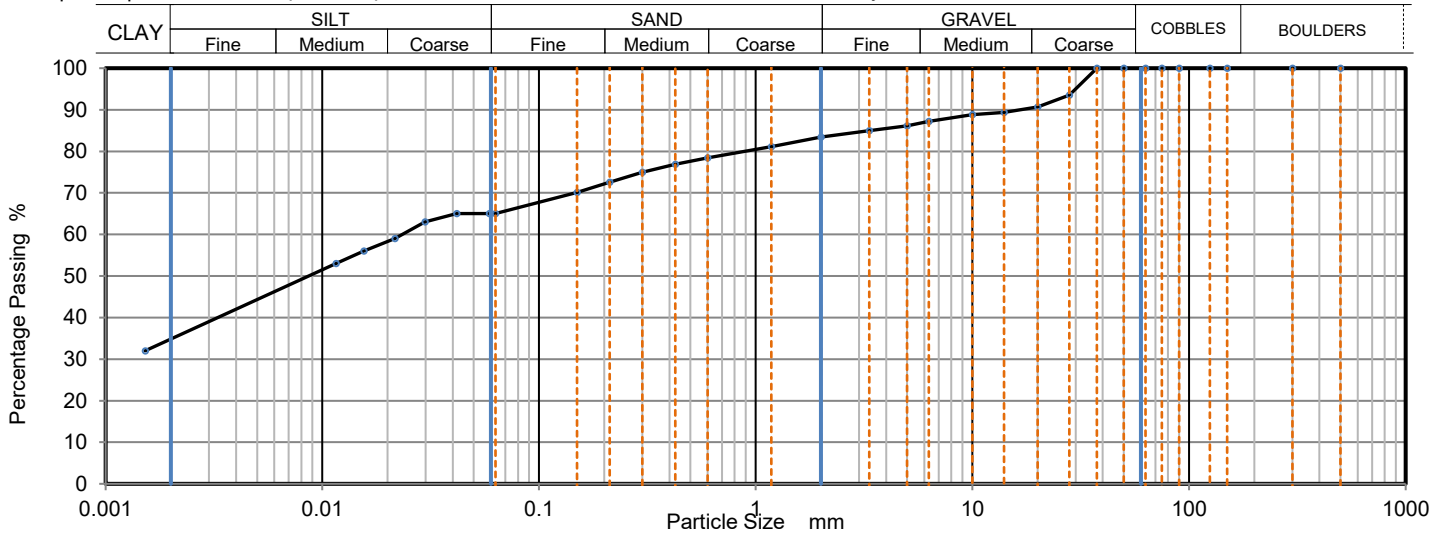
Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178520  
Hole No.: BH3  
Sample Reference: 2  
Sample Description: Grey gravelly sandy very silty CLAY with fragments of chalk  
Sample Preparation: Sample was quartered, oven dried at 106.4 °C and broken down by hand.

Depth Top [m]: 4.00  
Depth Base [m]: 4.45  
Sample Type: U



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0590	65
300	100	0.0417	65
150	100	0.0298	63
125	100	0.0216	59
90	100	0.0156	56
75	100	0.0116	53
63	100	0.0015	32
50	100		
37.5	100		
28	94		
20	91		
14	89		
10	89		
6.3	87		
5	86		
3.35	85		
2	83	Particle density (assumed) 2.65 Mg/m <sup>3</sup>	
1.18	81		
0.6	78		
0.425	77		
0.3	75		
0.212	73		
0.15	70		
0.063	65		

Sample Proportions	% dry mass
Very coarse	0
Gravel	17
Sand	19
Silt	29
Clay	35

Grading Analysis		
D100	mm	37.5
D60	mm	0.0237
D30	mm	
D10	mm	
Uniformity Coefficient		> 16
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

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i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

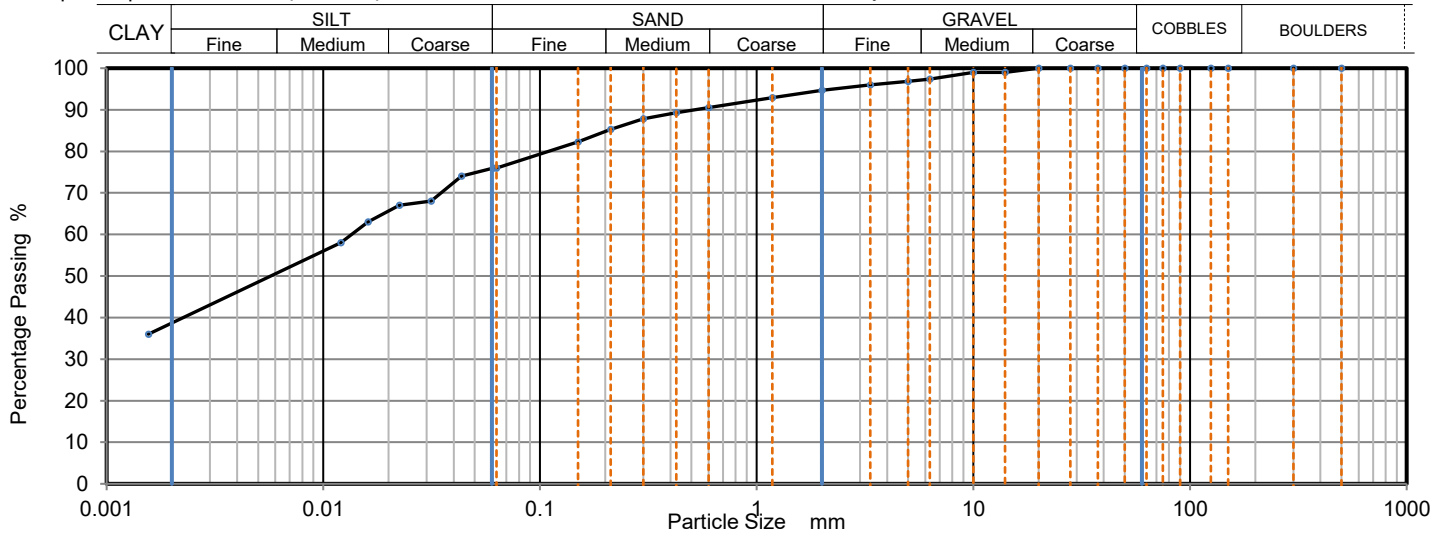
Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178521  
Hole No.: BH3  
Sample Reference: 3  
Sample Description: Brownish grey slightly gravelly sandy very silty CLAY with fragments of chalk  
Sample Preparation: Sample was quartered, oven dried at 106.4 °C and broken down by hand.

Depth Top [m]: 6.50  
Depth Base [m]: 6.95  
Sample Type: U



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0608	76
300	100	0.0434	74
150	100	0.0315	68
125	100	0.0224	67
90	100	0.0161	63
75	100	0.0120	58
63	100	0.0016	36
50	100		
37.5	100		
28	100		
20	100		
14	99		
10	99		
6.3	97		
5	97		
3.35	96		
2	95	Particle density (assumed) 2.65 Mg/m <sup>3</sup>	
1.18	93		
0.6	91		
0.425	89		
0.3	88		
0.212	85		
0.15	82		
0.063	76		

Sample Proportions	% dry mass
Very coarse	0
Gravel	5
Sand	19
Silt	37
Clay	39

Grading Analysis		
D100	mm	20
D60	mm	0.0136
D30	mm	
D10	mm	
Uniformity Coefficient		> 8.8
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF PARTICLE SIZE DISTRIBUTION

Tested in Accordance with: BS 1377-2: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178522

Hole No.: BH11

Sample Reference: 1

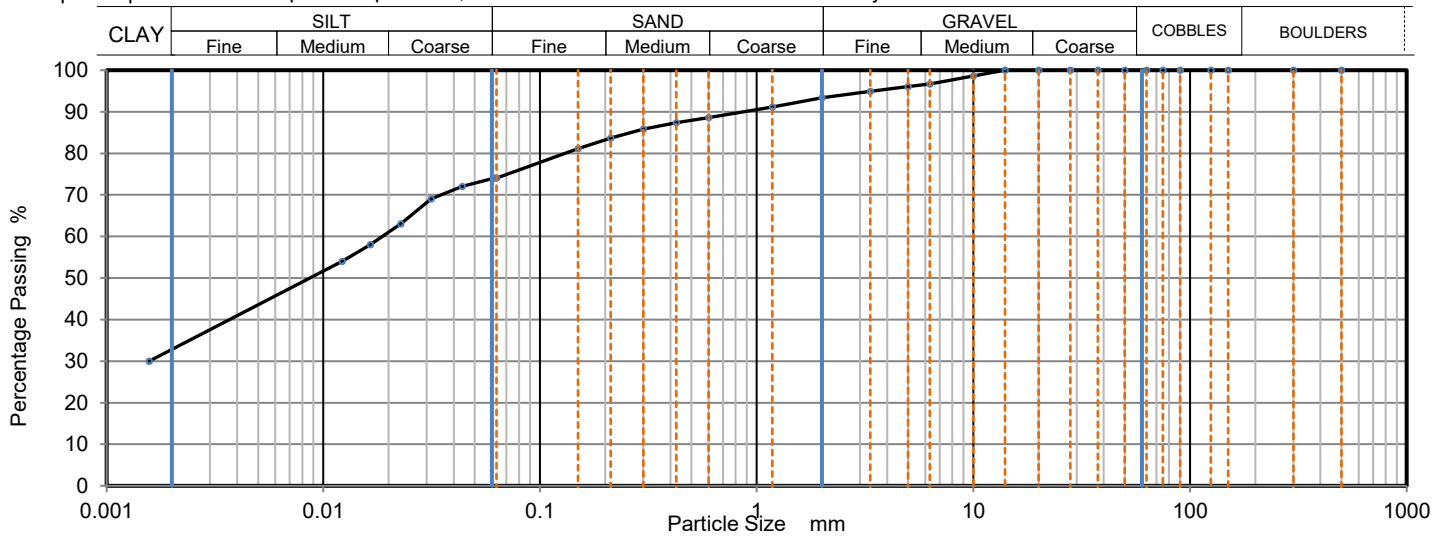
Sample Description: Grey slightly gravelly sandy very clayey SILT

Sample Preparation: Sample was quartered, oven dried at 106.4 °C and broken down by hand.

Depth Top [m]: 2.00

Depth Base [m]: 2.45

Sample Type: U



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0614	74
300	100	0.0438	72
150	100	0.0315	69
125	100	0.0228	63
90	100	0.0165	58
75	100	0.0122	54
63	100	0.0016	30
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	99		
6.3	97		
5	96		
3.35	95		
2	93	Particle density (measured) 2.70 Mg/m <sup>3</sup>	
1.18	91		
0.6	89		
0.425	87		
0.3	86		
0.212	84		
0.15	81		
0.063	74		

Sample Proportions	% dry mass
Very coarse	0
Gravel	7
Sand	19
Silt	41
Clay	33

Grading Analysis		
D100	mm	14
D60	mm	0.019
D30	mm	0.00162
D10	mm	
Uniformity Coefficient		> 12
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF PARTICLE SIZE DISTRIBUTION

Tested in Accordance with: BS 1377-2: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

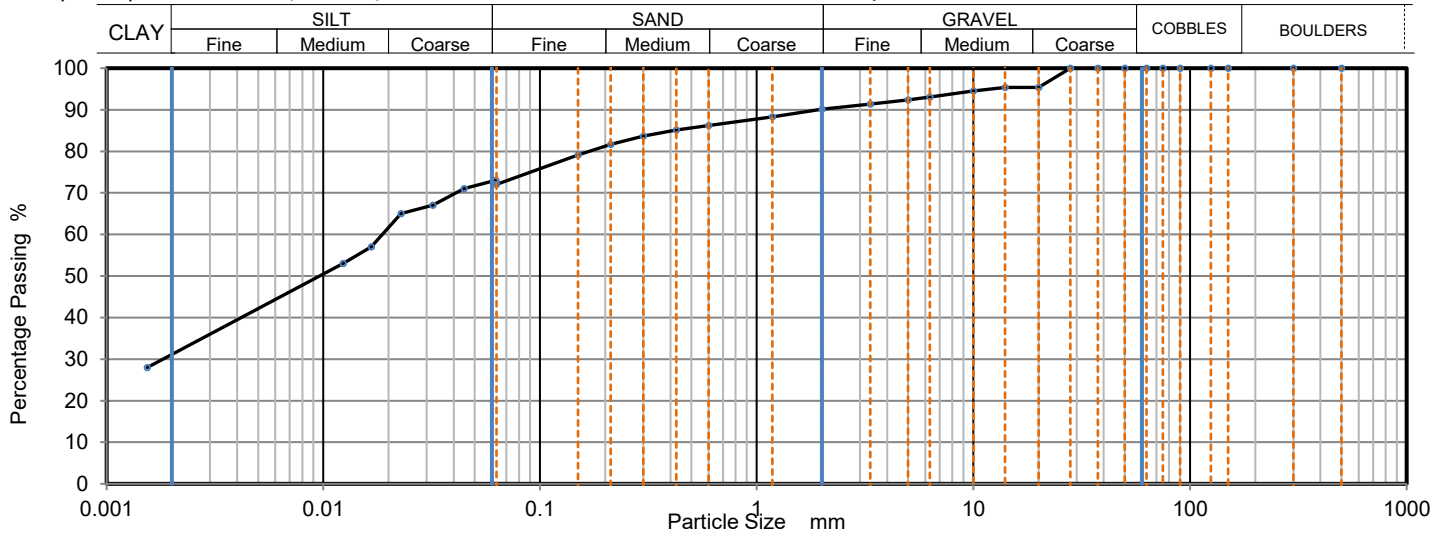
Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178523  
Hole No.: BH11  
Sample Reference: 2  
Sample Description: Greyish brown gravelly sandy very clayey SILT with fragments of chalk  
Sample Preparation: Sample was quartered, oven dried at 106.4 °C and broken down by hand.

Depth Top [m]: 4.00  
Depth Base [m]: 4.45  
Sample Type: U



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0625	73
300	100	0.0446	71
150	100	0.0320	67
125	100	0.0228	65
90	100	0.0166	57
75	100	0.0123	53
63	100	0.0015	28
50	100		
37.5	100		
28	100		
20	95		
14	95		
10	95		
6.3	93		
5	92		
3.35	91		
2	90	Particle density (measured) 2.69 Mg/m3	
1.18	88		
0.6	86		
0.425	85		
0.3	84		
0.212	82		
0.15	79		
0.063	73		

Sample Proportions	% dry mass
Very coarse	0
Gravel	10
Sand	17
Silt	42
Clay	31

Grading Analysis		
D100	mm	28
D60	mm	0.019
D30	mm	0.00179
D10	mm	
Uniformity Coefficient		> 12
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

*Katarzyna Koziel*

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF PARTICLE SIZE DISTRIBUTION

Tested in Accordance with: BS 1377-2: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

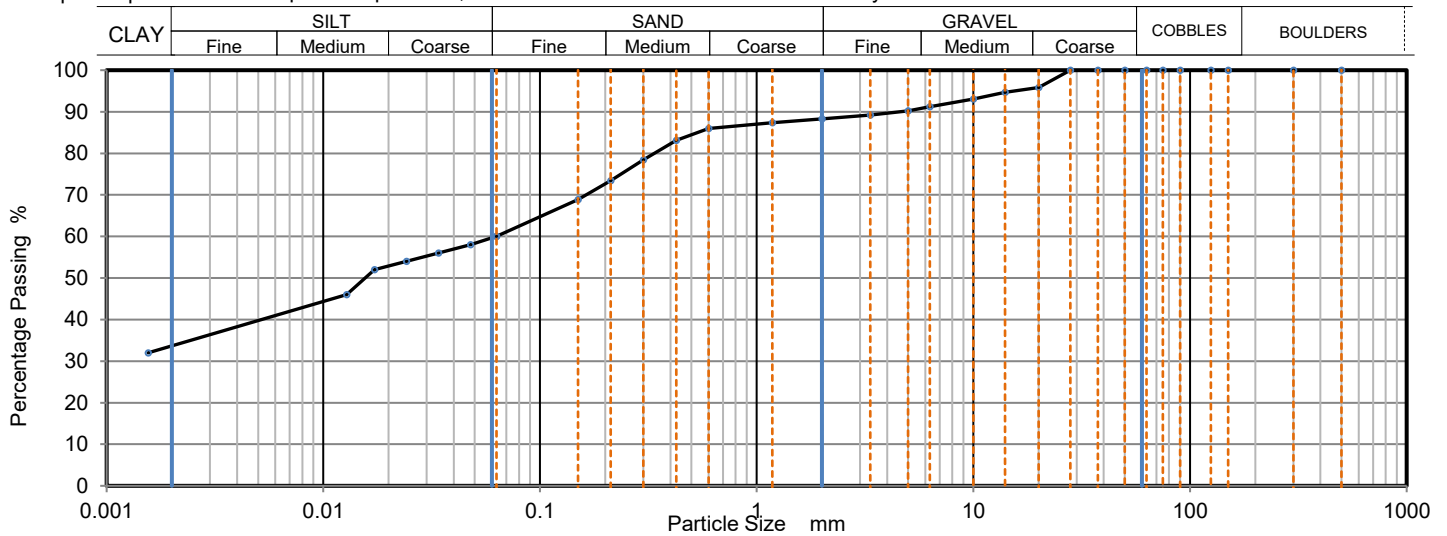
Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178524  
Hole No.: BH11  
Sample Reference: 3  
Sample Description: Grey to yellowish brown gravelly sandy very silty CLAY  
Sample Preparation: Sample was quartered, oven dried at 106.4 °C and broken down by hand.

Depth Top [m]: 11.00  
Depth Base [m]: 11.45  
Sample Type: U



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0630	60
300	100	0.0477	58
150	100	0.0340	56
125	100	0.0242	54
90	100	0.0172	52
75	100	0.0128	46
63	100	0.0016	32
50	100		
37.5	100		
28	100		
20	96		
14	95		
10	93		
6.3	91		
5	90		
3.35	89		
2	88	Particle density (assumed) 2.65 Mg/m <sup>3</sup>	
1.18	87		
0.6	86		
0.425	83		
0.3	78		
0.212	73		
0.15	69		
0.063	60		

Sample Proportions	% dry mass
Very coarse	0
Gravel	12
Sand	28
Silt	26
Clay	34

Grading Analysis		
D100	mm	28
D60	mm	0.0596
D30	mm	
D10	mm	
Uniformity Coefficient		> 38
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF DRY DENSITY/MOISTURE CONTENT RELATIONSHIP METHOD USING 2.5 KG RAMMER

Tested in Accordance with: BS 1377-4: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EFW

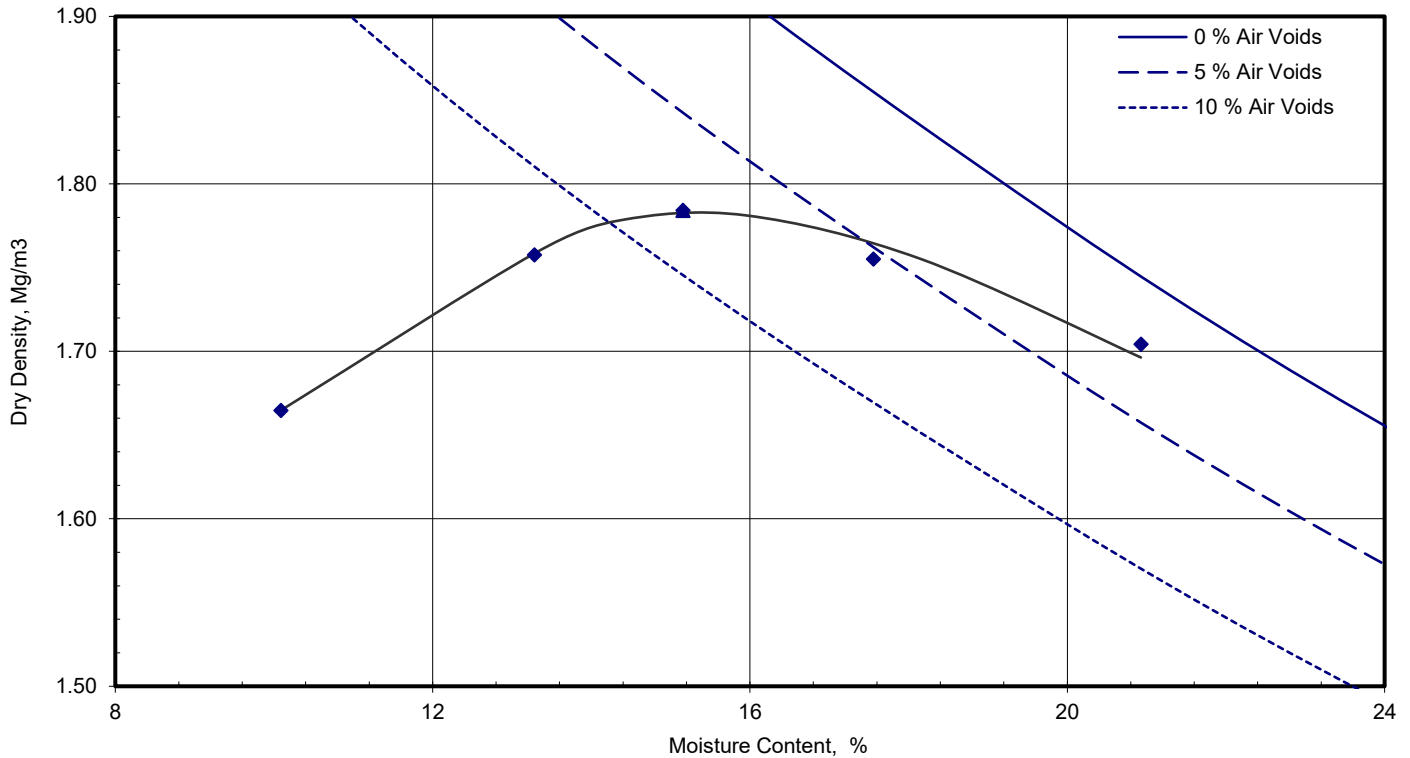
Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 04/02/2022  
Date Received: 08/02/2022  
Date Tested: 25/02/2022  
Sampled By: Not Given

### Test Results:

Laboratory Reference: 2178514  
Hole No.: TR-1  
Sample Reference: 1  
Sample Description: Brownish grey slightly gravelly sandy very silty CLAY  
Sample Preparation: Sample was quartered and broken down by hand. Material used was natural.

Depth Top [m]: 1.30  
Depth Base [m]: Not Given  
Sample Type: B



Compaction Point No.	1	2	3	4	5	
Moisture Content	%	10	13	15	18	21
Dry Density	Mg/m <sup>3</sup>	1.66	1.76	1.78	1.76	1.70

Mould Type	CBR	
Samples Used	Single sample tested	
Material Retained on 37.5 mm Sieve	%	0
Material Retained on 20.0 mm Sieve	%	1
Particle Density - Assumed	Mg/m <sup>3</sup>	2.75
As received Moisture Content	%	21
<b>Maximum Dry Density</b>	Mg/m <sup>3</sup>	<b>1.78</b>

<b>Optimum Moisture Content</b>	%	<b>15</b>
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Note: Tested in Accordance with BS 1377-4: 1990: Clause 3.4 using 2.5kg [light] Rammer

Remarks: Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF DRY DENSITY/MOISTURE CONTENT RELATIONSHIP METHOD USING 2.5 KG RAMMER

Tested in Accordance with: BS 1377-4: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EFW

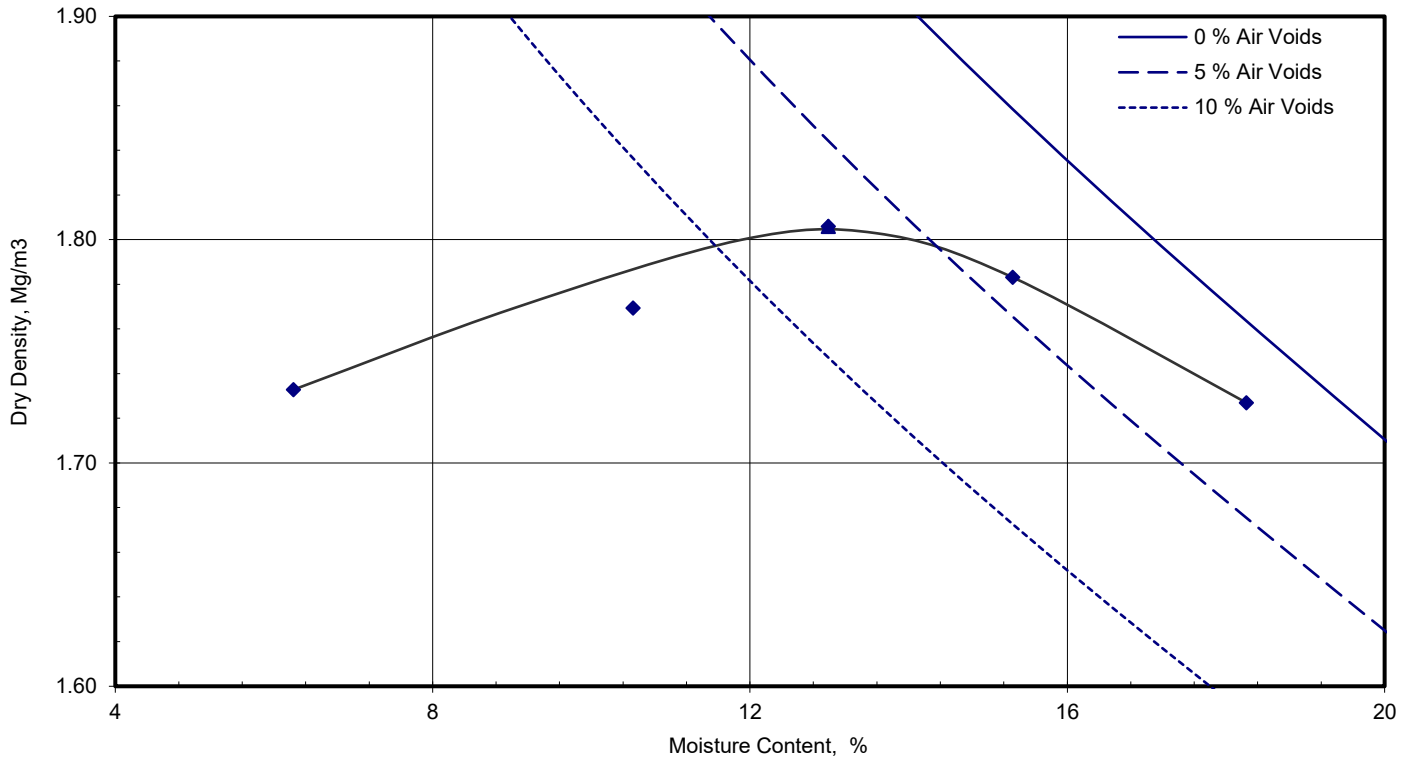
Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 04/02/2022  
Date Received: 08/02/2022  
Date Tested: 25/02/2022  
Sampled By: Not Given

### Test Results:

Laboratory Reference: 2178515  
Hole No.: TR-2  
Sample Reference: 1  
Sample Description: Brownish grey gravelly sandy very silty CLAY  
Sample Preparation: Sample was quartered and broken down by hand. Material used was natural.

Depth Top [m]: 0.40  
Depth Base [m]: Not Given  
Sample Type: B



Compaction Point No.	1	2	3	4	5	
Moisture Content	%	6.2	11	13	15	18
Dry Density	Mg/m <sup>3</sup>	1.73	1.77	1.81	1.78	1.73

Mould Type	CBR	
Samples Used	Single sample tested	
Material Retained on 37.5 mm Sieve	%	0
Material Retained on 20.0 mm Sieve	%	7
Particle Density - Assumed	Mg/m <sup>3</sup>	2.60
As received Moisture Content	%	20
<b>Maximum Dry Density</b>	Mg/m <sup>3</sup>	<b>1.81</b>

<b>Optimum Moisture Content</b>	%	<b>13</b>
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Note: Tested in Accordance with BS 1377-4: 1990: Clause 3.4 using 2.5kg [light] Rammer

Remarks: Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF DRY DENSITY/MOISTURE CONTENT RELATIONSHIP METHOD USING 2.5 KG RAMMER

Tested in Accordance with: BS 1377-4: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EFW

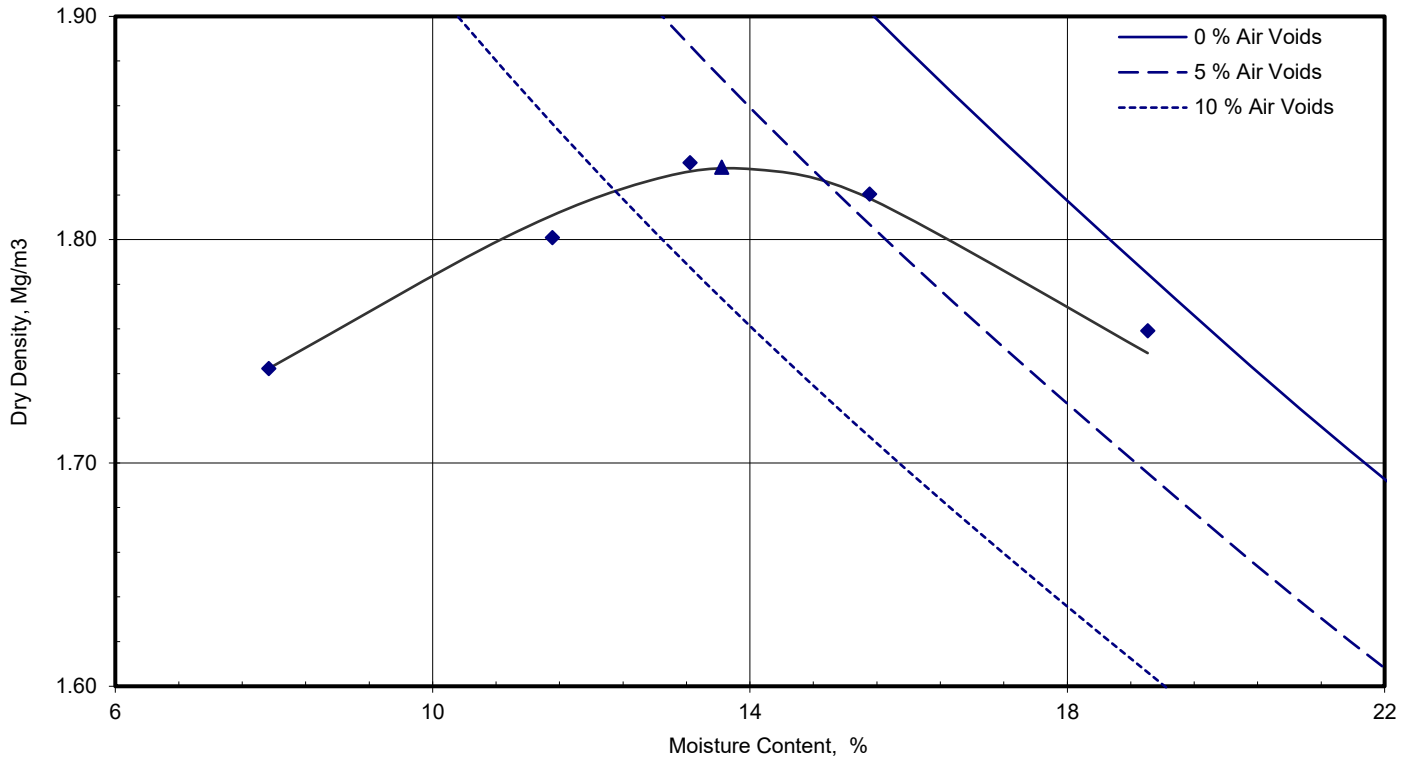
Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 04/02/2022  
Date Received: 08/02/2022  
Date Tested: 25/02/2022  
Sampled By: Not Given

### Test Results:

Laboratory Reference: 2178516  
Hole No.: TR-3  
Sample Reference: 1  
Sample Description: Grey gravelly sandy very silty CLAY  
Sample Preparation: Sample was quartered and broken down by hand. Material used was natural.

Depth Top [m]: 1.00  
Depth Base [m]: Not Given  
Sample Type: B



Compaction Point No.	1	2	3	4	5	
Moisture Content	%	7.9	12	13	16	19
Dry Density	Mg/m³	1.74	1.80	1.83	1.82	1.76

Mould Type	CBR	
Samples Used	Single sample tested	
Material Retained on 37.5 mm Sieve	%	0
Material Retained on 20.0 mm Sieve	%	2
Particle Density - Assumed	Mg/m³	2.70
As received Moisture Content	%	19
<b>Maximum Dry Density</b>	Mg/m³	<b>1.83</b>

<b>Optimum Moisture Content</b>	%	<b>14</b>
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Note: Tested in Accordance with BS 1377-4: 1990: Clause 3.4 using 2.5kg [light] Rammer

Remarks: Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF DRY DENSITY/MOISTURE CONTENT RELATIONSHIP METHOD USING 2.5 KG RAMMER

Tested in Accordance with: BS 1377-4: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EFW

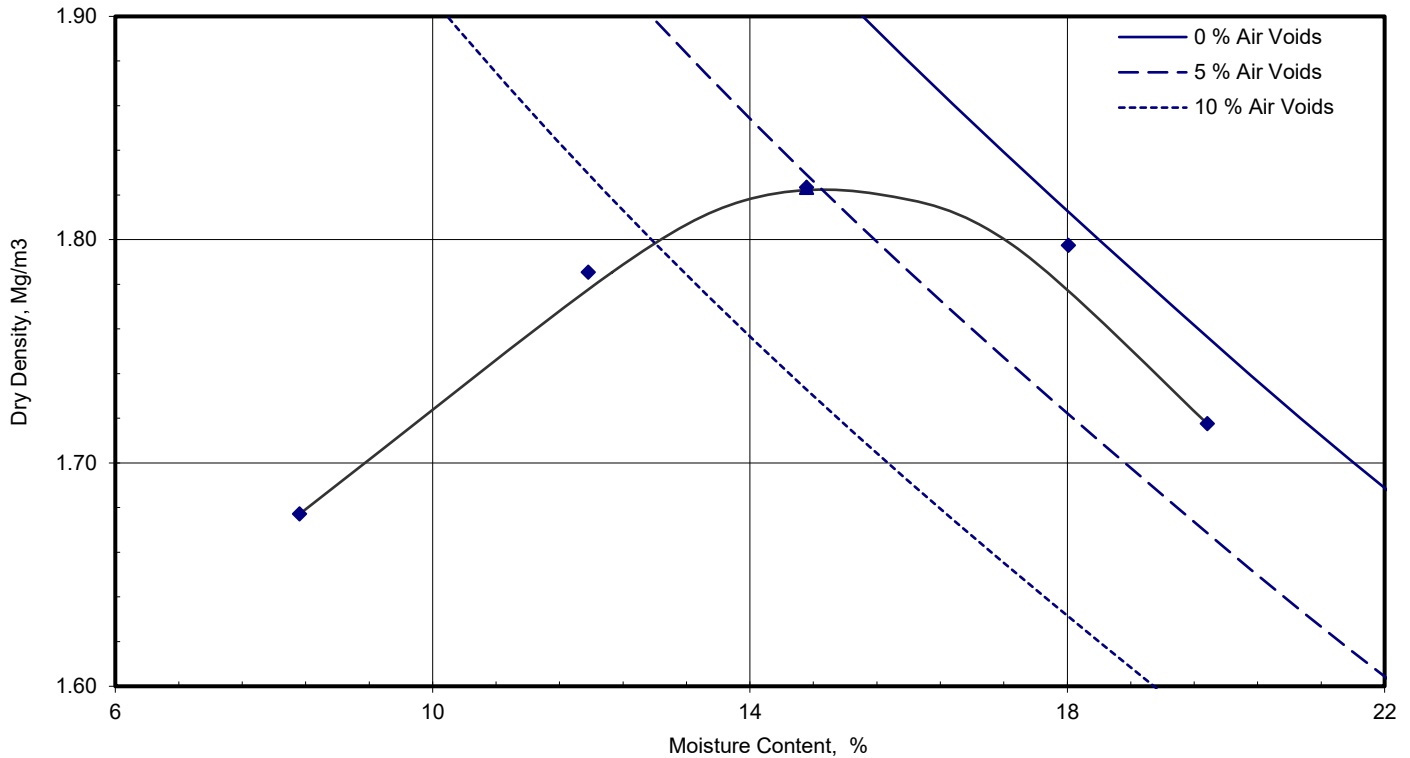
Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 04/02/2022  
Date Received: 08/02/2022  
Date Tested: 28/02/2022  
Sampled By: Not Given

### Test Results:

Laboratory Reference: 2178517  
Hole No.: TR-4A  
Sample Reference: 1  
Sample Description: Grey gravelly sandy very silty CLAY  
Sample Preparation: Sample was quartered and broken down by hand. Material used was natural.

Depth Top [m]: 0.60  
Depth Base [m]: Not Given  
Sample Type: B



Compaction Point No.	1	2	3	4	5	
Moisture Content	%	8.3	12	15	18	20
Dry Density	Mg/m <sup>3</sup>	1.68	1.79	1.82	1.80	1.72

Mould Type	CBR	
Samples Used	Single sample tested	
Material Retained on 37.5 mm Sieve	%	0
Material Retained on 20.0 mm Sieve	%	4
Particle Density - Measured using gas jar	Mg/m <sup>3</sup>	2.69
As received Moisture Content	%	19
<b>Maximum Dry Density</b>	Mg/m <sup>3</sup>	<b>1.82</b>

<b>Optimum Moisture Content</b>	%	<b>15</b>
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Note: Tested in Accordance with BS 1377-4: 1990: Clause 3.4 using 2.5kg [light] Rammer

Remarks: Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF DRY DENSITY/MOISTURE CONTENT RELATIONSHIP METHOD USING 2.5 KG RAMMER

Tested in Accordance with: BS 1377-4: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EFW

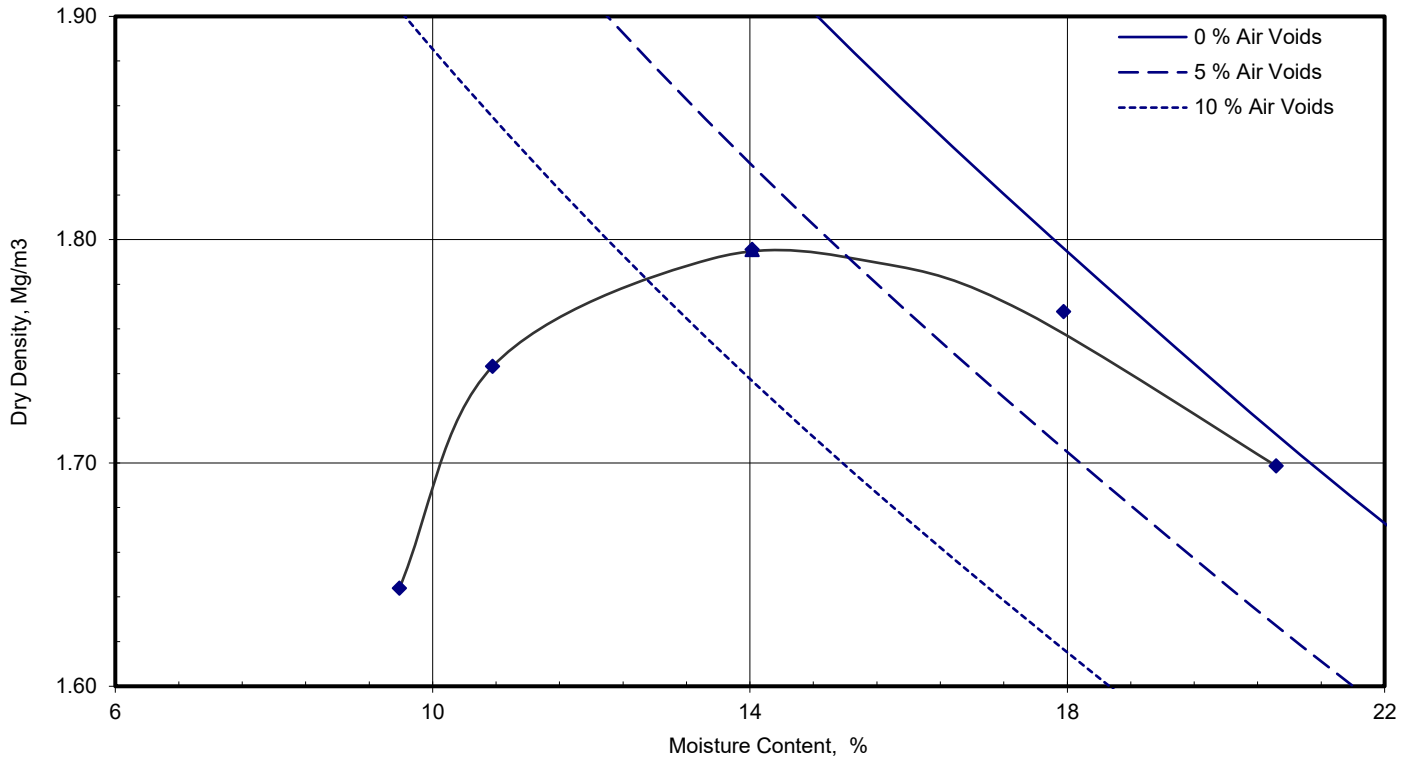
Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 04/02/2022  
Date Received: 08/02/2022  
Date Tested: 28/02/2022  
Sampled By: Not Given

### Test Results:

Laboratory Reference: 2178518  
Hole No.: TR-5  
Sample Reference: 2  
Sample Description: Greyish brown gravelly sandy very silty CLAY  
Sample Preparation: Sample was quartered and broken down by hand. Material used was natural.

Depth Top [m]: 0.50  
Depth Base [m]: Not Given  
Sample Type: B



Compaction Point No.	1	2	3	4	5	
Moisture Content	%	9.6	11	14	18	21
Dry Density	Mg/m³	1.64	1.74	1.80	1.77	1.70

Mould Type	CBR	
Samples Used	Single sample tested	
Material Retained on 37.5 mm Sieve	%	0
Material Retained on 20.0 mm Sieve	%	1
Particle Density - Assumed	Mg/m³	2.65
As received Moisture Content	%	19
<b>Maximum Dry Density</b>	Mg/m³	<b>1.80</b>

<b>Optimum Moisture Content</b>	%	<b>14</b>
---------------------------------	---	-----------

Note: Tested in Accordance with BS 1377-4: 1990: Clause 3.4 using 2.5kg [light] Rammer

Remarks: Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF THE CALIFORNIA BEARING RATIO (CBR)

Tested in Accordance with: BS 1377-4: 1990: Clause 7

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EFW

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 04/02/2022  
Date Received: 08/02/2022  
Date Tested: 28/02/2022  
Sampled By: Not Given

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178514  
Hole No.: TR-1  
Sample Reference: 1  
Sample Description: Brownish grey slightly gravelly sandy very silty CLAY

Depth Top [m]: 1.30  
Depth Base [m]: Not Given  
Sample Type: B

### Specimen Preparation:

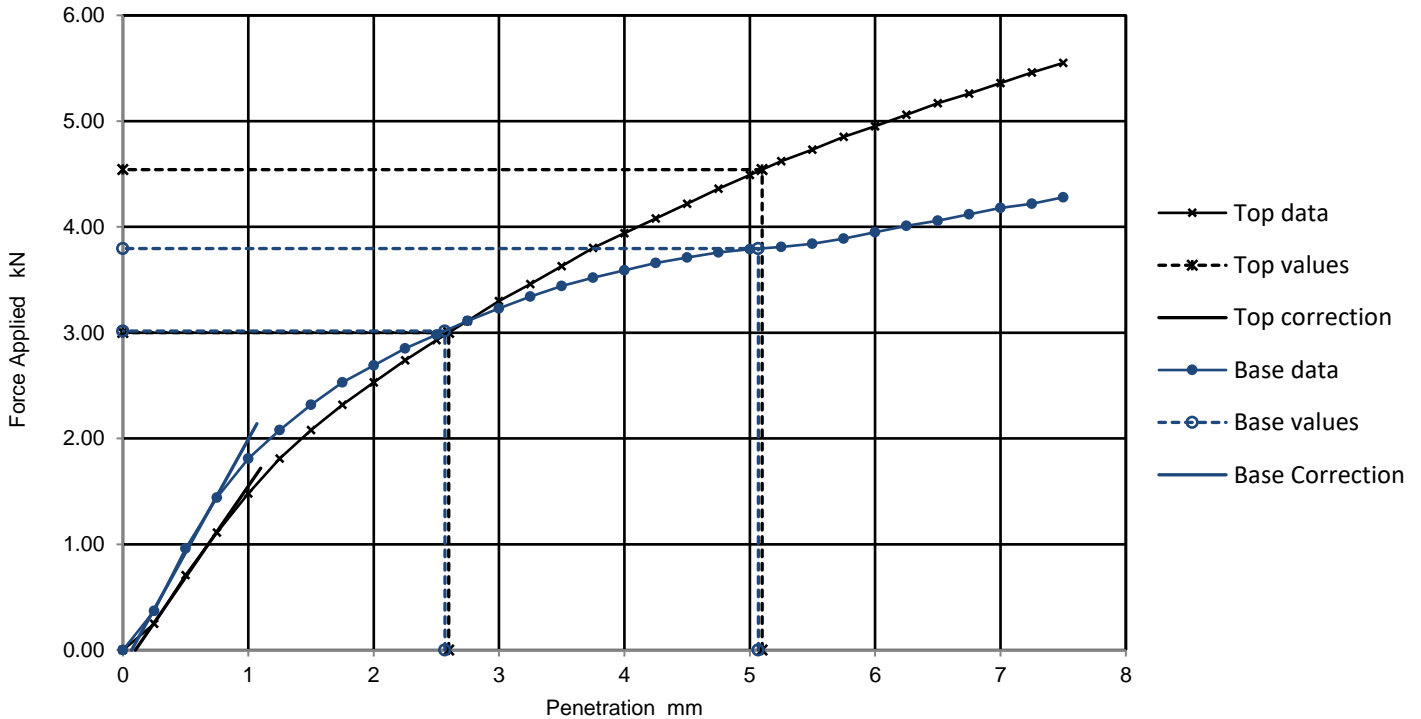
Condition Remoulded  
Details Recompacted with specified standard effort using 2.5kg rammer

Soaking details Not soaked  
Period of soaking days  
Time to surface days  
Amount of swell recorded mm  
Dry density after soaking Mg/m<sup>3</sup>

Material retained on 20mm sieve removed 1 %

Initial Specimen details Bulk density 2.05 Mg/m<sup>3</sup>  
Dry density 1.79 Mg/m<sup>3</sup>  
Moisture content 15 %  
Surcharge applied 8 kg  
4.8 kPa

Force v Penetration Plots



### Results

TOP  
BASE

Curve correction applied	CBR Values, %			
	2.5mm	5mm	Highest	Average
Yes	23.0	23.0	23.0	23.0
Yes	23.0	19.0	23.0	

Moisture Content %
13
14

Remarks: CBR tested at OMC = 15% of MC.  
Preliminary report

Test/ Specimen specific remarks:

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF THE CALIFORNIA BEARING RATIO (CBR)

Tested in Accordance with: BS 1377-4: 1990: Clause 7

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EFW

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 04/02/2022  
Date Received: 08/02/2022  
Date Tested: 28/02/2022  
Sampled By: Not Given

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178515  
Hole No.: TR-2  
Sample Reference: 1  
Sample Description: Brownish grey gravelly sandy very silty CLAY

Depth Top [m]: 0.40  
Depth Base [m]: Not Given  
Sample Type: B

### Specimen Preparation:

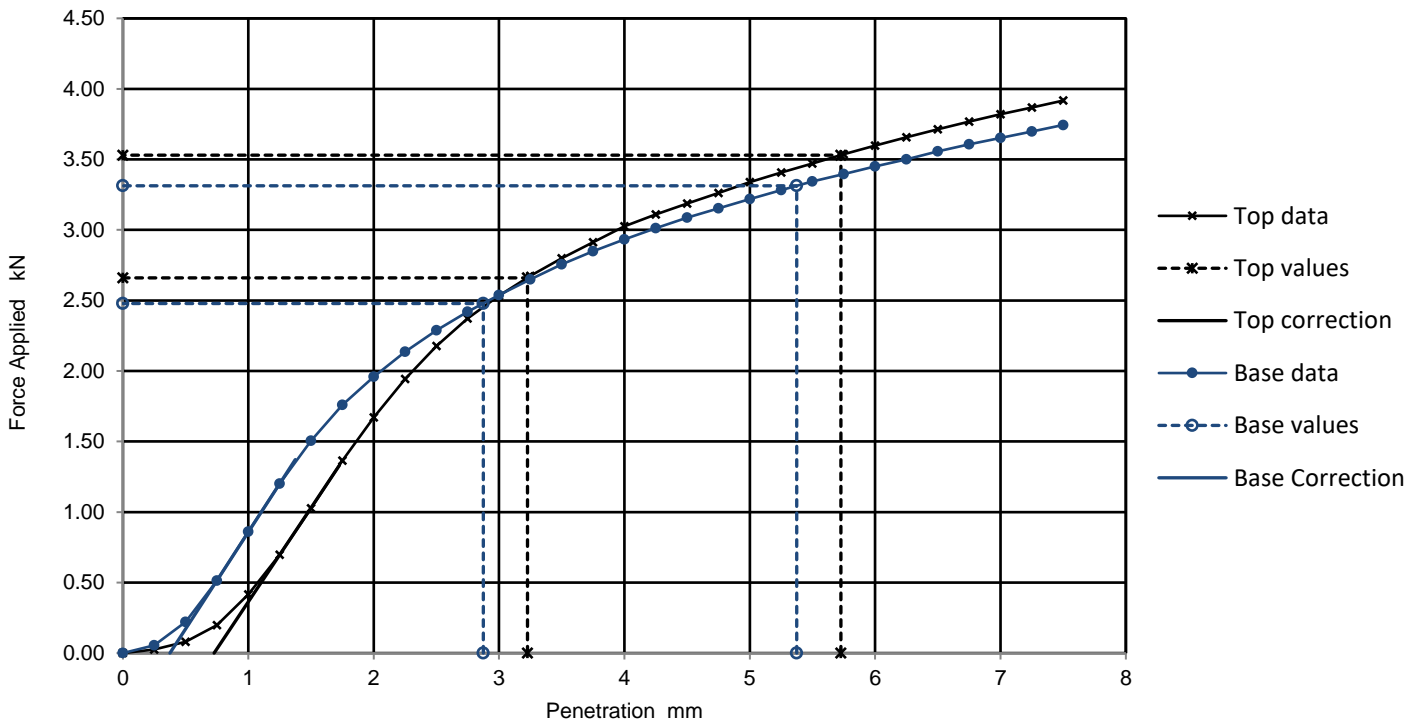
Condition Remoulded  
Details Recompacted with specified standard effort using 2.5kg rammer

Soaking details Not soaked  
Period of soaking days  
Time to surface days  
Amount of swell recorded mm  
Dry density after soaking Mg/m<sup>3</sup>

Material retained on 20mm sieve removed 8 %

Initial Specimen details Bulk density 2.04 Mg/m<sup>3</sup>  
Dry density 1.81 Mg/m<sup>3</sup>  
Moisture content 13 %  
Surcharge applied 8 kg  
4.9 kPa

Force v Penetration Plots



### Results

	Curve correction applied	CBR Values, %				Moisture Content %
		2.5mm	5mm	Highest	Average	
TOP	Yes	20.0	18.0	20.0	19.0	13
BASE	Yes	19.0	17.0	19.0		13

Remarks: CBR tested at OMC = 13% of MC.  
Preliminary report

Test/ Specimen specific remarks:

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF THE CALIFORNIA BEARING RATIO (CBR)

Tested in Accordance with: BS 1377-4: 1990: Clause 7

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EFW

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 04/02/2022  
Date Received: 08/02/2022  
Date Tested: 28/02/2022  
Sampled By: Not Given

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178516  
Hole No.: TR-3  
Sample Reference: 1  
Sample Description: Grey gravelly sandy very silty CLAY

Depth Top [m]: 1.00  
Depth Base [m]: Not Given  
Sample Type: B

### Specimen Preparation:

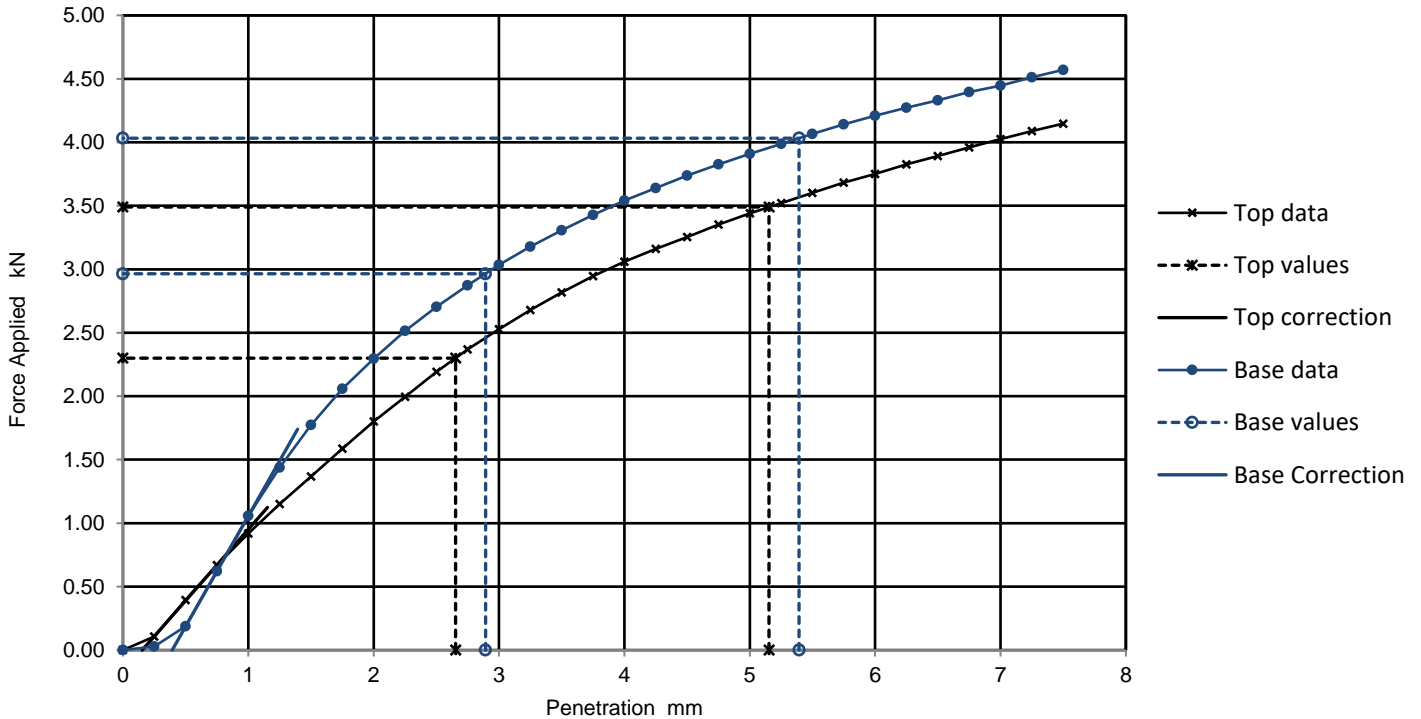
Condition Remoulded  
Details Recompacted with specified standard effort using 2.5kg rammer

Soaking details Not soaked  
Period of soaking days  
Time to surface days  
Amount of swell recorded mm  
Dry density after soaking Mg/m<sup>3</sup>

Material retained on 20mm sieve removed 2 %

Initial Specimen details Bulk density 2.08 Mg/m<sup>3</sup>  
Dry density 1.84 Mg/m<sup>3</sup>  
Moisture content 13 %  
Surcharge applied 8 kg  
4.9 kPa

Force v Penetration Plots



### Results

TOP  
BASE

Curve correction applied	CBR Values, %			
	2.5mm	5mm	Highest	Average
Yes	17.0	17.0	17.0	
Yes	22.0	20.0	22.0	

Moisture Content %
13
12

Remarks: CBR tested at OMC = 14% of MC.  
Preliminary report

Test/ Specimen specific remarks:

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF THE CALIFORNIA BEARING RATIO (CBR)

Tested in Accordance with: BS 1377-4: 1990: Clause 7

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 04/02/2022  
Date Received: 08/02/2022  
Date Tested: 28/02/2022  
Sampled By: Not Given

### Test Results:

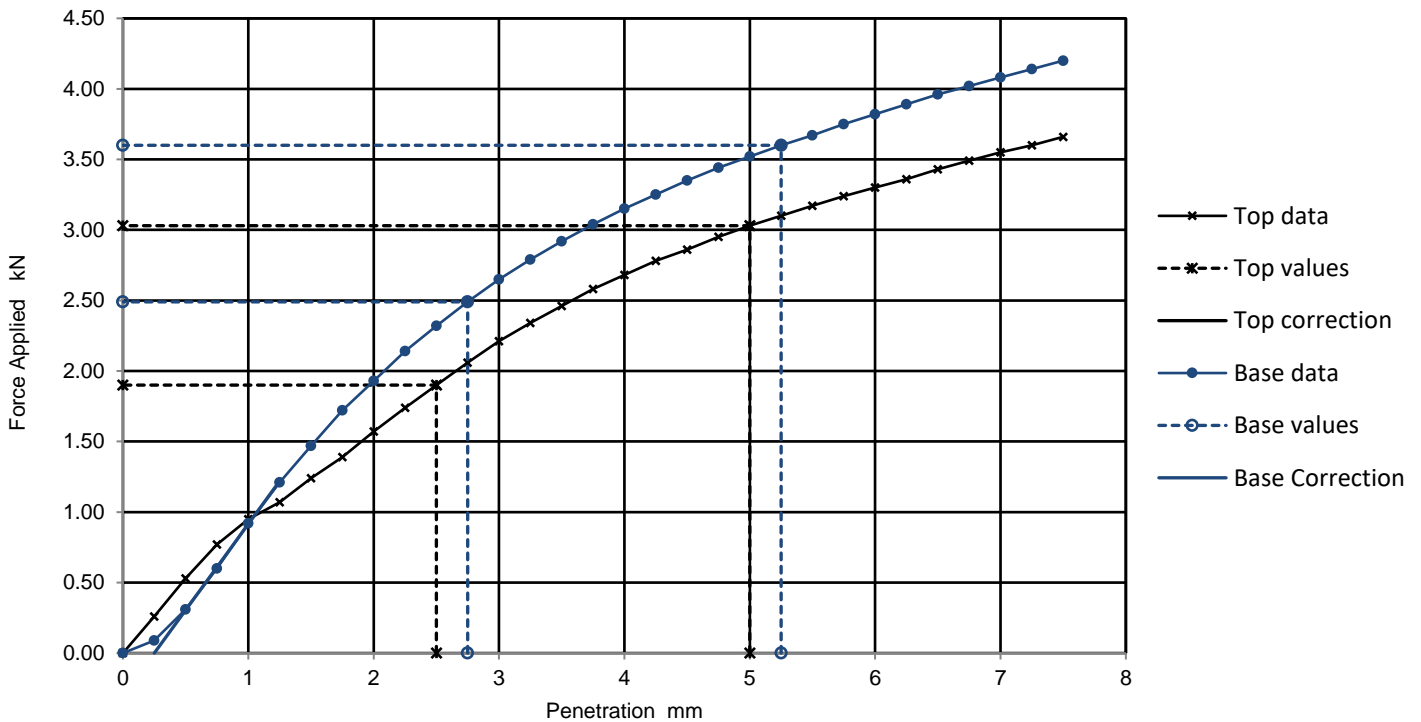
Laboratory Reference: 2178517  
Hole No.: TR-4A  
Sample Reference: 1  
Sample Description: Grey gravelly sandy very silty CLAY

Depth Top [m]: 0.60  
Depth Base [m]: Not Given  
Sample Type: B

### Specimen Preparation:

Condition	Remoulded	Soaking details	Not soaked
Details	Recompacted with specified standard effort using 2.5kg rammer	Period of soaking	days
		Time to surface	days
		Amount of swell recorded	mm
Material retained on 20mm sieve removed	4 %	Dry density after soaking	Mg/m <sup>3</sup>
Initial Specimen details	Bulk density 2.09 Mg/m <sup>3</sup>	Surcharge applied	8 kg
	Dry density 1.82 Mg/m <sup>3</sup>		4.9 kPa
	Moisture content 15 %		

Force v Penetration Plots



### Results

	Curve correction applied	CBR Values, %				Moisture Content %
		2.5mm	5mm	Highest	Average	
TOP	No	14.0	15.0	15.0		15
BASE	Yes	19.0	18.0	19.0		14

Remarks: CBR tested at OMC = 15% of MC.  
Preliminary report

Test/ Specimen specific remarks:

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

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Tested in Accordance with: BS 1377-4: 1990: Clause 7

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EFW

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 04/02/2022  
Date Received: 08/02/2022  
Date Tested: 28/02/2022  
Sampled By: Not Given

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178518  
Hole No.: TR-5  
Sample Reference: 2  
Sample Description: Greyish brown gravelly sandy very silty CLAY

Depth Top [m]: 0.50  
Depth Base [m]: Not Given  
Sample Type: B

### Specimen Preparation:

Condition Remoulded  
Details Recompacted with specified standard effort using 2.5kg rammer

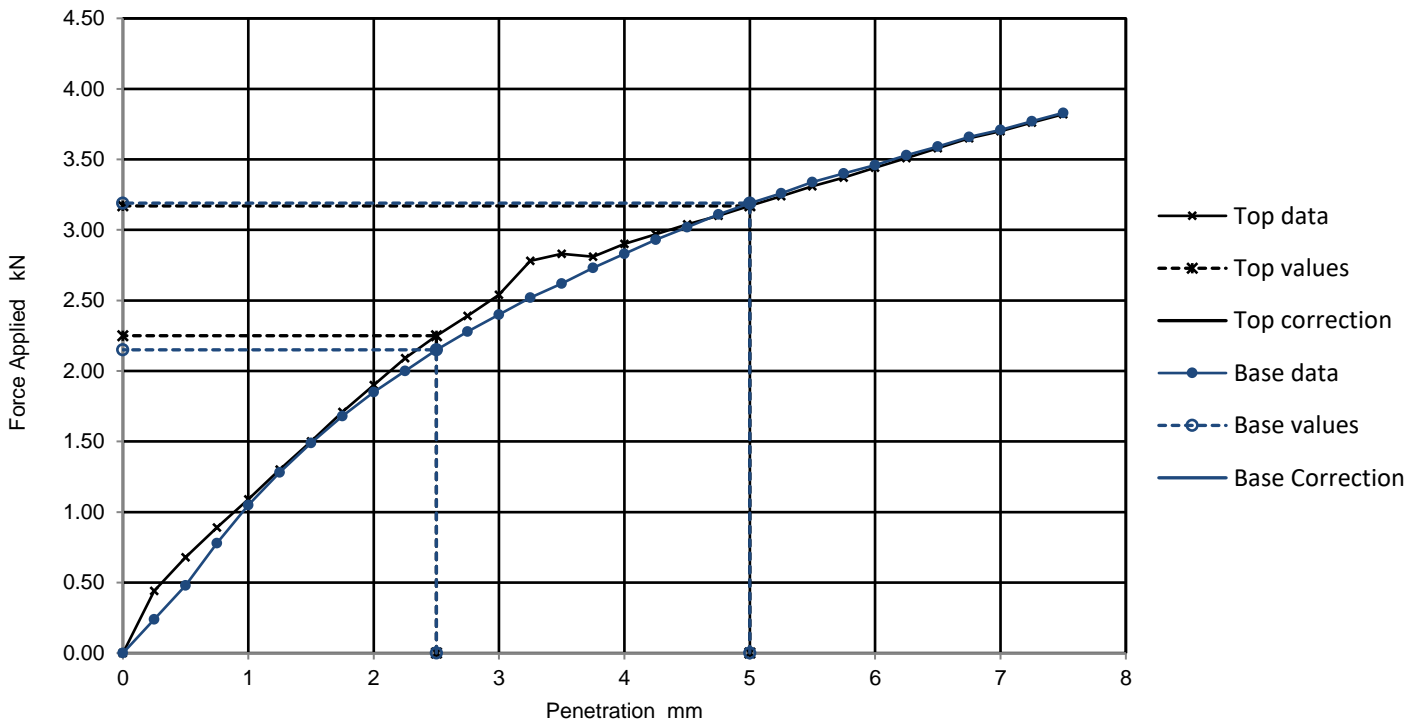
Soaking details Not soaked  
Period of soaking days  
Time to surface days  
Amount of swell recorded mm  
Dry density after soaking Mg/m<sup>3</sup>

Material retained on 20mm sieve removed 1 %

Initial Specimen details Bulk density 2.05 Mg/m<sup>3</sup>  
Dry density 1.80 Mg/m<sup>3</sup>  
Moisture content 14 %

Surcharge applied 8 kg  
4.9 kPa

Force v Penetration Plots



### Results

	Curve correction applied	CBR Values, %				Moisture Content %
		2.5mm	5mm	Highest	Average	
TOP	No	17.0	16.0	17.0	17.0	15
BASE	No	16.0	16.0	16.0		14

Remarks: CBR tested at OMC = 14% of MC.  
Preliminary report

Test/ Specimen specific remarks:

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

**Test Results:**

Laboratory Reference: 2178519  
Hole No.: BH3  
Sample Reference: 1  
Sample Description: Greyish brown gravelly sandy very clayey SILT with fragments of chalk  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

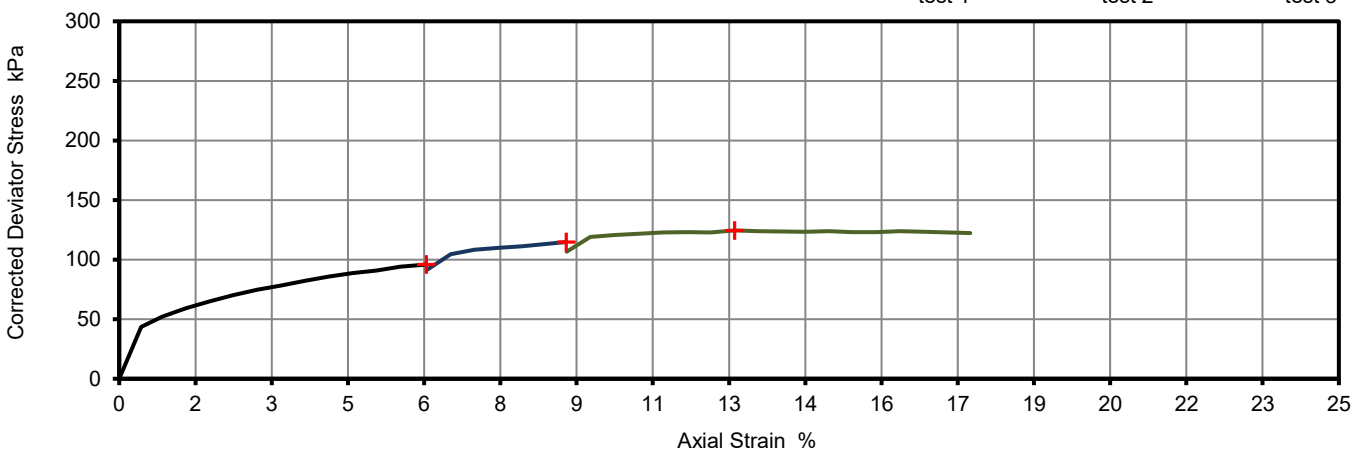
Depth Top [m]: 2.00  
Depth Base [m]: 2.45  
Sample Type: U

Length	140.10	mm
Diameter	69.50	mm
Bulk Density	2.11	Mg/m <sup>3</sup>
Moisture Content	22	%
Dry Density	1.74	Mg/m <sup>3</sup>
Membrane thickness	0.21	mm

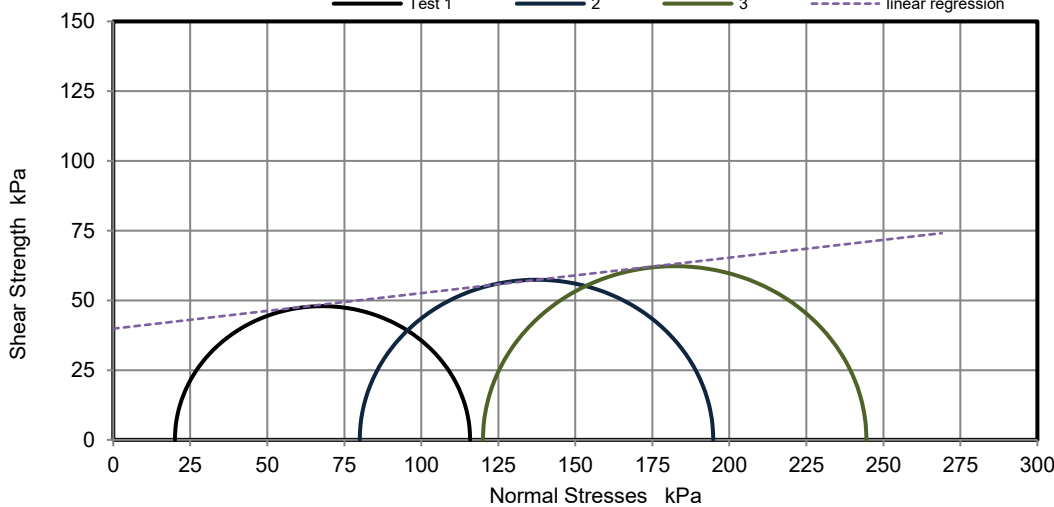
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )  
Shear strength, cu  
Mode of failure  
Membrane Correction

2.00			%/min
1	2	3	
20	80	120	kPa
6.3	9.2	12.6	%
96	115	125	kPa
48	57	62	kPa
Compound			
0.49	0.63	0.80	kPa

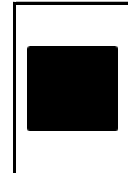
**Deviator Stress v Axial Strain**



**Mohr Circles**



Position within sample



Linear Regression  
 $\phi_u$  7.3 °  
cu 40 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 20kPa=12N, 80kPa=41N, 120kPa=62N.  
Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178520  
Hole No.: BH3  
Sample Reference: 2  
Sample Description: Grey gravelly sandy very silty CLAY with fragments of chalk  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

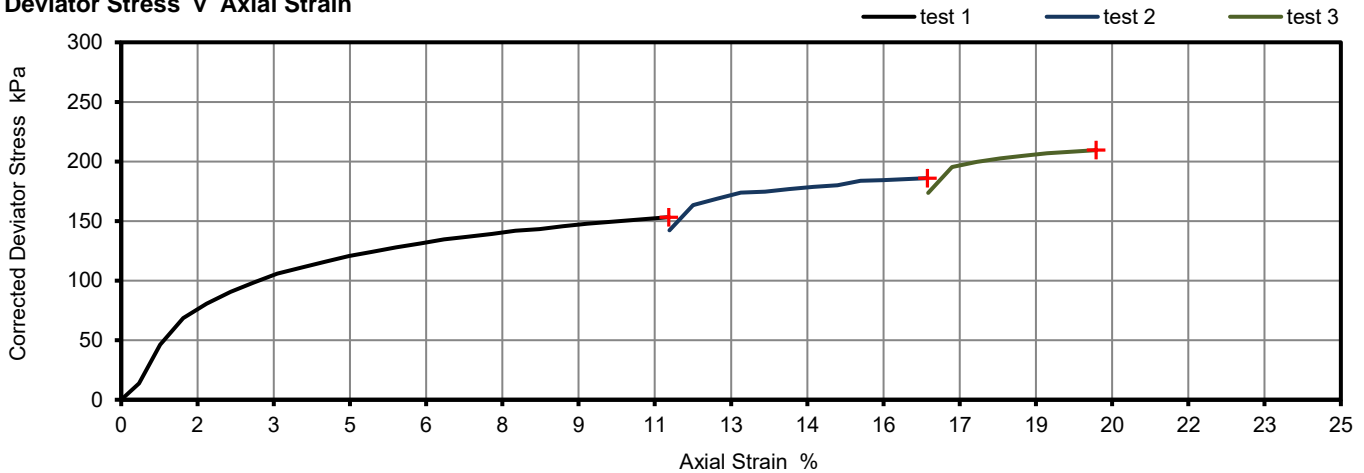
Depth Top [m]: 4.00  
Depth Base [m]: 4.45  
Sample Type: U

Length	141.40	mm
Diameter	69.45	mm
Bulk Density	2.09	Mg/m <sup>3</sup>
Moisture Content	18	%
Dry Density	1.77	Mg/m <sup>3</sup>
Membrane thickness	0.28	mm

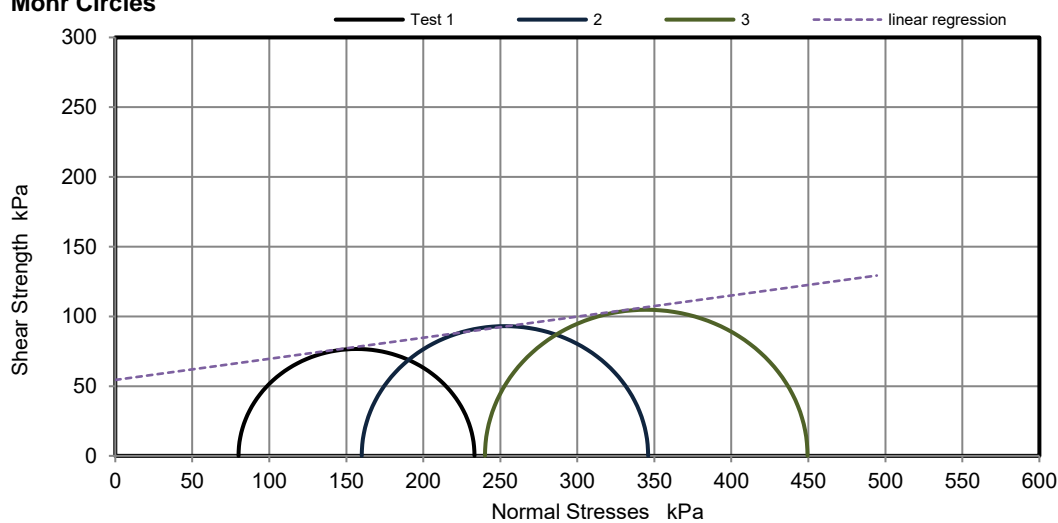
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )  
Shear strength,  $c_u$   
Mode of failure  
Membrane Correction

2.00			%/min
1	2	3	
80	160	240	kPa
11.2	16.5	20.0	%
153	186	209	kPa
77	93	105	kPa
Compound			
0.98	1.32	1.55	kPa

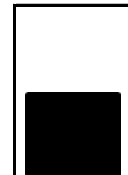
### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  8.6 °  
 $c_u$  54 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 80kPa=39N, 160kPa=77N, 240kPa=119N.  
Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

**Test Results:**

Laboratory Reference: 2178521  
Hole No.: BH3  
Sample Reference: 3  
Sample Description: Brownish grey slightly gravelly sandy very silty CLAY with fragments of chalk  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

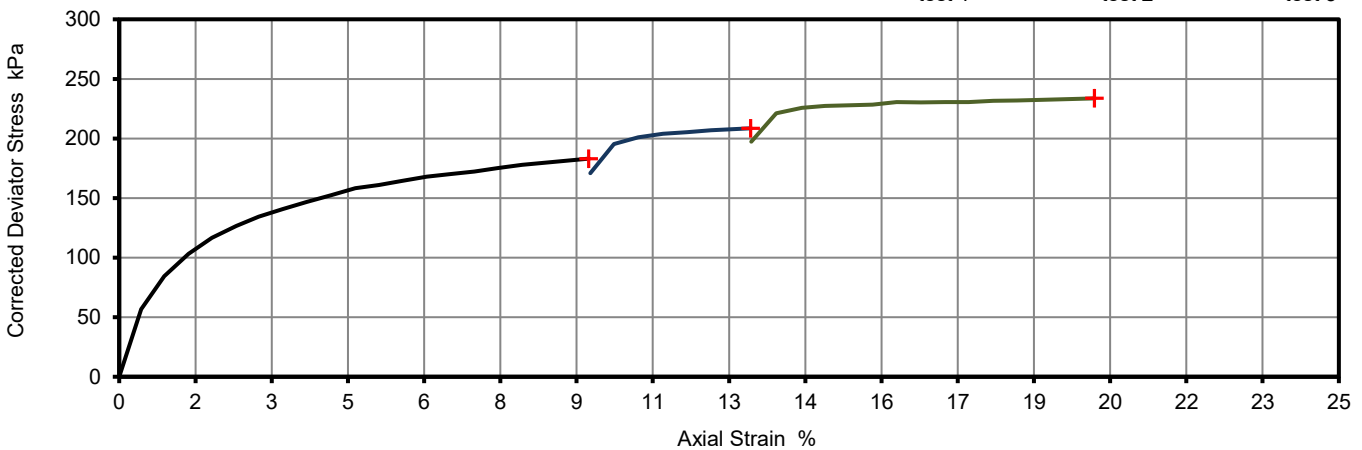
Depth Top [m]: 6.50  
Depth Base [m]: 6.95  
Sample Type: U

Length	140.32	mm
Diameter	68.93	mm
Bulk Density	2.11	Mg/m <sup>3</sup>
Moisture Content	21	%
Dry Density	1.74	Mg/m <sup>3</sup>
Membrane thickness	0.24	mm

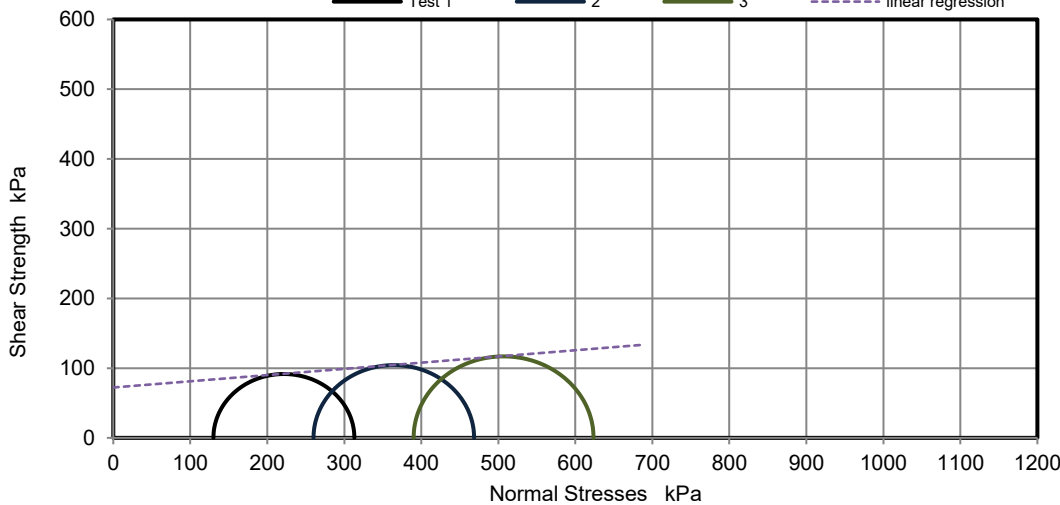
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )  
Shear strength, cu  
Mode of failure  
Membrane Correction

2.00			%/min
1	2	3	
130	260	390	kPa
9.6	12.9	20.0	%
183	209	234	kPa
92	104	117	kPa
Compound			
0.75	0.94	1.34	kPa

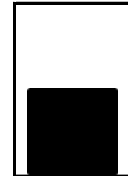
**Deviator Stress v Axial Strain**



**Mohr Circles**



Position within sample



Linear Regression  
 $\phi_u$  5.1 °  
cu 72 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 130kPa=67N, 260kPa=131N, 390kPa=189N.  
Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178522  
Hole No.: BH11  
Sample Reference: 1  
Sample Description: Grey slightly gravelly sandy very clayey SILT  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

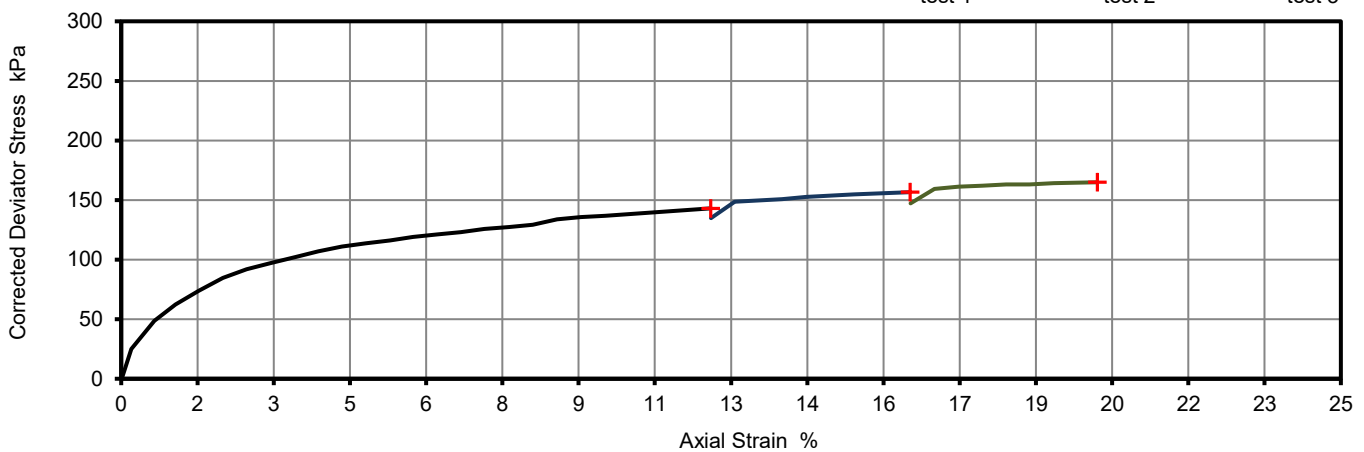
Depth Top [m]: 2.00  
Depth Base [m]: 2.45  
Sample Type: U

Length	140.55	mm
Diameter	69.16	mm
Bulk Density	2.13	Mg/m <sup>3</sup>
Moisture Content	19	%
Dry Density	1.79	Mg/m <sup>3</sup>
Membrane thickness	0.25	mm

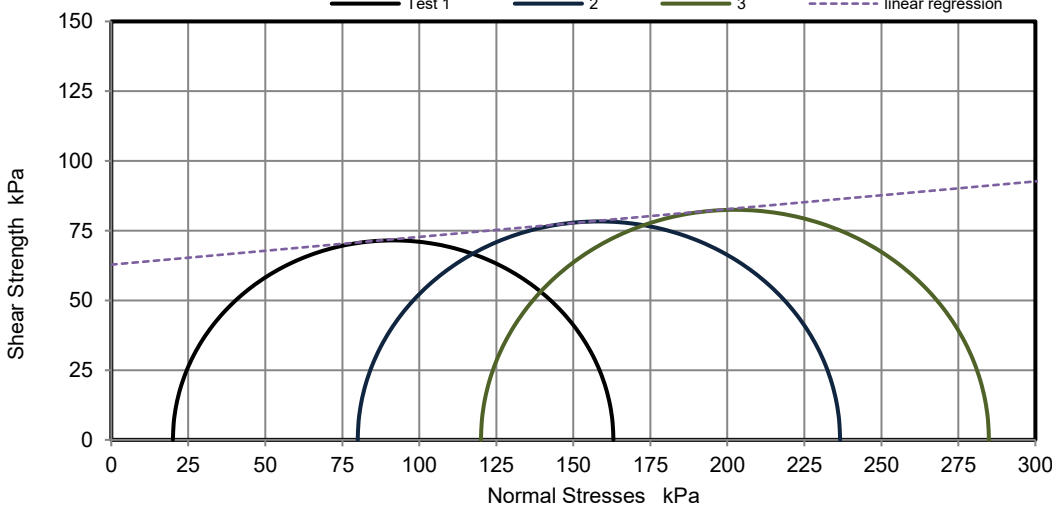
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )  
Shear strength,  $c_u$   
Mode of failure  
Membrane Correction

2.00			%/min
1	2	3	
20	80	120	kPa
12.1	16.2	20.0	%
143	157	165	kPa
72	78	82	kPa
Compound			
0.93	1.17	1.39	kPa

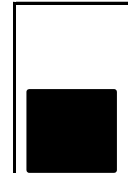
### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  5.7 °  
 $c_u$  63 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 20kPa=11N, 80kPa=40N, 120kPa=58N.  
Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178523  
Hole No.: BH11  
Sample Reference: 2  
Sample Description: Greyish brown gravelly sandy very clayey SILT with fragments of chalk  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

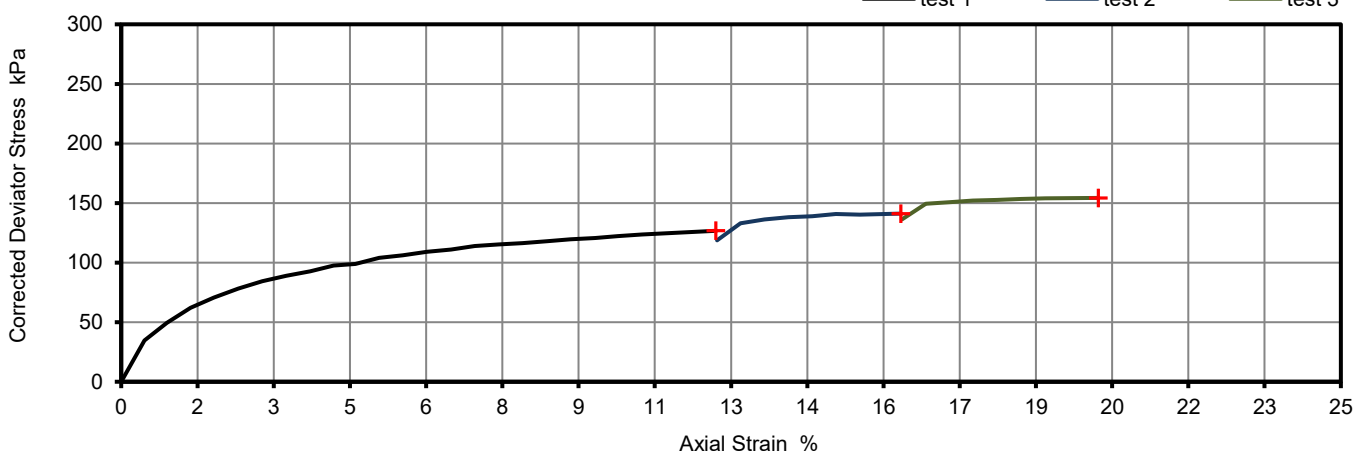
Depth Top [m]: 4.00  
Depth Base [m]: 4.45  
Sample Type: U

Length	141.24	mm
Diameter	69.10	mm
Bulk Density	2.08	Mg/m <sup>3</sup>
Moisture Content	20	%
Dry Density	1.73	Mg/m <sup>3</sup>
Membrane thickness	0.25	mm

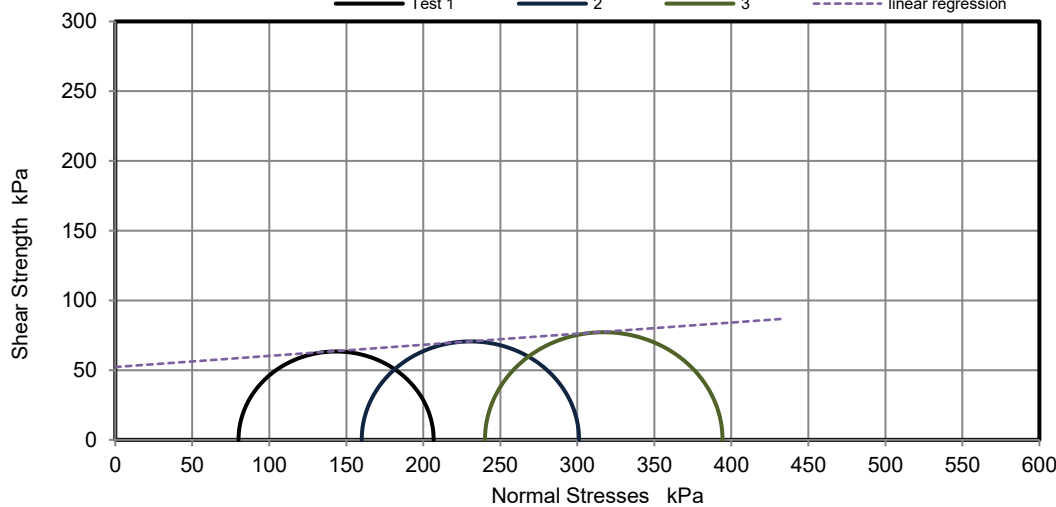
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )  
Shear strength, cu  
Mode of failure  
Membrane Correction

2.00			%/min
1	2	3	
80	160	240	kPa
12.2	16.0	20.0	%
127	141	154	kPa
63	71	77	kPa
Compound			
0.93	1.16	1.39	kPa

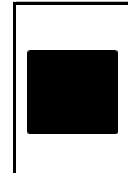
### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  4.6 °  
cu 52 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 80kPa=41N, 160kPa=80N, 240kPa=121N.  
Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15 0645 05  
Job Number: 22-40679  
Date Sampled: 07/02/2022  
Date Received: 08/02/2022  
Date Tested: 24/02/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EFW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2178524  
Hole No.: BH11  
Sample Reference: 3  
Sample Description: Grey to yellowish brown gravelly sandy very silty CLAY  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

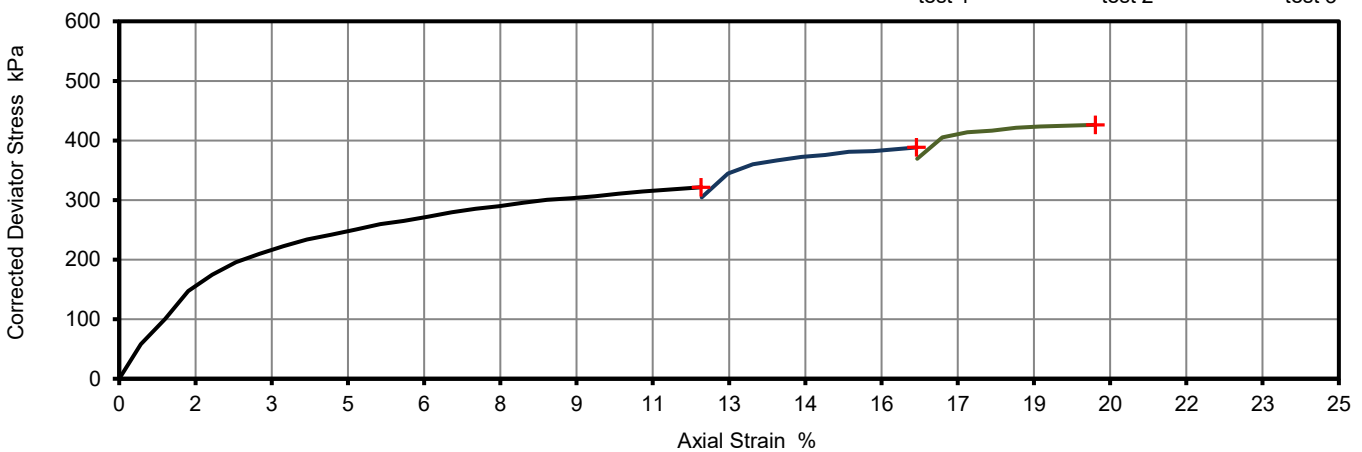
Depth Top [m]: 11.00  
Depth Base [m]: 11.45  
Sample Type: U

Length	141.29	mm
Diameter	69.24	mm
Bulk Density	2.14	Mg/m <sup>3</sup>
Moisture Content	16	%
Dry Density	1.84	Mg/m <sup>3</sup>
Membrane thickness	0.27	mm

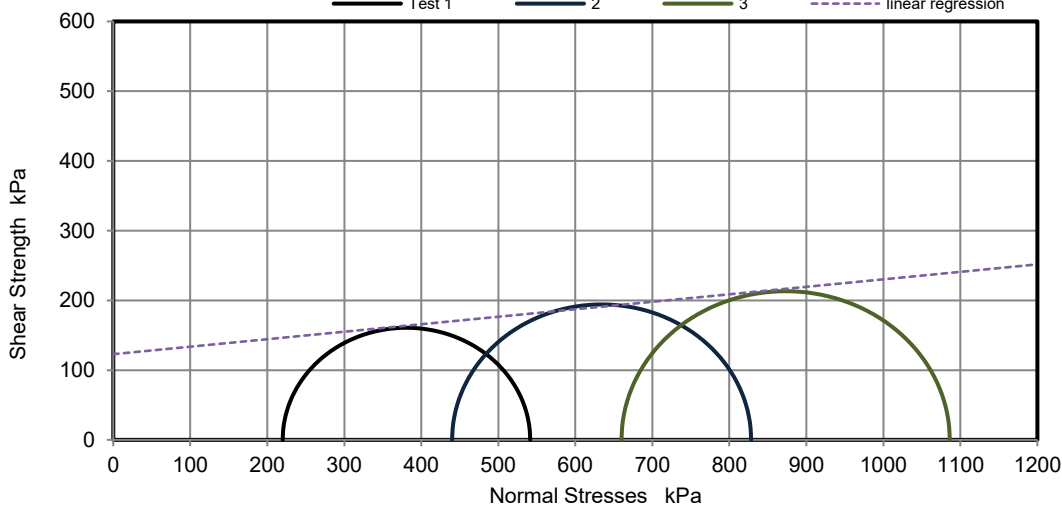
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )  
Shear strength,  $c_u$   
Mode of failure  
Membrane Correction

2.00			%/min
1	2	3	
220	440	660	kPa
11.9	16.3	20.0	%
321	388	426	kPa
161	194	213	kPa
Compound			
0.99	1.27	1.50	kPa

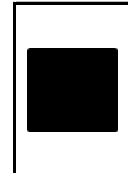
### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  6.1 °  
 $c_u$  123 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 220kPa=111N, 440kPa=219N, 660kPa=328N.  
Preliminary report

Signed:

Katarzyna Koziel  
Technical Reviewer  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 15/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

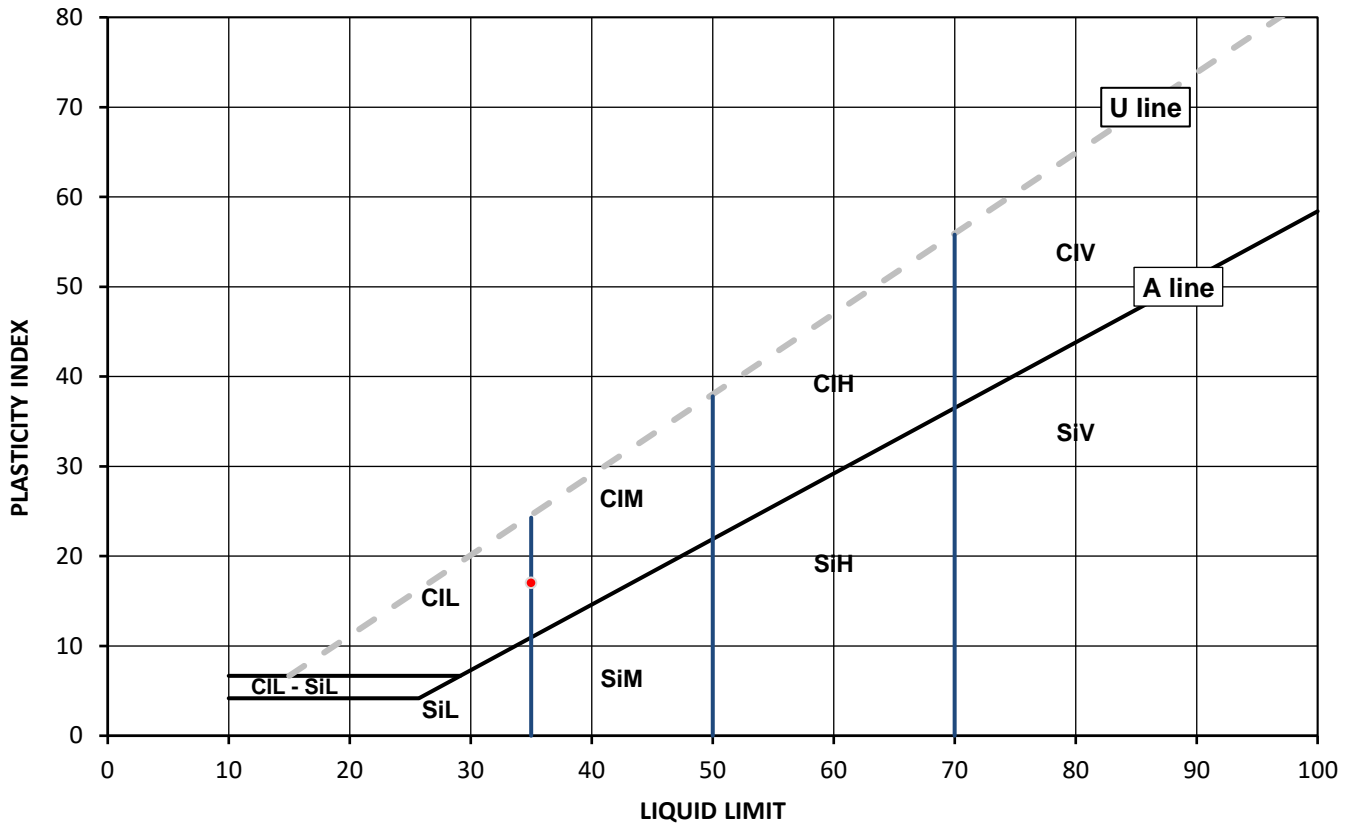
## Test Results:

Laboratory Reference: 2185934  
Hole No.: BH1  
Sample Reference: Not Given  
Sample Description: Multicolour slightly gravelly sandy CLAY

Depth Top [m]: 7.50  
Depth Base [m]: 7.95  
Sample Type: U

Sample Preparation: Tested after >425um removed by hand

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
15	35	18	17	98



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	Liquid Limit
Si	Silt	L	Low
		M	Medium
		H	High
		V	Very high
		O	Organic
			append to classification for organic material ( eg CIHO )
			below 35
			35 to 50
			50 to 70
			exceeding 70

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EfW

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 15/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

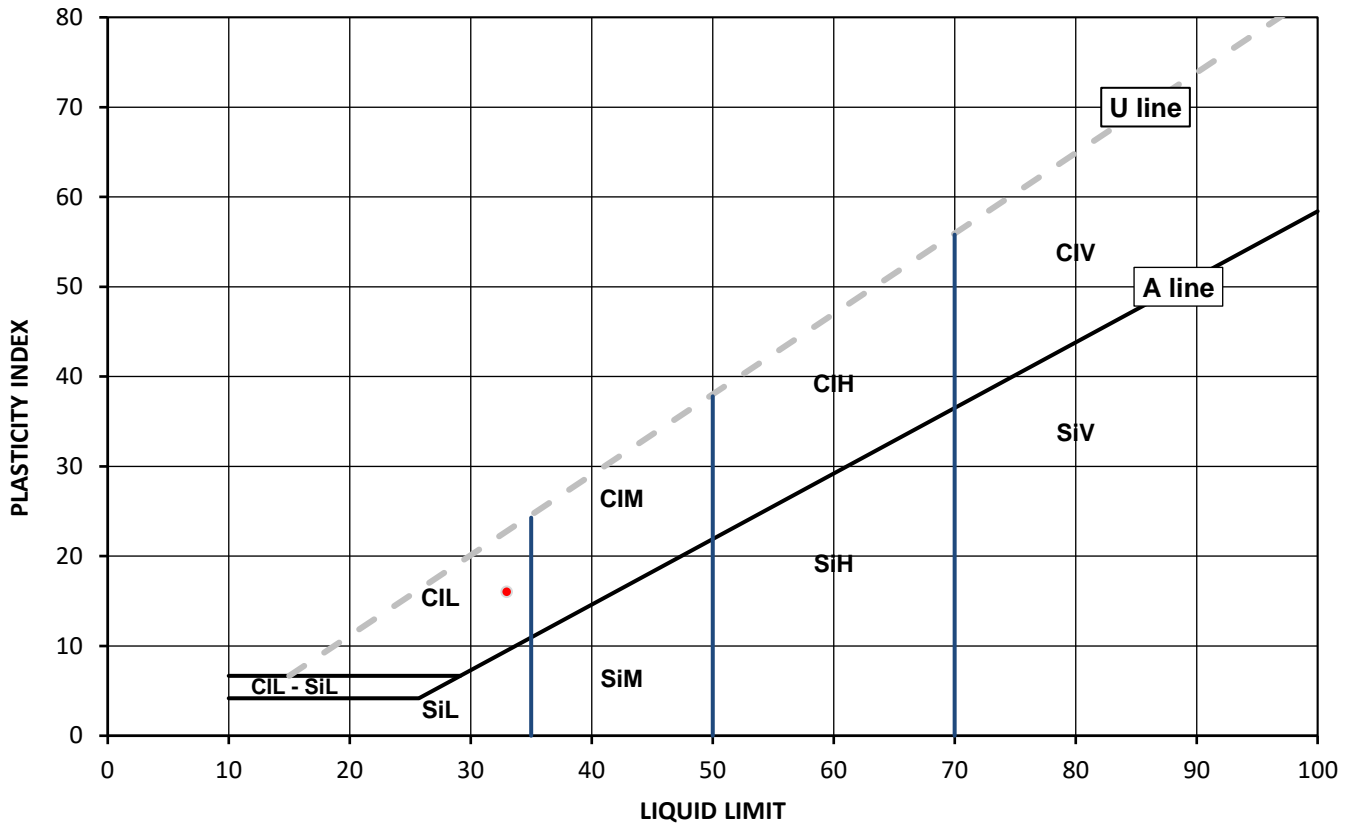
## Test Results:

Laboratory Reference: 2185935  
Hole No.: BH1  
Sample Reference: Not Given  
Sample Description: Multicolour slightly gravelly very sandy CLAY

Depth Top [m]: 12.00  
Depth Base [m]: 12.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
14	33	17	16	91



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	L	Low	Liquid Limit	below 35
Si	Silt		M	Medium		35 to 50
			H	High		50 to 70
			V	Very high		exceeding 70
			O	Organic		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 10/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

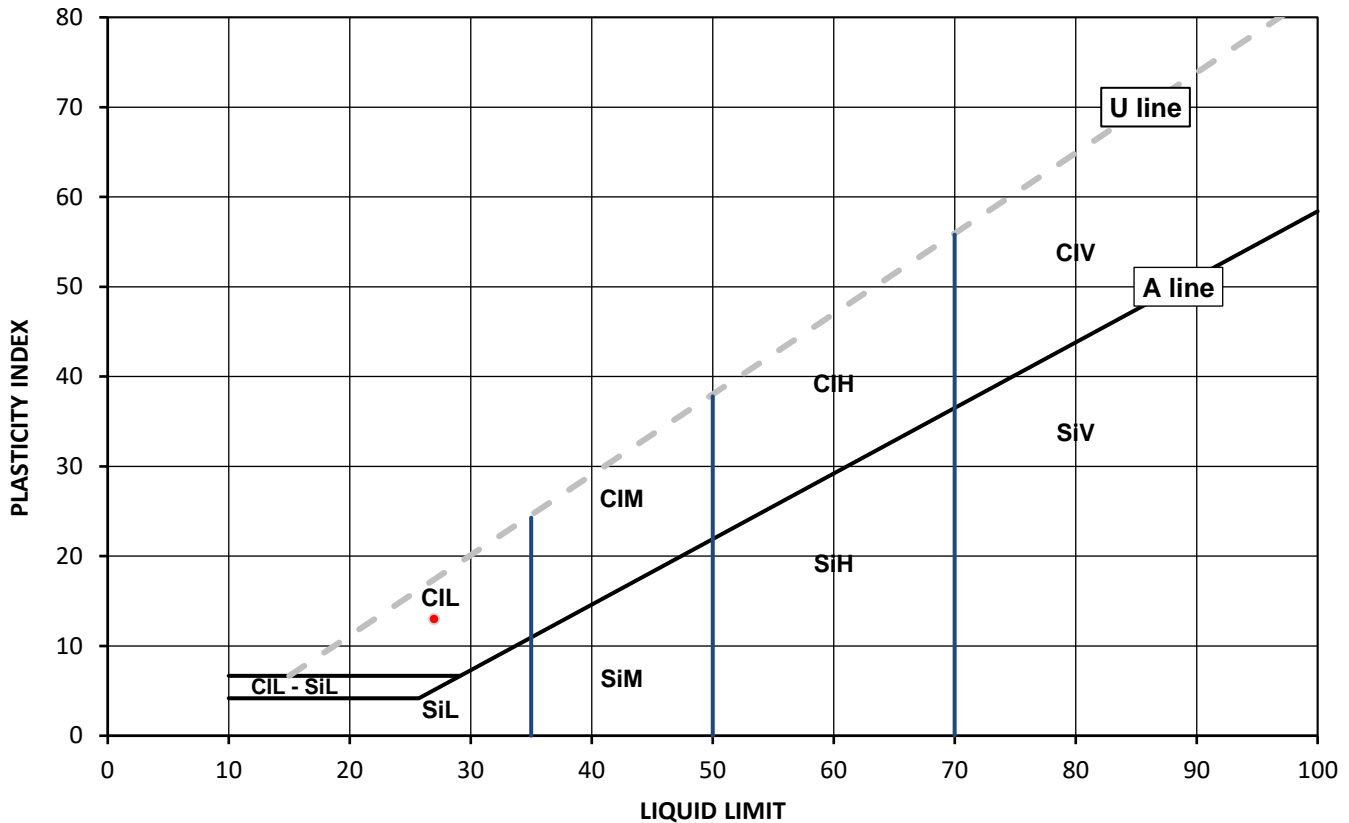
## Test Results:

Laboratory Reference: 2185937  
Hole No.: BH2  
Sample Reference: Not Given  
Sample Description: Yellowish brown to greyish brown slightly gravelly very sandy CLAY

Depth Top [m]: 8.00  
Depth Base [m]: 8.45  
Sample Type: U

Sample Preparation: Tested after >425um removed by hand

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
13	27	14	13	98



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

	Plasticity	Liquid Limit
Cl Clay	L Low	below 35
Si Silt	M Medium	35 to 50
	H High	50 to 70
	V Very high	exceeding 70
	O Organic	append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EfW

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 10/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

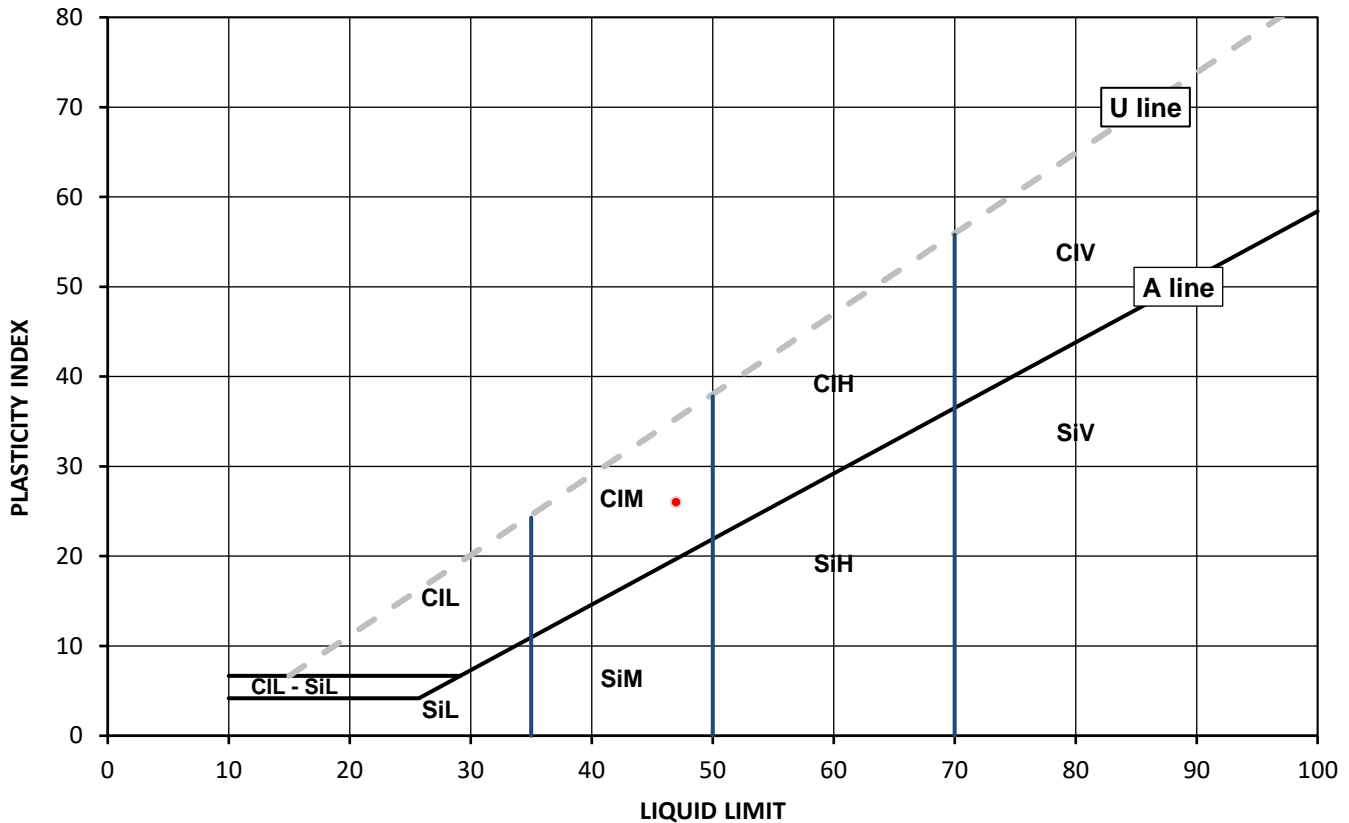
## Test Results:

Laboratory Reference: 2185938  
Hole No.: BH2  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly slightly sandy CLAY

Depth Top [m]: 15.50  
Depth Base [m]: 15.95  
Sample Type: U

Sample Preparation: Tested after >425um removed by hand

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
16	47	21	26	98



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	Liquid Limit
Si	Silt	L	Low
		M	Medium
		H	High
		V	Very high
		O	Organic
			append to classification for organic material ( eg CIHO )
			below 35
			35 to 50
			50 to 70
			exceeding 70

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

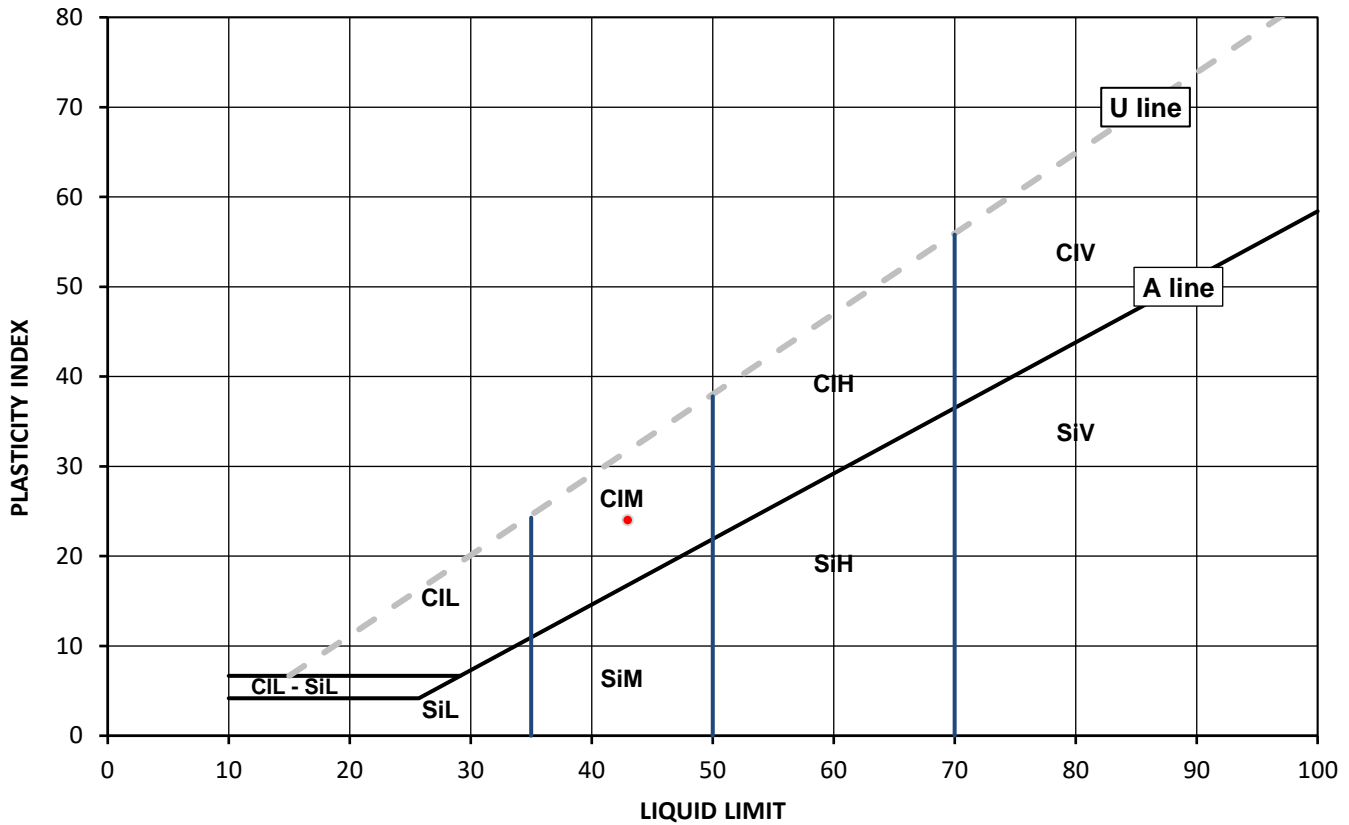
### Test Results:

Laboratory Reference: 2185958  
Hole No.: BH4  
Sample Reference: Not Given  
Sample Description: Grey slightly gravelly sandy CLAY with fragments of chalk

Depth Top [m]: 2.00  
Depth Base [m]: 2.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
20	43	19	24	94



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	L	Low	Liquid Limit	below 35
Si	Silt		M	Medium		35 to 50
			H	High		50 to 70
			V	Very high		exceeding 70
			O	Organic		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

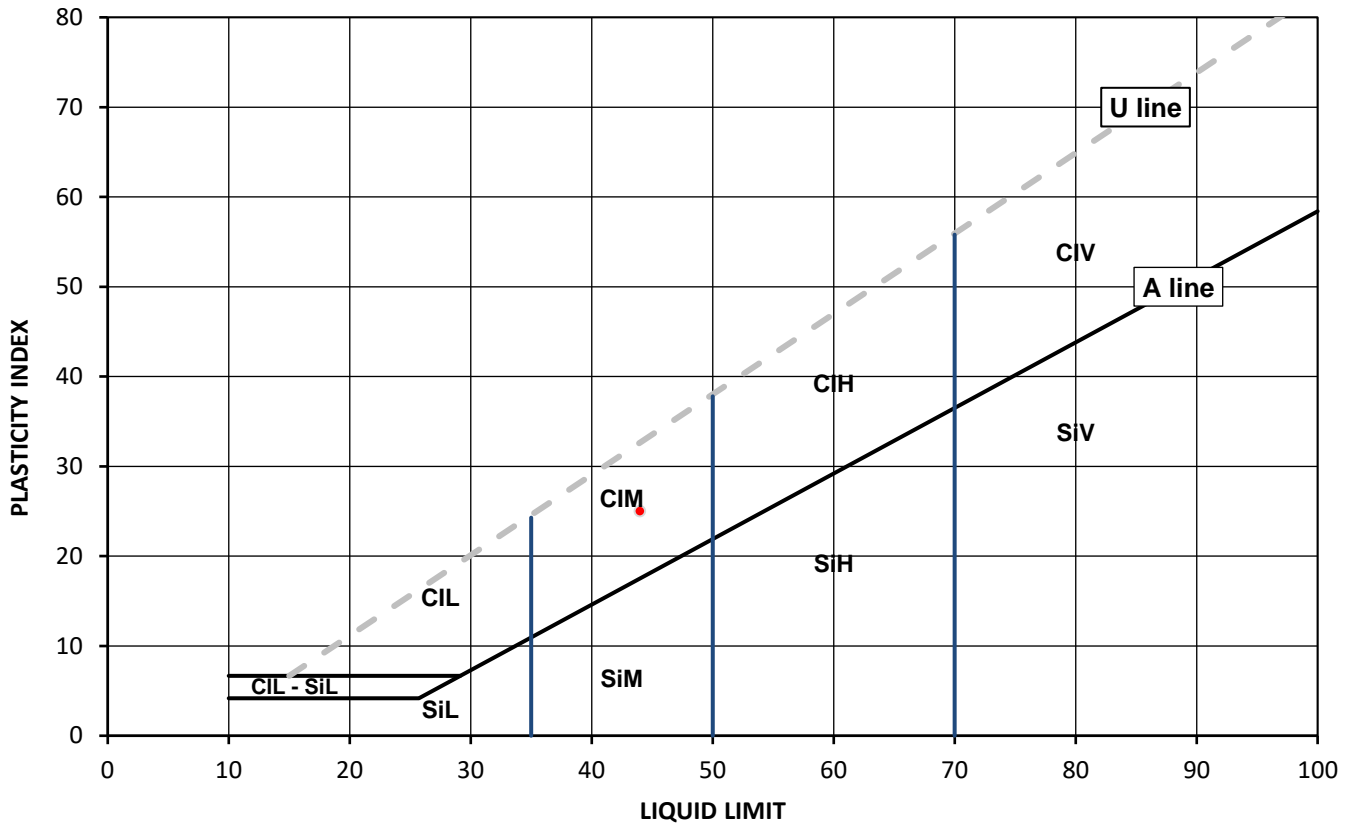
## Test Results:

Laboratory Reference: 2185960  
Hole No.: BH4  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY with fragments of chalk

Depth Top [m]: 4.00  
Depth Base [m]: 4.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
22	44	19	25	90



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	L	Low	Liquid Limit	below 35
Si	Silt		M	Medium		35 to 50
			H	High		50 to 70
			V	Very high		exceeding 70
			O	Organic		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

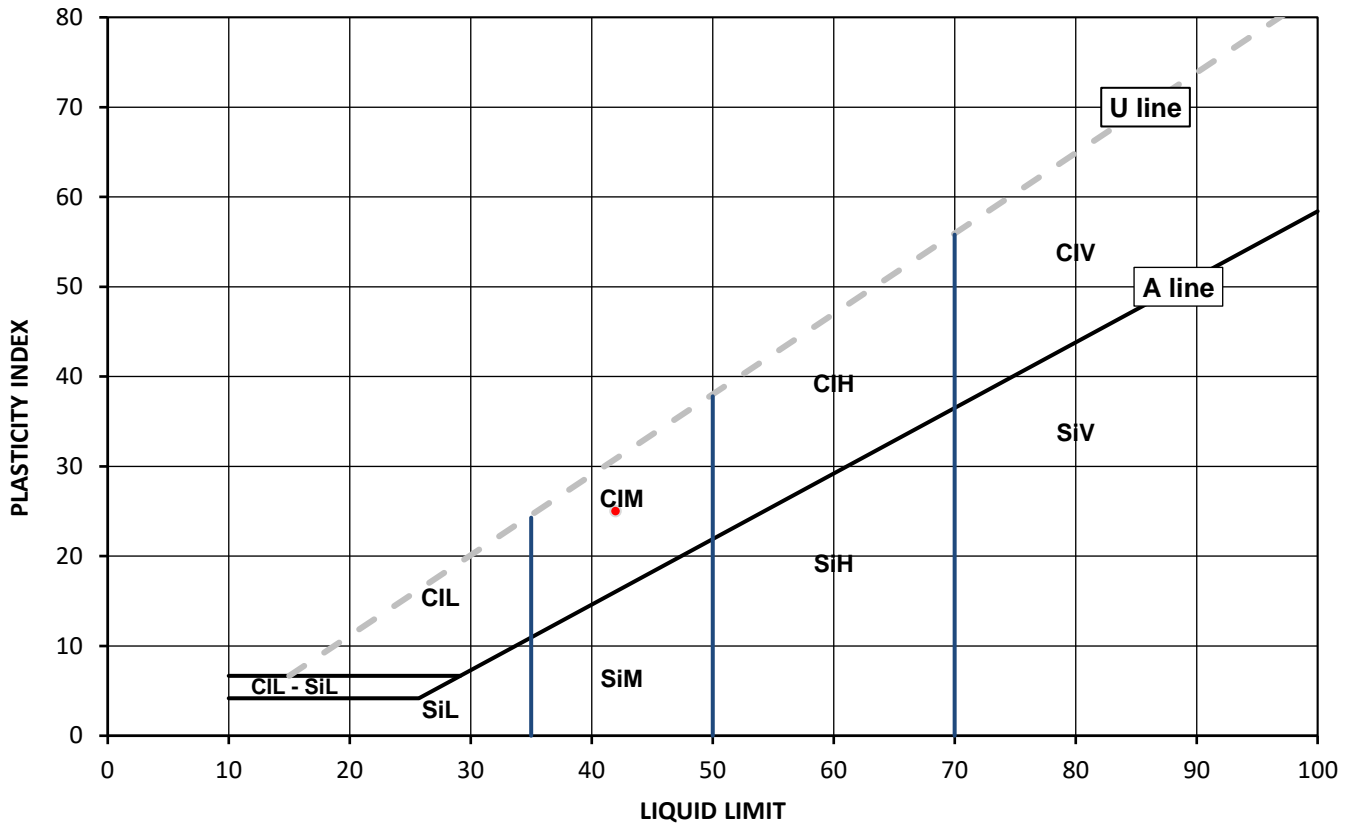
## Test Results:

Laboratory Reference: 2185961  
Hole No.: BH4  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY with fragments of chalk

Depth Top [m]: 6.45  
Depth Base [m]: 6.95  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
20	42	17	25	91



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

	Plasticity	Liquid Limit
Cl	Clay	below 35
Si	Silt	35 to 50
	L	Low
	M	Medium
	H	High
	V	Very high
	O	Organic
		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

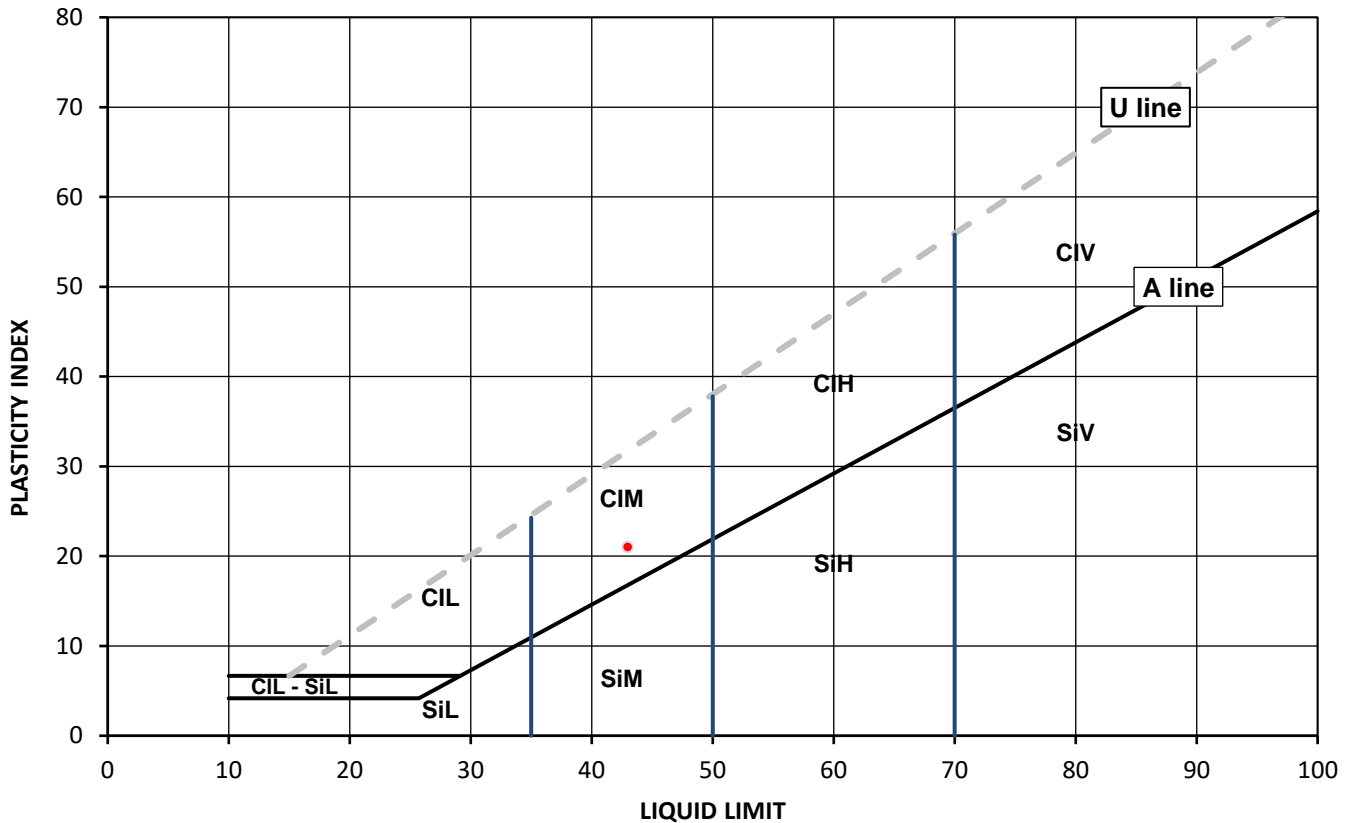
## Test Results:

Laboratory Reference: 2185963  
Hole No.: BH6  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY with fragments of chalk

Depth Top [m]: 2.00  
Depth Base [m]: Not Given  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
21	43	22	21	92



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

	Plasticity	Liquid Limit
Cl	Clay	below 35
Si	Silt	35 to 50
	L Low	50 to 70
	M Medium	exceeding 70
	H High	append to classification for organic material ( eg CIHO )
	V Very high	
	O Organic	

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

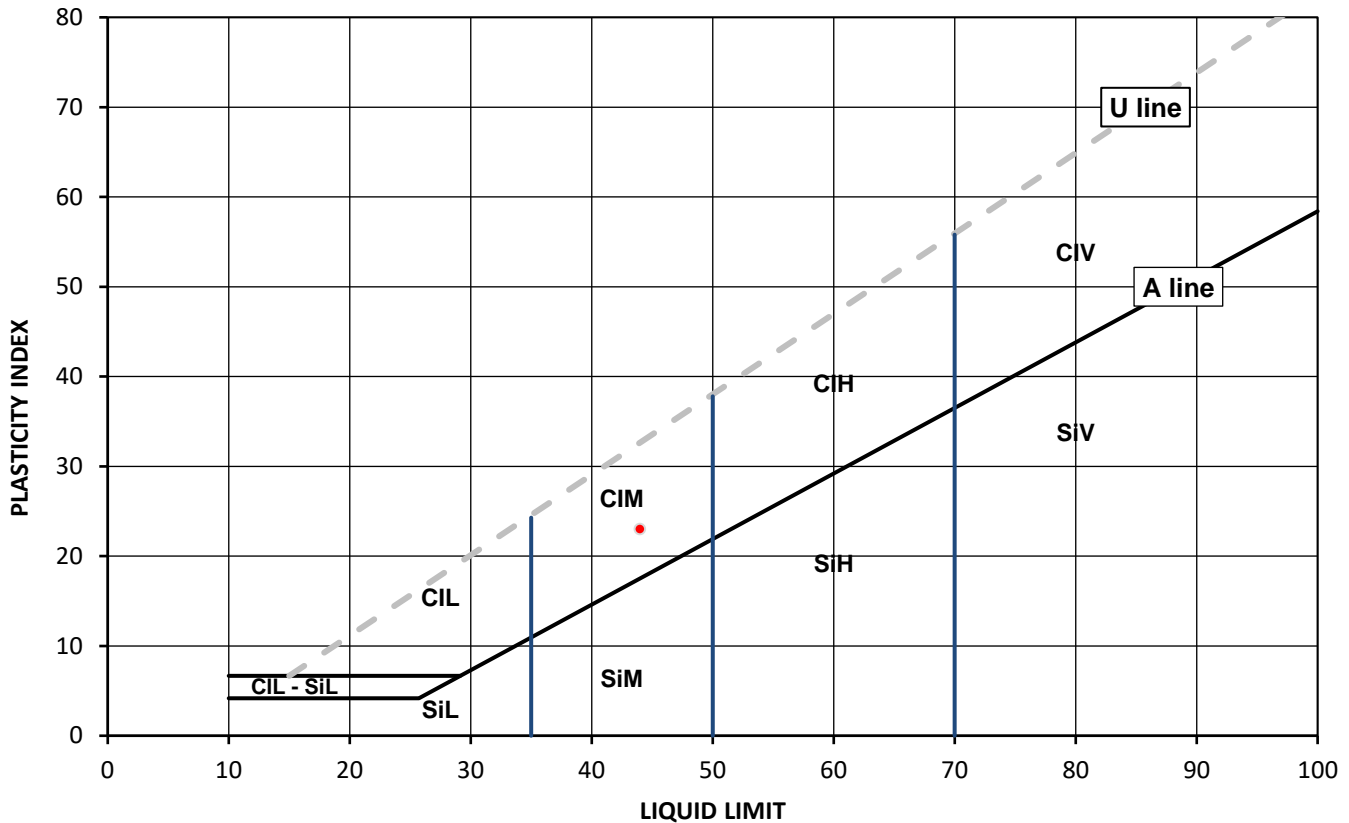
### Test Results:

Laboratory Reference: 2185964  
Hole No.: BH6  
Sample Reference: Not Given  
Sample Description: Greyish brown slightly gravelly sandy CLAY with fragments of chalk

Depth Top [m]: 4.00  
Depth Base [m]: Not Given  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
17	44	21	23	91



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	L	Low	Liquid Limit	below 35
Si	Silt		M	Medium		35 to 50
			H	High		50 to 70
			V	Very high		exceeding 70
			O	Organic		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

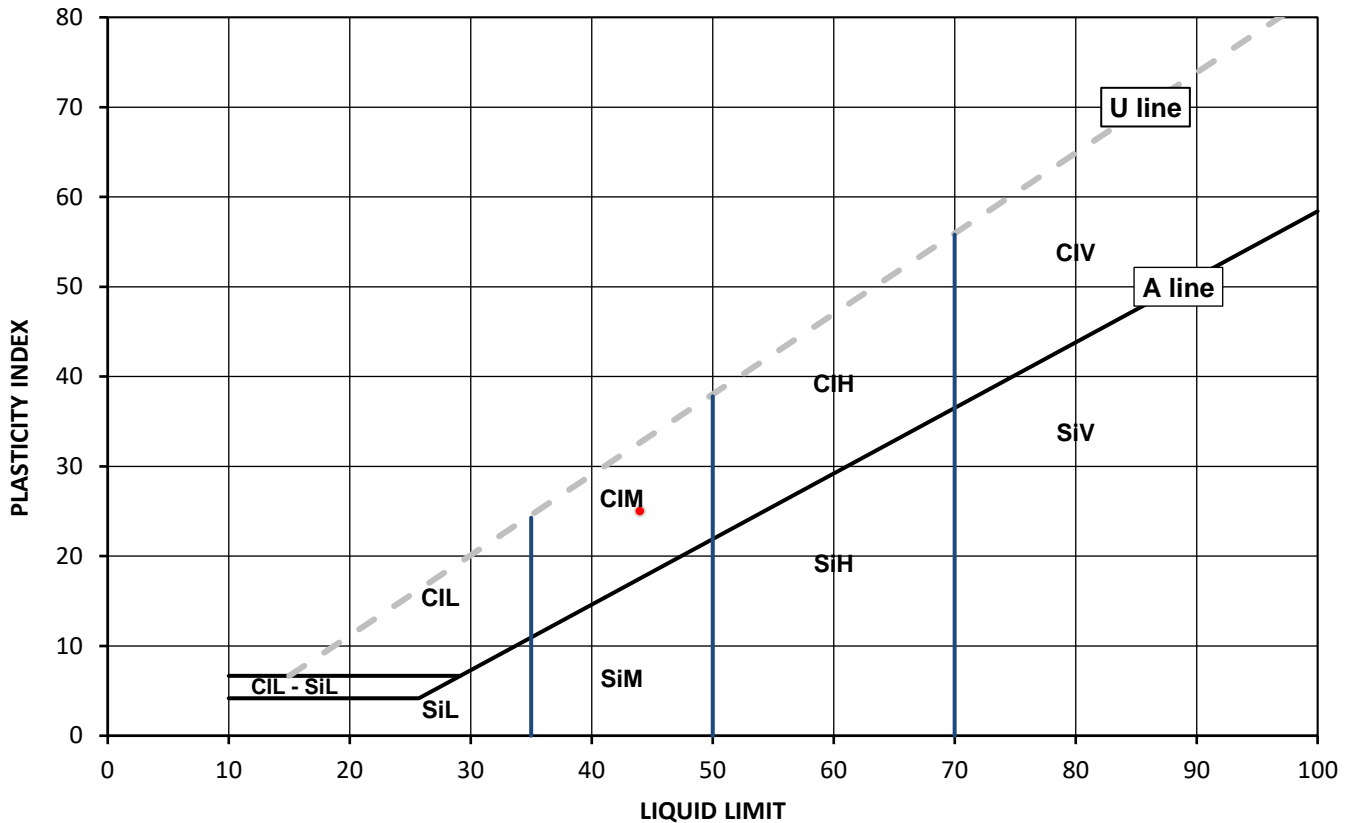
### Test Results:

Laboratory Reference: 2185965  
Hole No.: BH6  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY with fragments of chalk

Depth Top [m]: 6.50  
Depth Base [m]: Not Given  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
19	44	19	25	89



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

	Plasticity	Liquid Limit
Cl	Clay	below 35
Si	Silt	35 to 50
	L	Low
	M	Medium
	H	High
	V	Very high
	O	Organic
		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

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i2 Analytical Ltd  
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Environmental Science

4041

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Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 16/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

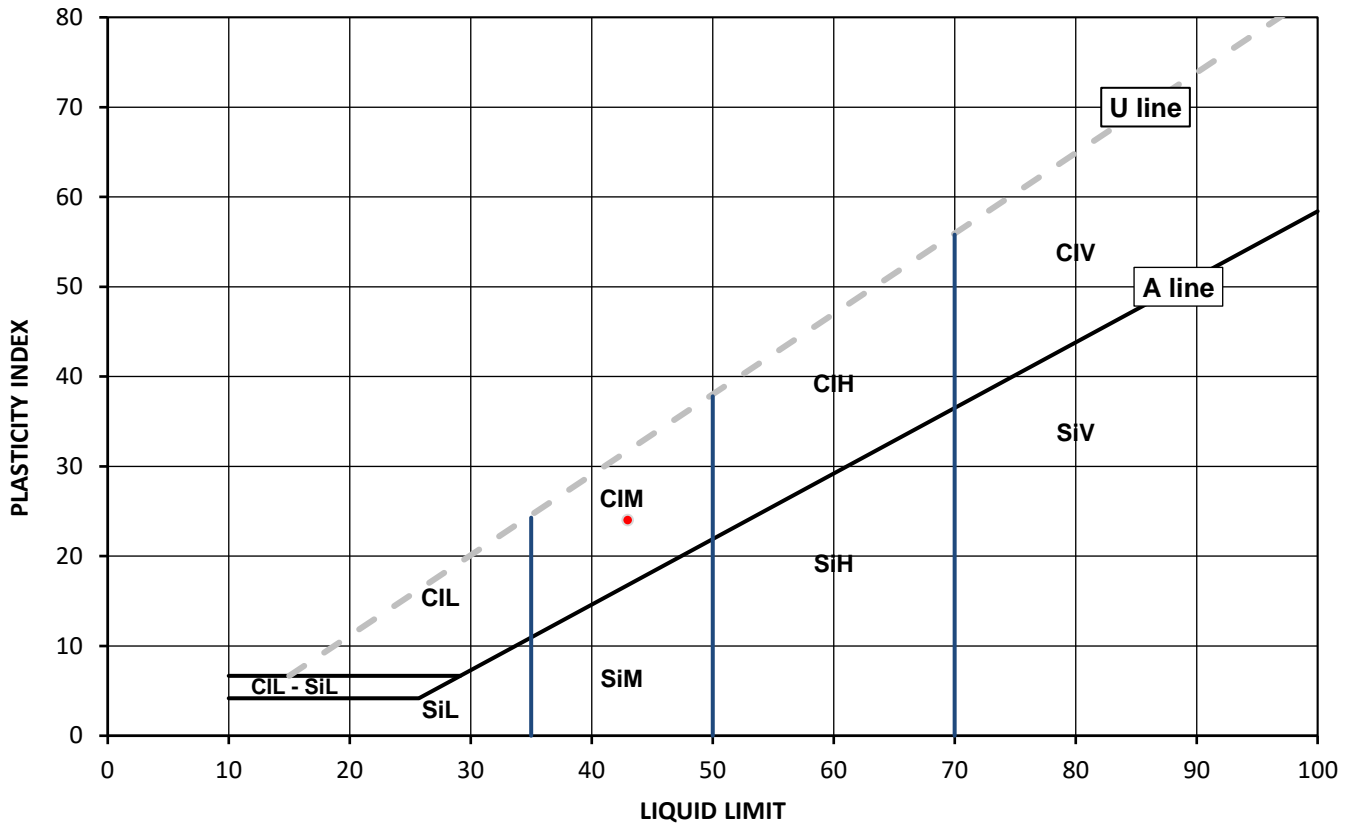
## Test Results:

Laboratory Reference: 2185967  
Hole No.: BH8  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY with fragments of chalk

Depth Top [m]: 1.50  
Depth Base [m]: 1.95  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
18	43	19	24	83



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	L	Low	Liquid Limit	below 35
Si	Silt		M	Medium		35 to 50
			H	High		50 to 70
			V	Very high		exceeding 70
			O	Organic		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

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i2 Analytical Ltd  
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Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

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Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 16/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

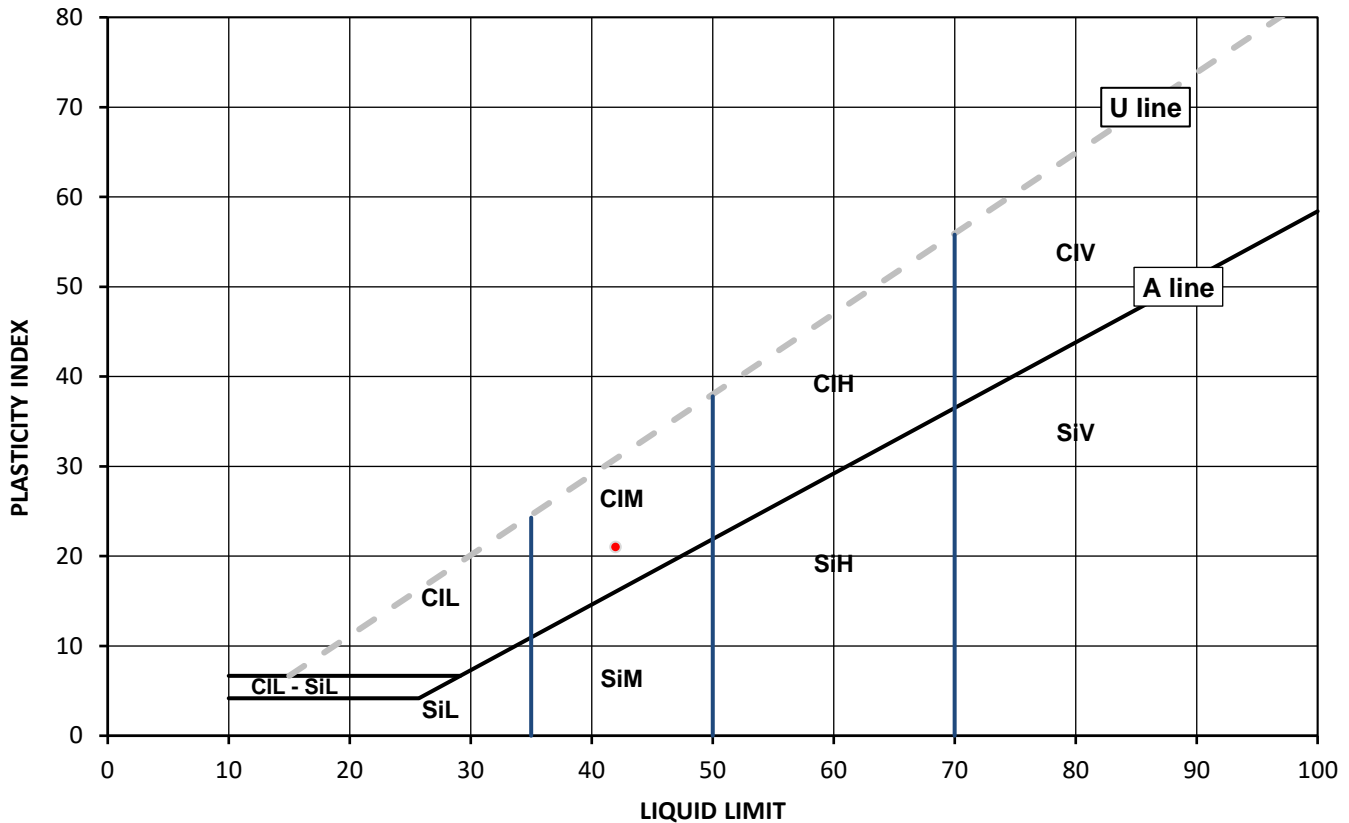
### Test Results:

Laboratory Reference: 2185968  
Hole No.: BH8  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY with fragments of chalk

Depth Top [m]: 3.50  
Depth Base [m]: 3.95  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
21	42	21	21	93



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	L	Low	Liquid Limit	below 35
Si	Silt		M	Medium		35 to 50
			H	High		50 to 70
			V	Very high		exceeding 70
			O	Organic		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

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Environmental Science

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Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 16/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

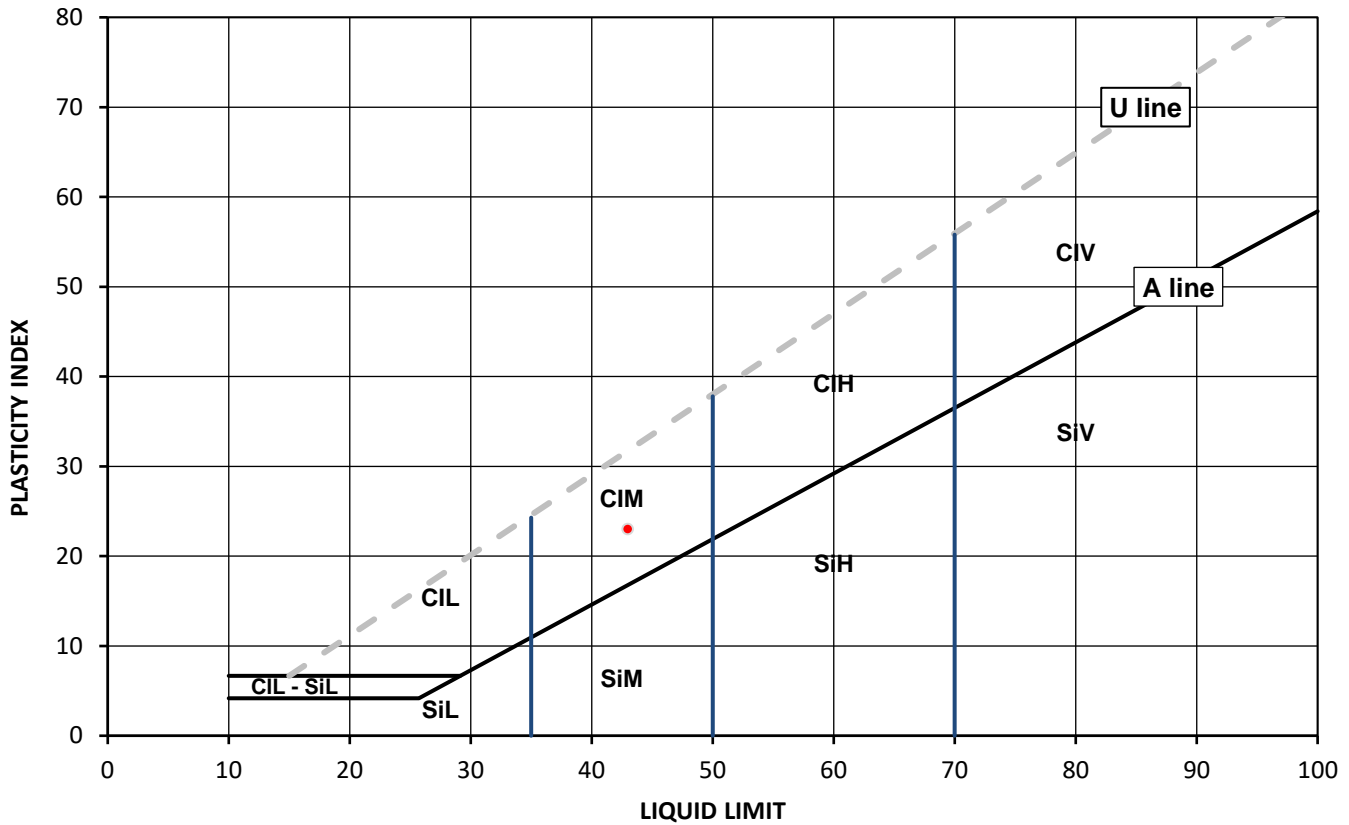
### Test Results:

Laboratory Reference: 2185969  
Hole No.: BH8  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY with fragments of chalk

Depth Top [m]: 6.00  
Depth Base [m]: 6.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
17	43	20	23	91



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	L	Low	Liquid Limit	below 35
Si	Silt		M	Medium		35 to 50
			H	High		50 to 70
			V	Very high		exceeding 70
			O	Organic		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

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Environmental Science

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Client Reference: 15-0645.05  
Job Number: 22-42014  
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Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

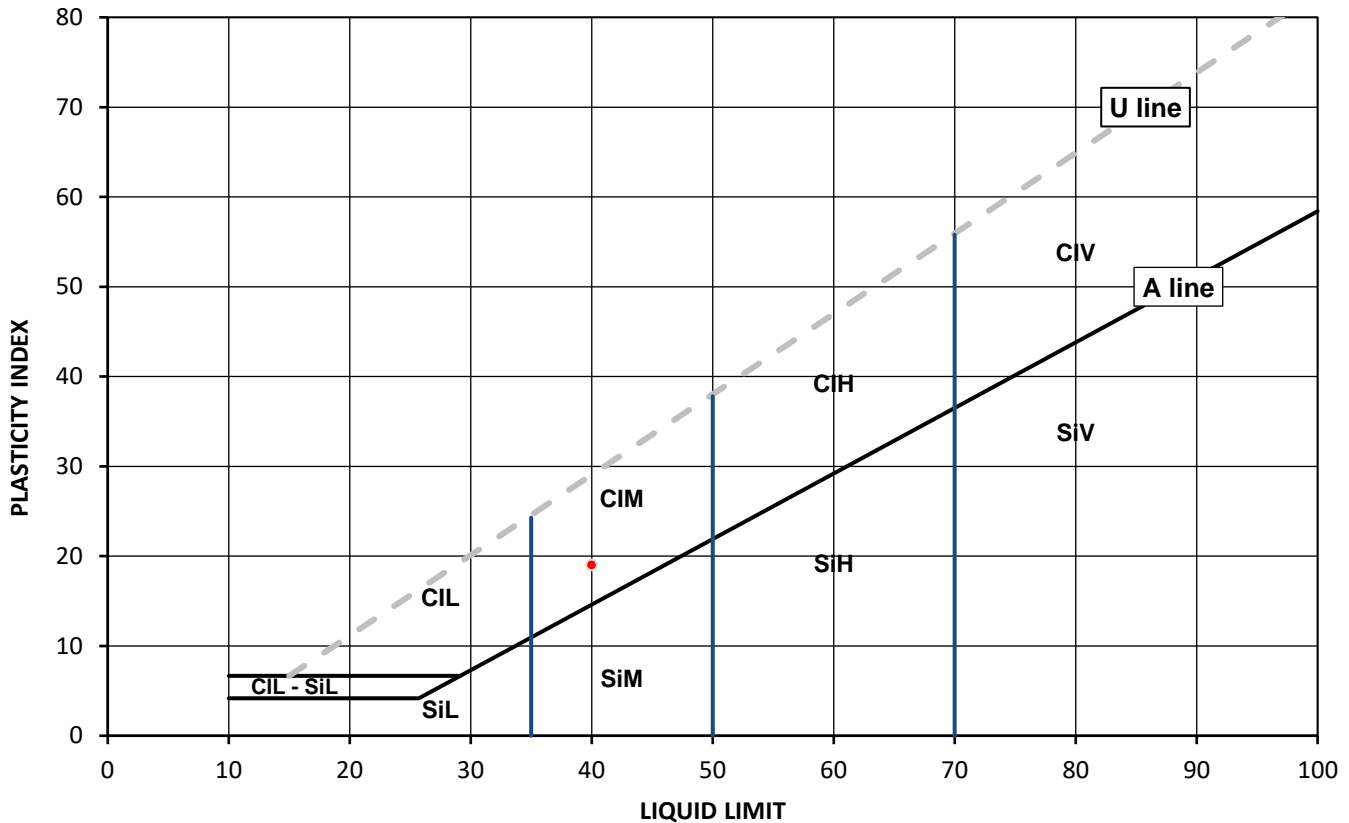
## Test Results:

Laboratory Reference: 2185971  
Hole No.: BH8  
Sample Reference: Not Given  
Sample Description: Greyish brown slightly gravelly sandy CLAY

Depth Top [m]: 9.00  
Depth Base [m]: 9.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
18	40	21	19	87



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

	Plasticity	Liquid Limit
Cl	Clay	below 35
Si	Silt	35 to 50
	L	Low
	M	Medium
	H	High
	V	Very high
	O	Organic
		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

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Date Sampled: 16/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

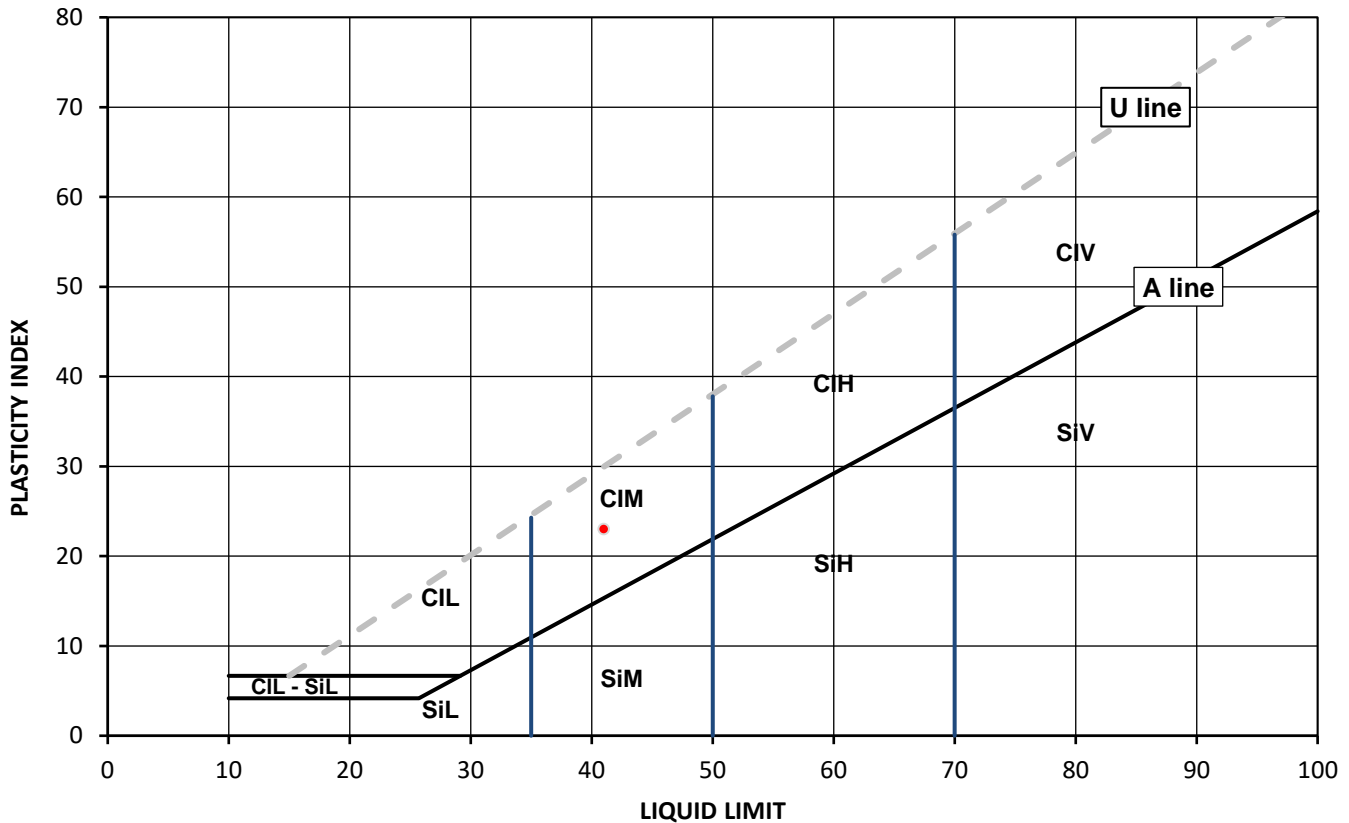
## Test Results:

Laboratory Reference: 2185972  
Hole No.: BH8  
Sample Reference: Not Given  
Sample Description: Multicolour slightly gravelly sandy CLAY

Depth Top [m]: 12.00  
Depth Base [m]: 12.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
18	41	18	23	90



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	Liquid Limit
Si	Silt	L	Low
		M	Medium
		H	High
		V	Very high
		O	Organic
			append to classification for organic material ( eg CIHO )
			below 35
			35 to 50
			50 to 70
			exceeding 70

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

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Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

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Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 16/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

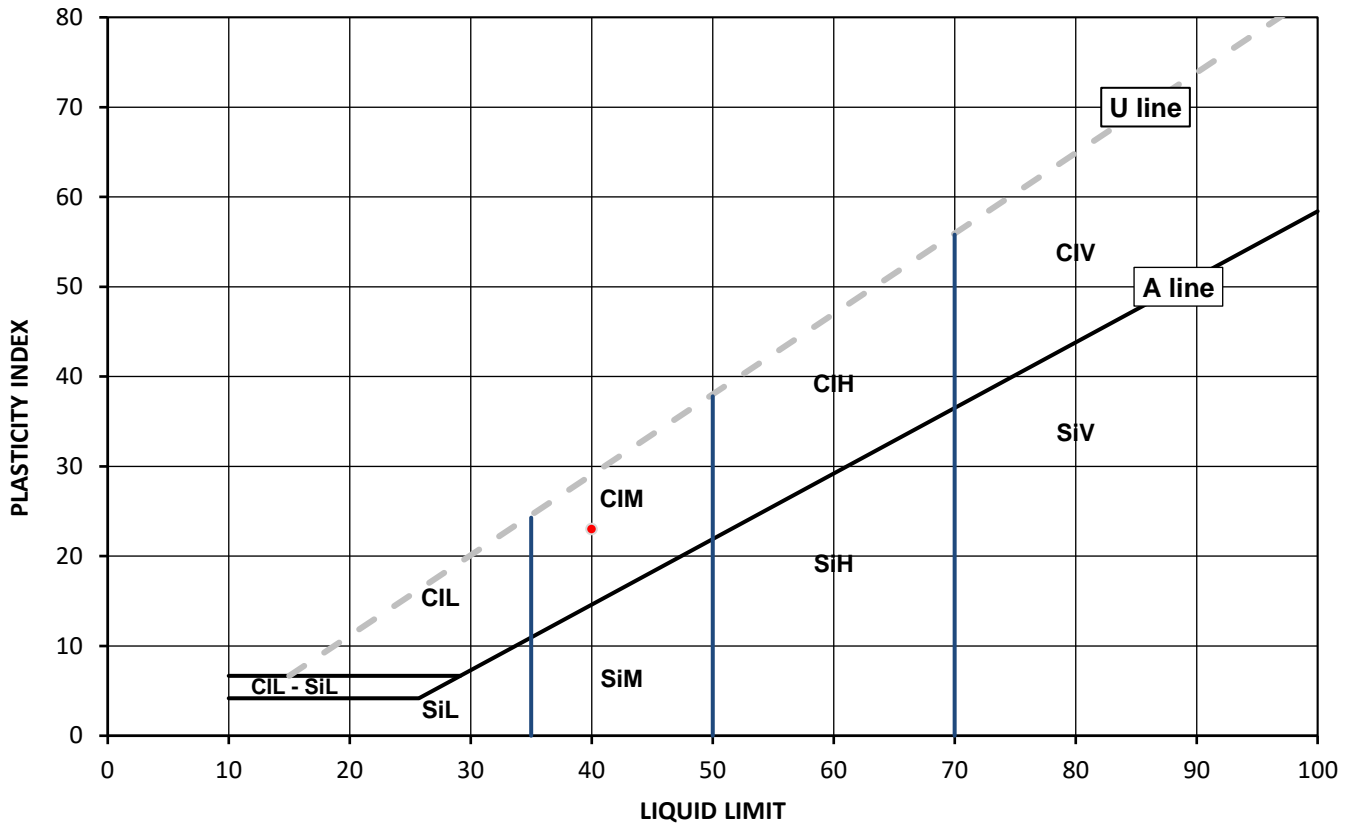
## Test Results:

Laboratory Reference: 2185974  
Hole No.: BH8  
Sample Reference: Not Given  
Sample Description: Multicolour slightly gravelly sandy CLAY

Depth Top [m]: 15.00  
Depth Base [m]: 15.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
19	40	17	23	92



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

	Plasticity	Liquid Limit
Cl	Clay	below 35
Si	Silt	35 to 50
	L Low	50 to 70
	M Medium	exceeding 70
	H High	append to classification for organic material ( eg CIHO )
	V Very high	
	O Organic	

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

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Environmental Science

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Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

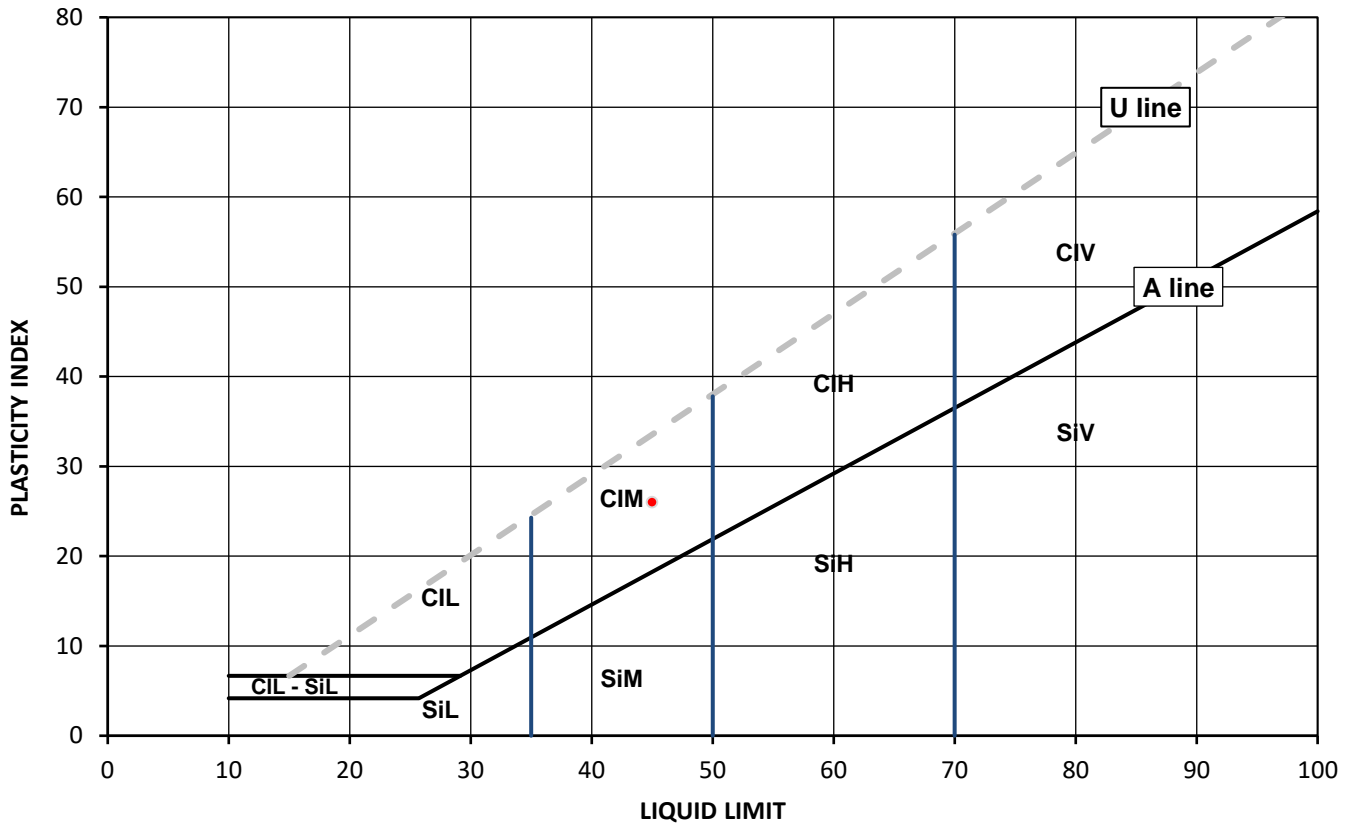
### Test Results:

Laboratory Reference: 2185987  
Hole No.: BH12  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly slightly sandy CLAY

Depth Top [m]: 1.20  
Depth Base [m]: 1.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
20	45	19	26	94



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	Liquid Limit
Si	Silt	L	Low
		M	Medium
		H	High
		V	Very high
		O	Organic
			below 35
			35 to 50
			50 to 70
			exceeding 70
			append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

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Environmental Science

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Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
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Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

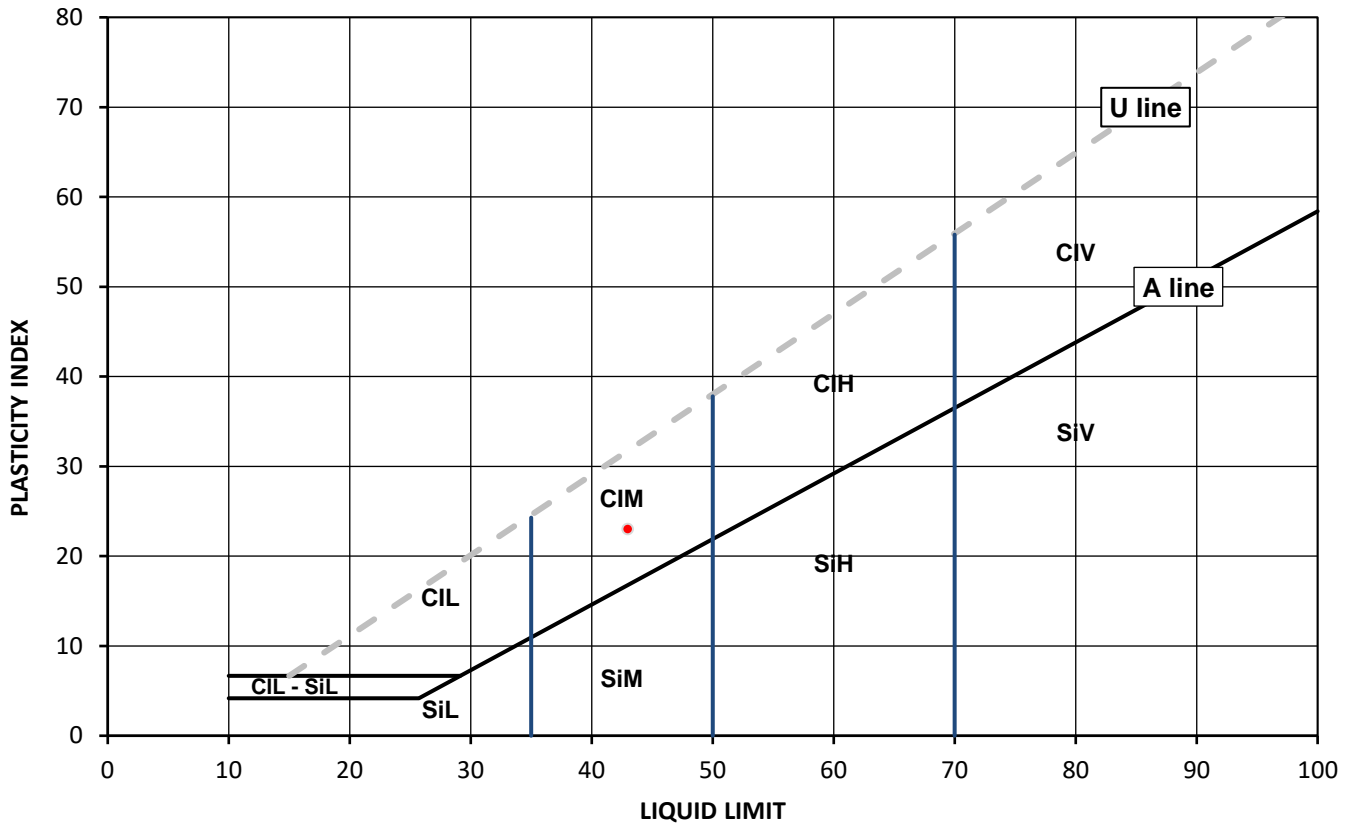
## Test Results:

Laboratory Reference: 2185989  
Hole No.: BH12  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY

Depth Top [m]: 3.00  
Depth Base [m]: 3.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
24	43	20	23	76



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	L	Low	Liquid Limit	below 35
Si	Silt		M	Medium		35 to 50
			H	High		50 to 70
			V	Very high		exceeding 70
			O	Organic		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

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Environmental Science

4041

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Date Sampled: 11/02/2022  
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Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

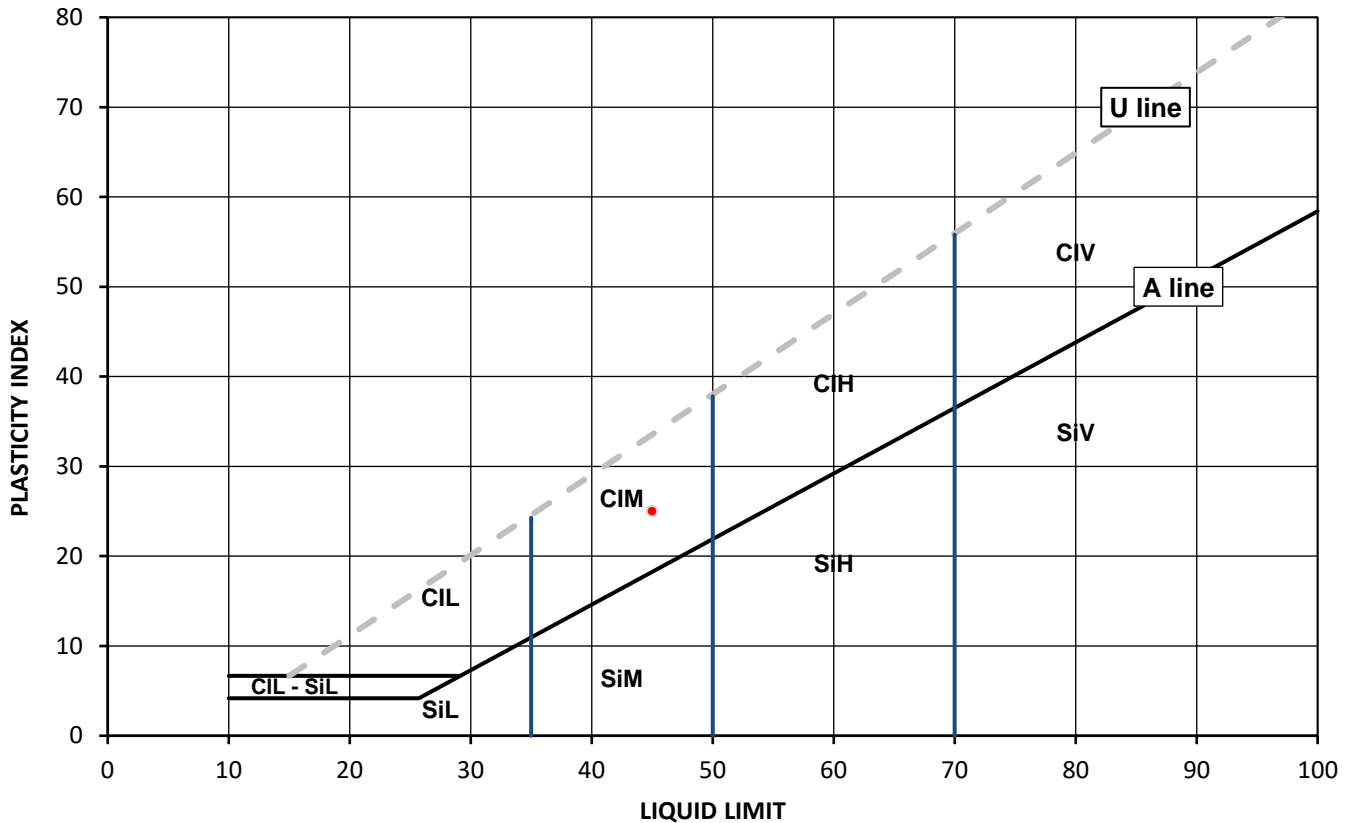
### Test Results:

Laboratory Reference: 2185991  
Hole No.: BH12  
Sample Reference: Not Given  
Sample Description: Greyish brown slightly gravelly slightly sandy CLAY

Depth Top [m]: 5.00  
Depth Base [m]: 5.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
22	45	20	25	93



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	Liquid Limit
Si	Silt	L	Low
		M	Medium
		H	High
		V	Very high
		O	Organic
			below 35
			35 to 50
			50 to 70
			exceeding 70
			append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

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4041

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Contact: Harry Whittle  
Site Address: Corby EfW

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
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Date Tested: 02/03/2022  
Sampled By: Not Given

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

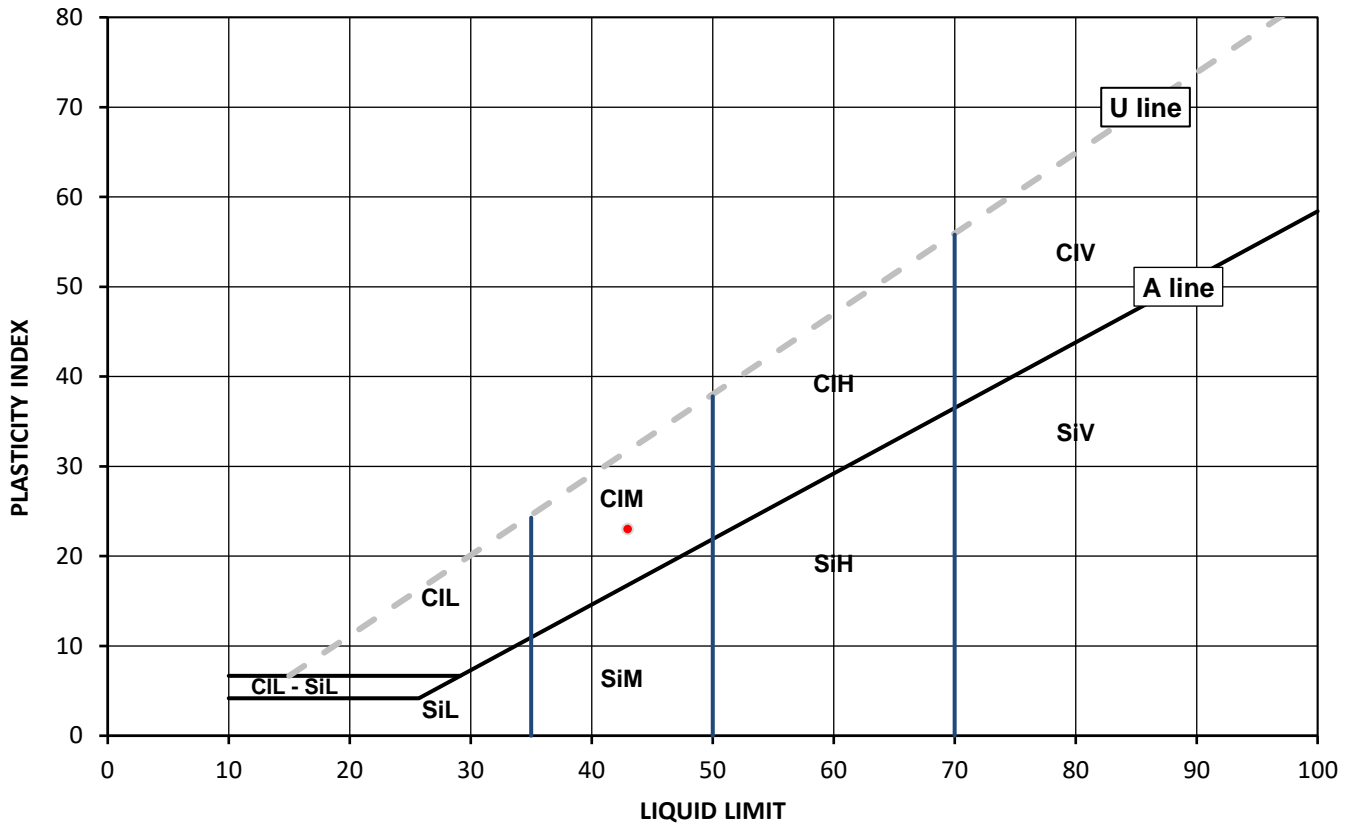
## Test Results:

Laboratory Reference: 2185992  
Hole No.: BH12  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY

Depth Top [m]: 8.00  
Depth Base [m]: 8.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
21	43	20	23	91



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	Liquid Limit
Si	Silt	L	Low
		M	Medium
		H	High
		V	Very high
		O	Organic
			below 35
			35 to 50
			50 to 70
			exceeding 70
			append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

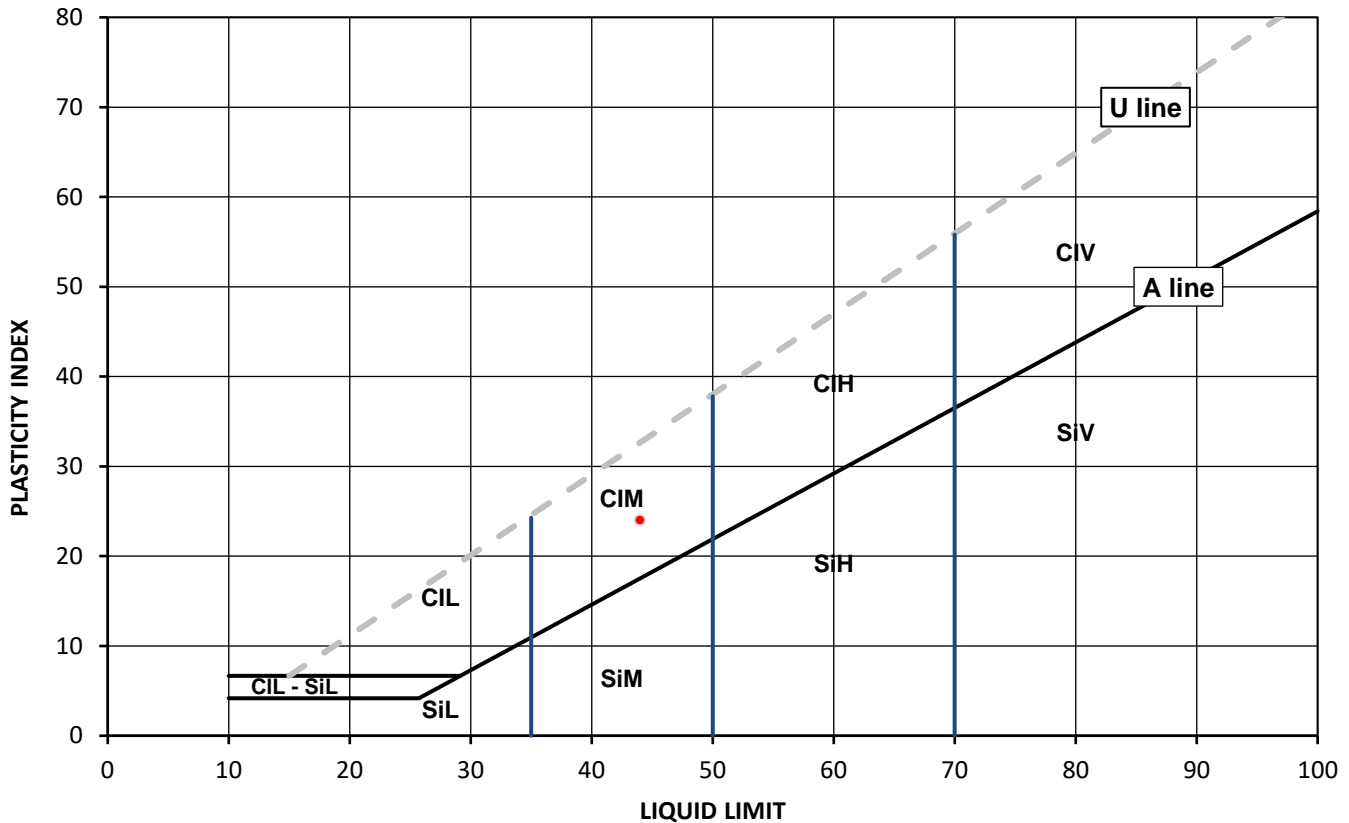
### Test Results:

Laboratory Reference: 2185993  
Hole No.: BH12  
Sample Reference: Not Given  
Sample Description: Grey slightly gravelly sandy CLAY

Depth Top [m]: 11.00  
Depth Base [m]: 11.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
19	44	20	24	89



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	Liquid Limit
Si	Silt	L	Low
		M	Medium
		H	High
		V	Very high
		O	Organic
			below 35
			35 to 50
			50 to 70
			exceeding 70
			append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

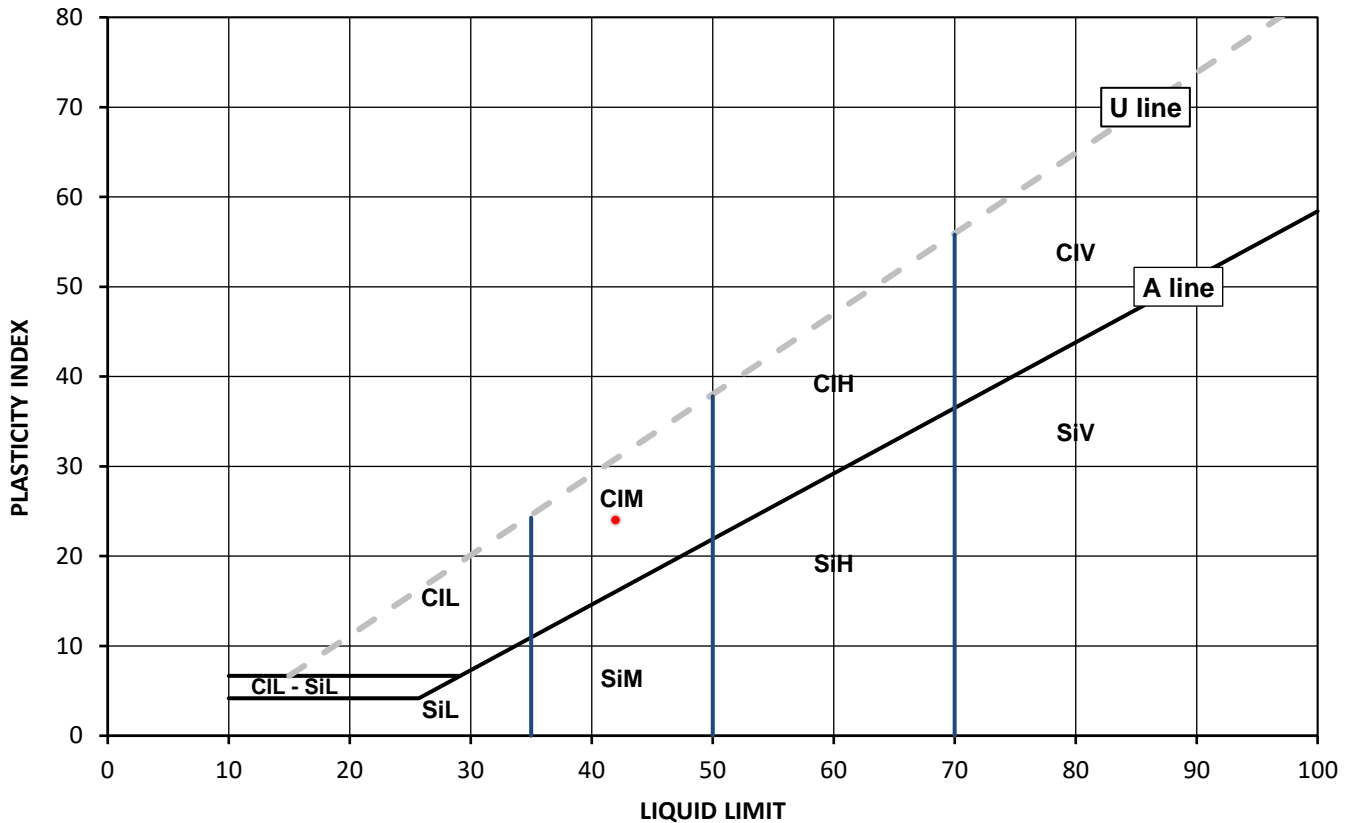
## Test Results:

Laboratory Reference: 2185994  
Hole No.: BH12  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY

Depth Top [m]: 14.00  
Depth Base [m]: 14.45  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
20	42	18	24	91



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

	Plasticity	Liquid Limit
Cl	Clay	below 35
Si	Silt	35 to 50
	L	Low
	M	Medium
	H	High
	V	Very high
	O	Organic
		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

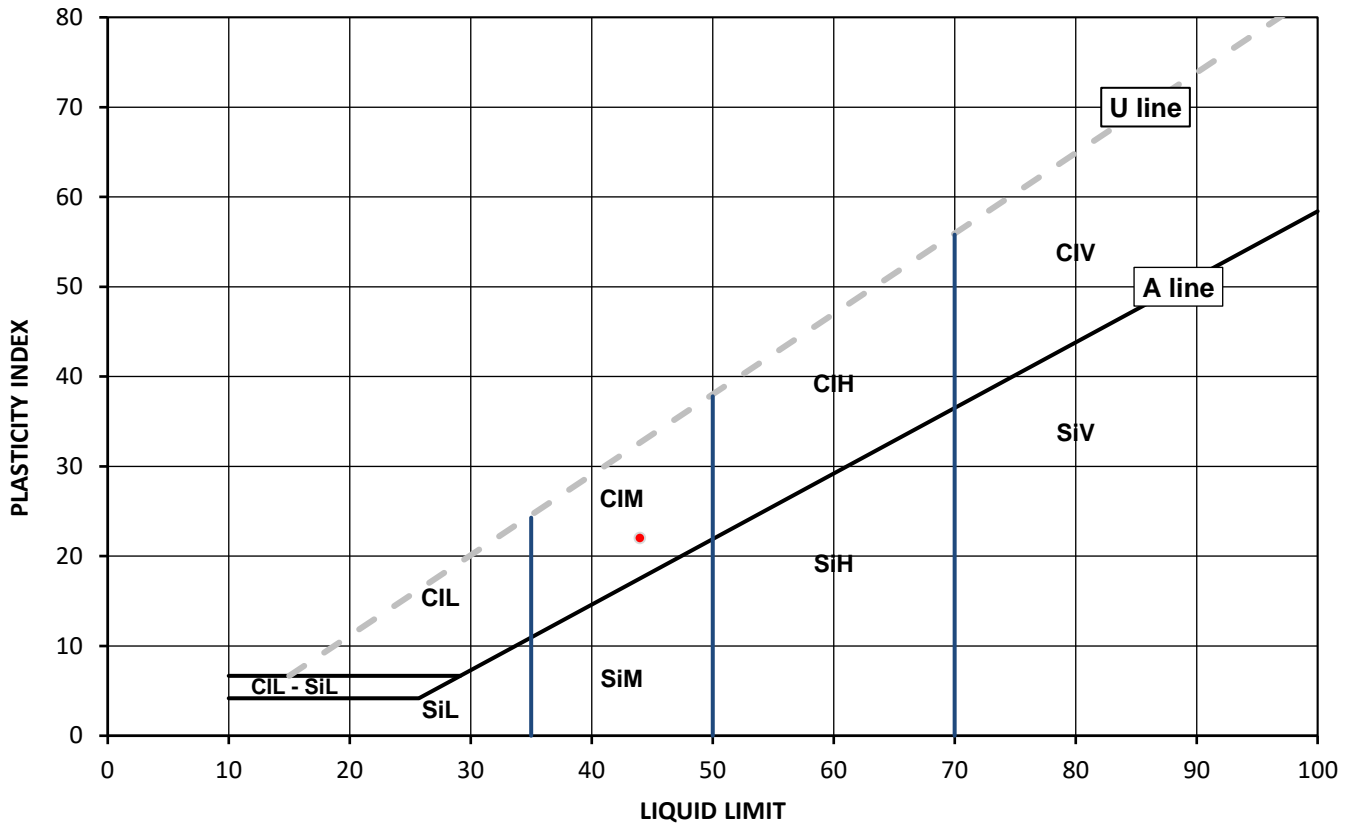
### Test Results:

Laboratory Reference: 2186002  
Hole No.: BH13  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY

Depth Top [m]: 3.00  
Depth Base [m]: Not Given  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
21	44	22	22	81



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	L	Low	Liquid Limit	below 35
Si	Silt		M	Medium		35 to 50
			H	High		50 to 70
			V	Very high		exceeding 70
			O	Organic		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

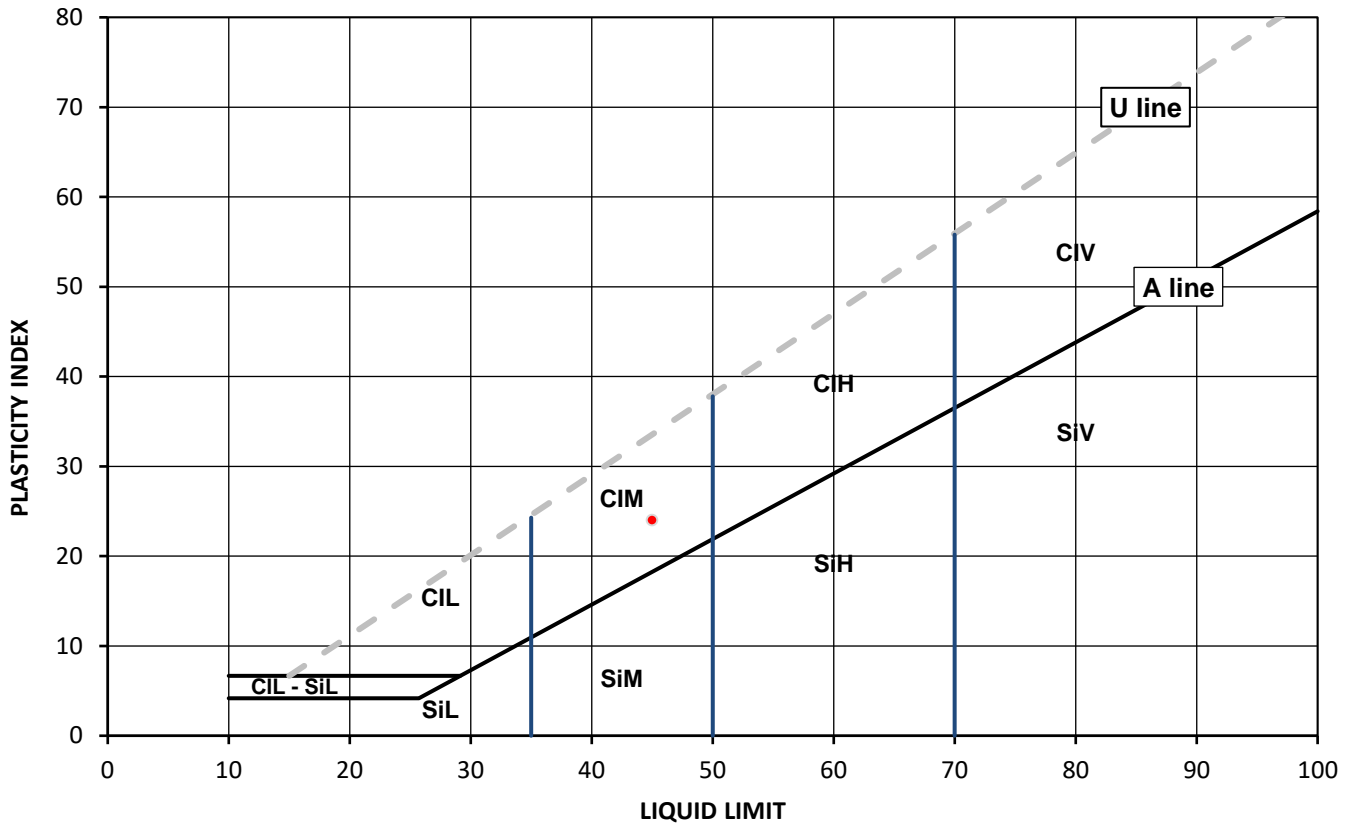
### Test Results:

Laboratory Reference: 2186340  
Hole No.: BH13  
Sample Reference: Not Given  
Sample Description: Dark brown slightly gravelly slightly sandy CLAY

Depth Top [m]: 1.20  
Depth Base [m]: 1.65  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
15	45	21	24	73



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	L	Low	Liquid Limit	below 35
Si	Silt		M	Medium		35 to 50
			H	High		50 to 70
			V	Very high		exceeding 70
			O	Organic		append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

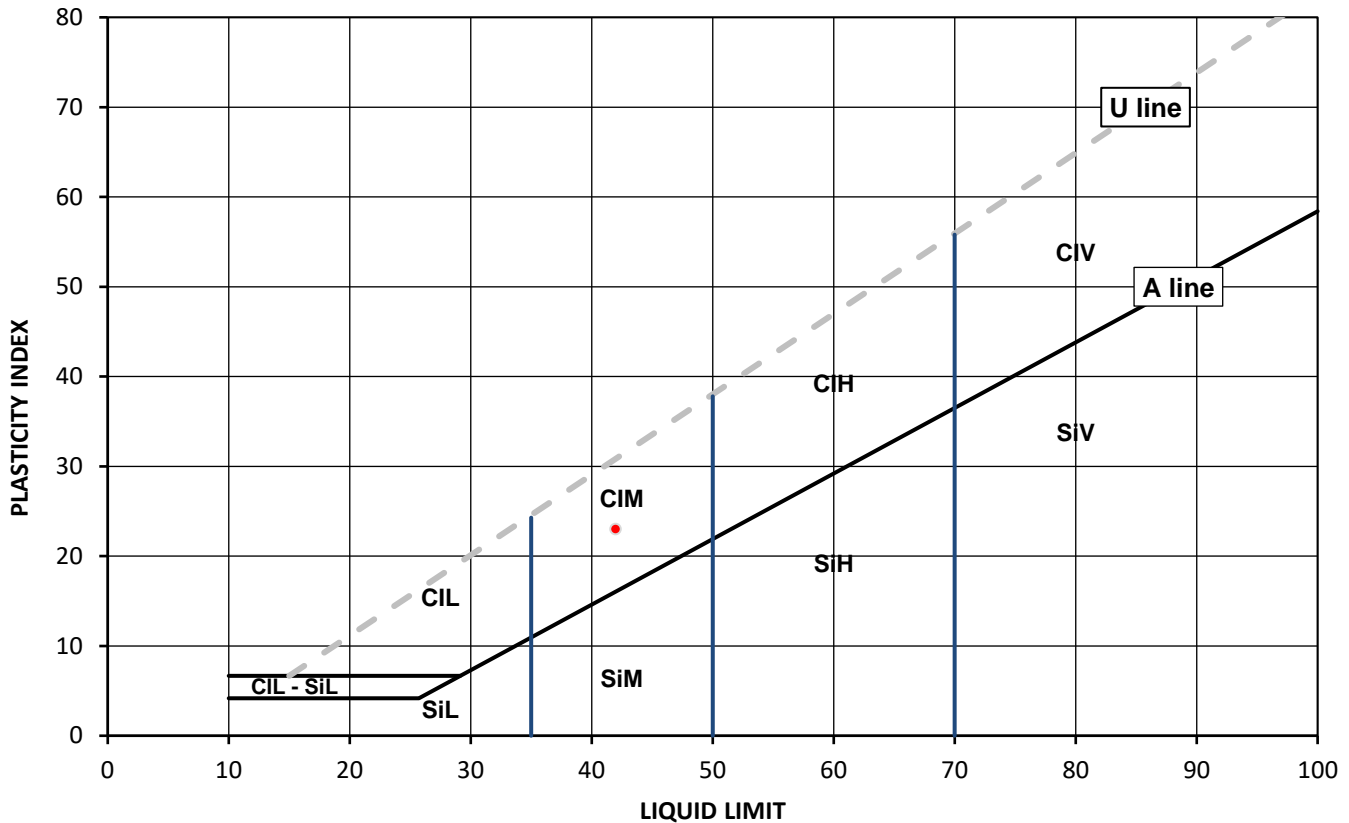
### Test Results:

Laboratory Reference: 2186341  
Hole No.: BH13  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY

Depth Top [m]: 5.00  
Depth Base [m]: Not Given  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
18	42	19	23	90



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

Cl	Clay	Plasticity	Liquid Limit
Si	Silt	L	Low
		M	Medium
		H	High
		V	Very high
		O	Organic
			append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

DETERMINATION OF LIQUID AND PLASTIC LIMITS  
Tested in Accordance with: BS 1377-2:1990: Clause 4.3 and 5

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

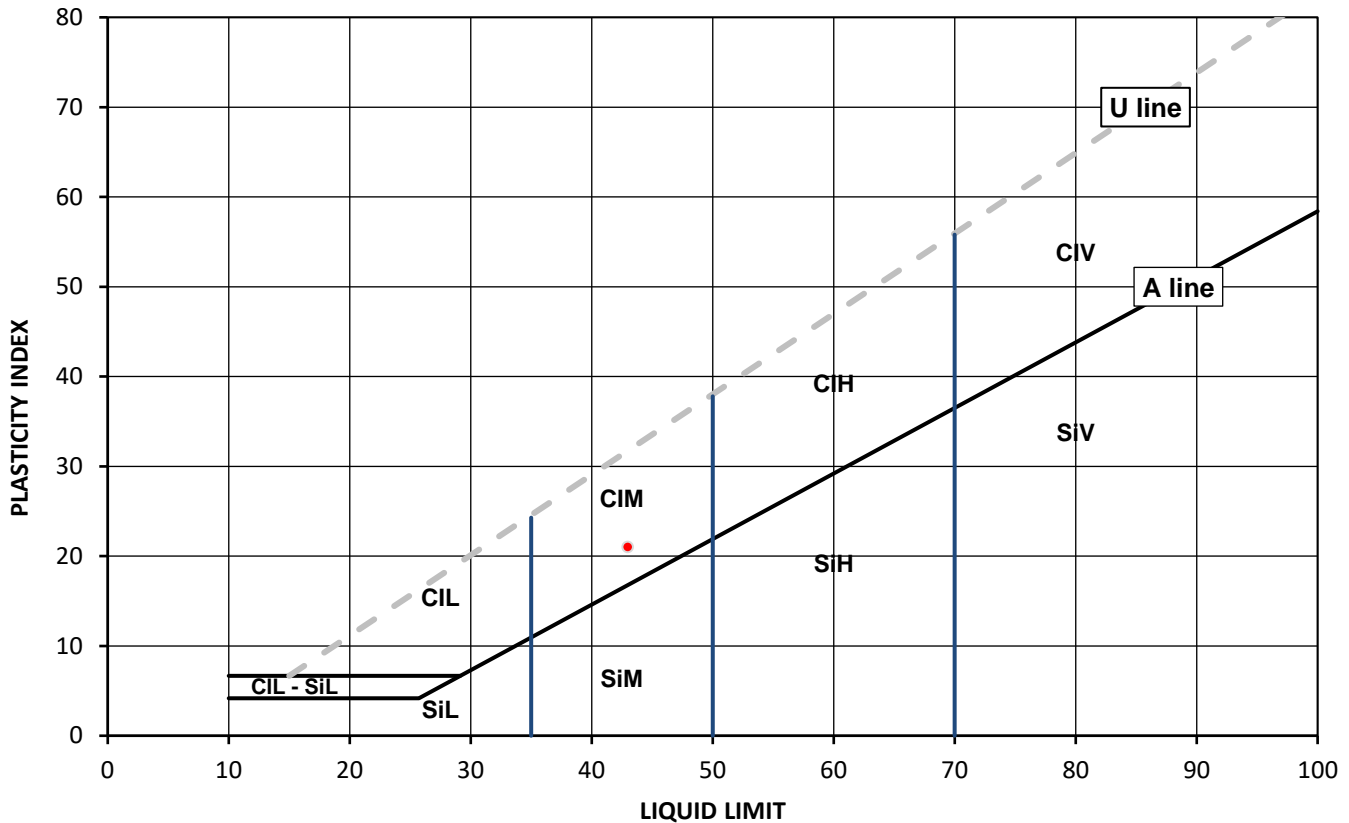
### Test Results:

Laboratory Reference: 2186342  
Hole No.: BH13  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY

Depth Top [m]: 8.00  
Depth Base [m]: Not Given  
Sample Type: U

Sample Preparation: Tested after washing to remove >425um

As Received Water Content [ W ] %	Liquid Limit [ WL ] %	Plastic Limit [ Wp ] %	Plasticity Index [ Ip ] %	% Passing 425µm BS Test Sieve
17	43	22	21	88



Legend, based on BS EN ISO 14688 2:2018 Geotechnical investigation and testing – Identification and classification of soil

	Plasticity	Liquid Limit
Cl Clay	L Low	below 35
Si Silt	M Medium	35 to 50
	H High	50 to 70
	V Very high	exceeding 70
	O Organic	append to classification for organic material ( eg CIHO )

Note: Water Content by BS 1377-2: 1990: Clause 3.2

Remarks: Preliminary report

Signed:

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Deputy Head of Geo Office Section  
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4041

Client: Delta-Simons  
 Client Address: 3 Henley Office Park, Doddington Road,  
 Lincoln, LN6 3QR

Contact: Harry Whittle  
 Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

## SUMMARY REPORT

### SUMMARY OF CLASSIFICATION TEST RESULTS

Tested in Accordance with:

; Atterberg by BS 1377-2: 1990: Clause 4.3 (4 Point Test), Clause 4.4 (1 Point Test) and 5; PD by BS 1377-2: 1990: Clause 8.2

i2 Analytical Ltd  
 Unit 8 Harrowden Road  
 Brackmills Industrial Estate  
 Northampton NN4 7EB



Environmental Science

Client Reference: 15-0645.05  
 Job Number: 22-42014  
 Date Sampled: 11/02 - 15/02/2022  
 Date Received: 24/02/2022  
 Date Tested: 02/03/2022  
 Sampled By: Not Given

#### Test results

Laboratory Reference	Hole No.	Sample				Description	Remarks	Water Content BS 1377-2 [ W ] %	Water Content BS EN ISO 17892-2 [ W ] %	Atterberg				Density			Total Porosity# %	
		Reference	Depth Top m	Depth Base m	Type					% Passing 425um	WL %	Wp %	Ip %	bulk Mg/m3	dry Mg/m3	PD Mg/m3		
2185933	BH1	Not Given	6.50	7.00	B	Greyish brown slightly gravelly silty very sandy CLAY												
2185934	BH1	Not Given	7.50	7.95	U	Multicolour slightly gravelly sandy CLAY	Atterberg 4 Point	15		98	35	18	17					
2185935	BH1	Not Given	12.00	12.45	U	Multicolour slightly gravelly very sandy CLAY	Atterberg 4 Point	14		91	33	17	16					
2185936	BH1	Not Given	13.00	13.50	B	Brownish grey gravelly very sandy very silty CLAY												2.76
2185987	BH12	Not Given	1.20	1.45	U	Brownish grey slightly gravelly slightly sandy CLAY	Atterberg 4 Point	20		94	45	19	26					
2185989	BH12	Not Given	3.00	3.45	U	Brownish grey slightly gravelly sandy CLAY	Atterberg 4 Point	24		76	43	20	23					
2185991	BH12	Not Given	5.00	5.45	U	Greyish brown slightly gravelly slightly sandy CLAY	Atterberg 4 Point	22		93	45	20	25					
2185992	BH12	Not Given	8.00	8.45	U	Brownish grey slightly gravelly sandy CLAY	Atterberg 4 Point	21		91	43	20	23					
2185993	BH12	Not Given	11.00	11.45	U	Grey slightly gravelly sandy CLAY	Atterberg 4 Point	19		89	44	20	24					
2185994	BH12	Not Given	14.00	14.45	U	Brownish grey slightly gravelly sandy CLAY	Atterberg 4 Point	20		91	42	18	24					

Note: # Non accredited; NP - Non plastic

Comments: Preliminary report

Signed:

*Dudzinska Anna*

Anna Dudzinska  
 Deputy Head of Geo Office Section  
 for and on behalf of i2 Analytical Ltd

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4041

Client: Delta-Simons

Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle

Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

**SUMMARY REPORT****SUMMARY OF CLASSIFICATION TEST RESULTS**

Tested in Accordance with:

Water Content by BS 1377-2:1990: Clause 3.2; Atterberg by BS 1377-2: 1990:  
Clause 4.3 (4 Point Test), Clause 4.4 (1 Point Test) and 5; PD by BS 1377-2:  
1990: Clause 8.2i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB

Environmental Science

Client Reference: 15-0645.05

Job Number: 22-42014

Date Sampled: 10/02 - 17/02/2022

Date Received: 24/02/2022

Date Tested: 02/03/2022

Sampled By: Not Given

**Test results**

Laboratory Reference	Hole No.	Sample				Description	Remarks	Water Content BS 1377-2 [ W ] %	Water Content BS EN ISO 17892-2 [ W ] %	Atterberg				Density			Total Porosity# %		
		Reference	Depth Top m	Depth Base m	Type					% Passing 425um	WL %	Wp %	Ip %	bulk Mg/m3	dry Mg/m3	PD Mg/m3			
2186340	BH13	Not Given	1.20	1.65	U	Dark brown slightly gravelly slightly sandy CLAY	Atterberg 4 Point	15		73	45	21	24						
2186002	BH13	Not Given	3.00	Not Given	U	Brownish grey slightly gravelly sandy CLAY	Atterberg 4 Point	21		81	44	22	22						
2186341	BH13	Not Given	5.00	Not Given	U	Brownish grey slightly gravelly sandy CLAY	Atterberg 4 Point	18		90	42	19	23						
2186342	BH13	Not Given	8.00	Not Given	U	Brownish grey slightly gravelly sandy CLAY	Atterberg 4 Point	17		88	43	22	21						
2185937	BH2	Not Given	8.00	8.45	U	Yellowish brown to greyish brown slightly gravelly very sandy CLAY	Atterberg 4 Point	13		98	27	14	13						
2185938	BH2	Not Given	15.50	15.95	U	Brownish grey slightly gravelly slightly sandy CLAY	Atterberg 4 Point	16		98	47	21	26						
2185958	BH4	Not Given	2.00	2.45	U	Grey slightly gravelly sandy CLAY with fragments of chalk	Atterberg 4 Point	20		94	43	19	24						
2185960	BH4	Not Given	4.00	4.45	U	Brownish grey slightly gravelly sandy CLAY with fragments of chalk	Atterberg 4 Point	22		90	44	19	25						
2185961	BH4	Not Given	6.45	6.95	U	Brownish grey slightly gravelly sandy CLAY with fragments of chalk	Atterberg 4 Point	20		91	42	17	25						
2185963	BH6	Not Given	2.00	Not Given	U	Brownish grey slightly gravelly sandy CLAY with fragments of chalk	Atterberg 4 Point	21		92	43	22	21						

Note: # Non accredited; NP - Non plastic

Comments: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road, Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

# SUMMARY REPORT

## SUMMARY OF CLASSIFICATION TEST RESULTS

Tested in Accordance with:

Water Content by BS 1377-2:1990: Clause 3.2; Atterberg by BS 1377-2: 1990: Clause 4.3 (4 Point Test), Clause 4.4 (1 Point Test) and 5; PD by BS 1377-2: 1990: Clause 8.2

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 16/02 - 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

### Test results

Laboratory Reference	Hole No.	Sample				Description	Remarks	Water Content BS 1377-2 [ W ] %	Water Content BS EN ISO 17892-2 [ W ] %	Atterberg				Density			Total Porosity# %	
		Reference	Depth Top m	Depth Base m	Type					% Passing 425um %	WL %	Wp %	Ip %	bulk Mg/m3	dry Mg/m3	PD Mg/m3		
2185964	BH6	Not Given	4.00	Not Given	U	Greyish brown slightly gravelly sandy CLAY with fragments of chalk	Atterberg 4 Point	17		91	44	21	23					
2185965	BH6	Not Given	6.50	Not Given	U	Brownish grey slightly gravelly sandy CLAY with fragments of chalk	Atterberg 4 Point	19		89	44	19	25					
2185967	BH8	Not Given	1.50	1.95	U	Brownish grey slightly gravelly sandy CLAY with fragments of chalk	Atterberg 4 Point	18		83	43	19	24					
2185968	BH8	Not Given	3.50	3.95	U	Brownish grey slightly gravelly sandy CLAY with fragments of chalk	Atterberg 4 Point	21		93	42	21	21					
2185969	BH8	Not Given	6.00	6.45	U	Brownish grey slightly gravelly sandy CLAY with fragments of chalk	Atterberg 4 Point	17		91	43	20	23					
2185971	BH8	Not Given	9.00	9.45	U	Greyish brown slightly gravelly sandy CLAY	Atterberg 4 Point	18		87	40	21	19					
2185972	BH8	Not Given	12.00	12.45	U	Multicolour slightly gravelly sandy CLAY	Atterberg 4 Point	18		90	41	18	23					
2185974	BH8	Not Given	15.00	15.45	U	Multicolour slightly gravelly sandy CLAY	Atterberg 4 Point	19		92	40	17	23					

Note: # Non accredited; NP - Non plastic

Comments: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# SUMMARY REPORT

## DETERMINATION OF WATER CONTENT

Tested in Accordance with: BS 1377-2: 1990: Clause 3.2

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EfW

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02 - 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test results

Laboratory Reference	Hole No.	Sample				Description	Remarks	WC %	Sample preparation / Oven temperature at the time of testing			
		Reference	Depth Top m	Depth Base m	Type							
2185934	BH1	Not Given	7.50	7.95	U	Multicolour slightly gravelly sandy CLAY		15	Sample was quartered, oven dried at 109 °C			
2185935	BH1	Not Given	12.00	12.45	U	Multicolour slightly gravelly very sandy CLAY		14	Sample was quartered, oven dried at 109 °C			
2185987	BH12	Not Given	1.20	1.45	U	Brownish grey slightly gravelly slightly sandy CLAY		20	Sample was quartered, oven dried at 106 °C			
2185989	BH12	Not Given	3.00	3.45	U	Brownish grey slightly gravelly sandy CLAY		24	Sample was quartered, oven dried at 109 °C			
2185991	BH12	Not Given	5.00	5.45	U	Greyish brown slightly gravelly slightly sandy CLAY		22	Sample was quartered, oven dried at 106.1 °C			
2185992	BH12	Not Given	8.00	8.45	U	Brownish grey slightly gravelly sandy CLAY		21	Sample was quartered, oven dried at 109 °C			
2185993	BH12	Not Given	11.00	11.45	U	Grey slightly gravelly sandy CLAY		19	Sample was quartered, oven dried at 109 °C			
2185994	BH12	Not Given	14.00	14.45	U	Brownish grey slightly gravelly sandy CLAY		20	Sample was quartered, oven dried at 109 °C			
2186340	BH13	Not Given	1.20	1.65	U	Dark brown slightly gravelly slightly sandy CLAY		15	Sample was quartered, oven dried at 109 °C			
2186002	BH13	Not Given	3.00	Not Given	U	Brownish grey slightly gravelly sandy CLAY		21	Sample was quartered, oven dried at 109 °C			

Comments: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# SUMMARY REPORT

## DETERMINATION OF WATER CONTENT

Tested in Accordance with: BS 1377-2: 1990: Clause 3.2

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EfW

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 10/02 - 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test results

Laboratory Reference	Hole No.	Sample				Description	Remarks	WC %	Sample preparation / Oven temperature at the time of testing			
		Reference	Depth Top m	Depth Base m	Type							
2186341	BH13	Not Given	5.00	Not Given	U	Brownish grey slightly gravelly sandy CLAY		18	Sample was quartered, oven dried at 109 °C			
2186342	BH13	Not Given	8.00	Not Given	U	Brownish grey slightly gravelly sandy CLAY		17	Sample was quartered, oven dried at 109 °C			
2185937	BH2	Not Given	8.00	8.45	U	Yellowish brown to greyish brown slightly gravelly very sandy CLAY		13	Sample was quartered, oven dried at 109 °C			
2185938	BH2	Not Given	15.50	15.95	U	Brownish grey slightly gravelly slightly sandy CLAY		16	Sample was quartered, oven dried at 106.4 °C			
2185958	BH4	Not Given	2.00	2.45	U	Grey slightly gravelly sandy CLAY with fragments of chalk		20	Sample was quartered, oven dried at 106.2 °C			
2185960	BH4	Not Given	4.00	4.45	U	Brownish grey slightly gravelly sandy CLAY with fragments of chalk		22	Sample was quartered, oven dried at 106.2 °C			
2185961	BH4	Not Given	6.45	6.95	U	Brownish grey slightly gravelly sandy CLAY with fragments of chalk		20	Sample was quartered, oven dried at 108.3 °C			
2185963	BH6	Not Given	2.00	Not Given	U	Brownish grey slightly gravelly sandy CLAY with fragments of chalk		21	Sample was quartered, oven dried at 106.5 °C			
2185964	BH6	Not Given	4.00	Not Given	U	Greyish brown slightly gravelly sandy CLAY with fragments of chalk		17	Sample was quartered, oven dried at 106 °C			
2185965	BH6	Not Given	6.50	Not Given	U	Brownish grey slightly gravelly sandy CLAY with fragments of chalk		19	Sample was quartered, oven dried at 106.2 °C			

Comments: Preliminary report

Signed:

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Deputy Head of Geo Office Section  
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Client Address: 3 Henley Office Park, Doddington Road, Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

# SUMMARY REPORT

## DETERMINATION OF WATER CONTENT

Tested in Accordance with: BS 1377-2: 1990: Clause 3.2

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 16/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

### Test results

Laboratory Reference	Hole No.	Sample				Description	Remarks	WC %	Sample preparation / Oven temperature at the time of testing			
		Reference	Depth Top m	Depth Base m	Type							
2185967	BH8	Not Given	1.50	1.95	U	Brownish grey slightly gravelly sandy CLAY with fragments of chalk		18	Sample was quartered, oven dried at 106.5 °C			
2185968	BH8	Not Given	3.50	3.95	U	Brownish grey slightly gravelly sandy CLAY with fragments of chalk		21	Sample was quartered, oven dried at 109 °C			
2185969	BH8	Not Given	6.00	6.45	U	Brownish grey slightly gravelly sandy CLAY with fragments of chalk		17	Sample was quartered, oven dried at 106 °C			
2185971	BH8	Not Given	9.00	9.45	U	Greyish brown slightly gravelly sandy CLAY		18	Sample was quartered, oven dried at 109 °C			
2185972	BH8	Not Given	12.00	12.45	U	Multicolour slightly gravelly sandy CLAY		18	Sample was quartered, oven dried at 106.2 °C			
2185974	BH8	Not Given	15.00	15.45	U	Multicolour slightly gravelly sandy CLAY		19	Sample was quartered, oven dried at 106 °C			

Comments: Preliminary report

Signed:

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Deputy Head of Geo Office Section  
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# TEST CERTIFICATE

## DETERMINATION OF PARTICLE SIZE DISTRIBUTION

Tested in Accordance with: BS 1377-2: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 15/02/2022  
Date Received: 24/02/2022  
Date Tested: 03/03/2022  
Sampled By: Not Given

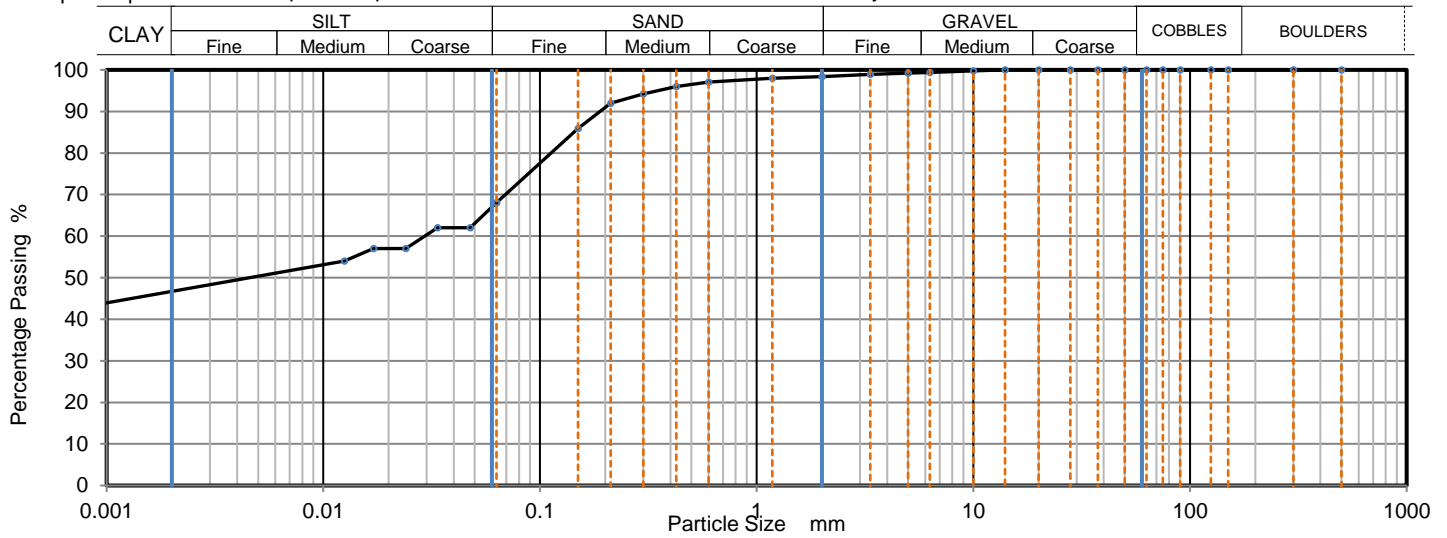
Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185933  
Hole No.: BH1  
Sample Reference: Not Given  
Sample Description: Greyish brown slightly gravelly silty very sandy CLAY  
Sample Preparation: Sample was quartered, oven dried at 106.0 °C and broken down by hand.

Depth Top [m]: 6.50  
Depth Base [m]: 7.00  
Sample Type: B



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0630	68
300	100	0.0475	62
150	100	0.0336	62
125	100	0.0241	57
90	100	0.0170	57
75	100	0.0125	54
63	100	0.0008	43
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	100		
6.3	99		
5	99		
3.35	99		
2	98	Particle density (measured) 2.82 Mg/m <sup>3</sup>	
1.18	98		
0.6	97		
0.425	96		
0.3	94		
0.212	92		
0.15	86		
0.063	68		

Sample Proportions	% dry mass
Very coarse	0
Gravel	2
Sand	30
Silt	22
Clay	46

Grading Analysis		
D100	mm	14
D60	mm	0.0293
D30	mm	
D10	mm	
Uniformity Coefficient		> 37
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

Anna Dudzinska  
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Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 15/02/2022  
Date Received: 24/02/2022  
Date Tested: 03/03/2022  
Sampled By: Not Given

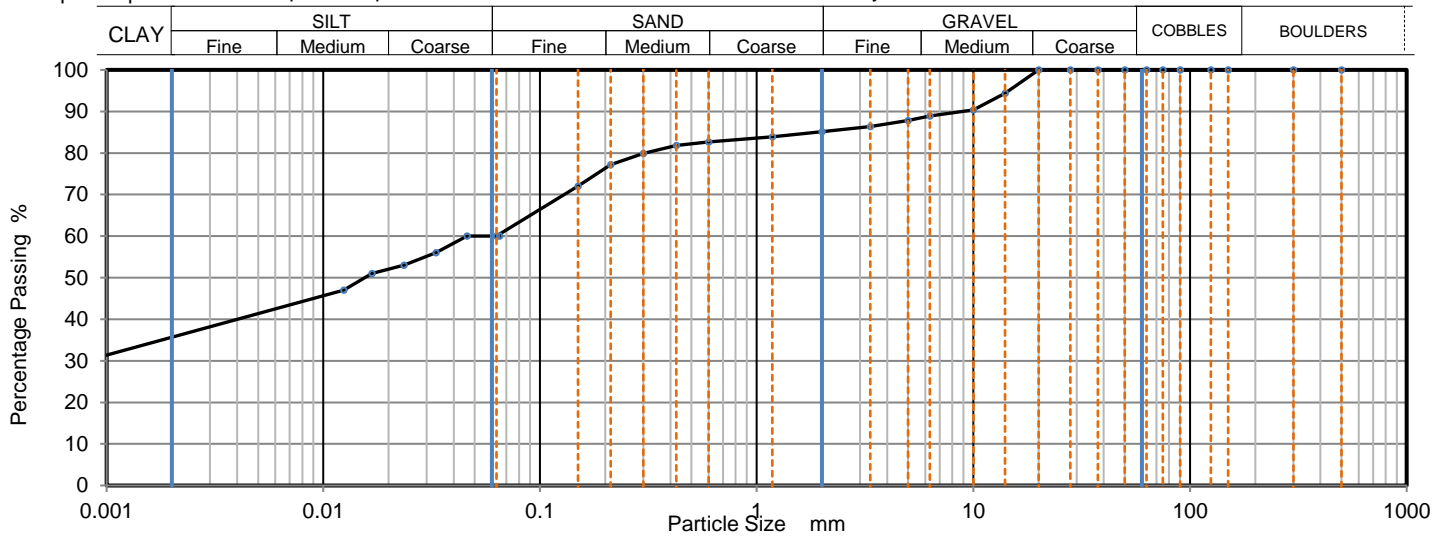
Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185936  
Hole No.: BH1  
Sample Reference: Not Given  
Sample Description: Brownish grey gravelly very sandy very silty CLAY  
Sample Preparation: Sample was quartered, oven dried at 106.9 °C and broken down by hand.

Depth Top [m]: 13.00  
Depth Base [m]: 13.50  
Sample Type: B



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0652	60
300	100	0.0461	60
150	100	0.0331	56
125	100	0.0235	53
90	100	0.0168	51
75	100	0.0124	47
63	100	0.0008	30
50	100		
37.5	100		
28	100		
20	100		
14	94		
10	90		
6.3	89		
5	88		
3.35	86		
2	85	Particle density (measured) 2.76 Mg/m3	
1.18	84		
0.6	83		
0.425	82		
0.3	80		
0.212	77		
0.15	72		
0.063	60		

Sample Proportions	% dry mass
Very coarse	0
Gravel	15
Sand	25
Silt	24
Clay	36

Grading Analysis		
D100	mm	20
D60	mm	0.0636
D30	mm	0.000807
D10	mm	
Uniformity Coefficient		> 79
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

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# TEST CERTIFICATE

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i2 Analytical Ltd  
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Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 07/02/2022  
Date Received: 24/02/2022  
Date Tested: 03/03/2022  
Sampled By: Not Given

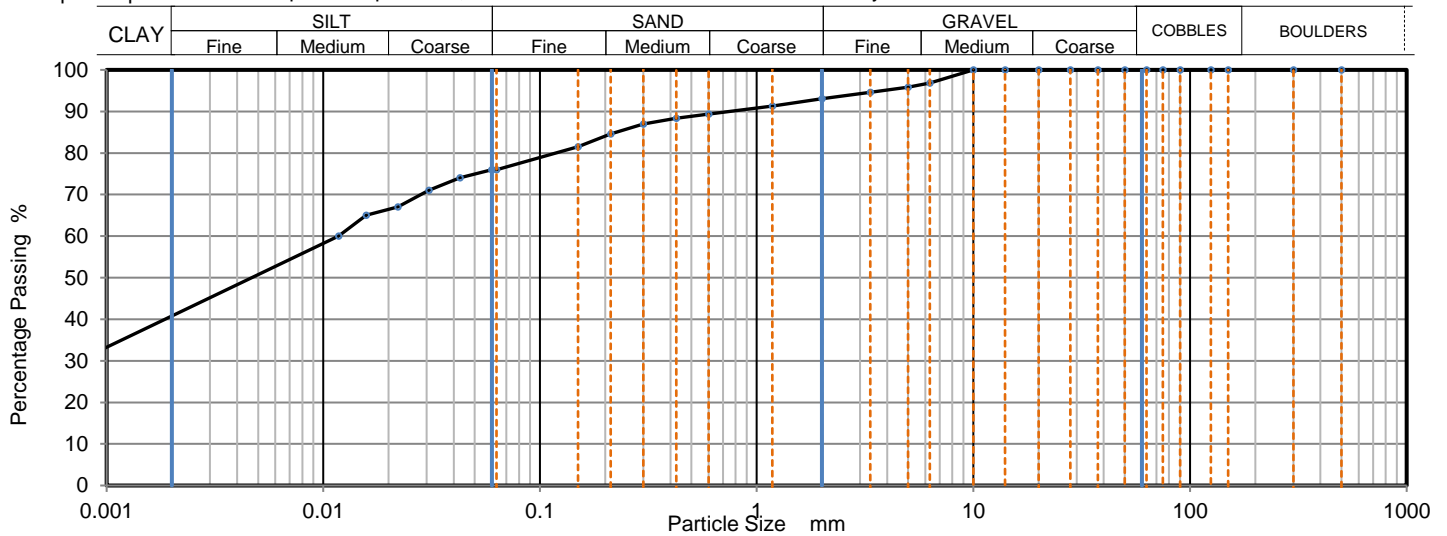
Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185952  
Hole No.: BH3  
Sample Reference: Not Given  
Sample Description: Greyish brown gravelly sandy very silty CLAY  
Sample Preparation: Sample was quartered, oven dried at 106.0 °C and broken down by hand.

Depth Top [m]: 4.65  
Depth Base [m]: 5.00  
Sample Type: D



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0598	76
300	100	0.0427	74
150	100	0.0307	71
125	100	0.0221	67
90	100	0.0157	65
75	100	0.0118	60
63	100	0.0008	31
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	100		
6.3	97		
5	96		
3.35	95		
2	93	Particle density (assumed) 2.65 Mg/m <sup>3</sup>	
1.18	91		
0.6	89		
0.425	88		
0.3	87		
0.212	85		
0.15	82		
0.063	76		

Sample Proportions	% dry mass
Very coarse	0
Gravel	7
Sand	17
Silt	35
Clay	41

Grading Analysis		
D100	mm	10
D60	mm	0.0115
D30	mm	
D10	mm	
Uniformity Coefficient		> 14
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

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# TEST CERTIFICATE

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Tested in Accordance with: BS 1377-2: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 07/02/2022  
Date Received: 24/02/2022  
Date Tested: 03/03/2022  
Sampled By: Not Given

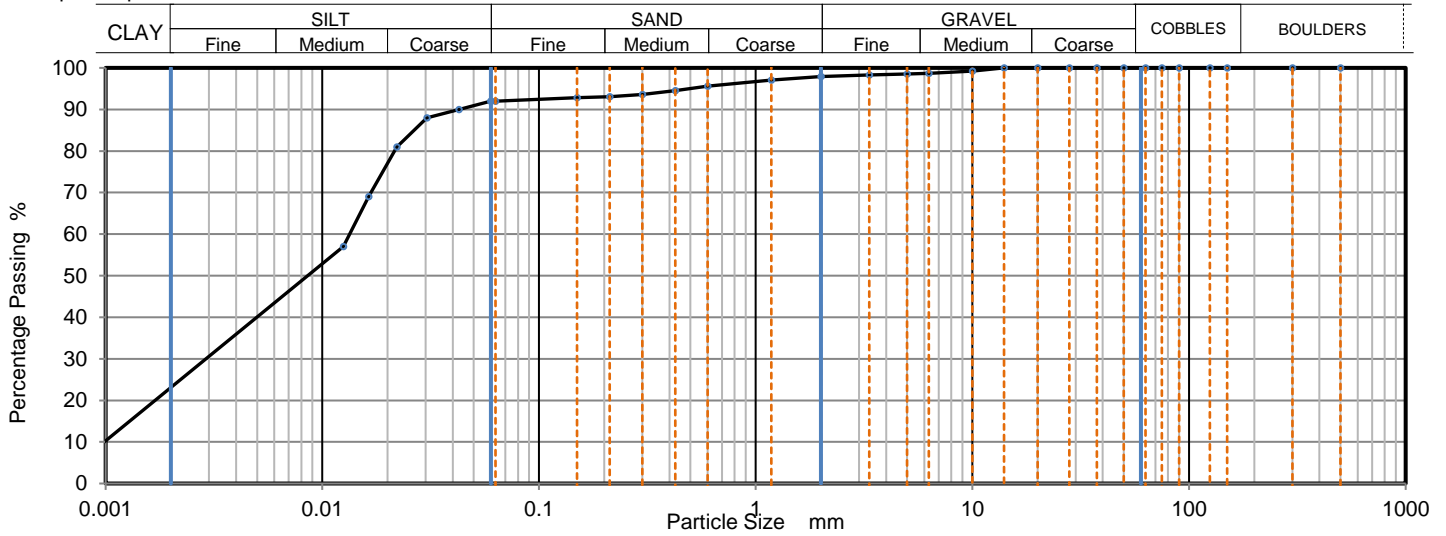
Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185953  
Hole No.: BH3  
Sample Reference: Not Given  
Sample Description: Dark brown slightly gravelly slightly sandy clayey SILT  
Sample Preparation: Sample was quartered, oven dried at 106.0 °C and broken down by hand.

Depth Top [m]: 7.15  
Depth Base [m]: 8.00  
Sample Type: D



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0598	92
300	100	0.0427	90
150	100	0.0304	88
125	100	0.0221	81
90	100	0.0164	69
75	100	0.0125	57
63	100	0.009	8
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	99		
6.3	99		
5	99		
3.35	98		
2	98	Particle density (assumed) 2.65 Mg/m3	
1.18	97		
0.6	96		
0.425	95		
0.3	94		
0.212	93		
0.15	93		
0.063	92		

Sample Proportions	% dry mass
Very coarse	0
Gravel	2
Sand	6
Silt	69
Clay	23

Grading Analysis		
D100	mm	14
D60	mm	0.0134
D30	mm	0.00289
D10	mm	0.000978
Uniformity Coefficient		14
Curvature Coefficient		0.64

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

*Dudzinska Anna*

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# TEST CERTIFICATE

## DETERMINATION OF PARTICLE SIZE DISTRIBUTION

Tested in Accordance with: BS 1377-2: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 03/03/2022  
Sampled By: Not Given

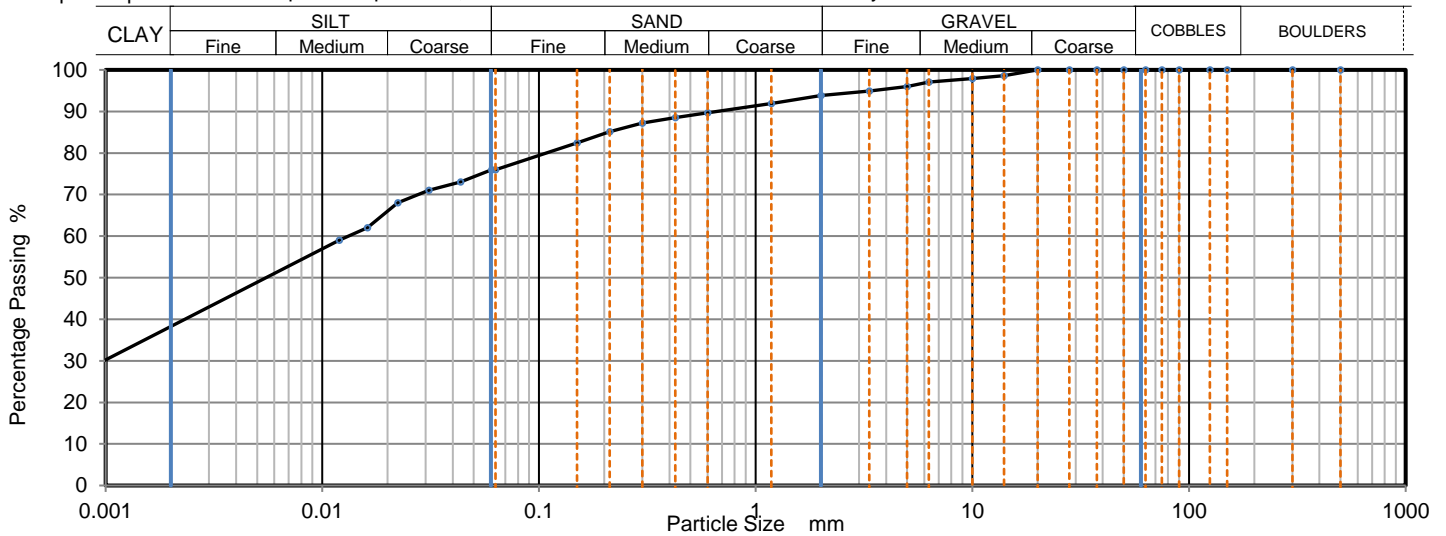
Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185959  
Hole No.: BH4  
Sample Reference: Not Given  
Sample Description: Greyish brown gravelly sandy SILT and CLAY  
Sample Preparation: Sample was quartered, oven dried at 106.0 °C and broken down by hand.

Depth Top [m]: 2.45  
Depth Base [m]: 2.65  
Sample Type: D



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0603	76
300	100	0.0434	73
150	100	0.0310	71
125	100	0.0223	68
90	100	0.0161	62
75	100	0.0120	59
63	100	0.0008	28
50	100		
37.5	100		
28	100		
20	100		
14	99		
10	98		
6.3	97		
5	96		
3.35	95		
2	94	Particle density (assumed) 2.65 Mg/m3	
1.18	92		
0.6	90		
0.425	89		
0.3	87		
0.212	85		
0.15	82		
0.063	76		

Sample Proportions	% dry mass
Very coarse	0
Gravel	6
Sand	18
Silt	38
Clay	38

Grading Analysis		
D100	mm	20
D60	mm	0.0132
D30	mm	0.001
D10	mm	
Uniformity Coefficient		> 16
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

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# TEST CERTIFICATE

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Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 03/03/2022  
Sampled By: Not Given

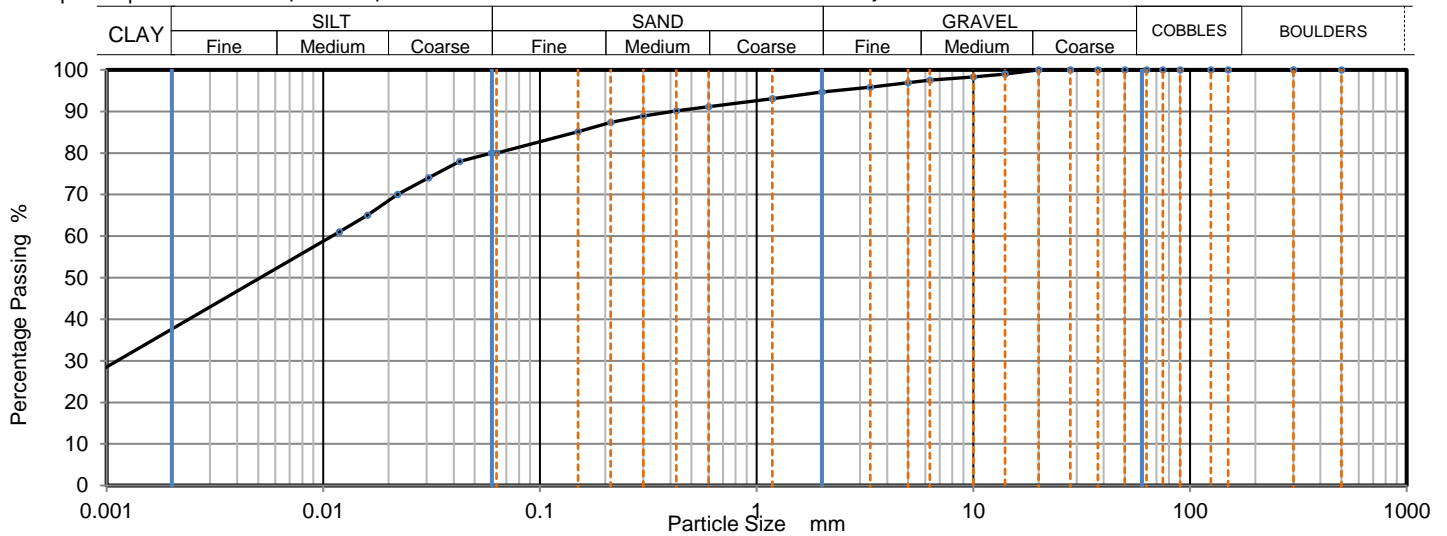
Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185962  
Hole No.: BH4  
Sample Reference: Not Given  
Sample Description: Greyish brown gravelly sandy very clayey SILT  
Sample Preparation: Sample was quartered, oven dried at 106.0 °C and broken down by hand.

Depth Top [m]: 6.95  
Depth Base [m]: 7.15  
Sample Type: D



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0596	80
300	100	0.0425	78
150	100	0.0306	74
125	100	0.0220	70
90	100	0.0160	65
75	100	0.0118	61
63	100	0.0008	26
50	100		
37.5	100		
28	100		
20	100		
14	99		
10	98		
6.3	98		
5	97		
3.35	96		
2	95	Particle density (assumed) 2.65 Mg/m <sup>3</sup>	
1.18	93		
0.6	91		
0.425	90		
0.3	89		
0.212	87		
0.15	85		
0.063	80		

Sample Proportions	% dry mass
Very coarse	0
Gravel	5
Sand	15
Silt	42
Clay	38

Grading Analysis		
D100	mm	20
D60	mm	0.0108
D30	mm	0.00112
D10	mm	
Uniformity Coefficient		> 13
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

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Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 03/03/2022  
Sampled By: Not Given

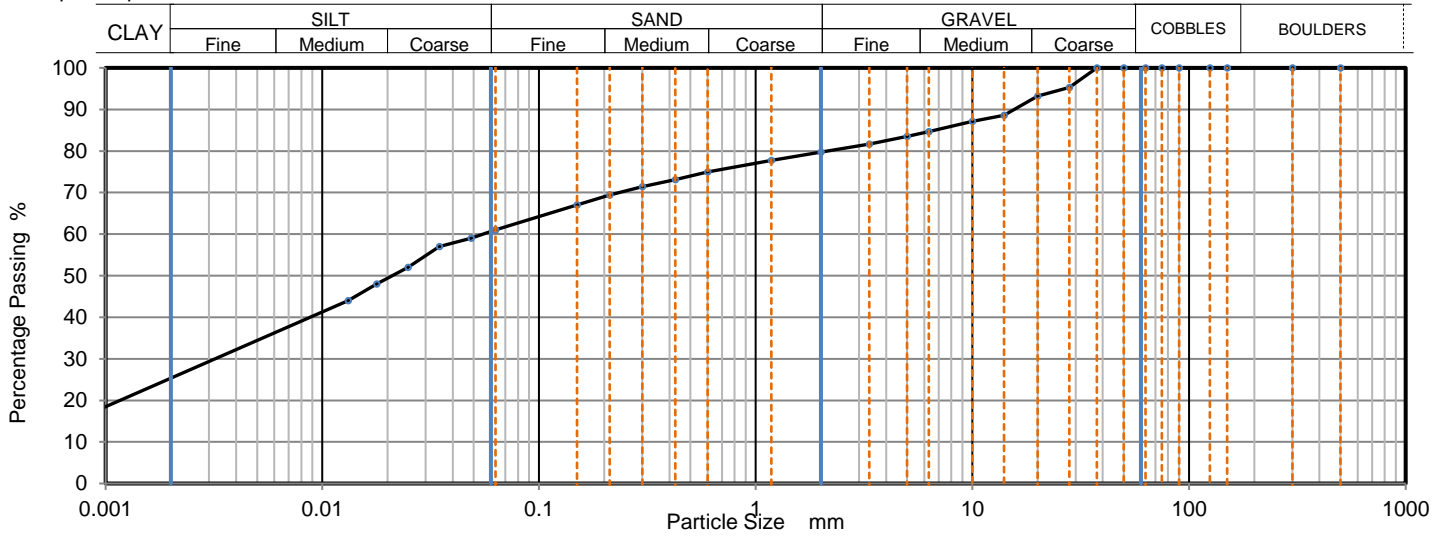
Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185966  
Hole No.: BH6  
Sample Reference: Not Given  
Sample Description: Grey very gravelly very sandy very clayey SILT  
Sample Preparation: Sample was quartered, oven dried at 106.3 °C and broken down by hand.

Depth Top [m]: 1.20  
Depth Base [m]: 1.65  
Sample Type: B



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0630	61
300	100	0.0487	59
150	100	0.0346	57
125	100	0.0248	52
90	100	0.0178	48
75	100	0.0132	44
63	100	0.009	17
50	100		
37.5	100		
28	95		
20	93		
14	89		
10	87		
6.3	85		
5	84		
3.35	82		
2	80	Particle density (assumed) 2.65 Mg/m3	
1.18	78		
0.6	75		
0.425	73		
0.3	71		
0.212	69		
0.15	67		
0.063	61		

Sample Proportions	% dry mass
Very coarse	0
Gravel	20
Sand	19
Silt	36
Clay	25

Grading Analysis		
D100	mm	37.5
D60	mm	0.0566
D30	mm	0.00321
D10	mm	
Uniformity Coefficient		> 66
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 16/02/2022  
Date Received: 24/02/2022  
Date Tested: 03/03/2022  
Sampled By: Not Given

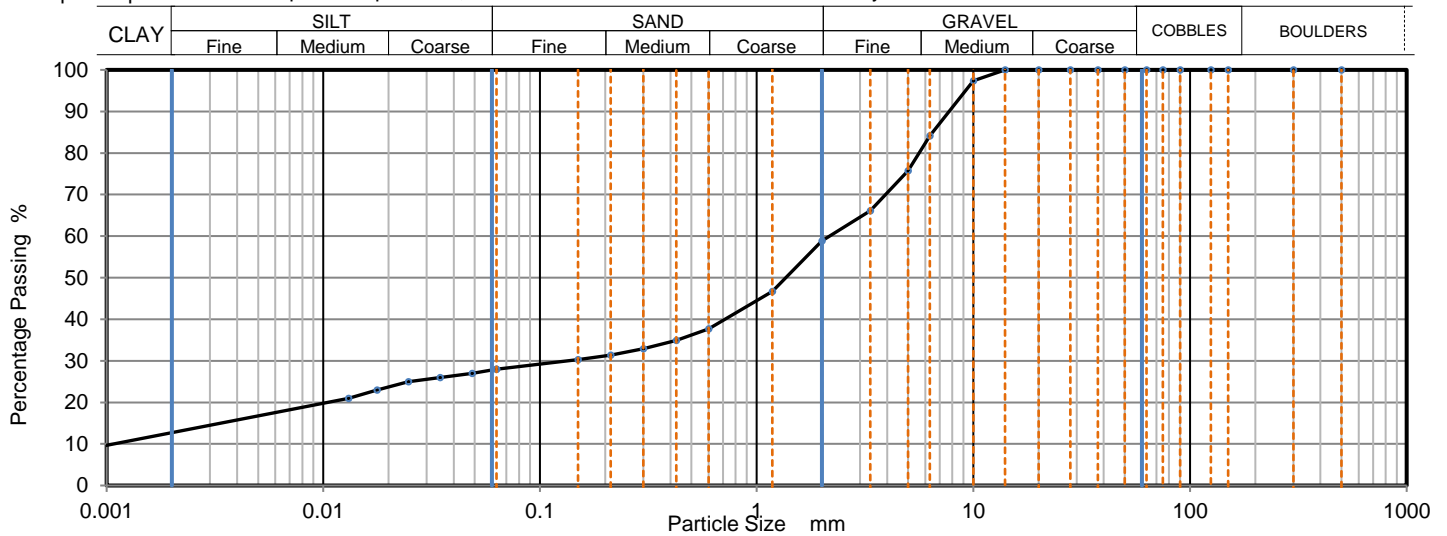
Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185970  
Hole No.: BH8  
Sample Reference: Not Given  
Sample Description: Dark brownish grey clayey silty very sandy organic GRAVEL  
Sample Preparation: Sample was quartered, oven dried at 106.9 °C and broken down by hand.

Depth Top [m]: 6.50  
Depth Base [m]: 7.00  
Sample Type: U



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0630	28
300	100	0.0486	27
150	100	0.0346	26
125	100	0.0247	25
90	100	0.0177	23
75	100	0.0131	21
63	100	0.009	9
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	97		
6.3	84		
5	76		
3.35	66		
2	59	Particle density (assumed) 2.65 Mg/m <sup>3</sup>	
1.18	47		
0.6	38		
0.425	35		
0.3	33		
0.212	31		
0.15	30		
0.063	28		

Sample Proportions	% dry mass
Very coarse	0
Gravel	41
Sand	31
Silt	15
Clay	13

Grading Analysis		
D100	mm	14
D60	mm	2.16
D30	mm	0.133
D10	mm	0.00108
Uniformity Coefficient		2000
Curvature Coefficient		7.6

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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4041

# TEST CERTIFICATE

## DETERMINATION OF PARTICLE SIZE DISTRIBUTION

Tested in Accordance with: BS 1377-2: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 16/02/2022  
Date Received: 24/02/2022  
Date Tested: 03/03/2022  
Sampled By: Not Given

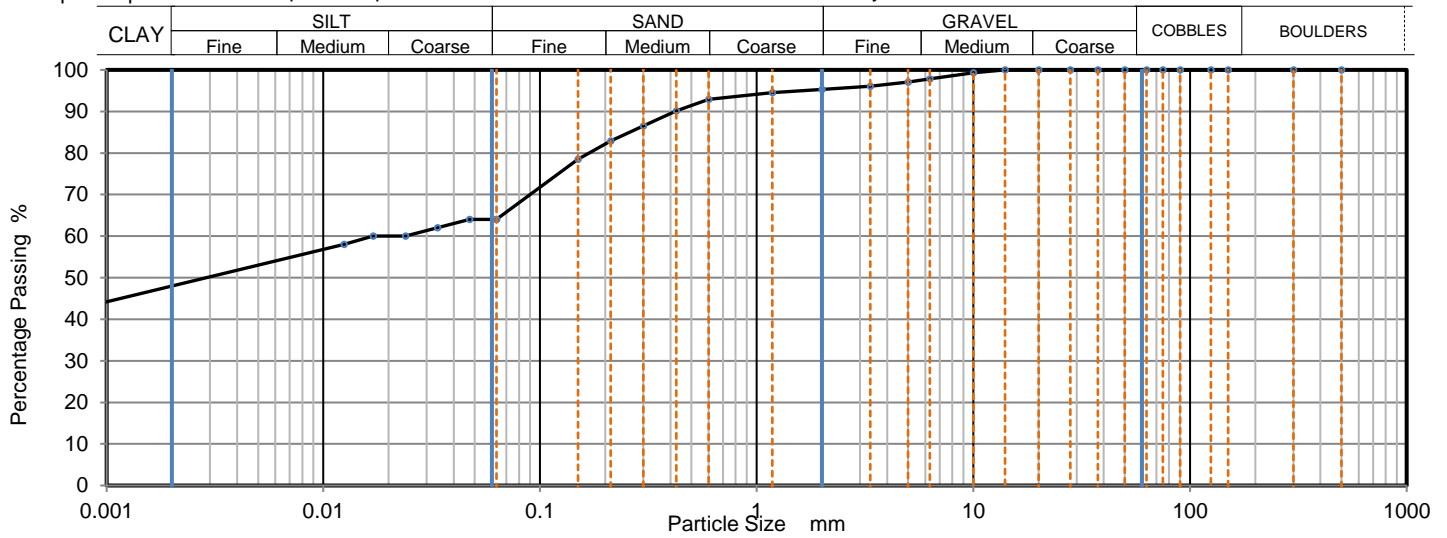
Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185973  
Hole No.: BH8  
Sample Reference: Not Given  
Sample Description: Brownish grey gravelly silty very sandy CLAY  
Sample Preparation: Sample was quartered, oven dried at 106.0 °C and broken down by hand.

Depth Top [m]: 14.50  
Depth Base [m]: 15.00  
Sample Type: B



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0630	64
300	100	0.0473	64
150	100	0.0337	62
125	100	0.0240	60
90	100	0.0170	60
75	100	0.0125	58
63	100	0.0008	43
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	99		
6.3	98		
5	97		
3.35	96		
2	95	Particle density (assumed) 2.65 Mg/m <sup>3</sup>	
1.18	95		
0.6	93		
0.425	90		
0.3	87		
0.212	83		
0.15	79		
0.063	64		

Sample Proportions	% dry mass
Very coarse	0
Gravel	5
Sand	31
Silt	16
Clay	48

Grading Analysis		
D100	mm	14
D60	mm	0.0245
D30	mm	
D10	mm	
Uniformity Coefficient		> 31
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF PARTICLE SIZE DISTRIBUTION

Tested in Accordance with: BS 1377-2: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 03/03/2022  
Sampled By: Not Given

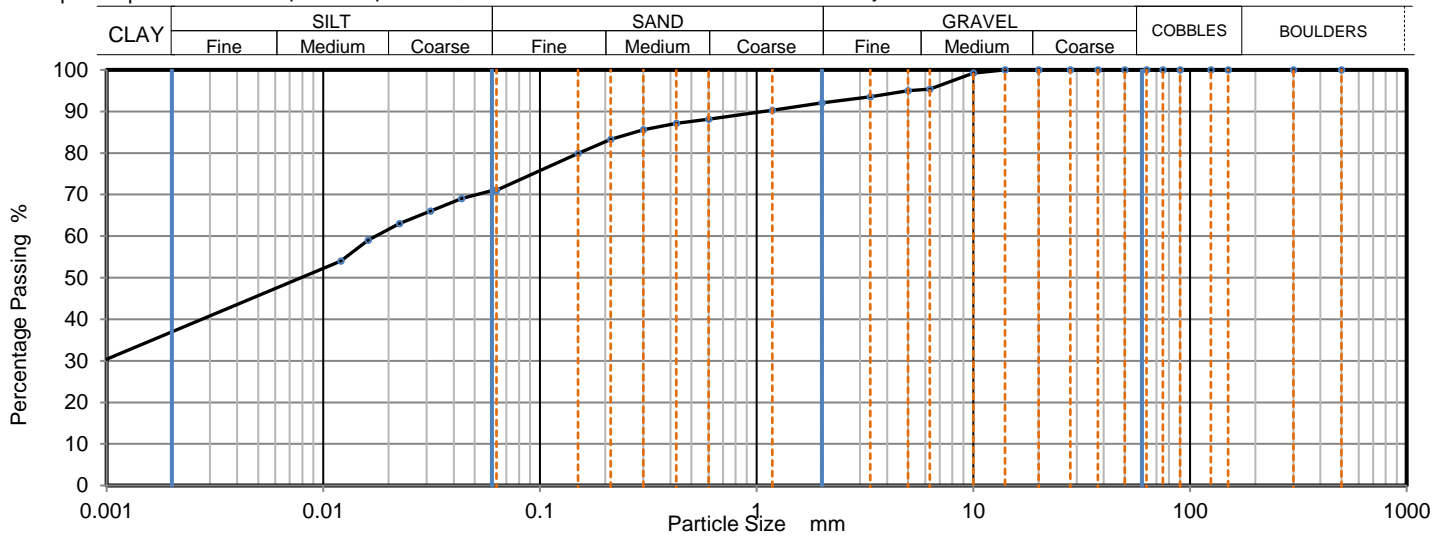
Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185988  
Hole No.: BH12  
Sample Reference: Not Given  
Sample Description: Greyish brown gravelly very sandy very silty CLAY  
Sample Preparation: Sample was quartered, oven dried at 106.0 °C and broken down by hand.

Depth Top [m]: 1.65  
Depth Base [m]: 1.80  
Sample Type: D



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0608	71
300	100	0.0434	69
150	100	0.0312	66
125	100	0.0224	63
90	100	0.0161	59
75	100	0.0120	54
63	100	0.0007	27
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	99		
6.3	95		
5	95		
3.35	94		
2	92	Particle density (assumed) 2.65 Mg/m <sup>3</sup>	
1.18	90		
0.6	88		
0.425	87		
0.3	86		
0.212	83		
0.15	80		
0.063	71		

Sample Proportions	% dry mass
Very coarse	0
Gravel	8
Sand	21
Silt	34
Clay	37

Grading Analysis		
D100	mm	14
D60	mm	0.0173
D30	mm	0.00095
D10	mm	
Uniformity Coefficient		> 25
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF PARTICLE SIZE DISTRIBUTION

Tested in Accordance with: BS 1377-2: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 03/03/2022  
Sampled By: Not Given

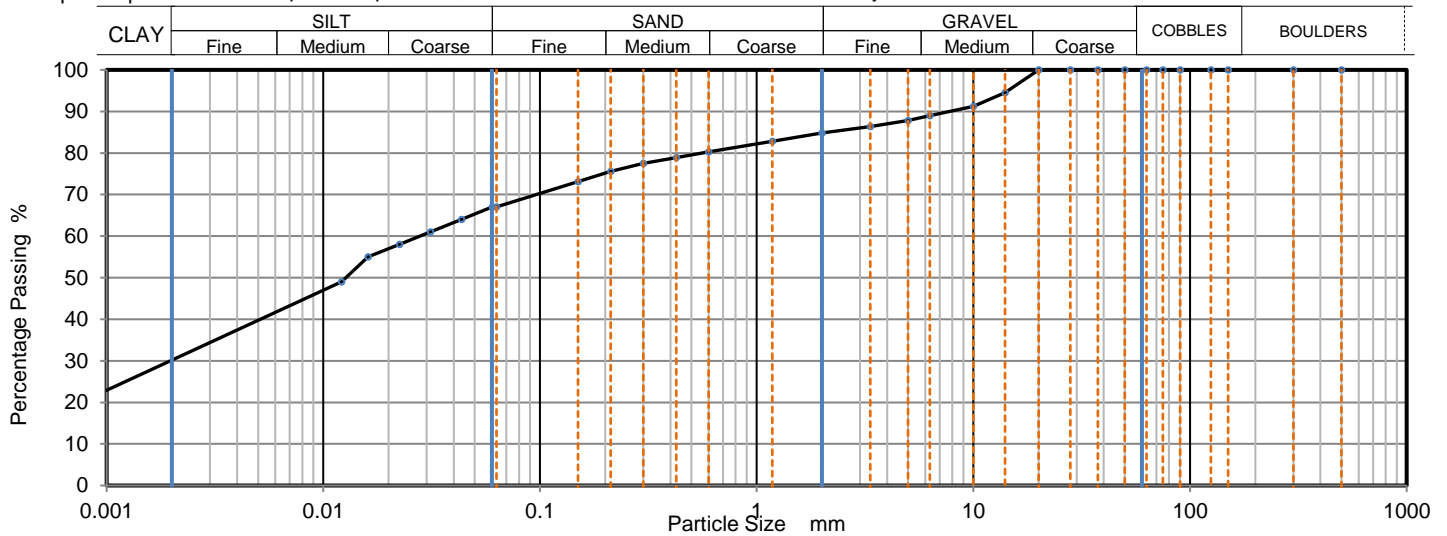
Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185990  
Hole No.: BH12  
Sample Reference: Not Given  
Sample Description: Greyish brown gravelly sandy very clayey SILT  
Sample Preparation: Sample was quartered, oven dried at 106.0 °C and broken down by hand.

Depth Top [m]: 4.45  
Depth Base [m]: 4.00  
Sample Type: D



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0603	67
300	100	0.0434	64
150	100	0.0312	61
125	100	0.0224	58
90	100	0.0161	55
75	100	0.0121	49
63	100	0.0008	21
50	100		
37.5	100		
28	100		
20	100		
14	95		
10	91		
6.3	89		
5	88		
3.35	86		
2	85	Particle density (assumed) 2.65 Mg/m3	
1.18	83		
0.6	80		
0.425	79		
0.3	78		
0.212	76		
0.15	73		
0.063	67		

Sample Proportions	% dry mass
Very coarse	0
Gravel	15
Sand	18
Silt	37
Clay	30

Grading Analysis		
D100	mm	20
D60	mm	0.0288
D30	mm	0.00196
D10	mm	
Uniformity Coefficient		> 35
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

*Dudzinska Anna*

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF PARTICLE SIZE DISTRIBUTION

Tested in Accordance with: BS 1377-2: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 03/03/2022  
Sampled By: Not Given

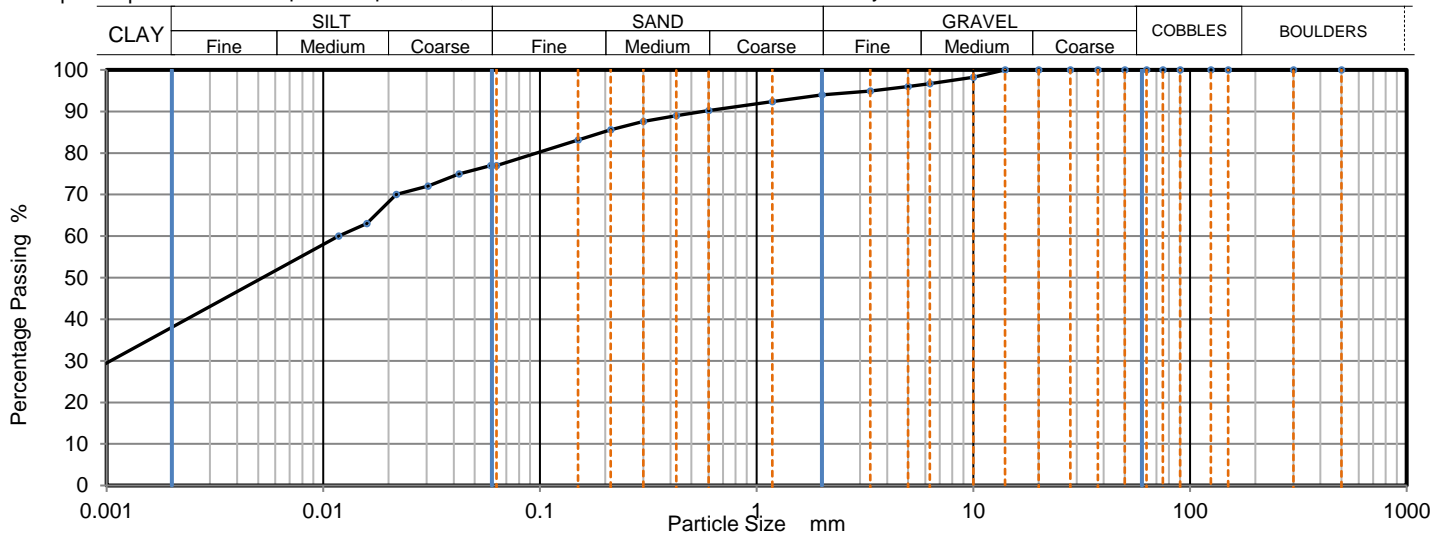
Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185996  
Hole No.: BH13  
Sample Reference: Not Given  
Sample Description: Greyish brown gravelly sandy CLAY and SILT  
Sample Preparation: Sample was quartered, oven dried at 106.0 °C and broken down by hand.

Depth Top [m]: 3.65  
Depth Base [m]: 4.00  
Sample Type: D



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0592	77
300	100	0.0423	75
150	100	0.0304	72
125	100	0.0217	70
90	100	0.0159	63
75	100	0.0118	60
63	100	0.0008	27
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	98		
6.3	97		
5	96		
3.35	95		
2	94	Particle density (assumed) 2.65 Mg/m <sup>3</sup>	
1.18	92		
0.6	90		
0.425	89		
0.3	88		
0.212	86		
0.15	83		
0.063	77		

Sample Proportions	% dry mass
Very coarse	0
Gravel	6
Sand	17
Silt	39
Clay	38

Grading Analysis		
D100	mm	14
D60	mm	0.0117
D30	mm	0.00101
D10	mm	
Uniformity Coefficient		> 14
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF PARTICLE SIZE DISTRIBUTION

Tested in Accordance with: BS 1377-2: 1990

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 03/03/2022  
Sampled By: Not Given

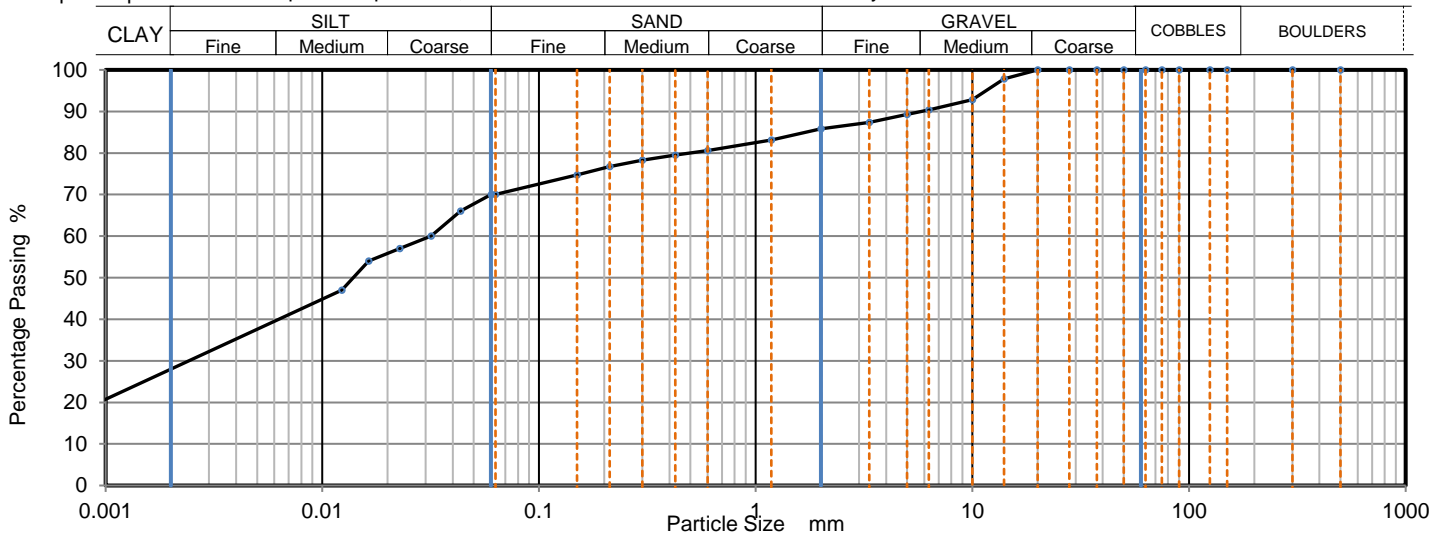
Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185997  
Hole No.: BH13  
Sample Reference: Not Given  
Sample Description: Greyish brown gravelly sandy very clayey SILT  
Sample Preparation: Sample was quartered, oven dried at 106.0 °C and broken down by hand.

Depth Top [m]: 8.45  
Depth Base [m]: 8.65  
Sample Type: D



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
500	100	0.0603	70
300	100	0.0434	66
150	100	0.0317	60
125	100	0.0228	57
90	100	0.0164	54
75	100	0.0123	47
63	100	0.0008	19
50	100		
37.5	100		
28	100		
20	100		
14	98		
10	93		
6.3	90		
5	89		
3.35	87		
2	86	Particle density (assumed) 2.65 Mg/m <sup>3</sup>	
1.18	83		
0.6	81		
0.425	80		
0.3	78		
0.212	77		
0.15	75		
0.063	70		

Sample Proportions	% dry mass
Very coarse	0
Gravel	14
Sand	16
Silt	42
Clay	28

Grading Analysis		
D100	mm	20
D60	mm	0.0316
D30	mm	0.00239
D10	mm	
Uniformity Coefficient		> 37
Curvature Coefficient		

Uniformity Coefficient calculated in accordance with BS EN ISO 14688-2:2018

Note: Tested in Accordance with BS1377:Part 2:1990, clauses 9.2 and 9.5

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

# SUMMARY REPORT

## DETERMINATION OF POINT LOAD STRENGTH

Tested in Accordance with: ISRM: 2007, pages 125-132

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 08/02 - 10/02/2022  
Date Received: 24/02/2022  
Date Tested: 07/03 - 08/03/2022  
Sampled By: Not Given

### Test results

Laboratory Reference	Hole No.	Sample				Description	Remarks # (including water content if measured)	Specimen Reference	Test Type see ISRM		Failure Valid (Y/N)	Dimensions				Force P kN	Equivalent diameter, De mm	Point Load Strength Index	
		Reference	Depth Top m	Depth Base m	Type				Type (D, A, I, B)	Direction (L, P or U)		Lne mm	W mm	Dps mm	Dps' mm			Is MPa	Is(50) MPa
2185976	BH11	Not Given	18.30	18.46	U	Greyish brown SANDSTONE	WC = 11.9%	1	A	U	YES	-	88.9	64.0	56.0	1.1	79.6	0.17	0.20
2185978	BH11	Not Given	19.85	20.34	U	Greyish brown SANDSTONE	WC = 14.6%	1	A	U	YES	-	89.7	61.0	39.0	2.4	66.7	0.53	0.60
2189957	BH2	Not Given	21.06	21.20	C	Greyish brown SANDSTONE	WC = 25.3%	1	A	U	YES	-	84.1	58.0	47.0	1.2	70.9	0.24	0.28
2185955	BH3	Not Given	19.84	19.99	U	Greyish brown SANDSTONE	WC = 14.9%	1	A	U	YES	-	87.4	51.0	32.0	2.9	59.7	0.80	0.87
2185956	BH3	Not Given	20.50	20.66	U	Greyish brown SANDSTONE	WC = 9.4%	1	A	U	YES	-	88.8	64.0	55.0	6.9	78.8	1.10	1.35

Note: # non accredited; Test Type: D - Diametral, A - Axial, I - Irregular Lump, B - Block; Direction: L - parallel to planes of weakness, P - perpendicular to planes of weakness, U - unknown or random;  
Dimensions: Dps - Distance between platens ( platen separation ), Dps' - at failure ( see ISRM note 6), Lne - Length from platens to nearest free end W - Width of shortest dimension perpendicular to load, P;  
Detailed legend for test and dimensions, based on ISRM, is shown above; Size factor, F = (De/50)0.45 for all tests

Comments: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# SUMMARY REPORT

## DETERMINATION OF UNIAXIAL COMPRESSIVE STRENGTH OF ROCK MATERIALS

Tested in Accordance with: ISRM, 2007, p153, part 1

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Contact: Harry Whittle  
Site Address: Corby EfW

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 08/02 - 14/02/2022  
Date Received: 24/02/2022  
Date Tested: 09/03/2022  
Sampled By: Not Given

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test results

Laboratory Reference	Hole No.	Sample				Description	Remarks	Specimen Dimensions (2)				Bulk density (2) Mg/m3	Water Content (1) %	Uniaxial Compression (3)			
		Reference	Depth Top m	Depth Base m	Type			Diameter mm	Length mm	H/D	Orientation of sample			Condition	Stress Rate Mpa/s	Mode of failure	UCS Mpa
2185977	BH11	Not Given	18.88	19.09	U	Greyish brown SANDSTONE	Sample is below recommended length to diameter ratio*	88.3	150.2	1.7	Vertical	2.37	15.3	as received	0.0163	MS + AC	3.64
2185939	BH2	Not Given	20.10	20.31	U	Light grey to orangish brown SANDSTONE	Sample is below recommended length to diameter ratio*	88.1	122.0	1.4	Vertical	2.24	19.6	as received	0.0328	MS	2.51

Note: 1 - ISRM p87 test 1, water content at 105 ± 3 oC, specimen as tested for UCS, 2 - ISRM p86 clause (vii), Caliper method used for determination of bulk volume and derivation of bulk density, 3 - ISRM p153 part 1, determination of Uniaxial Compressive Strength ( UCS ) of Rock Materials, above notes apply unless annotated otherwise in the remarks. Compaction machine: VJ Tech AUTOCON - VJT 51-3011; Mode of failure legend: S - Single shear, MS - multiple shear, AC - Axial cleavage, F - Fragmented

Comments: \*Duration of test, fell below time specified in ISRM method, 2007, p153, part1.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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**TEST CERTIFICATE**  
**DETERMINATION OF THE UNCONFINED**  
**COMPRESSIVE STRENGTH -**  
**LOAD FRAME METHOD**

i2 Analytical Ltd  
 Unit 8 Harrowden Road  
 Brackmills Industrial Estate  
 Northampton NN4 7EB



Tested in Accordance with: BS 1377-7: 1990: Clause 7.2

Client: Delta-Simons  
 Client Address: 3 Henley Office Park, Doddington Road,  
 Lincoln, LN6 3QR

Client Reference: 15-0645.05  
 Job Number: 22-42014  
 Date Sampled: 14/02/2022  
 Date Received: 24/02/2022  
 Date Tested: 09/03/2022  
 Sampled By: Not Given

Contact: Harry Whittle  
 Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

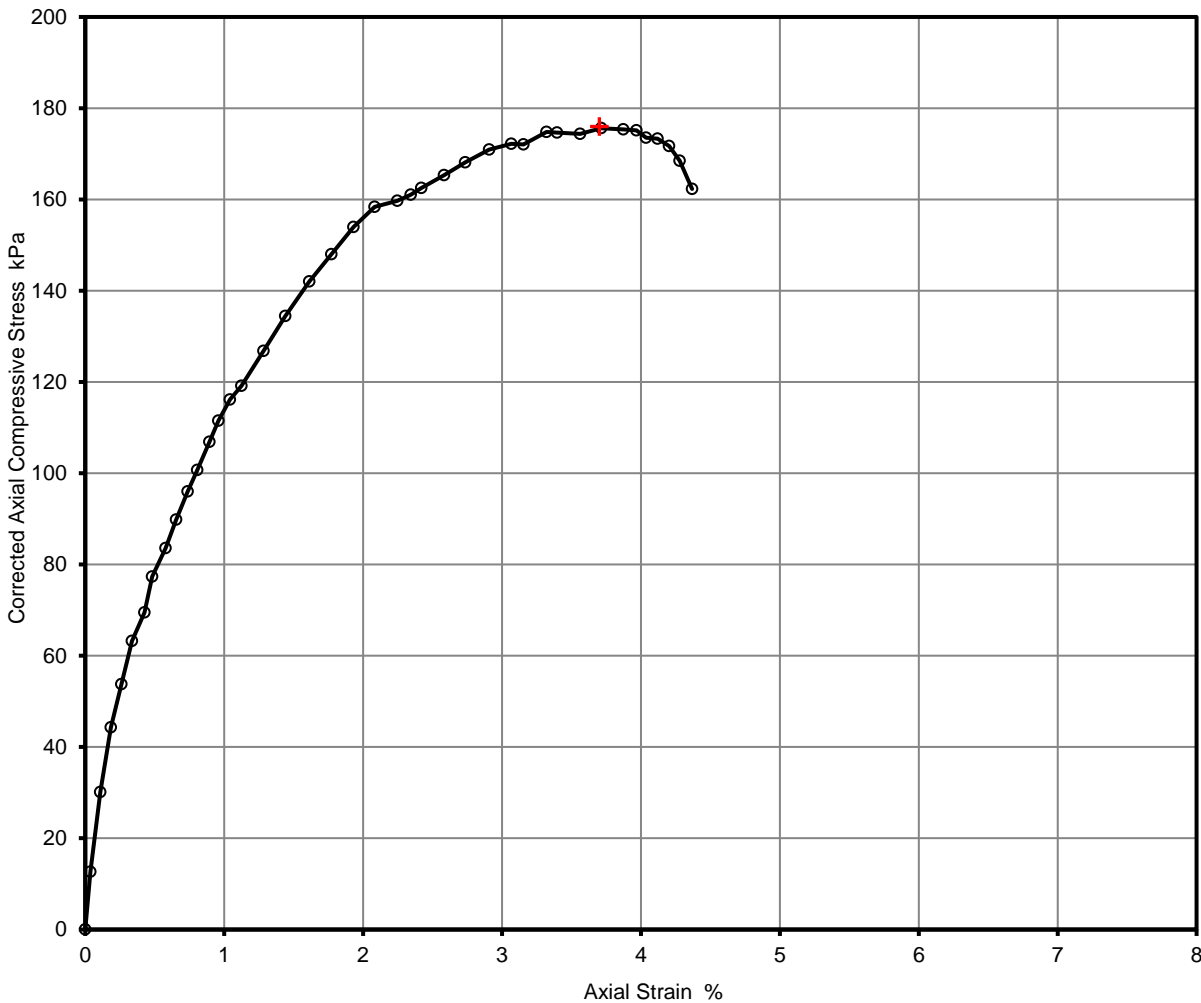
**Test Results:**

Laboratory Reference: 2185942  
 Hole No.: BH2  
 Sample Reference: Not Given  
 Sample Description: Dark grey silty CLAY  
 Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

Depth Top [m]: 22.23  
 Depth Base [m]: 22.45  
 Sample Type: U

Test Number	1	Rate of Strain	1.0	%/min
Length	157.5	Axial Strain at failure	3.7	%
Diameter	89.6	Unconfined Compressive Strength	176	kPa
Bulk Density	2.12	Mode of Failure	Brittle	
Moisture Content	16.0			
Dry Density	1.82			

**Axial Compressive Stress v Axial Strain**



Note: Axial compressive stress corrected for area change, and membrane effects (if used)

Remarks: Sample is below recommended length to diameter ratio.  
 Preliminary report

Signed:

Anna Dudzinska  
 Deputy Head of Geo Office Section  
 for and on behalf of i2 Analytical Ltd

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**TEST CERTIFICATE**  
**DETERMINATION OF THE UNCONFINED**  
**COMPRESSIVE STRENGTH -**  
**LOAD FRAME METHOD**

Tested in Accordance with: BS 1377-7: 1990: Clause 7.2

i2 Analytical Ltd  
 Unit 8 Harrowden Road  
 Brackmills Industrial Estate  
 Northampton NN4 7EB



Client: Delta-Simons  
 Client Address: 3 Henley Office Park, Doddington Road,  
 Lincoln, LN6 3QR

Client Reference: 15-0645.05  
 Job Number: 22-42014  
 Date Sampled: 14/02/2022  
 Date Received: 24/02/2022  
 Date Tested: 09/03/2022  
 Sampled By: Not Given

Contact: Harry Whittle  
 Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

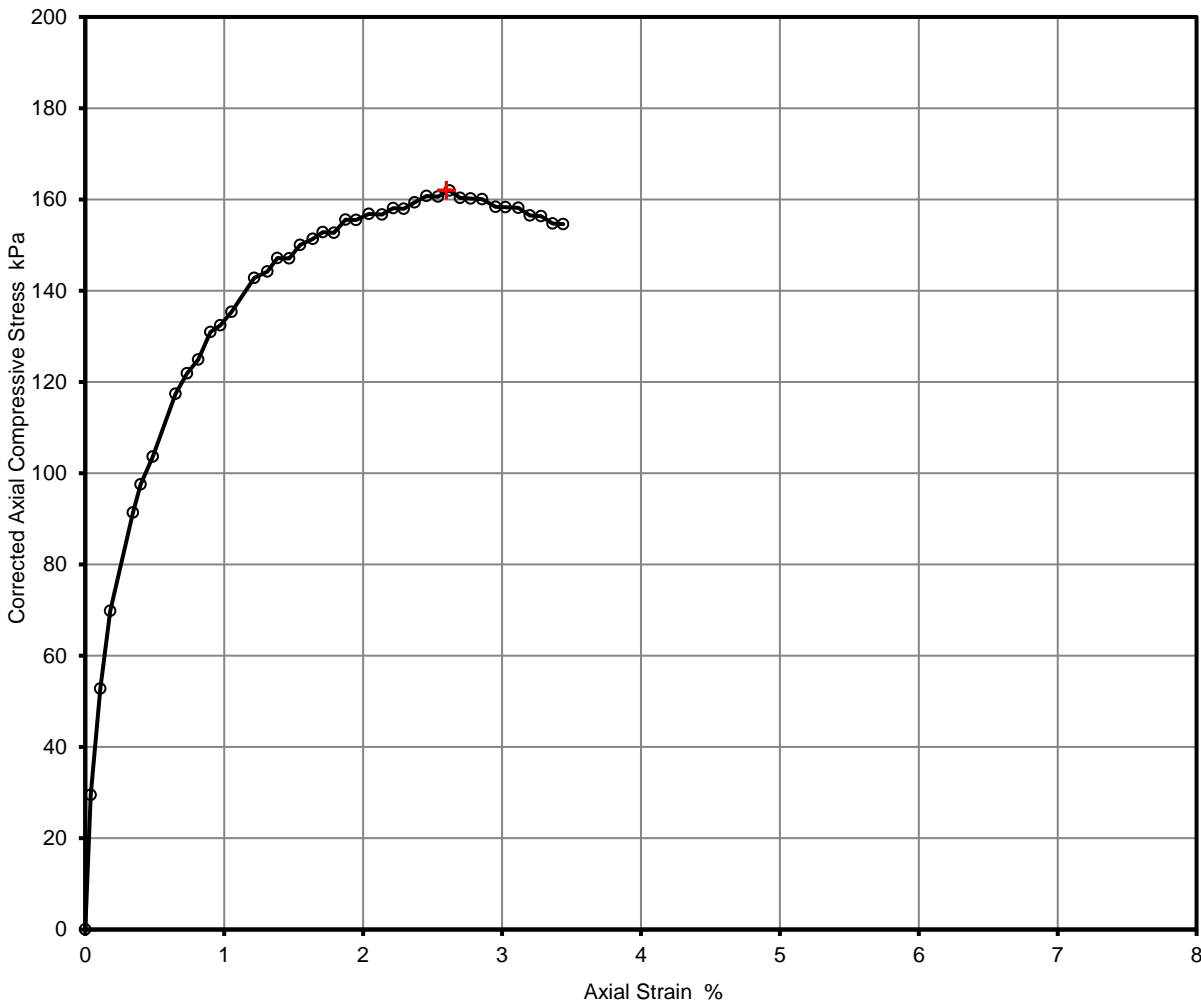
**Test Results:**

Laboratory Reference: 2185944  
 Hole No.: BH2  
 Sample Reference: Not Given  
 Sample Description: Dark grey SILT  
 Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

Depth Top [m]: 23.26  
 Depth Base [m]: 23.58  
 Sample Type: U

Test Number	1	Rate of Strain	1.0	%/min
Length	183.1	Axial Strain at failure	2.6	%
Diameter	90.5	Unconfined Compressive Strength	162	kPa
Bulk Density	2.14	Mode of Failure	Compound	
Moisture Content	13.0			
Dry Density	1.90			

**Axial Compressive Stress v Axial Strain**



Note: Axial compressive stress corrected for area change, and membrane effects (if used)

Remarks: Preliminary report

Signed:

Anna Dudzinska  
 Deputy Head of Geo Office Section  
 for and on behalf of i2 Analytical Ltd

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**TEST CERTIFICATE**  
**DETERMINATION OF THE UNCONFINED**  
**COMPRESSIVE STRENGTH -**  
**LOAD FRAME METHOD**

Tested in Accordance with: BS 1377-7: 1990: Clause 7.2

i2 Analytical Ltd  
 Unit 8 Harrowden Road  
 Brackmills Industrial Estate  
 Northampton NN4 7EB



Client: Delta-Simons  
 Client Address: 3 Henley Office Park, Doddington Road,  
 Lincoln, LN6 3QR

Client Reference: 15-0645.05  
 Job Number: 22-42014  
 Date Sampled: 14/02/2022  
 Date Received: 24/02/2022  
 Date Tested: 09/03/2022  
 Sampled By: Not Given

Contact: Harry Whittle  
 Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

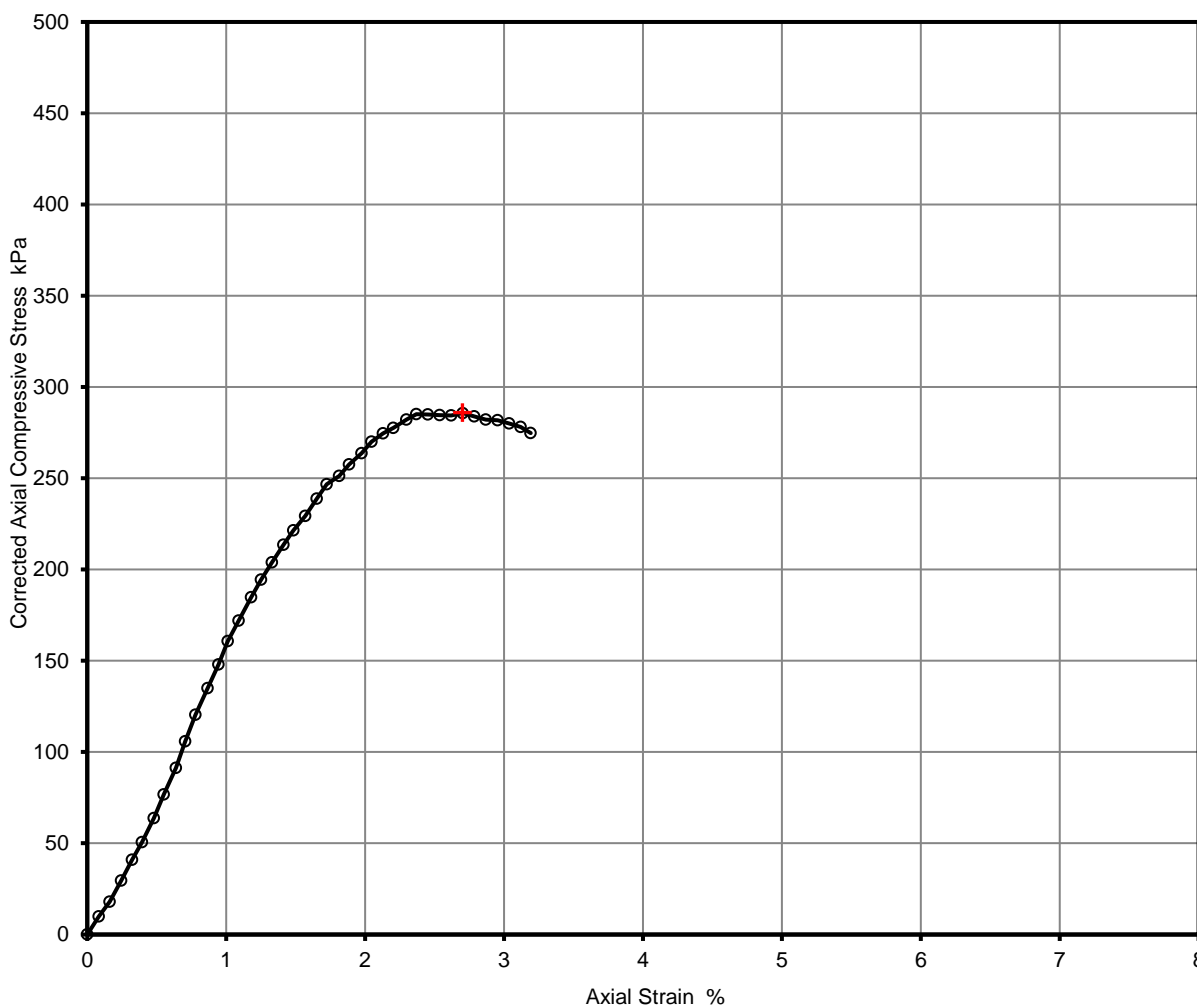
**Test Results:**

Laboratory Reference: 2185945  
 Hole No.: BH2  
 Sample Reference: Not Given  
 Sample Description: Dark grey SILT  
 Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

Depth Top [m]: 25.29  
 Depth Base [m]: 25.50  
 Sample Type: U

Test Number	1	Rate of Strain	1.0	%/min
Length	179.8	Axial Strain at failure	2.7	%
Diameter	88.1	Unconfined Compressive Strength	286	kPa
Bulk Density	2.10	Mode of Failure	Compound	
Moisture Content	20.0			
Dry Density	1.76			

**Axial Compressive Stress v Axial Strain**



Note: Axial compressive stress corrected for area change, and membrane effects (if used)

Remarks: Preliminary report

Signed:

Anna Dudzinska  
 Deputy Head of Geo Office Section  
 for and on behalf of i2 Analytical Ltd

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**TEST CERTIFICATE**  
**DETERMINATION OF THE UNCONFINED**  
**COMPRESSIVE STRENGTH -**  
**LOAD FRAME METHOD**

Tested in Accordance with: BS 1377-7: 1990: Clause 7.2

i2 Analytical Ltd  
 Unit 8 Harrowden Road  
 Brackmills Industrial Estate  
 Northampton NN4 7EB



Client: Delta-Simons  
 Client Address: 3 Henley Office Park, Doddington Road,  
 Lincoln, LN6 3QR  
 Contact: Harry Whittle  
 Site Address: Corby EfW

Client Reference: 15-0645.05  
 Job Number: 22-42014  
 Date Sampled: 15/02/2022  
 Date Received: 24/02/2022  
 Date Tested: 09/03/2022  
 Sampled By: Not Given

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

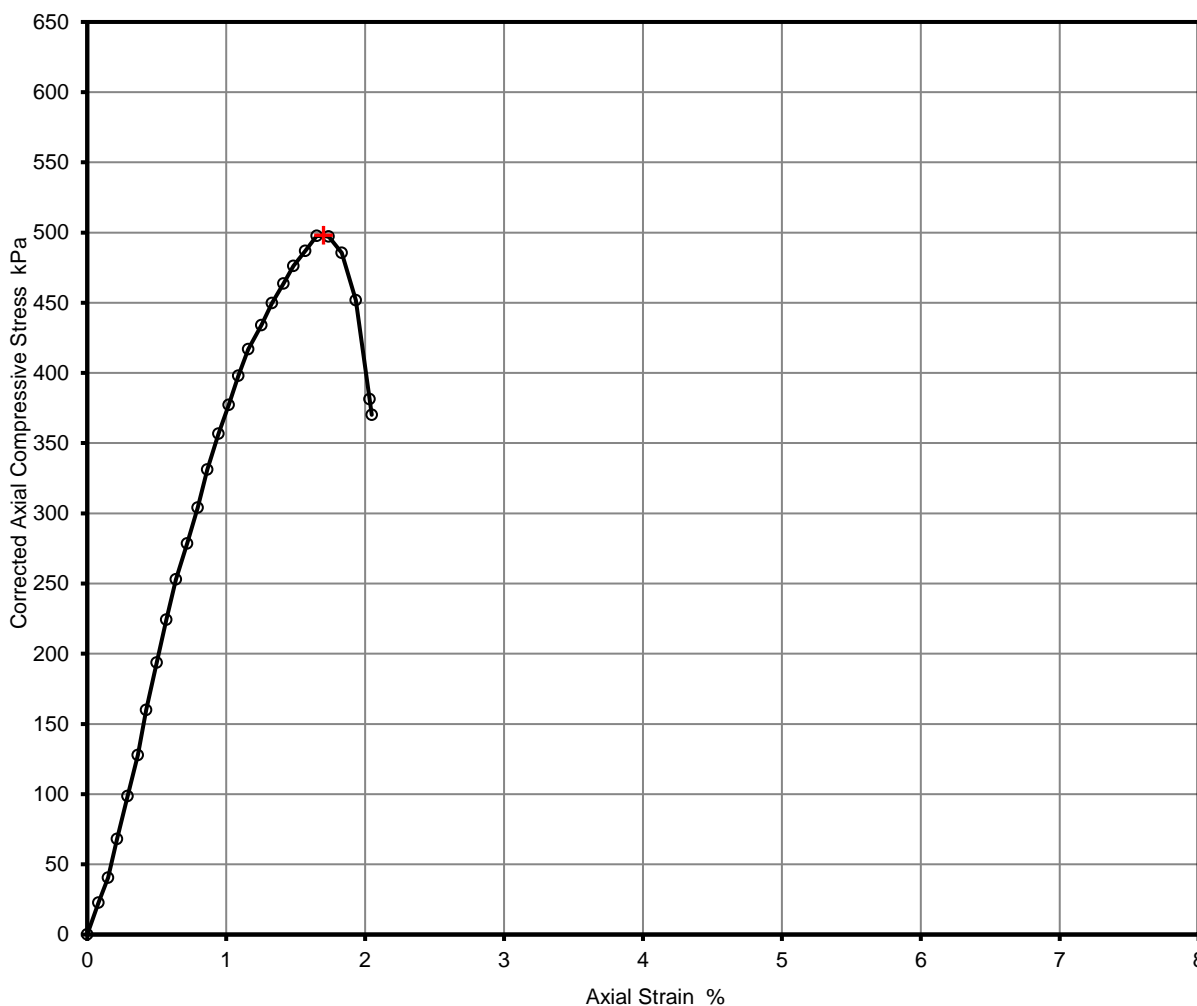
**Test Results:**

Laboratory Reference: 2185948  
 Hole No.: BH2  
 Sample Reference: Not Given  
 Sample Description: Dark grey clayey SILT  
 Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

Depth Top [m]: 27.14  
 Depth Base [m]: 27.49  
 Sample Type: U

Test Number	1	Rate of Strain	1.0	%/min
Length	200.2	Axial Strain at failure	1.7	%
Diameter	88.6	Unconfined Compressive Strength	498	kPa
Bulk Density	2.20	Mode of Failure	Brittle	
Moisture Content	12.0			
Dry Density	1.96			

**Axial Compressive Stress v Axial Strain**



Note: Axial compressive stress corrected for area change, and membrane effects (if used)

Remarks: Preliminary report

Signed:

Anna Dudzinska  
 Deputy Head of Geo Office Section  
 for and on behalf of i2 Analytical Ltd

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**TEST CERTIFICATE**  
**DETERMINATION OF THE UNCONFINED**  
**COMPRESSIVE STRENGTH -**  
**LOAD FRAME METHOD**

i2 Analytical Ltd  
 Unit 8 Harrowden Road  
 Brackmills Industrial Estate  
 Northampton NN4 7EB



Tested in Accordance with: BS 1377-7: 1990: Clause 7.2

Client: Delta-Simons  
 Client Address: 3 Henley Office Park, Doddington Road,  
 Lincoln, LN6 3QR

Client Reference: 15-0645.05  
 Job Number: 22-42014  
 Date Sampled: 15/02/2022  
 Date Received: 24/02/2022  
 Date Tested: 09/03/2022  
 Sampled By: Not Given

Contact: Harry Whittle  
 Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

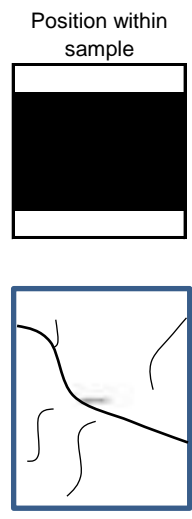
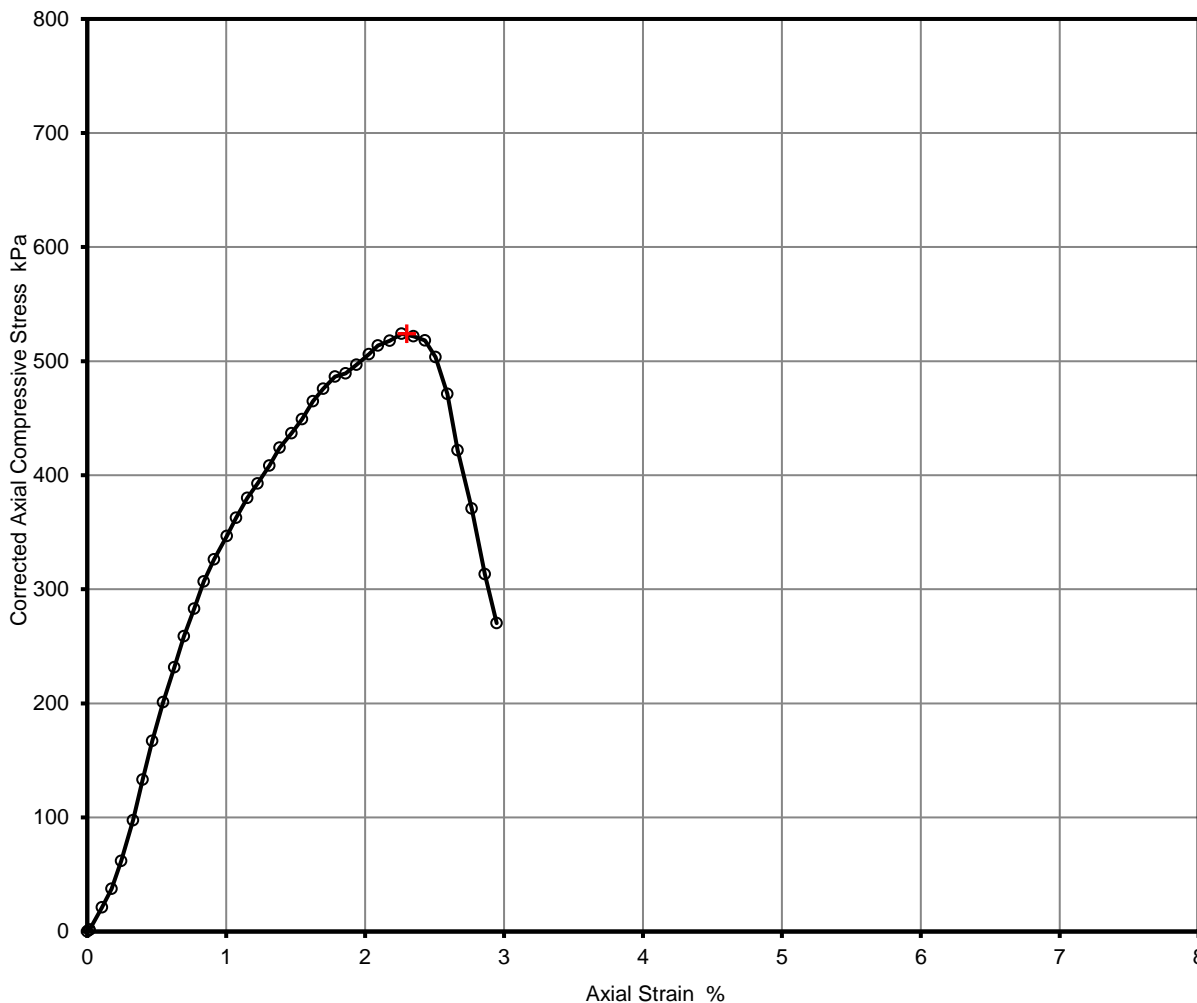
**Test Results:**

Laboratory Reference: 2185950  
 Hole No.: BH2  
 Sample Reference: Not Given  
 Sample Description: Dark grey silty CLAY  
 Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

Depth Top [m]: 29.06  
 Depth Base [m]: 29.37  
 Sample Type: U

Test Number	1	Rate of Strain	1.0	%/min
Length	188.3	Axial Strain at failure	2.3	%
Diameter	88.4	Unconfined Compressive Strength	524	kPa
Bulk Density	2.21	Mode of Failure	Brittle	
Moisture Content	8.8			
Dry Density	2.04			

**Axial Compressive Stress v Axial Strain**



Note: Axial compressive stress corrected for area change, and membrane effects (if used)

Remarks: Unable to take a photo.  
 Preliminary report

Signed:

Anna Dudzinska  
 Deputy Head of Geo Office Section  
 for and on behalf of i2 Analytical Ltd

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**TEST CERTIFICATE**  
**DETERMINATION OF THE UNCONFINED**  
**COMPRESSIVE STRENGTH -**  
**LOAD FRAME METHOD**

i2 Analytical Ltd  
 Unit 8 Harrowden Road  
 Brackmills Industrial Estate  
 Northampton NN4 7EB



Tested in Accordance with: BS 1377-7: 1990: Clause 7.2

Client: Delta-Simons  
 Client Address: 3 Henley Office Park, Doddington Road,  
 Lincoln, LN6 3QR

Client Reference: 15-0645.05  
 Job Number: 22-42014  
 Date Sampled: 10/02/2022  
 Date Received: 24/02/2022  
 Date Tested: 09/03/2022  
 Sampled By: Not Given

Contact: Harry Whittle  
 Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

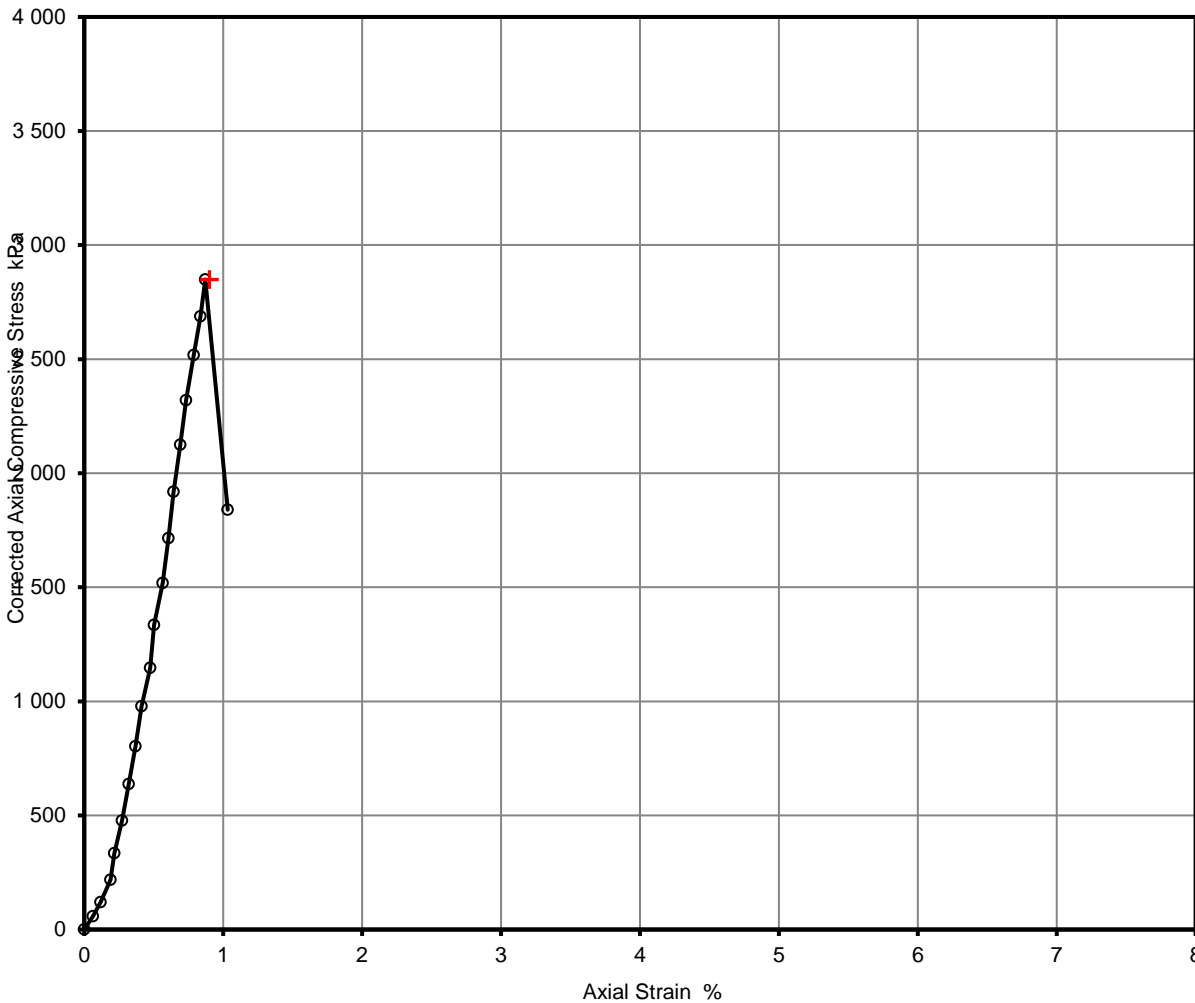
**Test Results:**

Laboratory Reference: 2185954  
 Hole No.: BH3  
 Sample Reference: Not Given  
 Sample Description: Greyish brown slightly clayey silty SAND  
 Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

Depth Top [m]: 19.65  
 Depth Base [m]: 19.84  
 Sample Type: U

Test Number	1	Rate of Strain	1.0	%/min
Length	143.3	Axial Strain at failure	0.9	%
Diameter	86.7	Unconfined Compressive Strength	2849	kPa
Bulk Density	2.37	Mode of Failure	Brittle	
Moisture Content	15.0			
Dry Density	2.06			

**Axial Compressive Stress v Axial Strain**



Note: Axial compressive stress corrected for area change, and membrane effects (if used)

Remarks: Sample is below recommended length to diameter ratio.  
 Preliminary report

Signed:

Anna Dudzinska  
 Deputy Head of Geo Office Section  
 for and on behalf of i2 Analytical Ltd

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**TEST CERTIFICATE**  
**DETERMINATION OF THE UNCONFINED**  
**COMPRESSIVE STRENGTH -**  
**LOAD FRAME METHOD**

Tested in Accordance with: BS 1377-7: 1990: Clause 7.2

i2 Analytical Ltd  
 Unit 8 Harrowden Road  
 Brackmills Industrial Estate  
 Northampton NN4 7EB



Client: Delta-Simons  
 Client Address: 3 Henley Office Park, Doddington Road,  
 Lincoln, LN6 3QR

Client Reference: 15-0645.05  
 Job Number: 22-42014  
 Date Sampled: 10/02/2022  
 Date Received: 24/02/2022  
 Date Tested: 09/03/2022  
 Sampled By: Not Given

Contact: Harry Whittle  
 Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

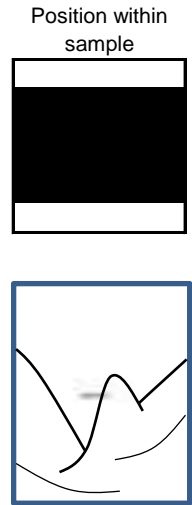
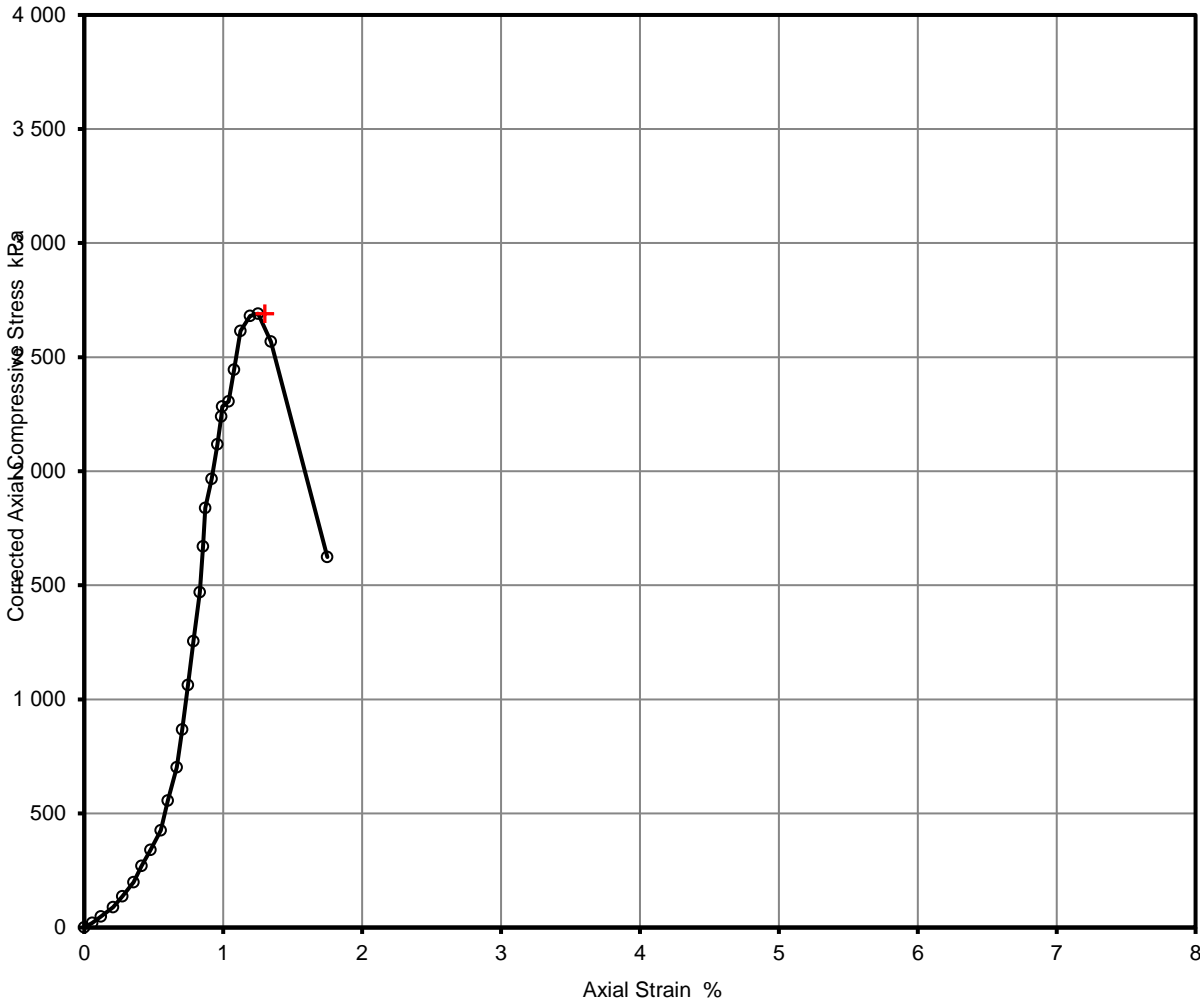
**Test Results:**

Laboratory Reference: 2185957  
 Hole No.: BH3  
 Sample Reference: Not Given  
 Sample Description: Dark grey sandy SILT  
 Sample Preparation: Sample is below recommended length to diameter ratio.

Depth Top [m]: 21.03  
 Depth Base [m]: 21.25  
 Sample Type: U

Test Number	1	Rate of Strain	1.0	%/min
Length	174.3	Axial Strain at failure	1.3	%
Diameter	86.9	Unconfined Compressive Strength	2691	kPa
Bulk Density	2.41	Mode of Failure	Compound	
Moisture Content	15.0			
Dry Density	2.09			

**Axial Compressive Stress v Axial Strain**



Note: Axial compressive stress corrected for area change, and membrane effects (if used)

Remarks: Unable to take a photo.  
 Preliminary report

Signed:

Anna Dudzinska  
 Deputy Head of Geo Office Section  
 for and on behalf of i2 Analytical Ltd

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**TEST CERTIFICATE**  
**DETERMINATION OF THE UNCONFINED**  
**COMPRESSIVE STRENGTH -**  
**LOAD FRAME METHOD**

i2 Analytical Ltd  
 Unit 8 Harrowden Road  
 Brackmills Industrial Estate  
 Northampton NN4 7EB



Tested in Accordance with: BS 1377-7: 1990: Clause 7.2

Client: Delta-Simons  
 Client Address: 3 Henley Office Park, Doddington Road,  
 Lincoln, LN6 3QR

Client Reference: 15-0645.05  
 Job Number: 22-42014  
 Date Sampled: 08/02/2022  
 Date Received: 24/02/2022  
 Date Tested: 09/03/2022  
 Sampled By: Not Given

Contact: Harry Whittle  
 Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

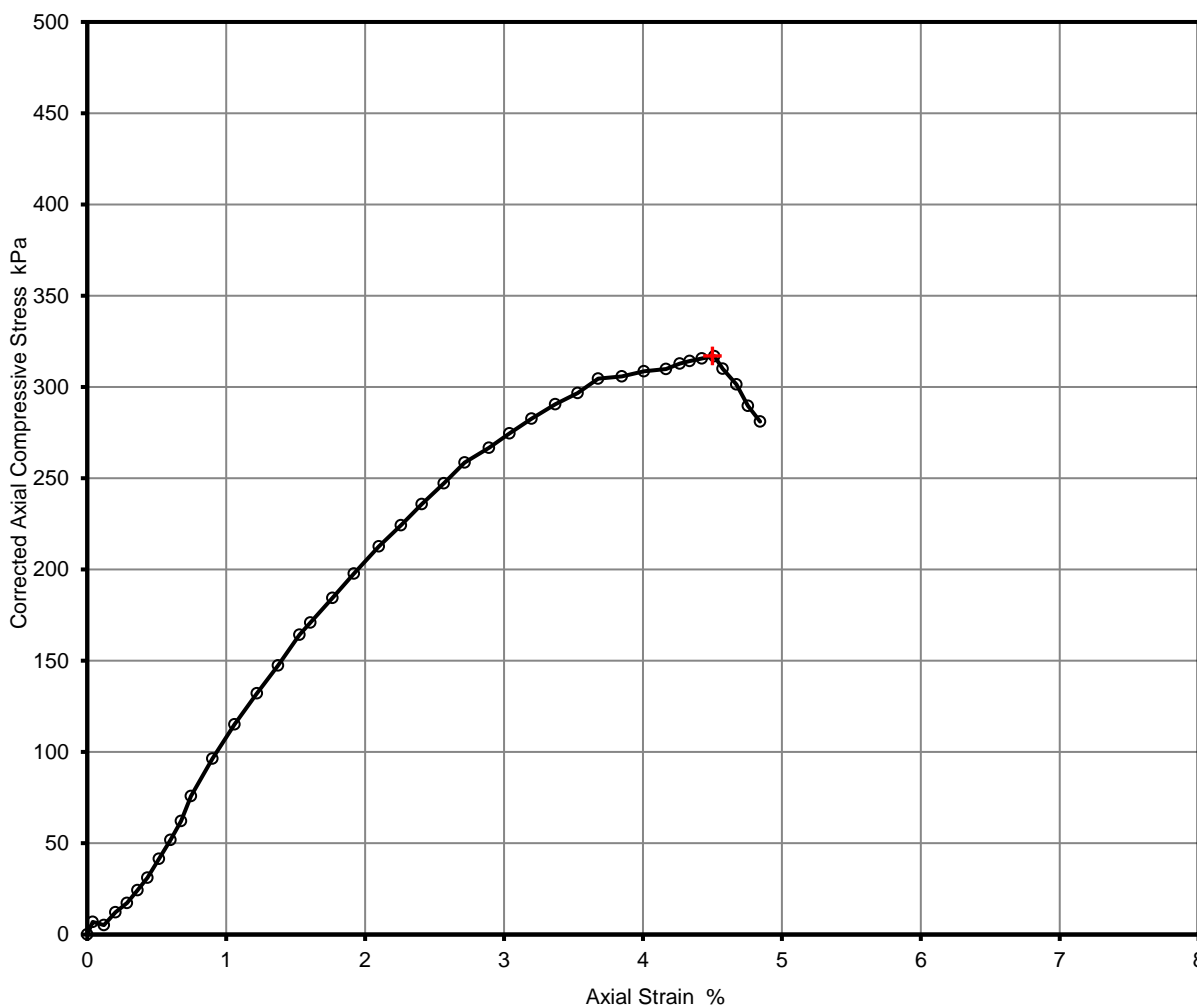
**Test Results:**

Laboratory Reference: 2185979  
 Hole No.: BH11  
 Sample Reference: Not Given  
 Sample Description: Dark grey silty CLAY  
 Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

Depth Top [m]: 21.26  
 Depth Base [m]: 21.73  
 Sample Type: U

Test Number	1	Rate of Strain	1.0	%/min
Length	181.9	Axial Strain at failure	4.5	%
Diameter	85.6	Unconfined Compressive Strength	317	kPa
Bulk Density	2.15	Mode of Failure	Brittle	
Moisture Content	11.0			
Dry Density	1.93			

**Axial Compressive Stress v Axial Strain**



Note: Axial compressive stress corrected for area change, and membrane effects (if used)

Remarks: Preliminary report

Signed:

Anna Dudzinska  
 Deputy Head of Geo Office Section  
 for and on behalf of i2 Analytical Ltd

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**TEST CERTIFICATE**  
**DETERMINATION OF THE UNCONFINED**  
**COMPRESSIVE STRENGTH -**  
**LOAD FRAME METHOD**

Tested in Accordance with: BS 1377-7: 1990: Clause 7.2

i2 Analytical Ltd  
 Unit 8 Harrowden Road  
 Brackmills Industrial Estate  
 Northampton NN4 7EB



Client: Delta-Simons  
 Client Address: 3 Henley Office Park, Doddington Road,  
 Lincoln, LN6 3QR

Client Reference: 15-0645.05  
 Job Number: 22-42014  
 Date Sampled: 08/02/2022  
 Date Received: 24/02/2022  
 Date Tested: 09/03/2022  
 Sampled By: Not Given

Contact: Harry Whittle  
 Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

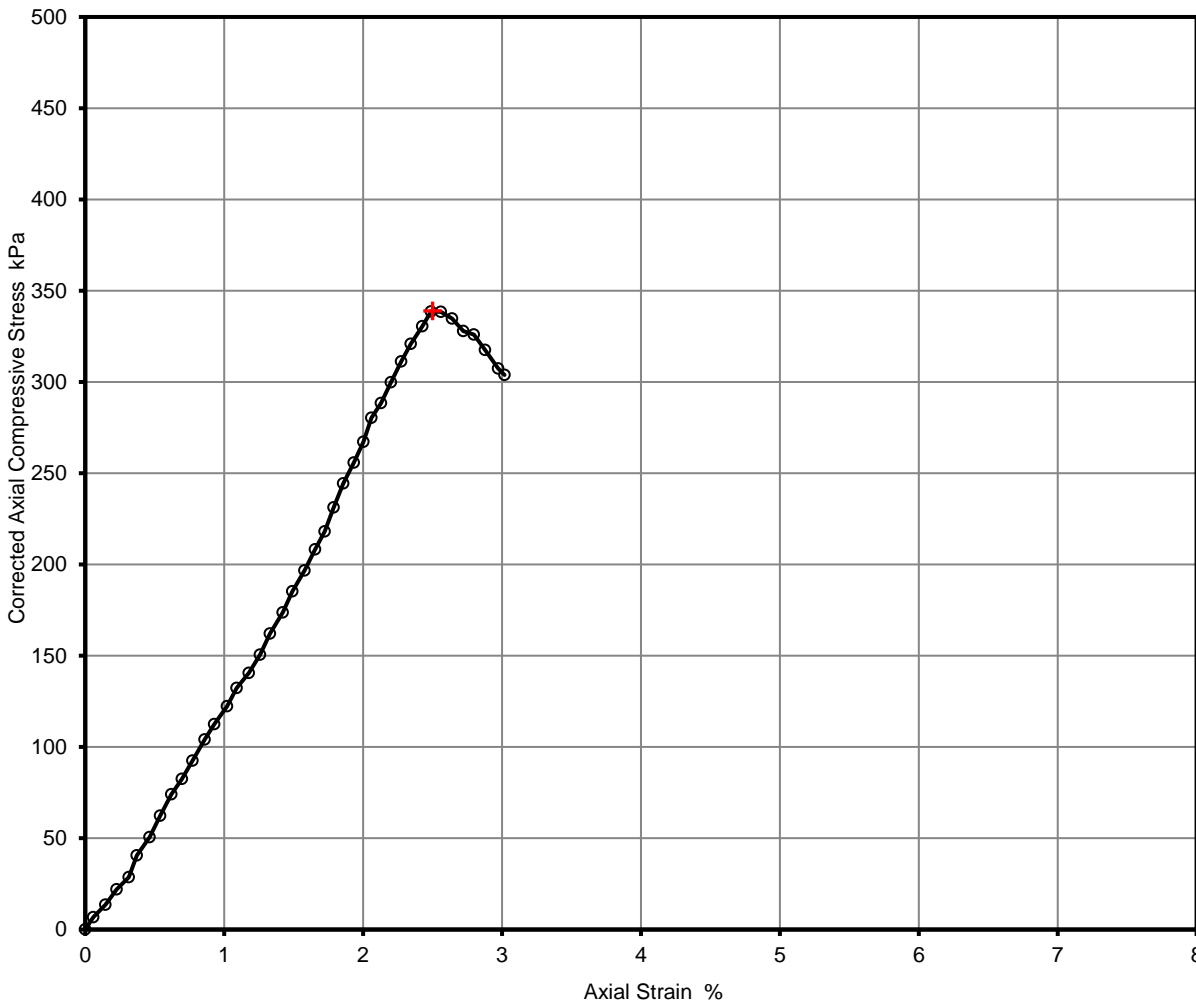
**Test Results:**

Laboratory Reference: 2185981  
 Hole No.: BH11  
 Sample Reference: Not Given  
 Sample Description: Dark grey SILT  
 Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

Depth Top [m]: 21.94  
 Depth Base [m]: 22.34  
 Sample Type: U

Test Number	1	Rate of Strain	1.0	%/min
Length	172.3	Axial Strain at failure	2.5	%
Diameter	86.7	Unconfined Compressive Strength	339	kPa
Bulk Density	2.16	Mode of Failure	Compound	
Moisture Content	16.0			
Dry Density	1.87			

**Axial Compressive Stress v Axial Strain**



Note: Axial compressive stress corrected for area change, and membrane effects (if used)

Remarks: Preliminary report

Signed:

Anna Dudzinska  
 Deputy Head of Geo Office Section  
 for and on behalf of i2 Analytical Ltd

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**TEST CERTIFICATE**  
**DETERMINATION OF THE UNCONFINED**  
**COMPRESSIVE STRENGTH -**  
**LOAD FRAME METHOD**

i2 Analytical Ltd  
 Unit 8 Harrowden Road  
 Brackmills Industrial Estate  
 Northampton NN4 7EB



Tested in Accordance with: BS 1377-7: 1990: Clause 7.2

Client: Delta-Simons  
 Client Address: 3 Henley Office Park, Doddington Road,  
 Lincoln, LN6 3QR

Client Reference: 15-0645.05  
 Job Number: 22-42014  
 Date Sampled: 08/02/2022  
 Date Received: 24/02/2022  
 Date Tested: 09/03/2022  
 Sampled By: Not Given

Contact: Harry Whittle  
 Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

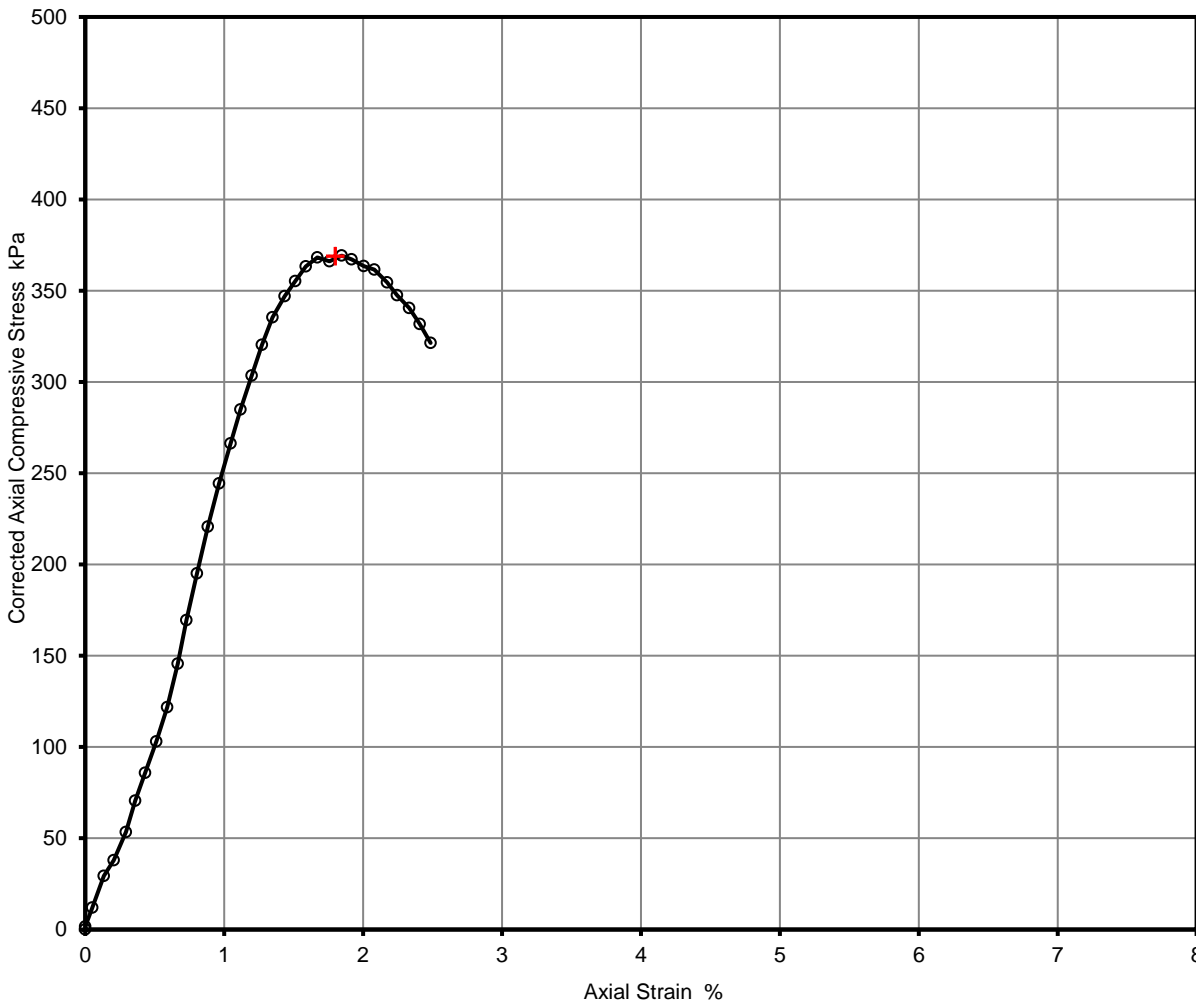
**Test Results:**

Laboratory Reference: 2185983  
 Hole No.: BH11  
 Sample Reference: Not Given  
 Sample Description: Dark grey SILT  
 Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

Depth Top [m]: 23.27  
 Depth Base [m]: 23.57  
 Sample Type: U

Test Number	1	Rate of Strain	1.0	%/min
Length	195.1	Axial Strain at failure	1.8	%
Diameter	85.9	Unconfined Compressive Strength	369	kPa
Bulk Density	2.19	Mode of Failure	Brittle	
Moisture Content	13.0			
Dry Density	1.93			

**Axial Compressive Stress v Axial Strain**



Note: Axial compressive stress corrected for area change, and membrane effects (if used)

Remarks: Preliminary report

Signed:

Anna Dudzinska  
 Deputy Head of Geo Office Section  
 for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF THE UNCONFINED COMPRESSIVE STRENGTH - LOAD FRAME METHOD

Tested in Accordance with: BS 1377-7: 1990: Clause 7.2

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 08/02/2022  
Date Received: 24/02/2022  
Date Tested: 09/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

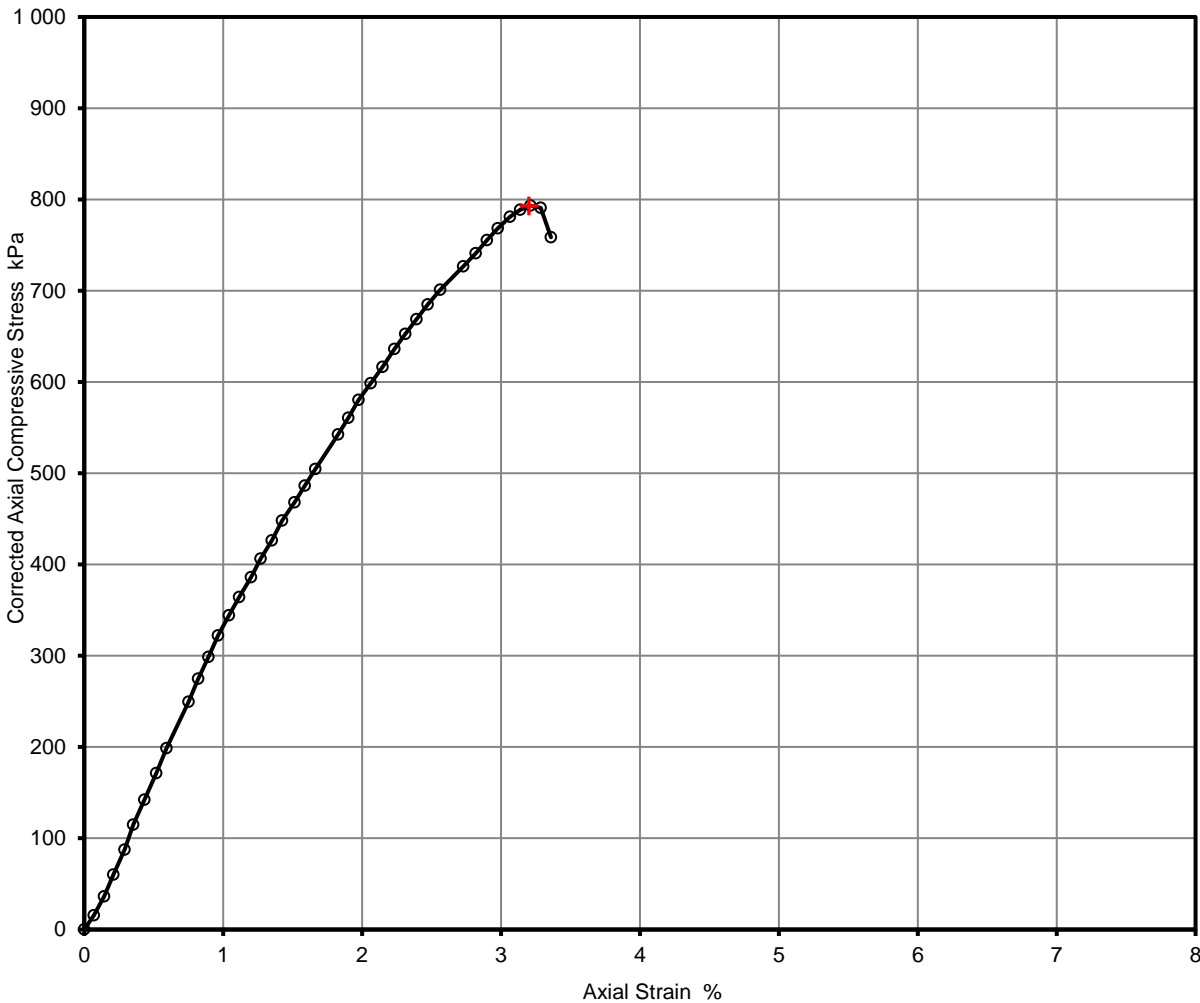
### Test Results:

Laboratory Reference: 2185985  
Hole No.: BH11  
Sample Reference: Not Given  
Sample Description: Dark grey SILT  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

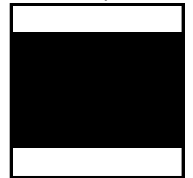
Depth Top [m]: 25.89  
Depth Base [m]: 26.50  
Sample Type: U

Test Number	1	Rate of Strain	1.0	%/min
Length	175.6	Axial Strain at failure	3.2	%
Diameter	86.0	Unconfined Compressive Strength	793	kPa
Bulk Density	2.24	Mode of Failure	Compound	
Moisture Content	12.0			
Dry Density	1.99			

Axial Compressive Stress v Axial Strain



Position within sample



Note: Axial compressive stress corrected for area change, and membrane effects (if used)

Remarks: Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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**TEST CERTIFICATE**  
**DETERMINATION OF THE UNCONFINED**  
**COMPRESSIVE STRENGTH -**  
**LOAD FRAME METHOD**

i2 Analytical Ltd  
 Unit 8 Harrowden Road  
 Brackmills Industrial Estate  
 Northampton NN4 7EB



Tested in Accordance with: BS 1377-7: 1990: Clause 7.2

Client: Delta-Simons  
 Client Address: 3 Henley Office Park, Doddington Road,  
 Lincoln, LN6 3QR

Client Reference: 15-0645.05  
 Job Number: 22-42014  
 Date Sampled: 11/02/2022  
 Date Received: 24/02/2022  
 Date Tested: 09/03/2022  
 Sampled By: Not Given

Contact: Harry Whittle  
 Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

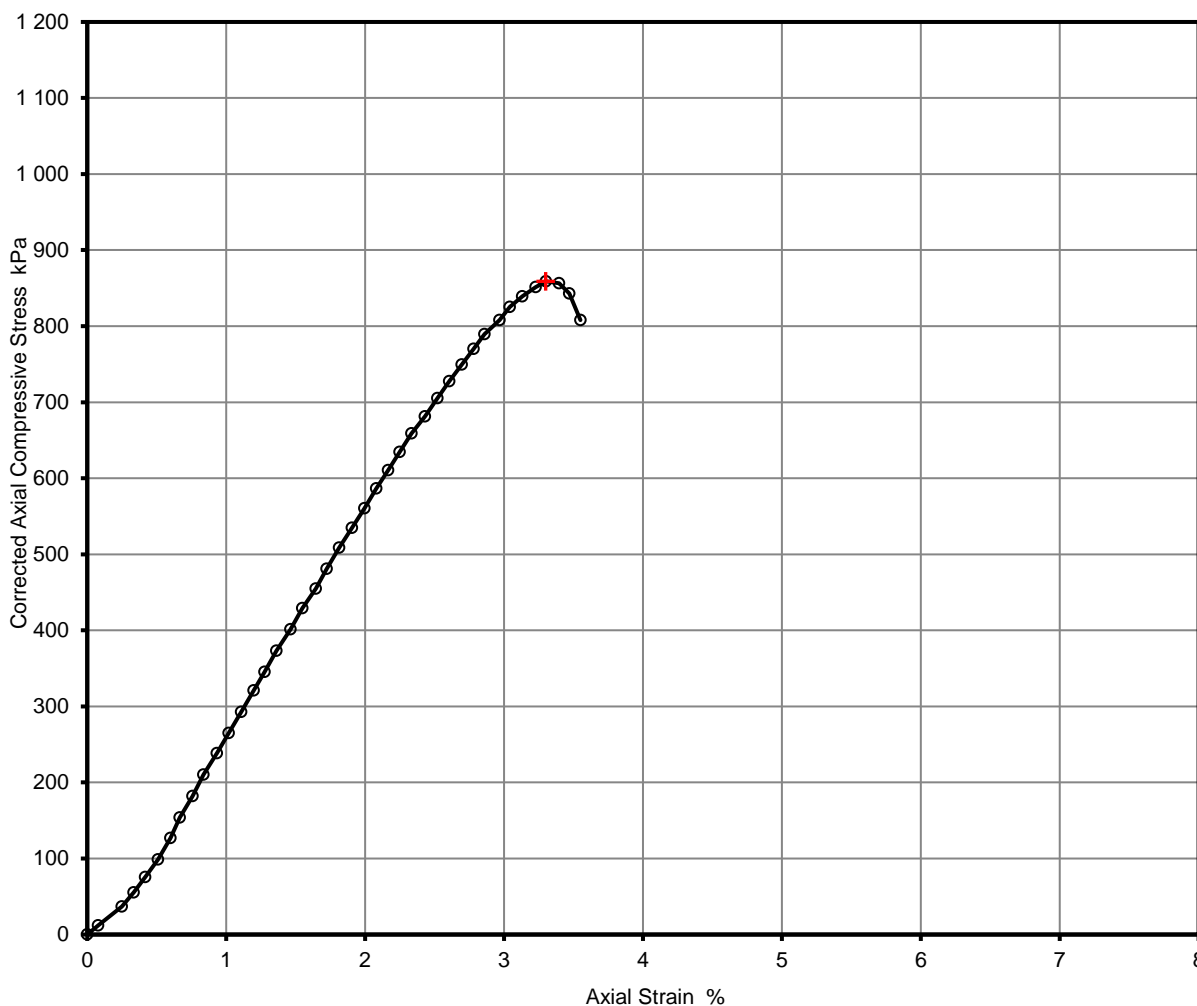
**Test Results:**

Laboratory Reference: 2185986  
 Hole No.: BH11  
 Sample Reference: Not Given  
 Sample Description: Dark grey SILT  
 Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

Depth Top [m]: 29.66  
 Depth Base [m]: 30.05  
 Sample Type: U

Test Number	1	Rate of Strain	1.1	%/min
Length	176.9	Axial Strain at failure	3.3	%
Diameter	87.0	Unconfined Compressive Strength	859	kPa
Bulk Density	2.19	Mode of Failure	Compound	
Moisture Content	13.0			
Dry Density	1.94			

**Axial Compressive Stress v Axial Strain**



Note: Axial compressive stress corrected for area change, and membrane effects (if used)

Remarks: Preliminary report

Signed:

Anna Dudzinska  
 Deputy Head of Geo Office Section  
 for and on behalf of i2 Analytical Ltd

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 8

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 15/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

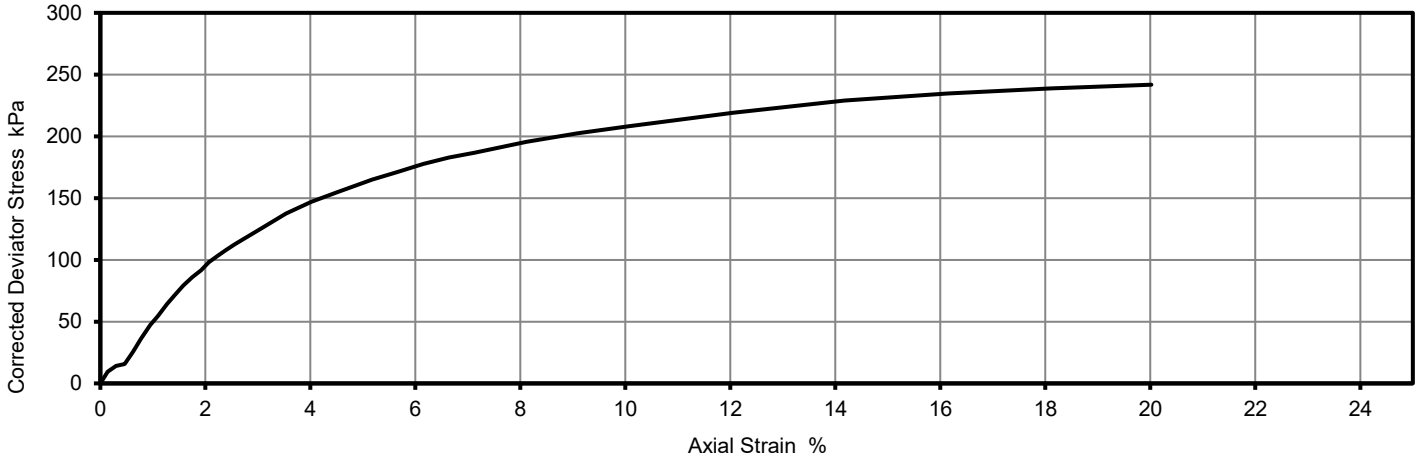
*Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland*

**Test Results:**

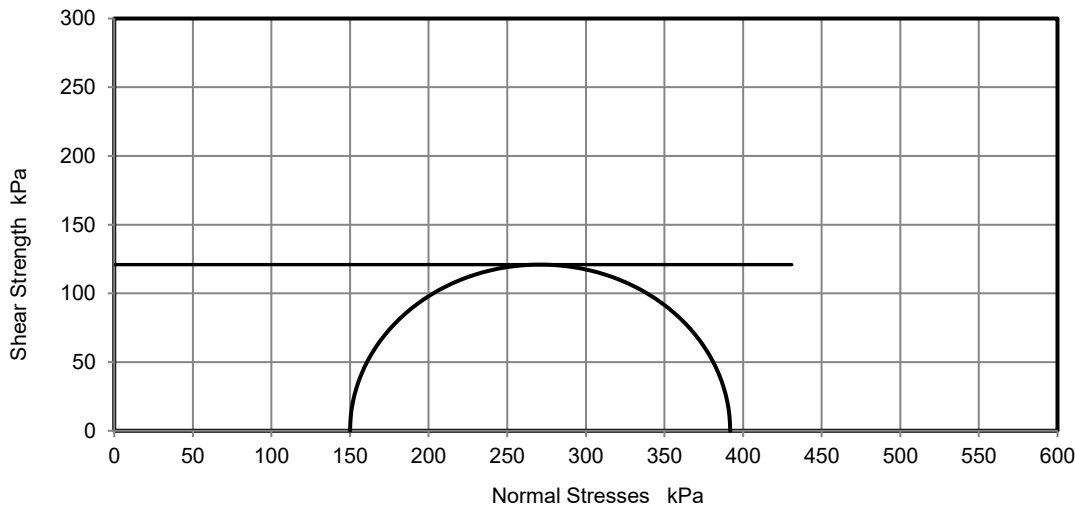
Laboratory Reference: 2185934	Depth Top [m]: 7.50
Hole No.: BH1	Depth Base [m]: 7.95
Sample Reference: Not Given	Sample Type: U
Sample Description: Multicolour slightly gravelly sandy CLAY	
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.	

Test Number	1	Rate of Strain	2.00	%/min
Length	198.21	Cell Pressure	150	kPa
Diameter	102.43	Axial Strain at failure	20.0	%
Bulk Density	2.14	Deviator Stress, ( $\sigma_1 - \sigma_3$ ) <sub>f</sub>	242	kPa
Moisture Content	15	Undrained Shear Strength, $c_u$	121	kPa $\frac{1}{2}(\sigma_1 - \sigma_3)_f$
Dry Density	1.86	Mode of Failure	Plastic	
Membrane Correction	1.01	Membrane thickness	0.27	mm

**Deviator Stress v Axial Strain**



**Mohr Circles**



Position within sample



Note: Deviator stress corrected for area change and membrane effects. Mohr circles and their interpretation is not covered by BS1377. This is provided for information only.

Remarks: No failure occurred until 20% Axial Strain - reported as a single stage test.  
Preliminary report

**Signed:**

Anna Dudzinska  
Deputy Head of Geo Office Section  
**for and on behalf of i2 Analytical Ltd**

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 8

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

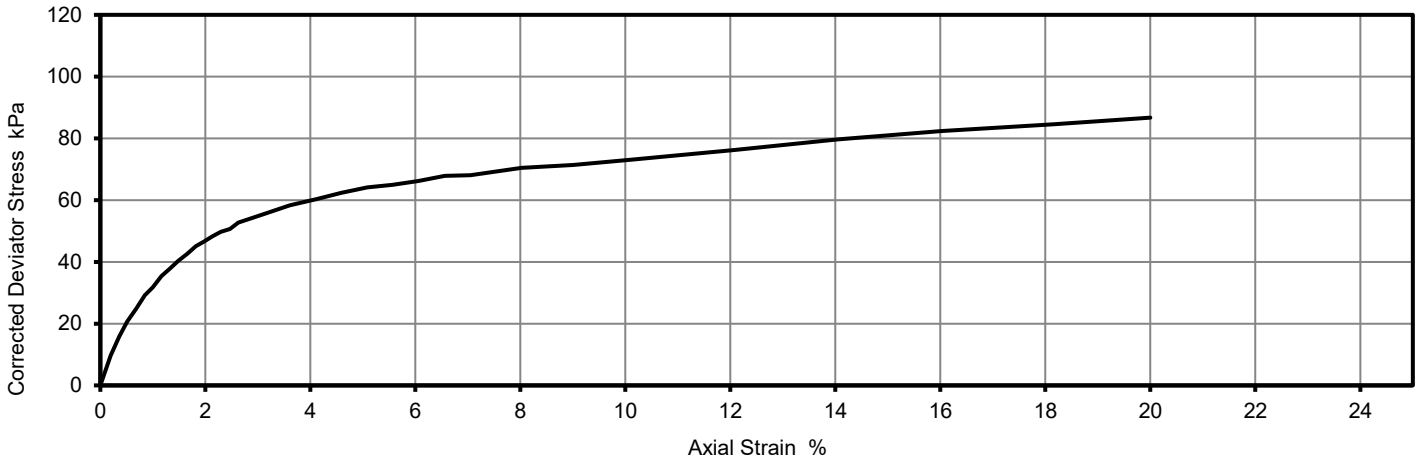
*Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland*

**Test Results:**

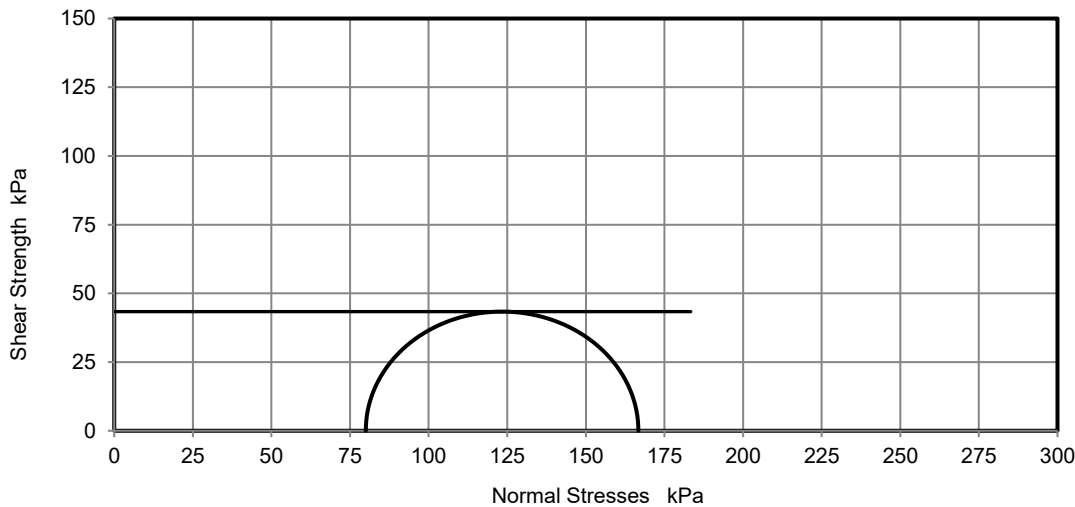
Laboratory Reference: 2185960	Depth Top [m]: 4.00
Hole No.: BH4	Depth Base [m]: 4.45
Sample Reference: Not Given	Sample Type: U
Sample Description: Brownish grey slightly gravelly sandy CLAY with fragments of chalk	
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.	

Test Number	1	Rate of Strain	2.00	%/min
Length	200.05	Cell Pressure	80	kPa
Diameter	101.75	Axial Strain at failure	20.0	%
Bulk Density	2.11	Deviator Stress, ( $\sigma_1 - \sigma_3$ ) <sub>f</sub>	87	kPa
Moisture Content	22	Undrained Shear Strength, cu	43	kPa $\frac{1}{2}(\sigma_1 - \sigma_3)_f$
Dry Density	1.72	Mode of Failure	Plastic	
Membrane Correction	1.06	Membrane thickness	0.28	mm

**Deviator Stress v Axial Strain**



**Mohr Circles**



Position within sample



Note: Deviator stress corrected for area change and membrane effects. Mohr circles and their interpretation is not covered by BS1377. This is provided for information only.

Remarks: No failure occurred until 20% Axial Strain - reported as a single stage test.  
Preliminary report

**Signed:**

Anna Dudzinska  
Deputy Head of Geo Office Section  
**for and on behalf of i2 Analytical Ltd**

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 8

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

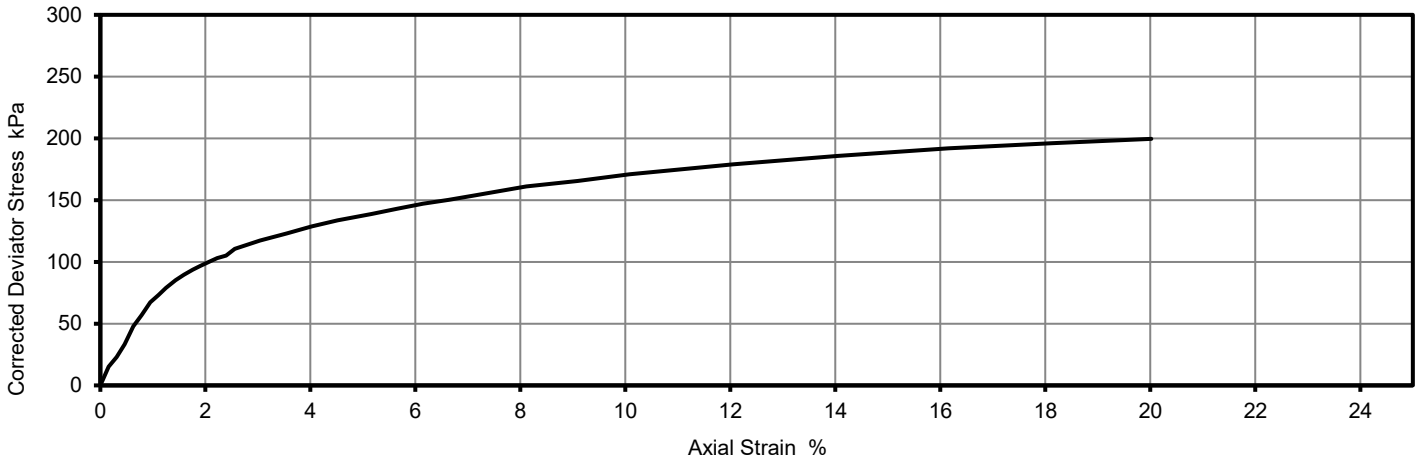
*Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland*

**Test Results:**

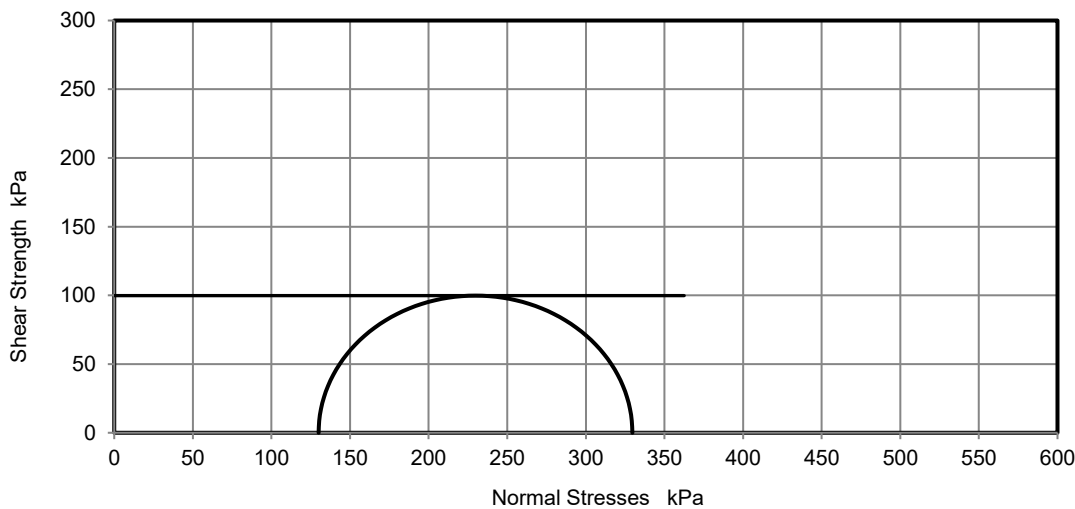
Laboratory Reference: 2185961	Depth Top [m]: 6.45
Hole No.: BH4	Depth Base [m]: 6.95
Sample Reference: Not Given	Sample Type: U
Sample Description: Brownish grey slightly gravelly sandy CLAY with fragments of chalk	
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.	

Test Number	1	Rate of Strain	2.00	%/min
Length	139.72	Cell Pressure	130	kPa
Diameter	69.42	Axial Strain at failure	20.0	%
Bulk Density	2.08	Deviator Stress, ( $\sigma_1 - \sigma_3$ ) <sub>f</sub>	200	kPa
Moisture Content	20	Undrained Shear Strength, $c_u$	100	kPa $\frac{1}{2}(\sigma_1 - \sigma_3)_f$
Dry Density	1.74	Mode of Failure	Plastic	
Membrane Correction	1.39	Membrane thickness	0.25	mm

**Deviator Stress v Axial Strain**



**Mohr Circles**



Position within sample



Note: Deviator stress corrected for area change and membrane effects. Mohr circles and their interpretation is not covered by BS1377. This is provided for information only.

Remarks: No failure occurred until 20% Axial Strain - reported as a single stage test.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 8

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 16/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

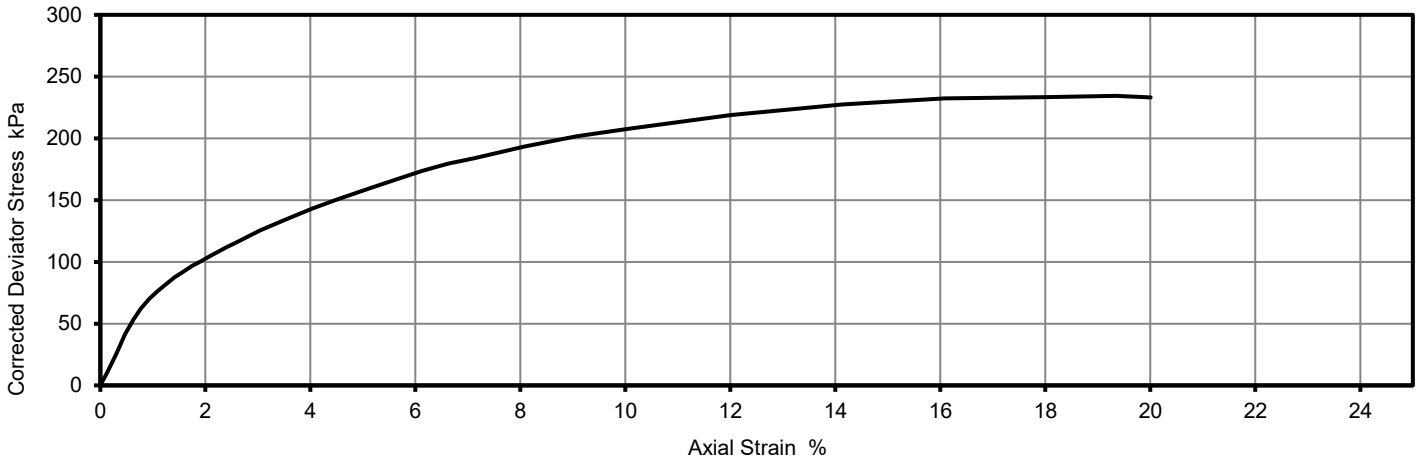
Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

**Test Results:**

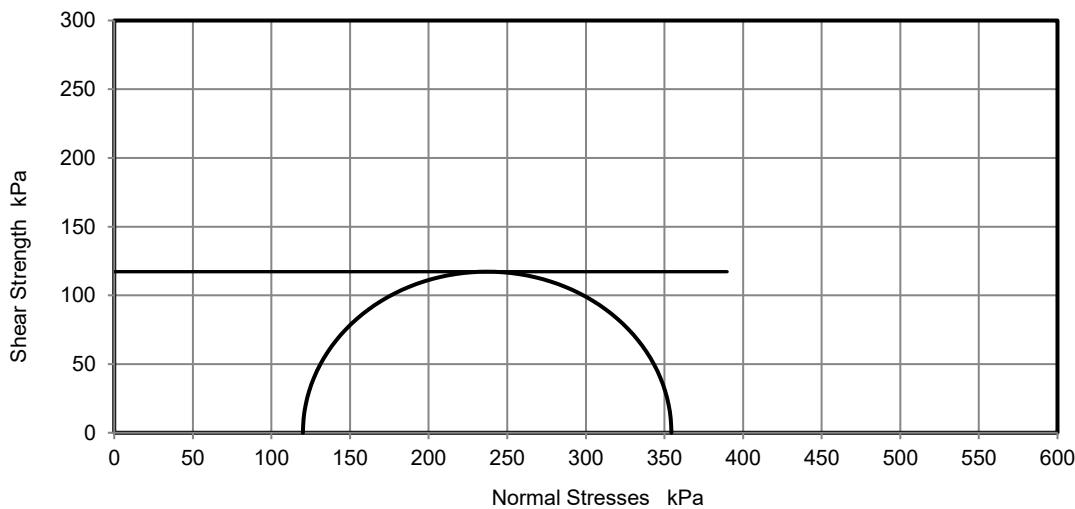
Laboratory Reference: 2185969	Depth Top [m]: 6.00
Hole No.: BH8	Depth Base [m]: 6.45
Sample Reference: Not Given	Sample Type: U
Sample Description: Brownish grey gravelly sandy CLAY with fragments of chalk	
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.	

Test Number	1	Rate of Strain	2.00	%/min
Length	194.99	Cell Pressure	120	kPa
Diameter	102.41	Axial Strain at failure	19.3	%
Bulk Density	2.17	Deviator Stress, ( $\sigma_1 - \sigma_3$ ) <sub>f</sub>	234	kPa
Moisture Content	17	Undrained Shear Strength, $c_u$	117	kPa $\frac{1}{2}(\sigma_1 - \sigma_3)_f$
Dry Density	1.85	Mode of Failure	Plastic	
Membrane Correction	0.99	Membrane thickness	0.27	mm

**Deviator Stress v Axial Strain**



**Mohr Circles**



Position within sample



Note: Deviator stress corrected for area change and membrane effects. Mohr circles and their interpretation is not covered by BS1377. This is provided for information only.

Remarks: No failure occurred until 20% Axial Strain - reported as a single stage test.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF THE UNDRAINED SHEAR STRENGTH IN TRIAXIAL COMPRESSION WITHOUT MEASUREMENT OF PORE PRESSURE

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Tested in Accordance with: BS 1377-7: 1990: Clause 8

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

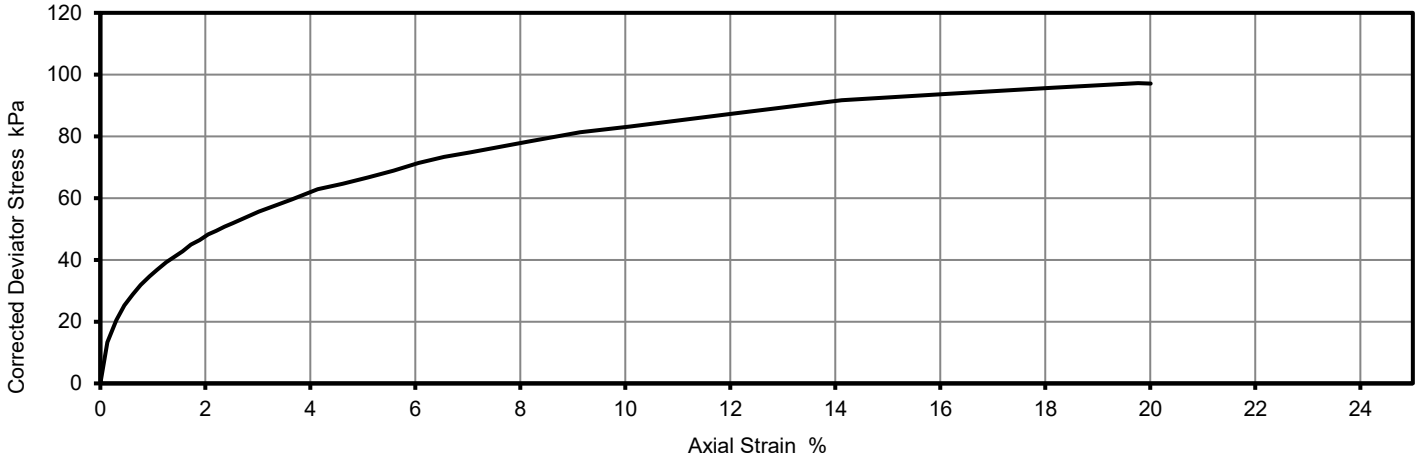
### Test Results:

Laboratory Reference: 2185991  
Hole No.: BH12  
Sample Reference: Not Given  
Sample Description: Greyish brown slightly gravelly slightly sandy CLAY  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

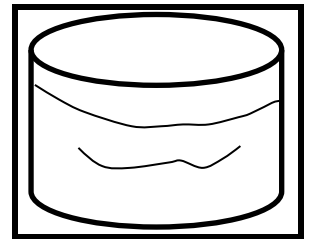
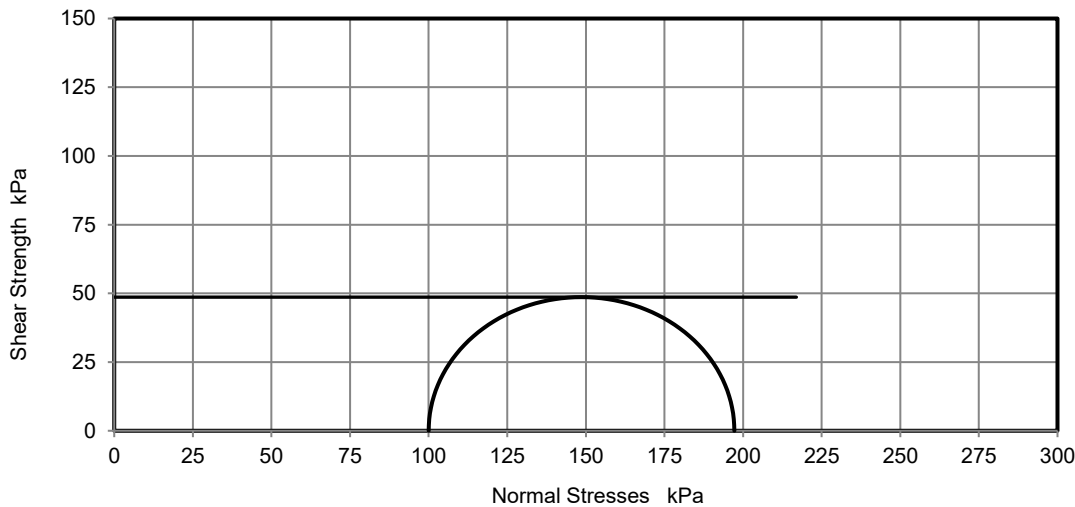
Depth Top [m]: 5.00  
Depth Base [m]: 5.45  
Sample Type: U

Test Number	1	Rate of Strain	1.96	%/min
Length	203.99	Cell Pressure	100	kPa
Diameter	101.39	Axial Strain at failure	19.8	%
Bulk Density	2.05	Deviator Stress, ( $\sigma_1 - \sigma_3$ ) <sub>f</sub>	97	kPa
Moisture Content	22	Undrained Shear Strength, cu	49	kPa $\frac{1}{2}(\sigma_1 - \sigma_3)_f$
Dry Density	1.68	Mode of Failure	Plastic	
Membrane Correction	1.05	Membrane thickness	0.28	mm

### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Note: Deviator stress corrected for area change and membrane effects. Mohr circles and their interpretation is not covered by BS1377. This is provided for information only.

Remarks: No failure occurred until 20% Axial Strain - reported as a single stage test. Unable to take a photo.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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*Anna Dudzinska*

4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 10/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185938  
Hole No.: BH2  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly slightly sandy CLAY  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

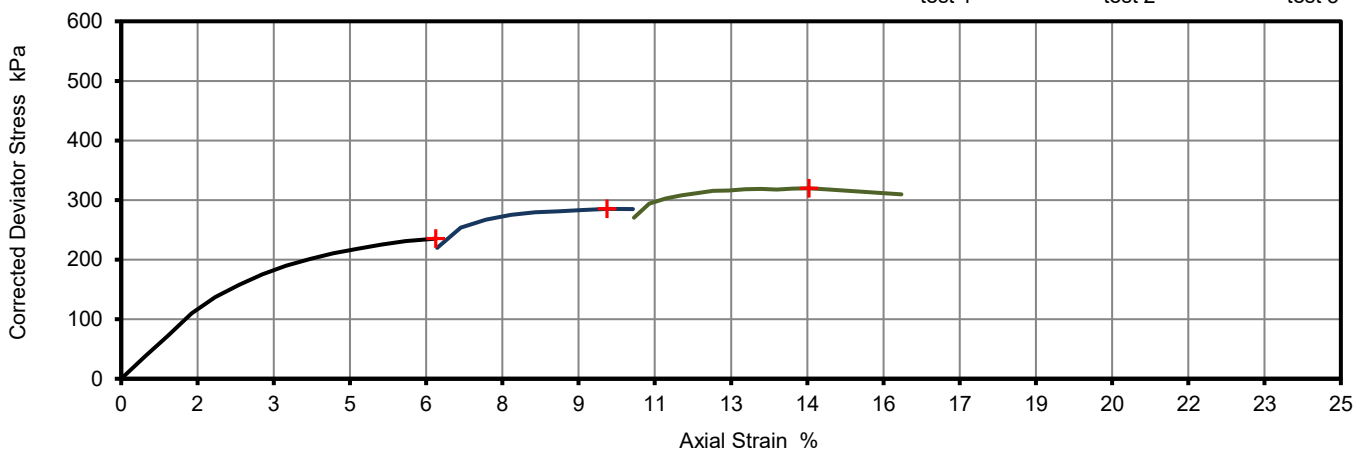
Depth Top [m]: 15.50  
Depth Base [m]: 15.95  
Sample Type: U

Length	196.10	mm
Diameter	102.67	mm
Bulk Density	2.15	Mg/m <sup>3</sup>
Moisture Content	16	%
Dry Density	1.85	Mg/m <sup>3</sup>
Membrane thickness	0.27	mm

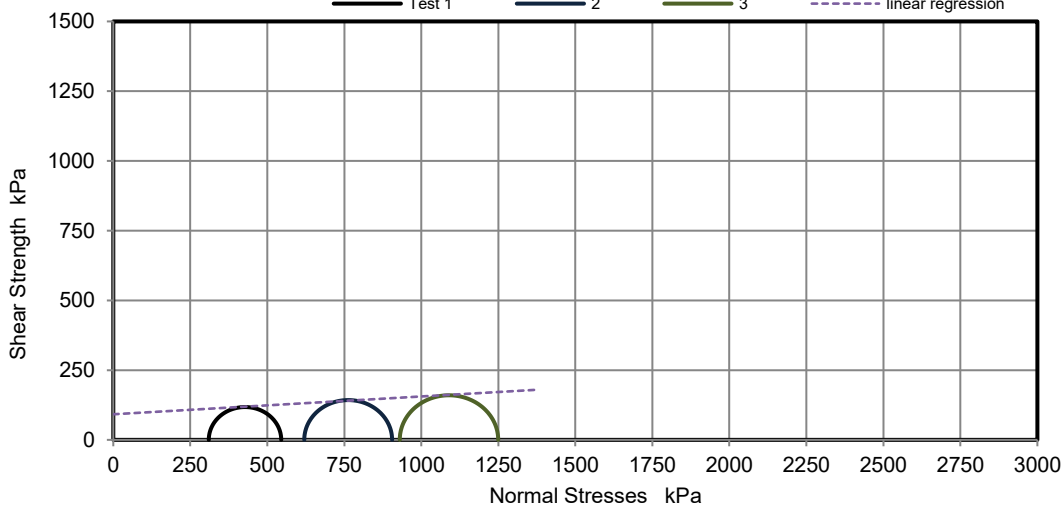
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )  
Shear strength, cu  
Mode of failure  
Membrane Correction

2.00			%/min
1	2	3	
310	620	930	kPa
6.4	10.0	14.1	%
235	285	320	kPa
118	143	160	kPa
Plastic			
0.43	0.58	0.76	kPa

### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  3.7 °  
cu 92 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 310kPa=160N, 620kPa=311N, 930kPa=477N.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185958  
Hole No.: BH4  
Sample Reference: Not Given  
Sample Description: Grey slightly gravelly sandy CLAY with fragments of chalk  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

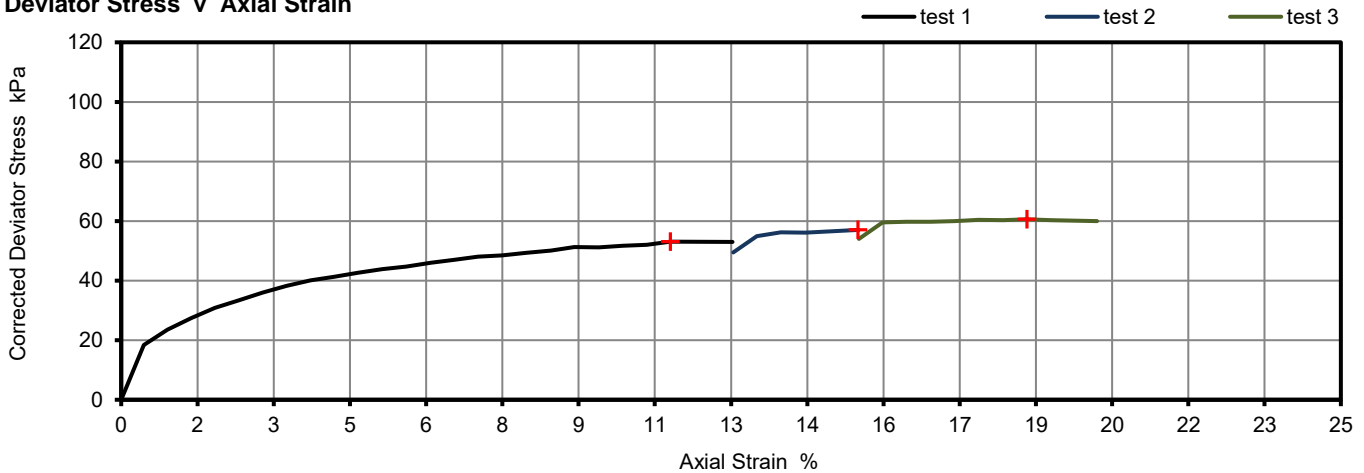
Depth Top [m]: 2.00  
Depth Base [m]: 2.45  
Sample Type: U

Length	200.32	mm
Diameter	102.04	mm
Bulk Density	2.14	Mg/m <sup>3</sup>
Moisture Content	20	%
Dry Density	1.78	Mg/m <sup>3</sup>
Membrane thickness	0.27	mm

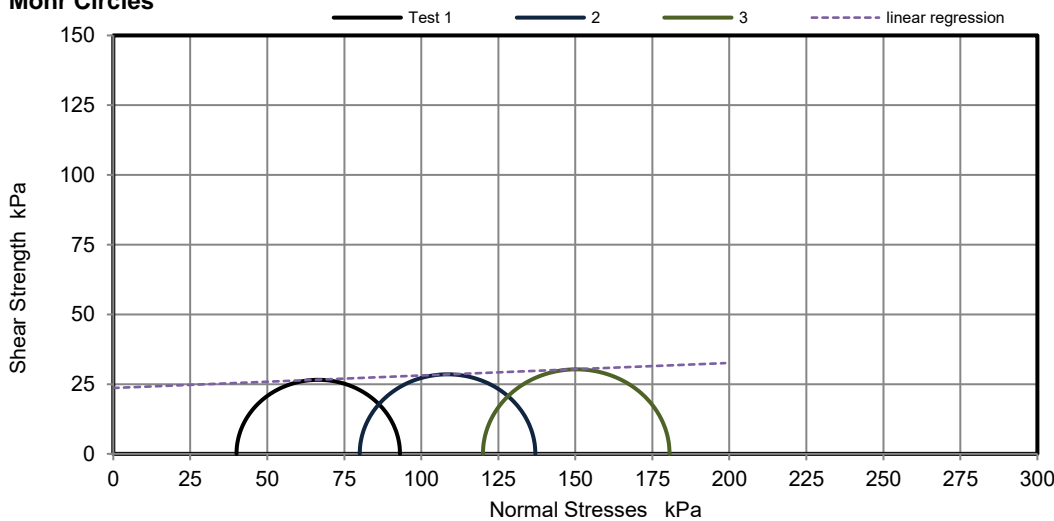
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )  
Shear strength, cu  
Mode of failure  
Membrane Correction

2.00			%/min
1	2	3	
40	80	120	kPa
11.3	15.1	18.6	%
53	57	61	kPa
27	29	30	kPa
Plastic			
0.64	0.81	0.96	kPa

### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  2.6 °  
cu 24 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 40kPa=22N, 80kPa=47N, 120kPa=69N.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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# TEST CERTIFICATE

## DETERMINATION OF THE UNDRAINED SHEAR STRENGTH IN TRIAXIAL COMPRESSION WITHOUT MEASUREMENT OF PORE PRESSURE

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185963  
Hole No.: BH6  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY with fragments of chalk  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

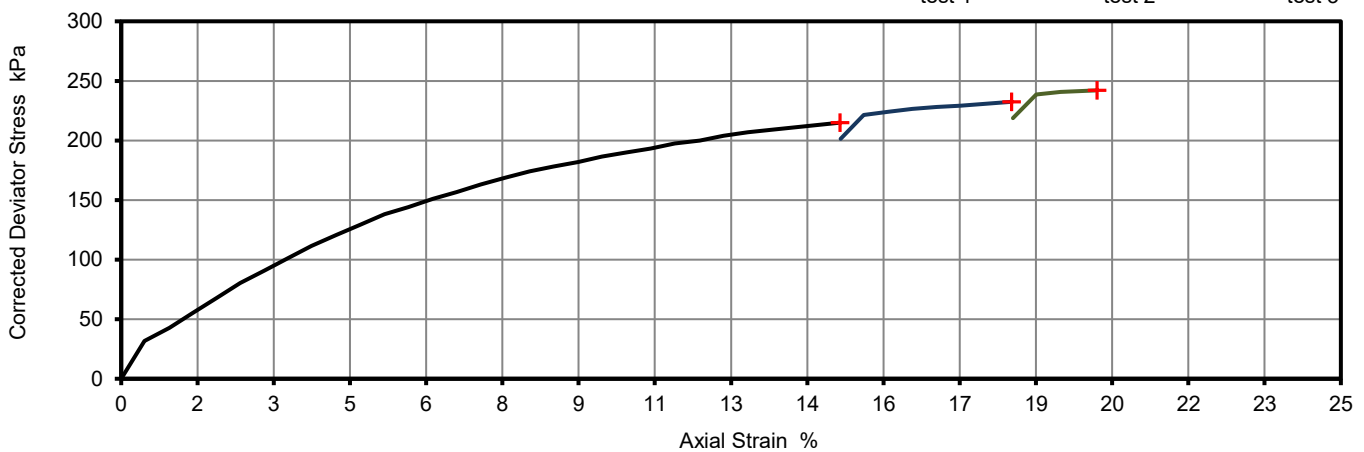
Depth Top [m]: 2.00  
Depth Base [m]: Not Given  
Sample Type: U

Length	199.58	mm
Diameter	101.78	mm
Bulk Density	2.18	Mg/m <sup>3</sup>
Moisture Content	21	%
Dry Density	1.80	Mg/m <sup>3</sup>
Membrane thickness	0.29	mm

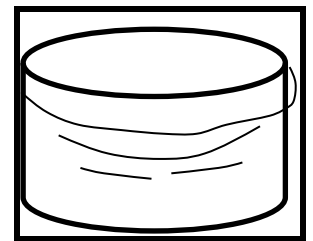
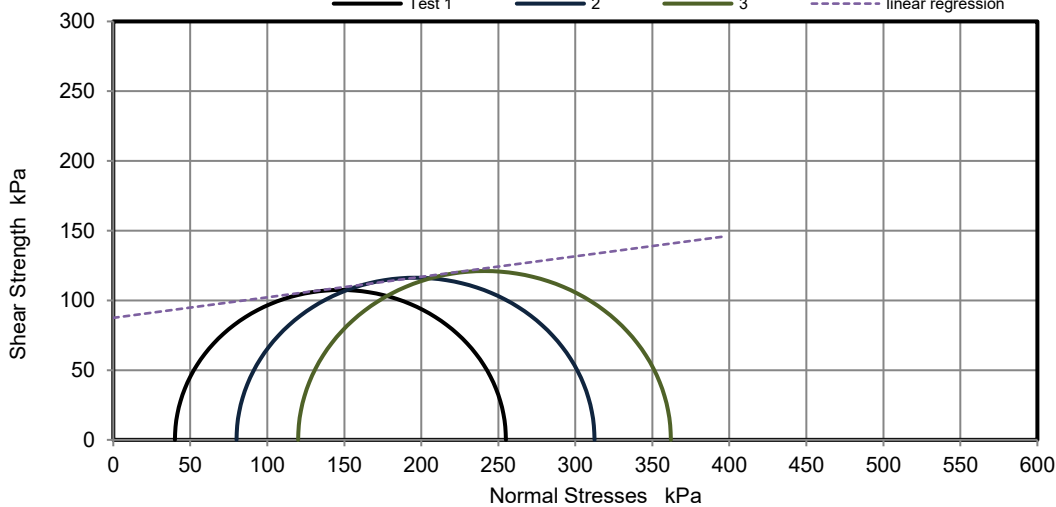
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )  
Shear strength,  $c_u$   
Mode of failure  
Membrane Correction

2.00			%/min
1	2	3	
40	80	120	kPa
14.7	18.3	20.0	%
215	232	242	kPa
107	116	121	kPa
Plastic			
0.85	1.02	1.10	kPa

### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  8.4 °  
 $c_u$  87 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 40kPa=21N, 80kPa=42N, 120kPa=66N. Unable to take a photo.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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*Anna Dudzinska*

4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185964  
Hole No.: BH6  
Sample Reference: Not Given  
Sample Description: Greyish brown slightly gravelly sandy CLAY with fragments of chalk  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

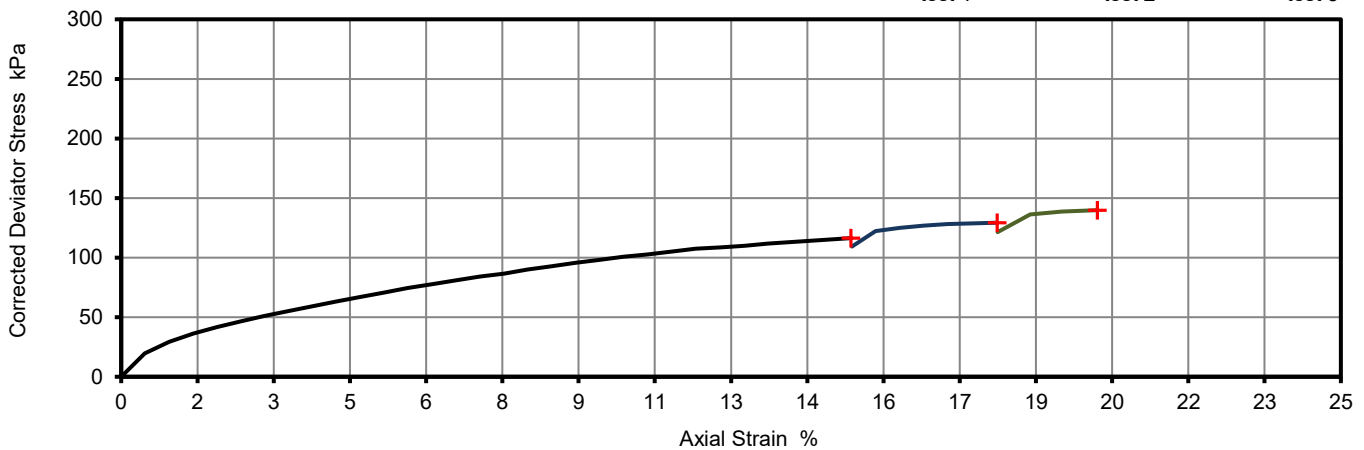
Depth Top [m]: 4.00  
Depth Base [m]: Not Given  
Sample Type: U

Length	199.68	mm
Diameter	102.26	mm
Bulk Density	2.08	Mg/m <sup>3</sup>
Moisture Content	17	%
Dry Density	1.77	Mg/m <sup>3</sup>
Membrane thickness	0.29	mm

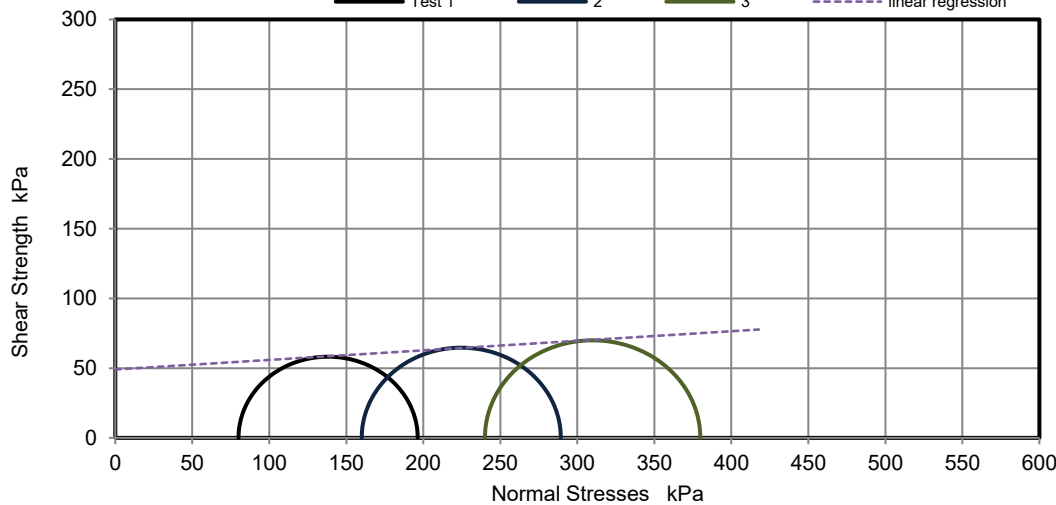
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ ) f  
Shear strength, cu  
Mode of failure  
Membrane Correction

2.00			%/min
1	2	3	
80	160	240	kPa
15.0	18.0	20.0	%
116	129	140	kPa
58	65	70	kPa
Plastic			
0.86	1.00	1.09	kPa

### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  3.9 °  
cu 49 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 80kPa=44N, 160kPa=88N, 240kPa=166N.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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## DETERMINATION OF THE UNDRAINED SHEAR STRENGTH IN TRIAXIAL COMPRESSION WITHOUT MEASUREMENT OF PORE PRESSURE

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB

4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185965  
Hole No.: BH6  
Sample Reference: Not Given  
Sample Description: Brownish grey gravelly sandy CLAY with fragments of chalk  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

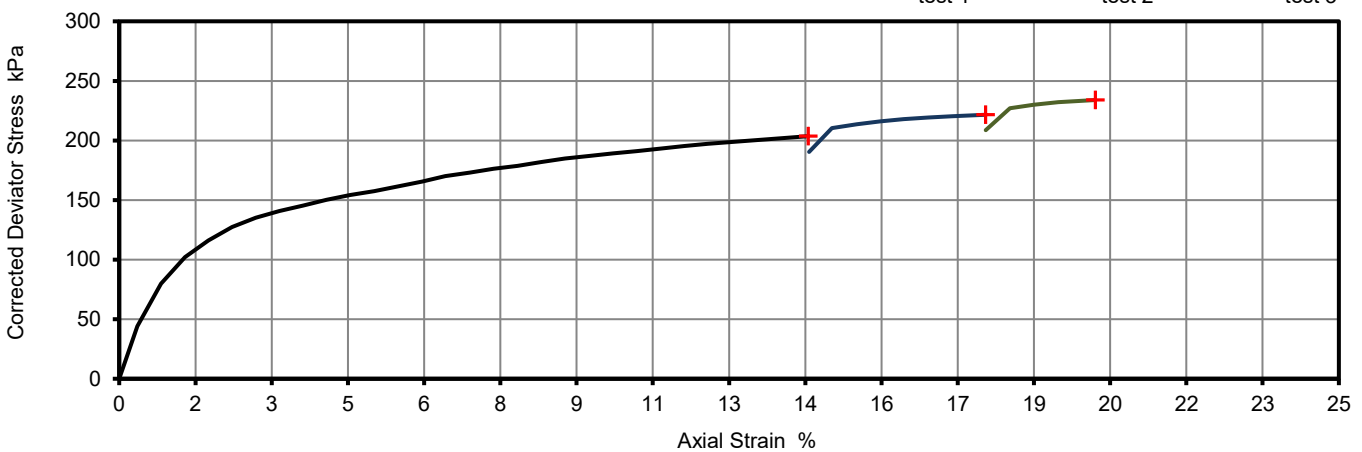
Depth Top [m]: 6.50  
Depth Base [m]: Not Given  
Sample Type: U

Length	199.70	mm
Diameter	102.35	mm
Bulk Density	2.14	Mg/m <sup>3</sup>
Moisture Content	19	%
Dry Density	1.80	Mg/m <sup>3</sup>
Membrane thickness	0.28	mm

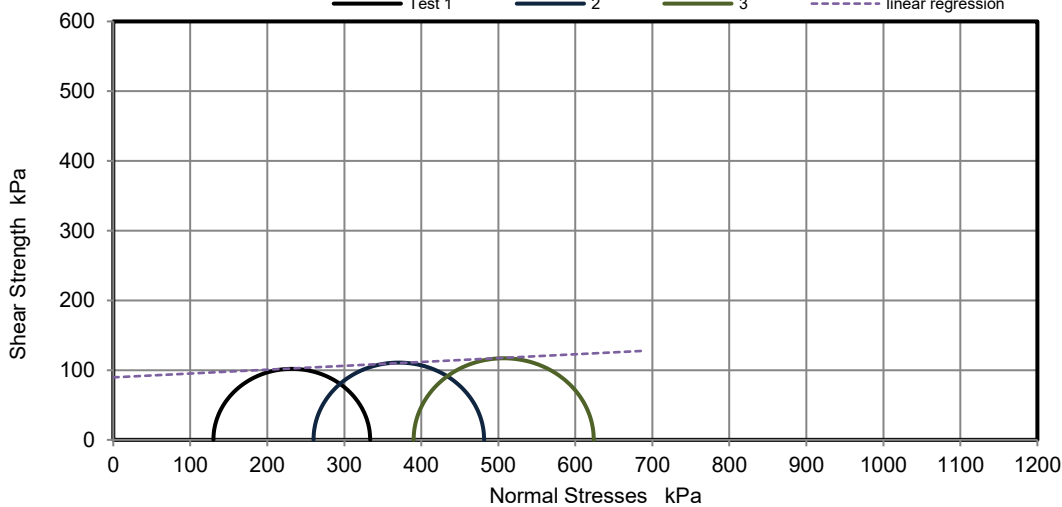
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )  
Shear strength, cu  
Mode of failure  
Membrane Correction

2.00			%/min
1	2	3	
130	260	390	kPa
14.1	17.8	20.0	%
204	222	234	kPa
102	111	117	kPa
Plastic			
0.79	0.95	1.05	kPa

### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  3.2 °  
cu 90 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 130kPa=69N, 260kPa=147N, 390kPa=201N.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 16/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185967  
Hole No.: BH8  
Sample Reference: Not Given  
Sample Description: Brownish grey gravelly sandy CLAY with fragments of chalk  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

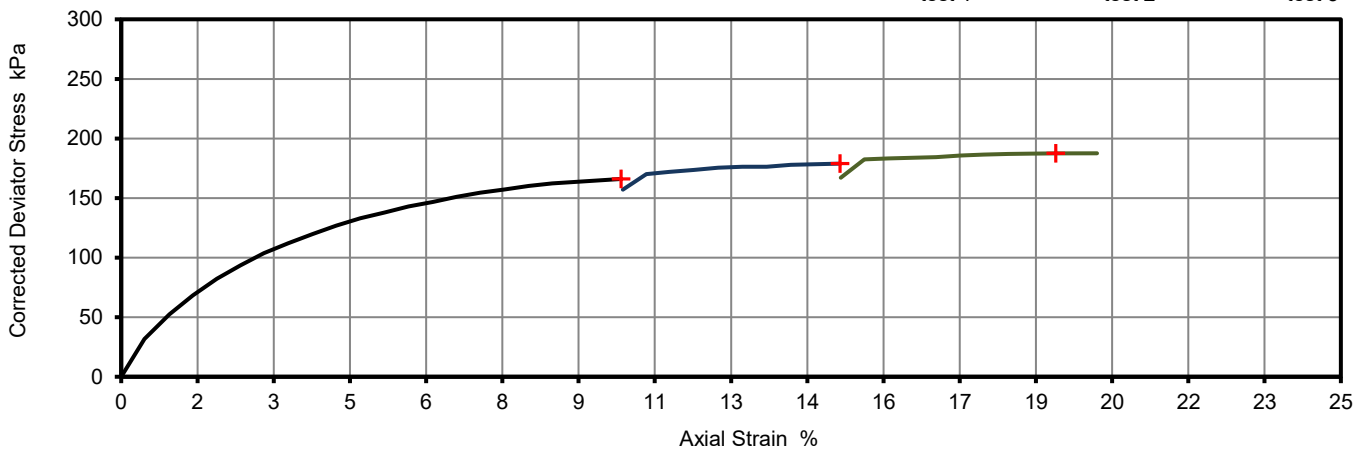
Depth Top [m]: 1.50  
Depth Base [m]: 1.95  
Sample Type: U

Length	198.58	mm
Diameter	102.00	mm
Bulk Density	2.14	Mg/m <sup>3</sup>
Moisture Content	18	%
Dry Density	1.81	Mg/m <sup>3</sup>
Membrane thickness	0.28	mm

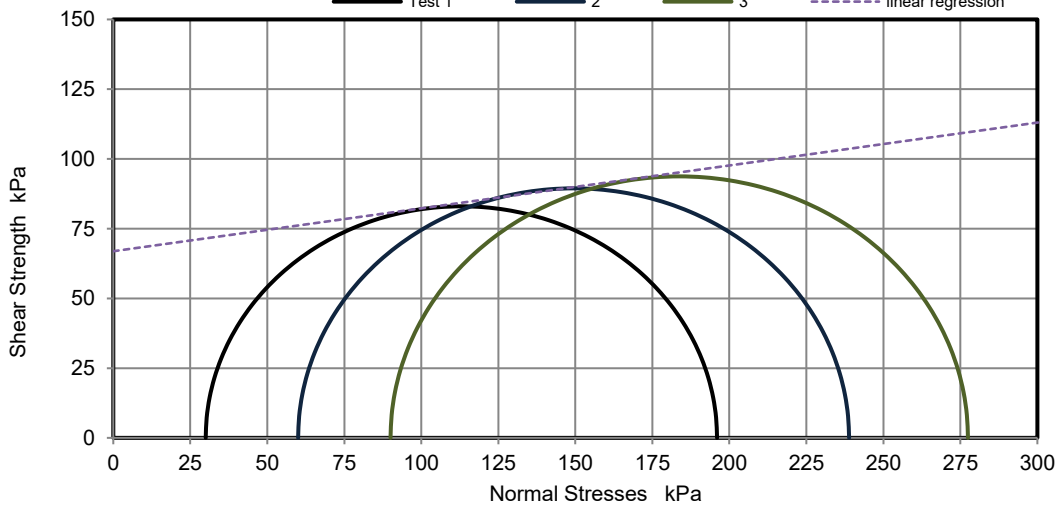
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )  
Shear strength,  $c_u$   
Mode of failure  
Membrane Correction

2.00			%/min
1	2	3	
30	60	90	kPa
10.2	14.7	19.2	%
166	179	187	kPa
83	89	94	kPa
Plastic			
0.62	0.82	1.02	kPa

### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  8.7 °  
 $c_u$  67 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 30kPa=21N, 60kPa=39N, 90kPa=44N.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 16/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185968  
Hole No.: BH8  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY with fragments of chalk  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

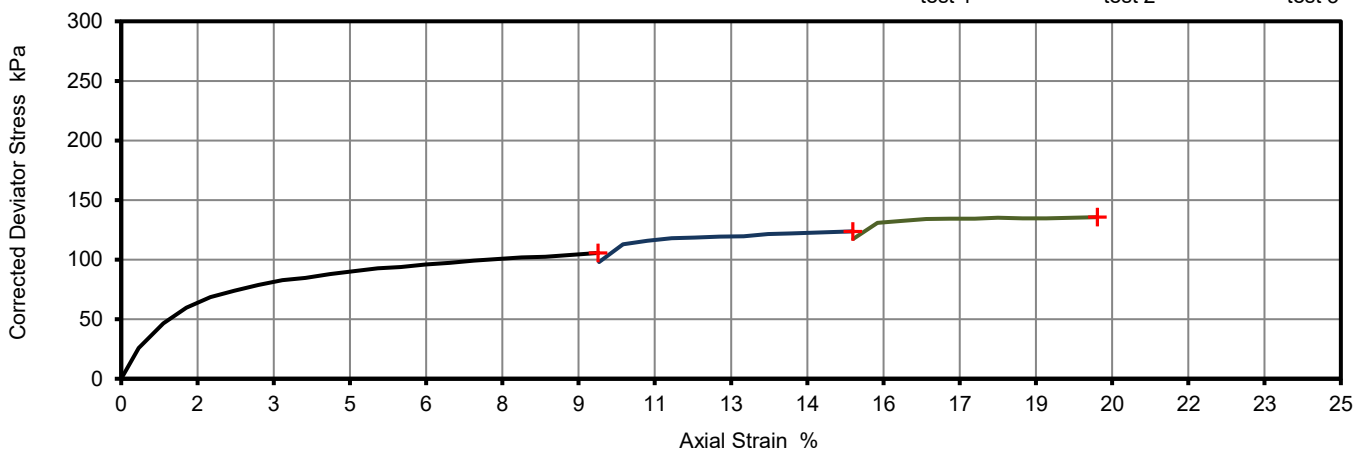
Depth Top [m]: 3.50  
Depth Base [m]: 3.95  
Sample Type: U

Length	138.74	mm
Diameter	69.55	mm
Bulk Density	2.06	Mg/m <sup>3</sup>
Moisture Content	21	%
Dry Density	1.70	Mg/m <sup>3</sup>
Membrane thickness	0.26	mm

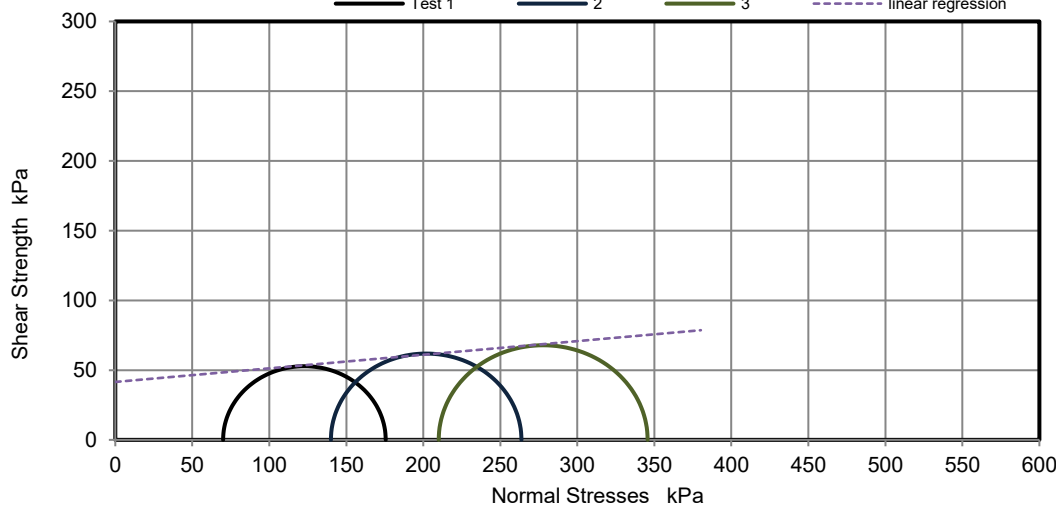
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )  
Shear strength, cu  
Mode of failure  
Membrane Correction

2.00			%/min
1	2	3	
70	140	210	kPa
9.8	15.0	20.0	%
106	124	136	kPa
53	62	68	kPa
Plastic			
0.82	1.13	1.44	kPa

### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  5.6 °  
cu 42 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 70kPa=35N, 140kPa=77N, 210kPa=157N.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road, □  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 16/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

**Test Results:**

Laboratory Reference: 2185972  
Hole No.: BH8  
Sample Reference: Not Given  
Sample Description: Multicolour slightly gravelly sandy CLAY  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

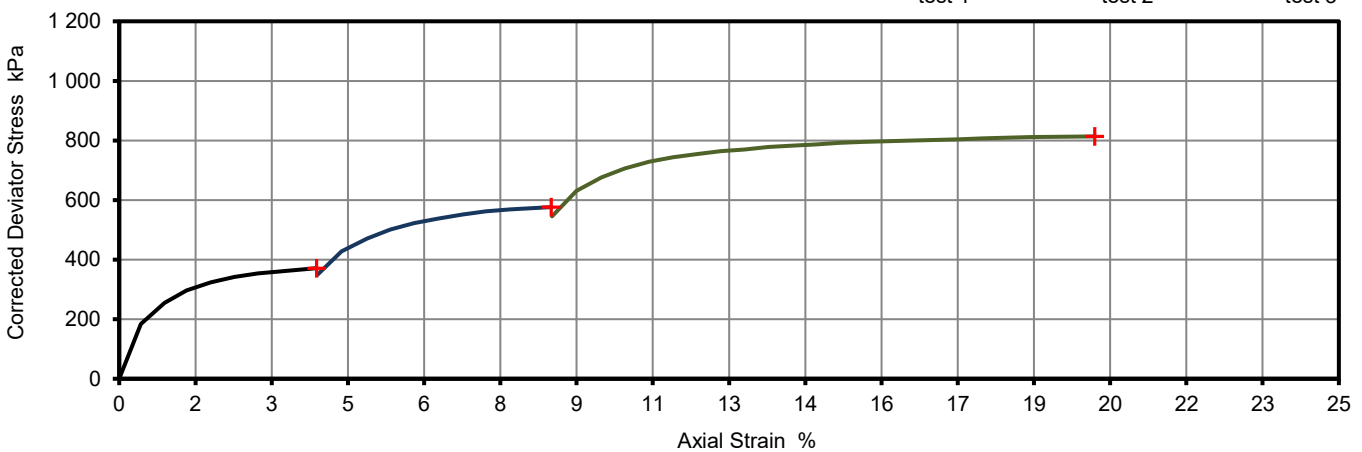
Depth Top [m]: 12.00  
Depth Base [m]: 12.45  
Sample Type: U

Length	140.23	mm
Diameter	69.81	mm
Bulk Density	2.03	Mg/m <sup>3</sup>
Moisture Content	18	%
Dry Density	1.73	Mg/m <sup>3</sup>
Membrane thickness	0.25	mm

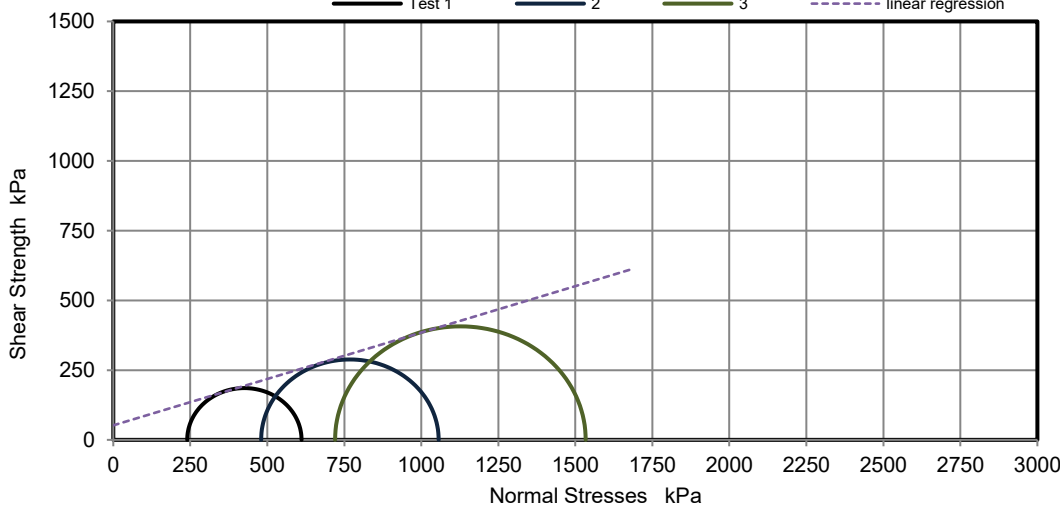
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, (σ<sub>1</sub> - σ<sub>3</sub>)<sub>f</sub>  
Shear strength, c<sub>u</sub>  
Mode of failure  
Membrane Correction

2.00			%/min
1	2	3	
240	480	720	kPa
4.0	8.9	20.0	%
371	576	814	kPa
186	288	407	kPa
Plastic			
0.40	0.73	1.38	kPa

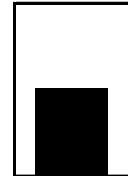
**Deviator Stress v Axial Strain**



**Mohr Circles**



Position within sample



Linear Regression  
φ<sub>u</sub> 18.4 °  
c<sub>u</sub> 52 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 240kPa=110N, 480kPa=247N, 720kPa=499N.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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## DETERMINATION OF THE UNDRAINED SHEAR STRENGTH IN TRIAXIAL COMPRESSION WITHOUT MEASUREMENT OF PORE PRESSURE

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB



Environmental Science

4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 16/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185974  
Hole No.: BH8  
Sample Reference: Not Given  
Sample Description: Multicolour slightly gravelly sandy CLAY  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

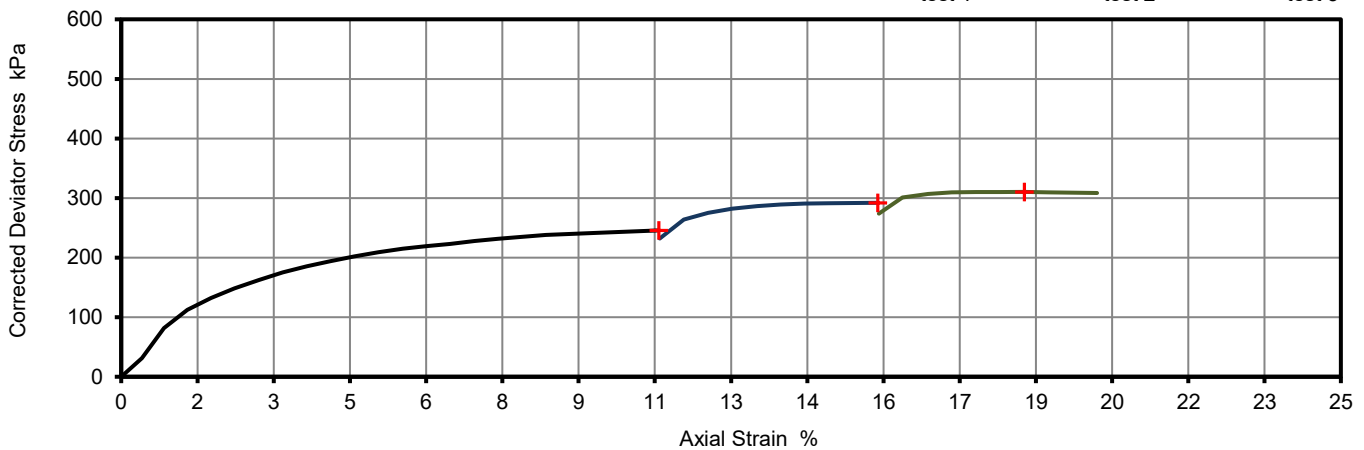
Depth Top [m]: 15.00  
Depth Base [m]: 15.45  
Sample Type: U

Length	199.03	mm
Diameter	102.63	mm
Bulk Density	2.12	Mg/m <sup>3</sup>
Moisture Content	19	%
Dry Density	1.78	Mg/m <sup>3</sup>
Membrane thickness	0.28	mm

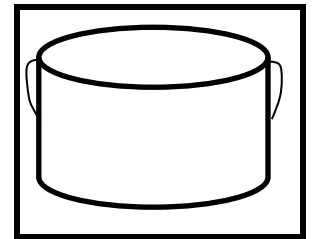
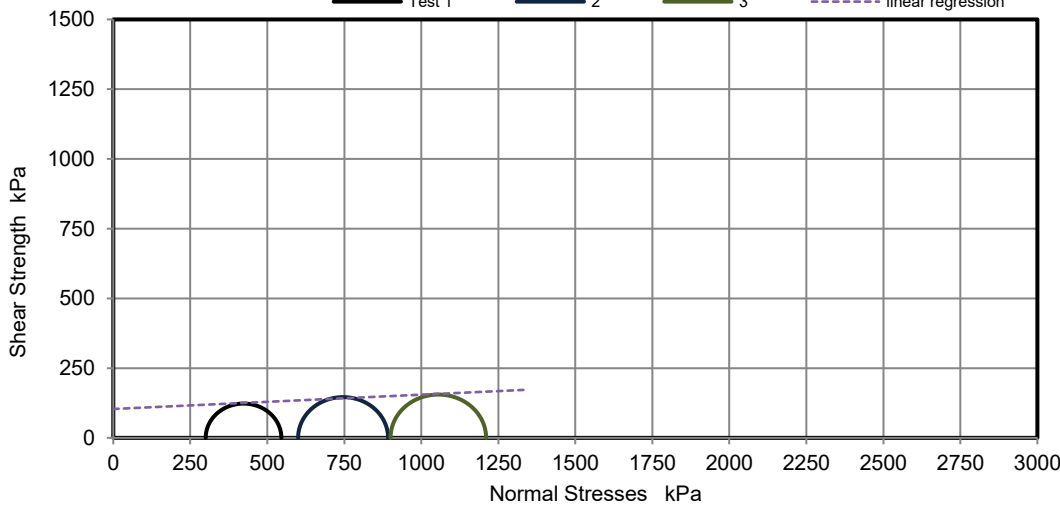
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )  
Shear strength, cu  
Mode of failure  
Membrane Correction

2.00			%/min
1	2	3	
300	600	900	kPa
11.0	15.5	18.5	%
246	292	310	kPa
123	146	155	kPa
Compound			
0.65	0.85	0.98	kPa

### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  2.9 °  
cu 103 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: kPa=N, kPa=N, kPa=N. Unable to take a photo.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185989  
Hole No.: BH12  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

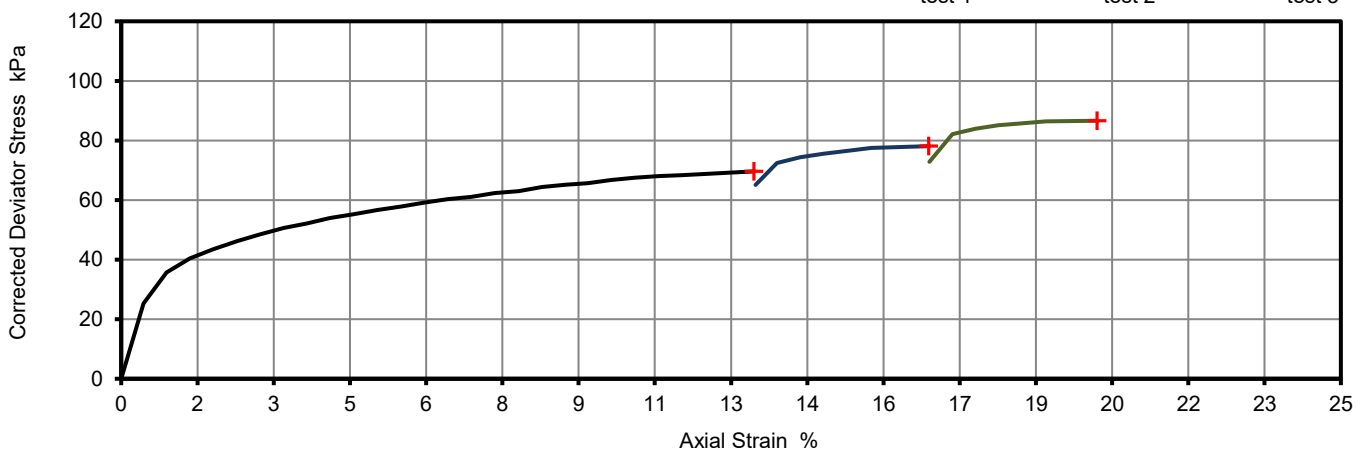
Depth Top [m]: 3.00  
Depth Base [m]: 3.45  
Sample Type: U

Length	203.97	mm
Diameter	101.57	mm
Bulk Density	2.10	Mg/m <sup>3</sup>
Moisture Content	24	%
Dry Density	1.69	Mg/m <sup>3</sup>
Membrane thickness	0.28	mm

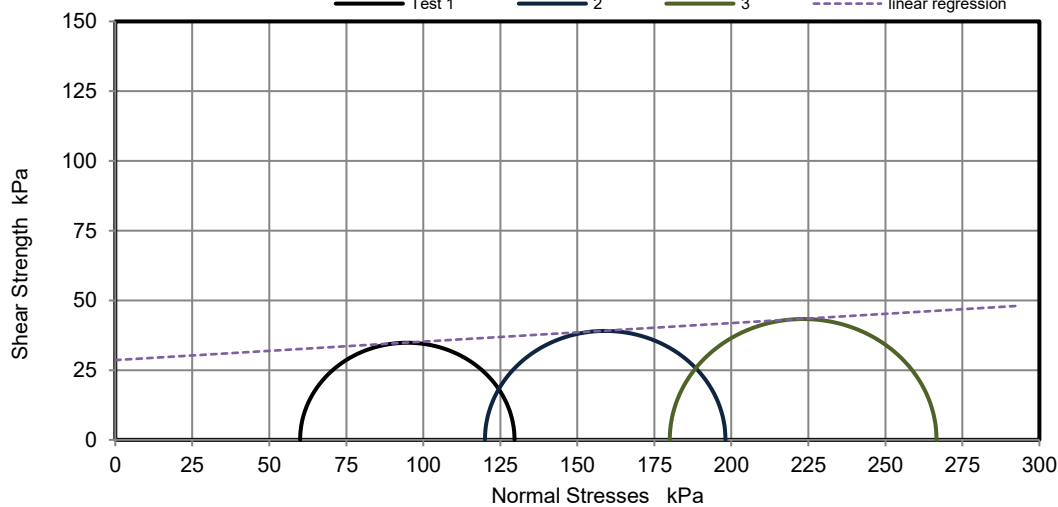
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )  
Shear strength, cu  
Mode of failure  
Membrane Correction

1.96			%/min
1	2	3	
60	120	180	kPa
13.0	16.6	20.0	%
70	78	87	kPa
35	39	43	kPa
Plastic			
0.75	0.91	1.06	kPa

### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  3.8 °  
cu 29 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 60kPa=31N, 120kPa=69N, 180kPa=94N.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185992  
Hole No.: BH12  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

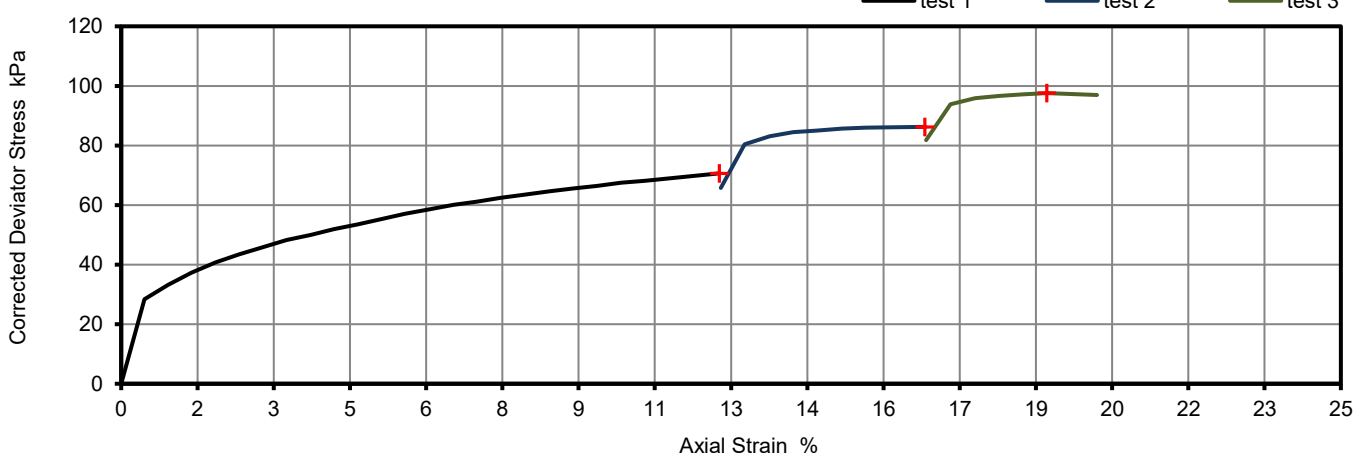
Depth Top [m]: 8.00  
Depth Base [m]: 8.45  
Sample Type: U

Length	201.54	mm
Diameter	102.81	mm
Bulk Density	2.09	Mg/m <sup>3</sup>
Moisture Content	21	%
Dry Density	1.72	Mg/m <sup>3</sup>
Membrane thickness	0.28	mm

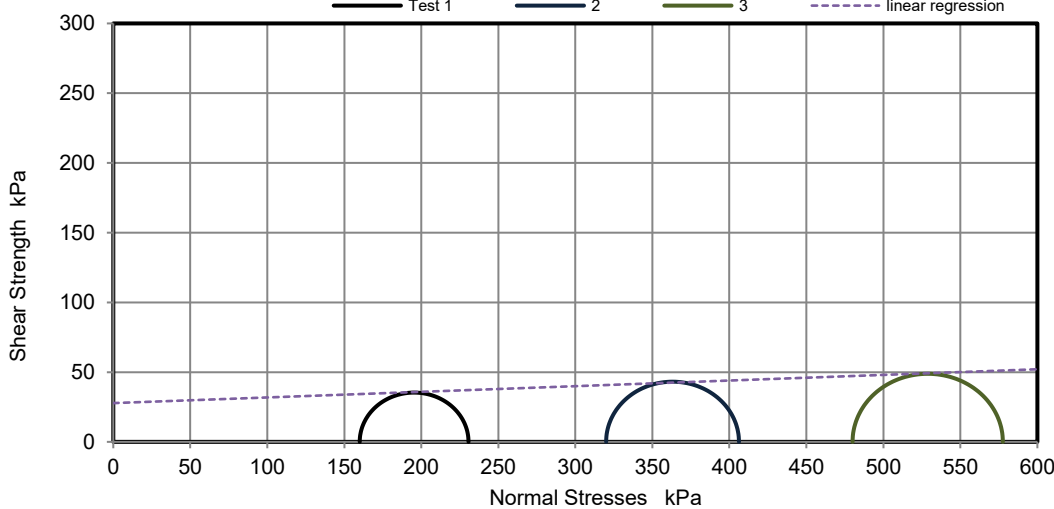
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )  
Shear strength, cu  
Mode of failure  
Membrane Correction

1.98			%/min
1	2	3	
160	320	480	kPa
12.3	16.5	19.0	%
71	86	98	kPa
35	43	49	kPa
Plastic			
0.71	0.89	1.00	kPa

### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  2.3 °  
cu 28 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 160kPa=84N, 320kPa=166N, 480kPa=247N.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185993  
Hole No.: BH12  
Sample Reference: Not Given  
Sample Description: Grey slightly gravelly slightly sandy CLAY  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

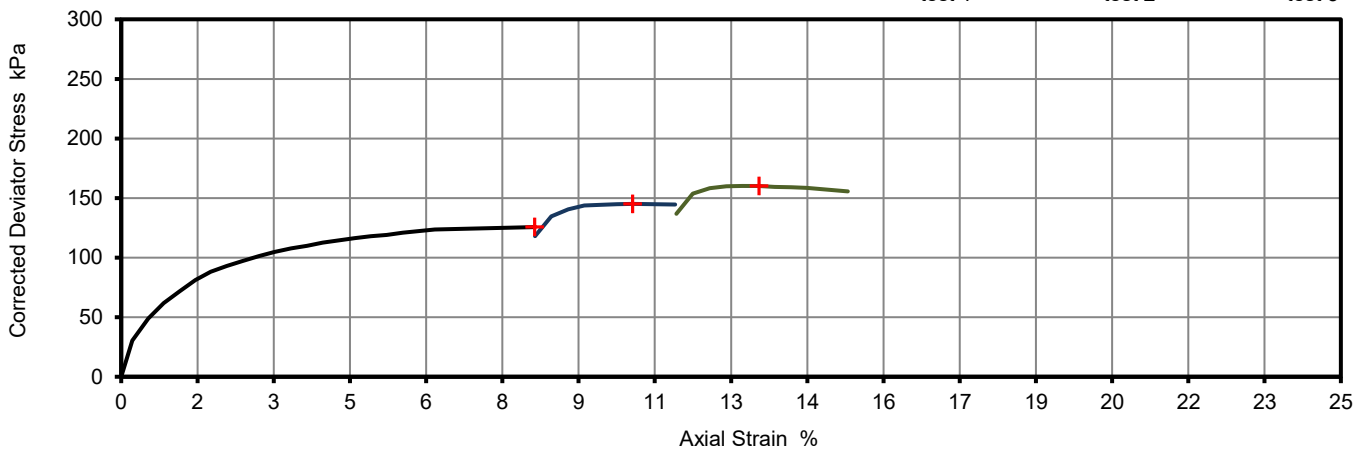
Depth Top [m]: 11.00  
Depth Base [m]: 11.45  
Sample Type: U

Length	200.89	mm
Diameter	103.52	mm
Bulk Density	2.11	Mg/m <sup>3</sup>
Moisture Content	19	%
Dry Density	1.77	Mg/m <sup>3</sup>
Membrane thickness	0.28	mm

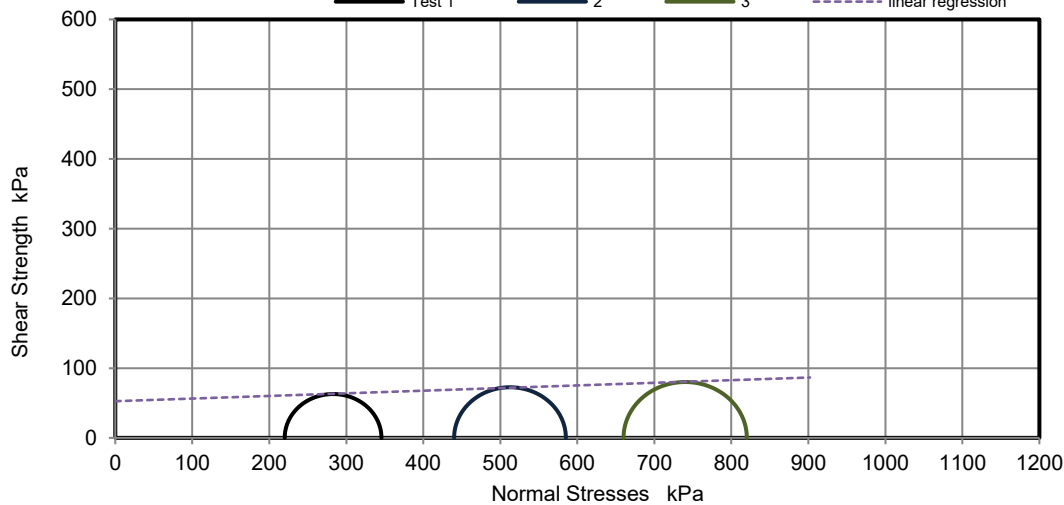
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )<sub>f</sub>  
Shear strength, cu  
Mode of failure  
Membrane Correction

1.99			%/min
1	2	3	
220	440	660	kPa
8.5	10.5	13.1	%
126	145	160	kPa
63	73	80	kPa
Compound			
0.54	0.62	0.74	kPa

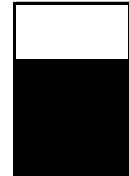
### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  2.2 °  
cu 53 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 220kPa=107N, 440kPa=211N, 660kPa=313N.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 11/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2185994  
Hole No.: BH12  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly slightly sandy CLAY  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

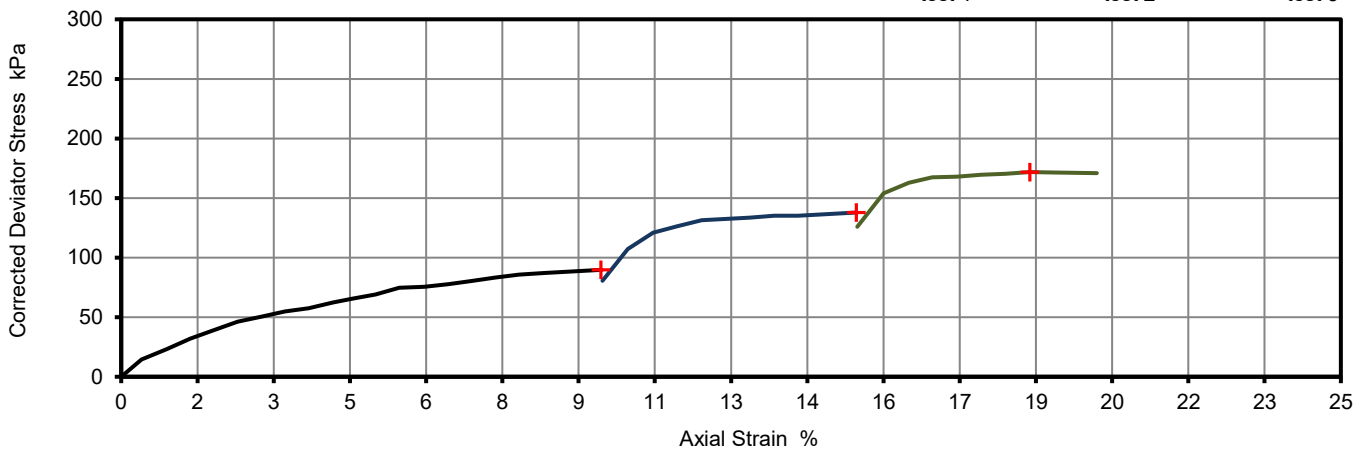
Depth Top [m]: 14.00  
Depth Base [m]: 14.45  
Sample Type: U

Length	140.91	mm
Diameter	69.99	mm
Bulk Density	2.07	Mg/m <sup>3</sup>
Moisture Content	20	%
Dry Density	1.72	Mg/m <sup>3</sup>
Membrane thickness	0.24	mm

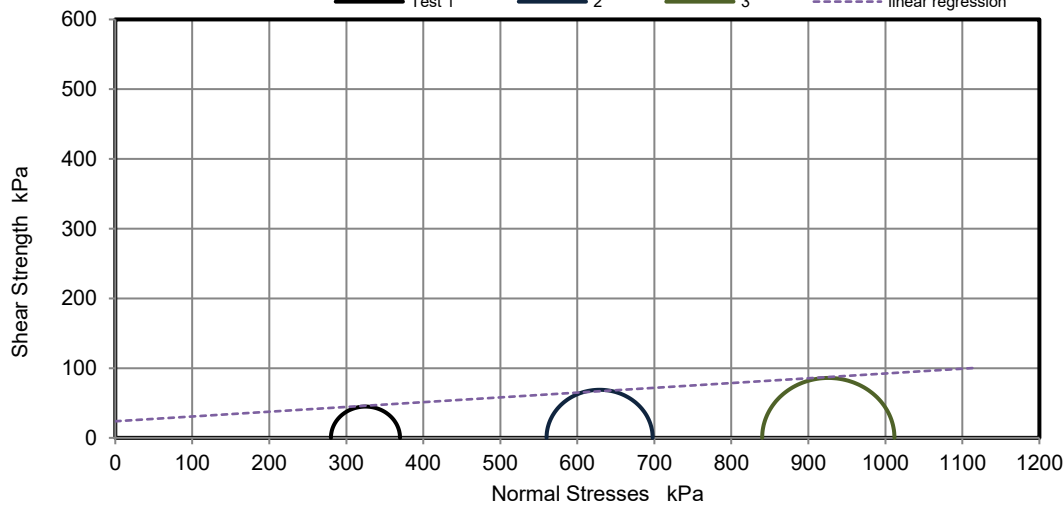
Rate of Strain: 2.00 %/min  
Stage Number: 1  
Cell Pressure: 280 kPa  
Axial Strain at failure: 9.8 %  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )<sub>f</sub>: 90 kPa  
Shear strength,  $c_u$ : 45 kPa  
Mode of failure: 45  
Membrane Correction: 0.75 kPa

2.00			%/min
1	2	3	
280	560	840	kPa
9.8	15.1	18.6	%
90	138	172	kPa
45	69	86	kPa
Compound			
0.75	1.04	1.24	kPa

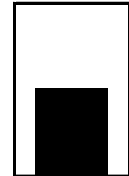
### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  3.9 °  
 $c_u$  24 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 280kPa=144N, 540kPa=294N, 840kPa=419N.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2186002  
Hole No.: BH13  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly sandy CLAY  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

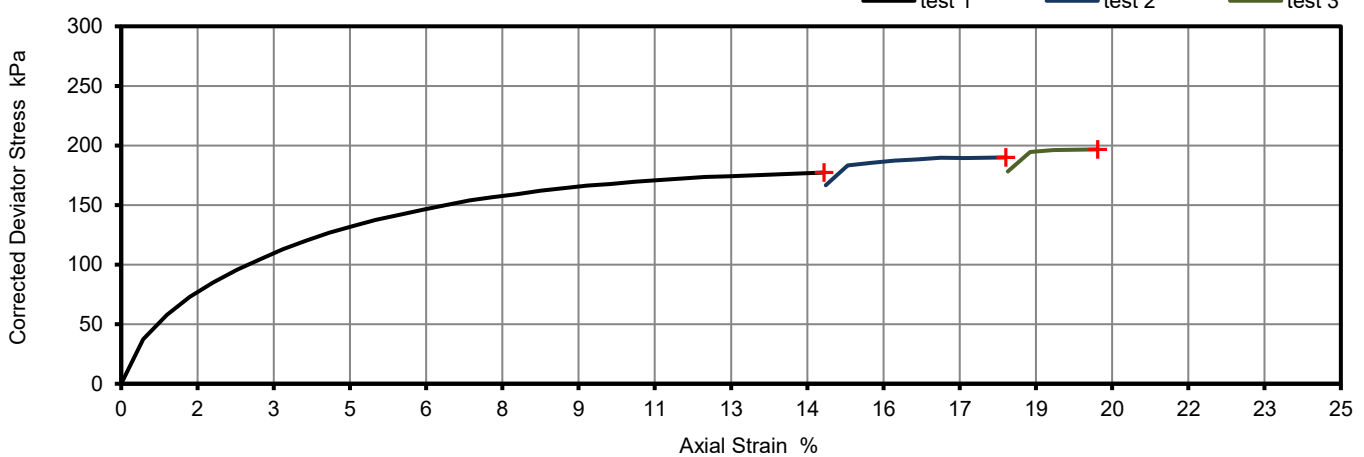
Depth Top [m]: 3.00  
Depth Base [m]: Not Given  
Sample Type: U

Length	203.71	mm
Diameter	103.39	mm
Bulk Density	2.13	Mg/m <sup>3</sup>
Moisture Content	21	%
Dry Density	1.76	Mg/m <sup>3</sup>
Membrane thickness	0.29	mm

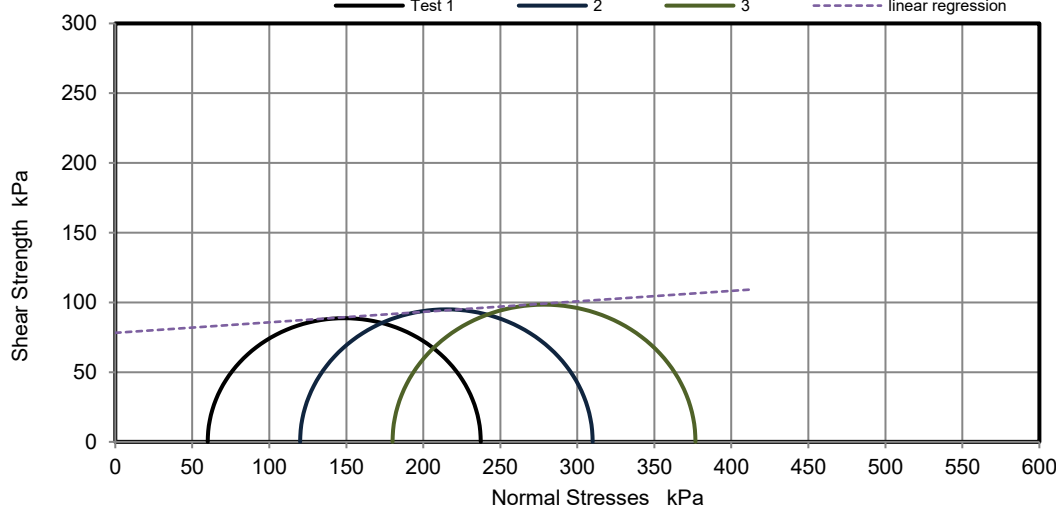
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )  
Shear strength, cu  
Mode of failure  
Membrane Correction

1.96			%/min
1	2	3	
60	120	180	kPa
14.4	18.1	20.0	%
177	190	197	kPa
89	95	98	kPa
Plastic			
0.82	0.99	1.08	kPa

### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  4.3 °  
cu 78 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 60kPa=33N, 120kPa=54N, 180kPa=98N.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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## DETERMINATION OF THE UNDRAINED SHEAR STRENGTH IN TRIAXIAL COMPRESSION WITHOUT MEASUREMENT OF PORE PRESSURE

i2 Analytical Ltd  
Unit 8 Harrowden Road  
Brackmills Industrial Estate  
Northampton NN4 7EB

4041

Tested in Accordance with: BS 1377-7: 1990: Clause 9

Client: Delta-Simons  
Client Address: 3 Henley Office Park, Doddington Road,  
Lincoln, LN6 3QR

Client Reference: 15-0645.05  
Job Number: 22-42014  
Date Sampled: 17/02/2022  
Date Received: 24/02/2022  
Date Tested: 02/03/2022  
Sampled By: Not Given

Contact: Harry Whittle  
Site Address: Corby EfW

Testing carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### Test Results:

Laboratory Reference: 2186341  
Hole No.: BH13  
Sample Reference: Not Given  
Sample Description: Brownish grey slightly gravelly slightly sandy CLAY  
Sample Preparation: Sample prepared in accordance with BS 1377-1:2016 Clause 9.1.1.

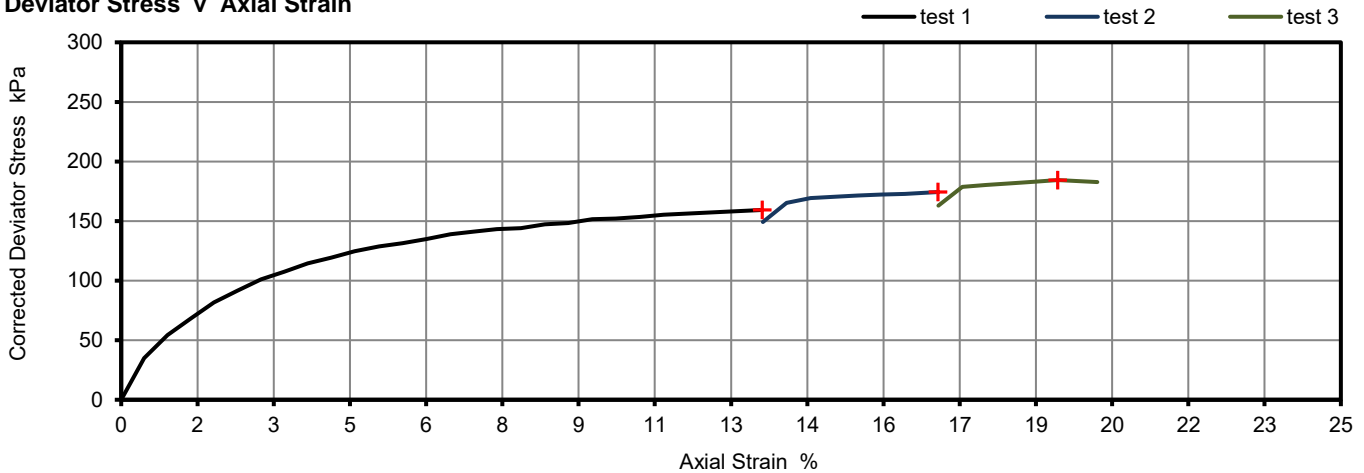
Depth Top [m]: 5.00  
Depth Base [m]: Not Given  
Sample Type: U

Length	202.92	mm
Diameter	102.63	mm
Bulk Density	2.13	Mg/m <sup>3</sup>
Moisture Content	18	%
Dry Density	1.80	Mg/m <sup>3</sup>
Membrane thickness	0.28	mm

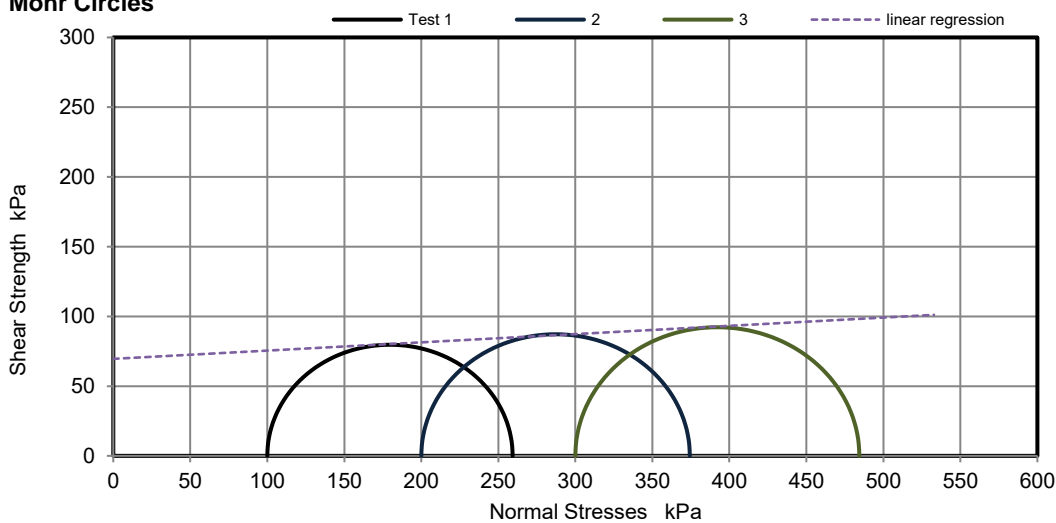
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ )<sub>f</sub>  
Shear strength, cu  
Mode of failure  
Membrane Correction

1.97			%/min
1	2	3	
100	200	300	kPa
13.1	16.7	19.2	%
159	174	184	kPa
80	87	92	kPa
Plastic			
0.75	0.91	1.01	kPa

### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  3.4 °  
cu 70 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 100kPa=57N, 200kPa=100N, 300kPa=144N.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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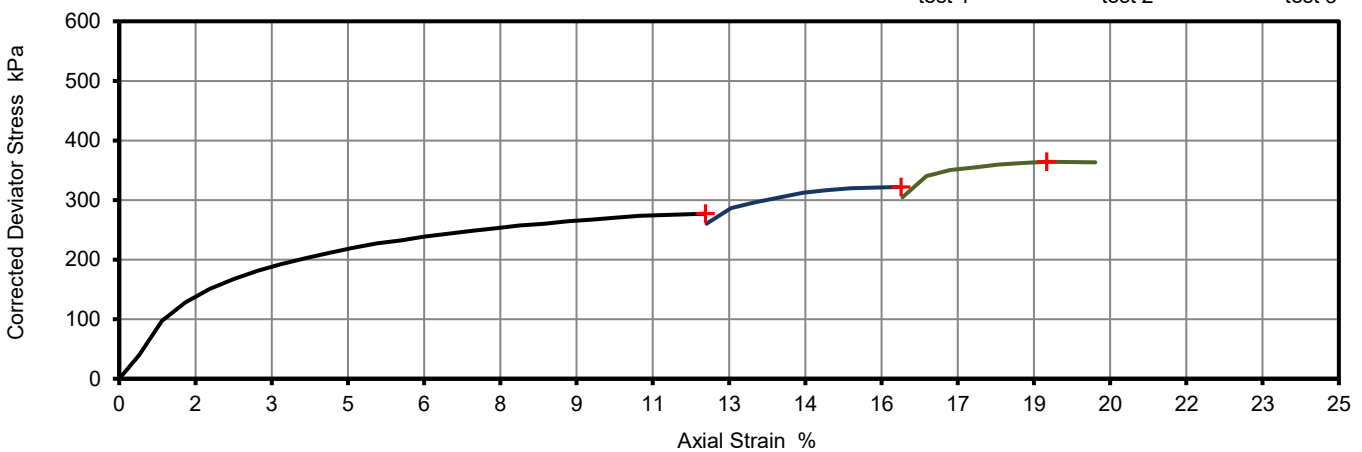
Depth Top [m]: 8.00  
Depth Base [m]: Not Given  
Sample Type: U

Length	140.95	mm
Diameter	69.61	mm
Bulk Density	2.07	Mg/m <sup>3</sup>
Moisture Content	17	%
Dry Density	1.77	Mg/m <sup>3</sup>
Membrane thickness	0.23	mm

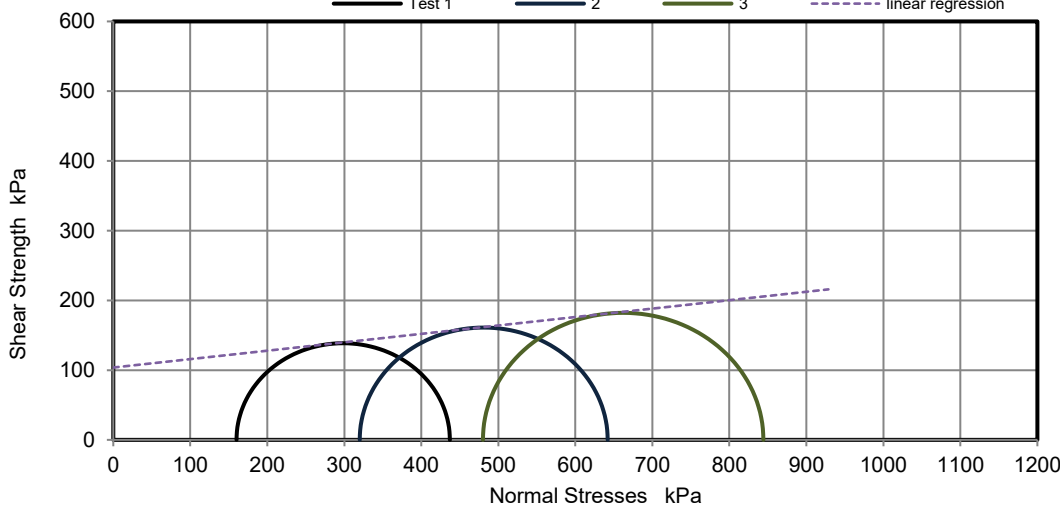
Rate of Strain  
Stage Number  
Cell Pressure  
Axial Strain at failure  
Deviator Stress, ( $\sigma_1 - \sigma_3$ ) f  
Shear strength, cu  
Mode of failure  
Membrane Correction

2.00			%/min
1	2	3	
160	320	480	kPa
12.0	16.0	19.0	%
277	322	364	kPa
139	161	182	kPa
Compound			
0.84	1.06	1.22	kPa

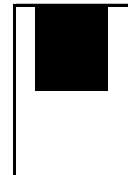
### Deviator Stress v Axial Strain



### Mohr Circles



Position within sample



Linear Regression  
 $\phi_u$  6.9 °  
cu 104 kPa

Note: Mohr circles and their interpretation is not covered by BS1377. These are provided for information only.

Remarks: Correction values: 160kPa=87N, 320kPa=160N, 460kPa=233N.  
Preliminary report

Signed:

Anna Dudzinska  
Deputy Head of Geo Office Section  
for and on behalf of i2 Analytical Ltd

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## Appendix F - Field Monitoring Data/Gas Monitoring Data/Soakaway Testing





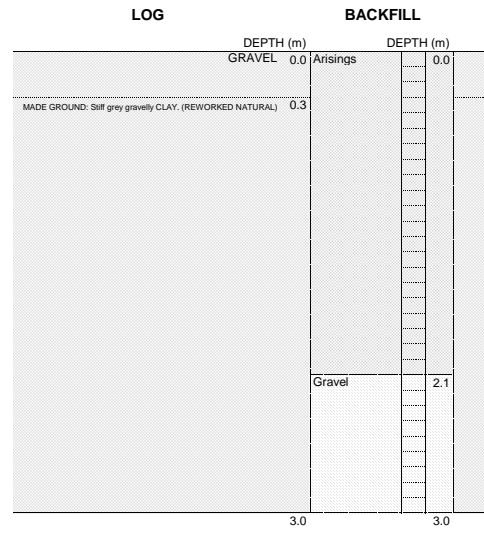
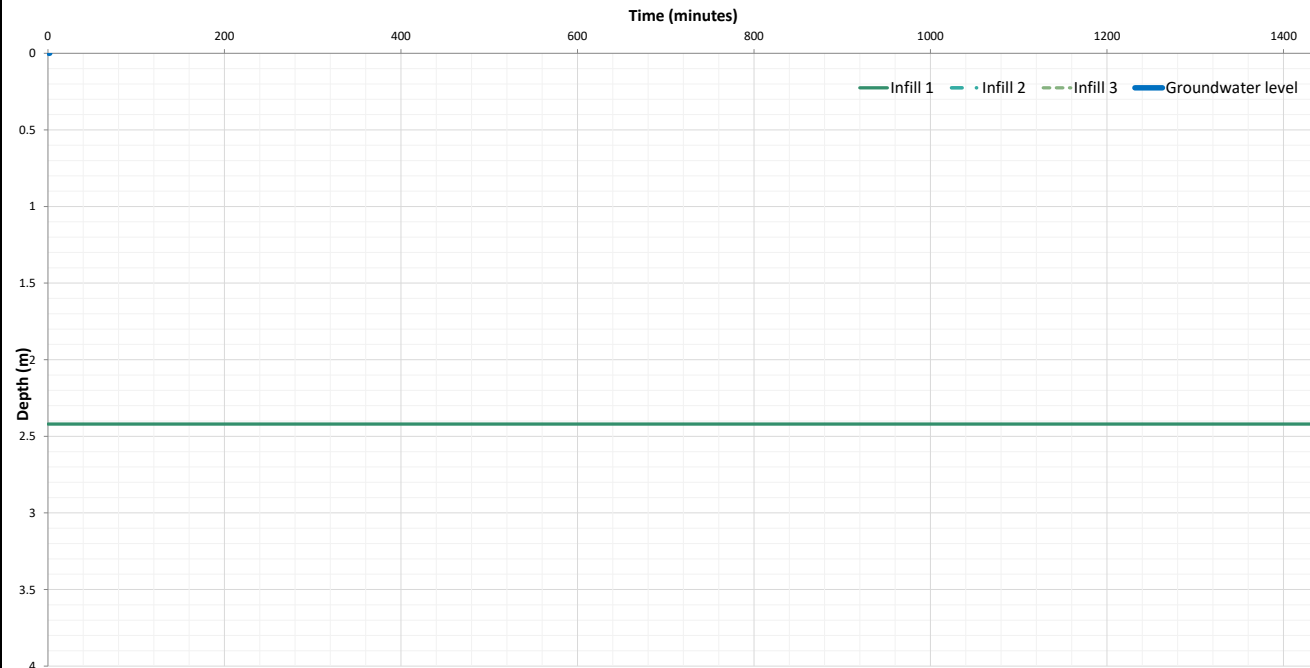


	units	Infill 1	Infill 2	Infill 3
Length	m		2.40	
Width	m		0.60	
Depth	m		3.00	
Gravel type		20mm single size		
Voids ratio		0.40		
Resting groundwater level at time of testing	m	Dry		
Depth of first reading	m	2.42	0.00	0.00
Depth of final reading	m	2.42	0.00	0.00
Did soakage test reach 25% of maximum fill depth?		No	No	No
Depth at 75% full/effective depth	m	2.42	0.00	0.00
Depth at 25% full/effective depth	m	2.42	0.00	0.00
Time at 75% full/effective depth	mins	#DIV/0!	#N/A	#N/A
Time at 25% full/effective depth	mins	#DIV/0!	#N/A	#N/A
Vp75 - 25 (volume outflowing between 75% and 25% full/effective depth)	m3	0.00	0.00	0.00
Mean surface area for outflow (50% full/effective depth)	m2	1.44	1.44	1.44
tp75 (time for the water level to fall from 75% to 25% full/effective depth)	mins	#DIV/0!	#N/A	#N/A
Soil infiltration rate, f =	m/s	#DIV/0!	#N/A	#N/A
or	m/s	#DIV/0!	#N/A	#N/A

Recommended soil infiltration rate

#DIV/0!	m/s
---------	-----

**Note:**  
*Where water level did not fall below the 25% of the maximum fill level, soil infiltration rate is based on effective drainage achieved only.*



TITLE: Soakaway Test Results  
 Corby  
 Mytilineous

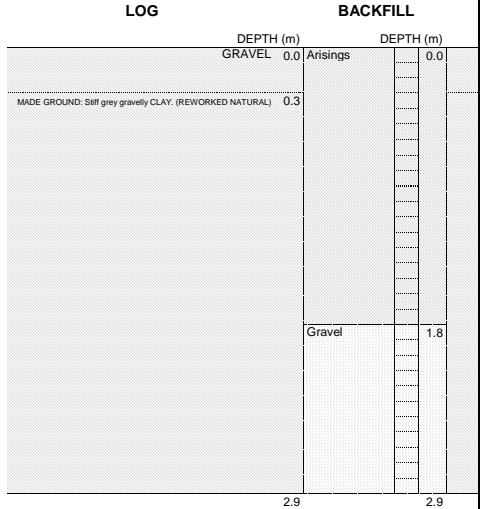
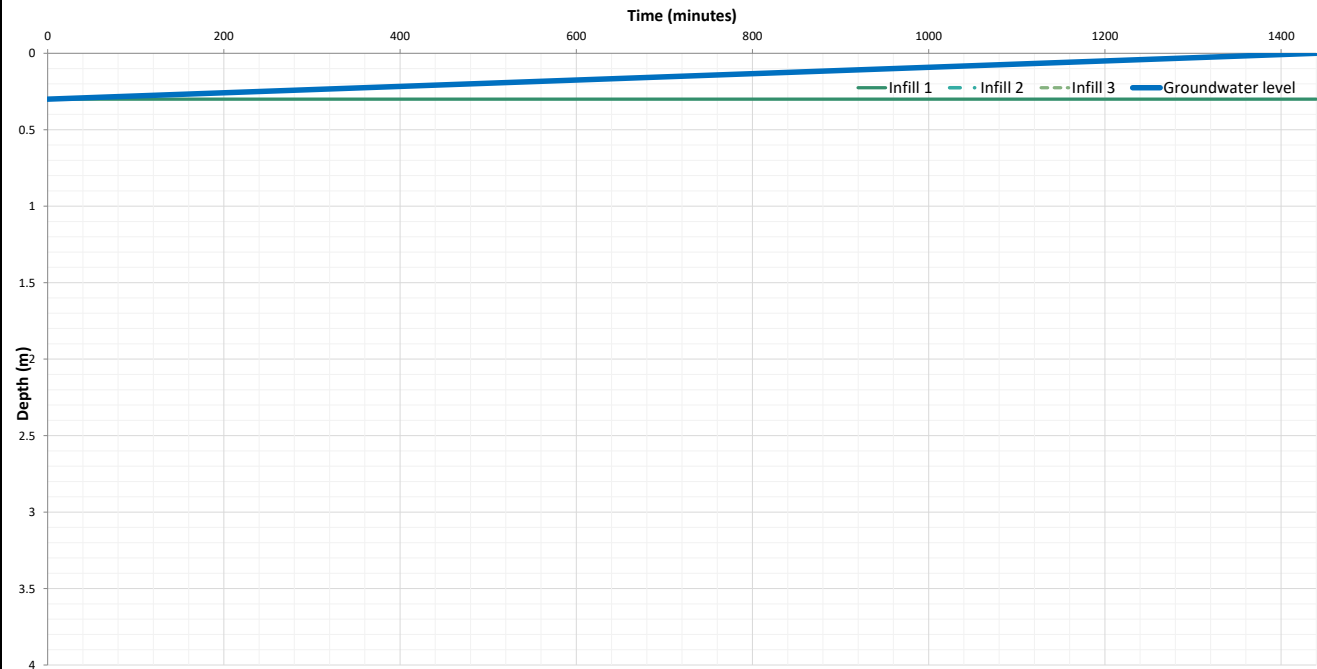
*In accordance with BRE Digest 365 (2016)*

DRAWN BY: CB	SCALE: Not to Scale	PROJECT NUMBER: 15-0645.05
CHECKED BY: SS	REVISION: 1	SOAKAWAY NUMBER: TR-1
DATE: 04/02/2022		

	units	Infill 1	Infill 2	Infill 3
Length	m		2.40	
Width	m		0.60	
Depth	m		2.90	
Gravel type		20mm single size		
Voids ratio		0.40		
Resting groundwater level at time of testing	m	0.30		
Depth of first reading	m	0.30	0.00	0.00
Depth of final reading	m	0.30	0.00	0.00
Did soakage test reach 25% of maximum fill depth?		No	No	No
Depth at 75% full/effective depth	m	0.30	0.00	0.00
Depth at 25% full/effective depth	m	0.30	0.00	0.00
Time at 75% full/effective depth	mins	#DIV/0!	#N/A	#N/A
Time at 25% full/effective depth	mins	#DIV/0!	#N/A	#N/A
Vp75 - 25 (volume outflowing between 75% and 25% full/effective depth)	m3	0.00	0.00	0.00
Mean surface area for outflow (50% full/effective depth)	m2	1.44	1.44	1.44
tp75 (time for the water level to fall from 75% to 25% full/effective depth)	mins	#DIV/0!	#N/A	#N/A
Soil infiltration rate, f =	m/s	#DIV/0!	#N/A	#N/A
or	m/s	#DIV/0!	#N/A	#N/A

Recommended soil infiltration rate	
#DIV/0!	m/s

**Note:**  
*Where water level did not fall below the 25% of the maximum fill level, soil infiltration rate is based on effective drainage achieved only.*



TITLE: Soakaway Test Results  
 Corby  
 Mytilineous

*In accordance with BRE Digest 365 (2016)*

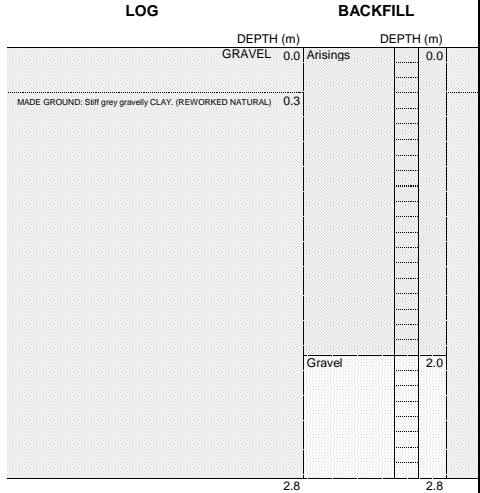
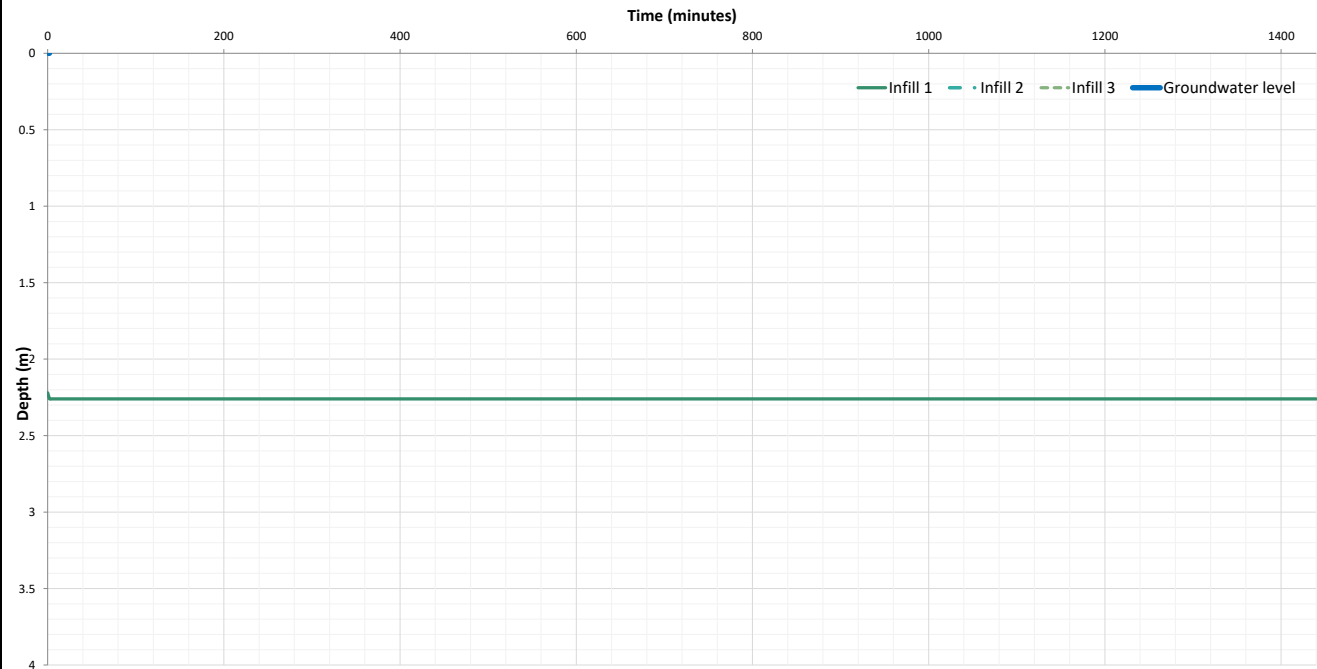
DRAWN BY: CB	SCALE: Not to Scale	PROJECT NUMBER: 15-0645.05
CHECKED BY: SS	REVISION: 1	SOAKAWAY NUMBER: TR-2
DATE: 04/02/2022		



	units	Infill 1	Infill 2	Infill 3
Length	m		2.60	
Width	m		0.60	
Depth	m		2.80	
Gravel type		20mm single size		
Voids ratio		0.40		
Resting groundwater level at time of testing	m	Dry		
Depth of first reading	m	2.22	0.00	0.00
Depth of final reading	m	2.26	0.00	0.00
Did soakage test reach 25% of maximum fill depth?		No	No	No
Depth at 75% full/effective depth	m	2.23	0.00	0.00
Depth at 25% full/effective depth	m	2.25	0.00	0.00
Time at 75% full/effective depth	mins	0.50	#N/A	#N/A
Time at 25% full/effective depth	mins	1.50	#N/A	#N/A
Vp75 - 25 (volume outflowing between 75% and 25% full/effective depth)	m3	0.01	0.00	0.00
Mean surface area for outflow (50% full/effective depth)	m2	1.69	1.56	1.56
tp75 (time for the water level to fall from 75% to 25% full/effective depth)	mins	1.00	#N/A	#N/A
Soil infiltration rate, f =	m/s	0.00012322	#N/A	#N/A
or	m/s	1.2E-04	#N/A	#N/A

Recommended soil infiltration rate	
#N/A	m/s

**Note:**  
Where water level did not fall below the 25% of the maximum fill level, soil infiltration rate is based on effective drainage achieved only.



TITLE: Soakaway Test Results  
Corby  
Mytilineous

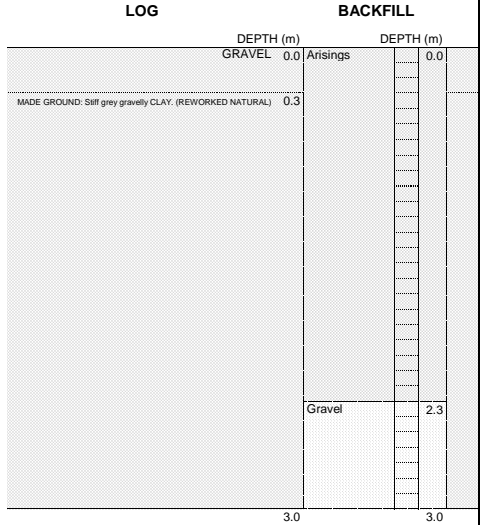
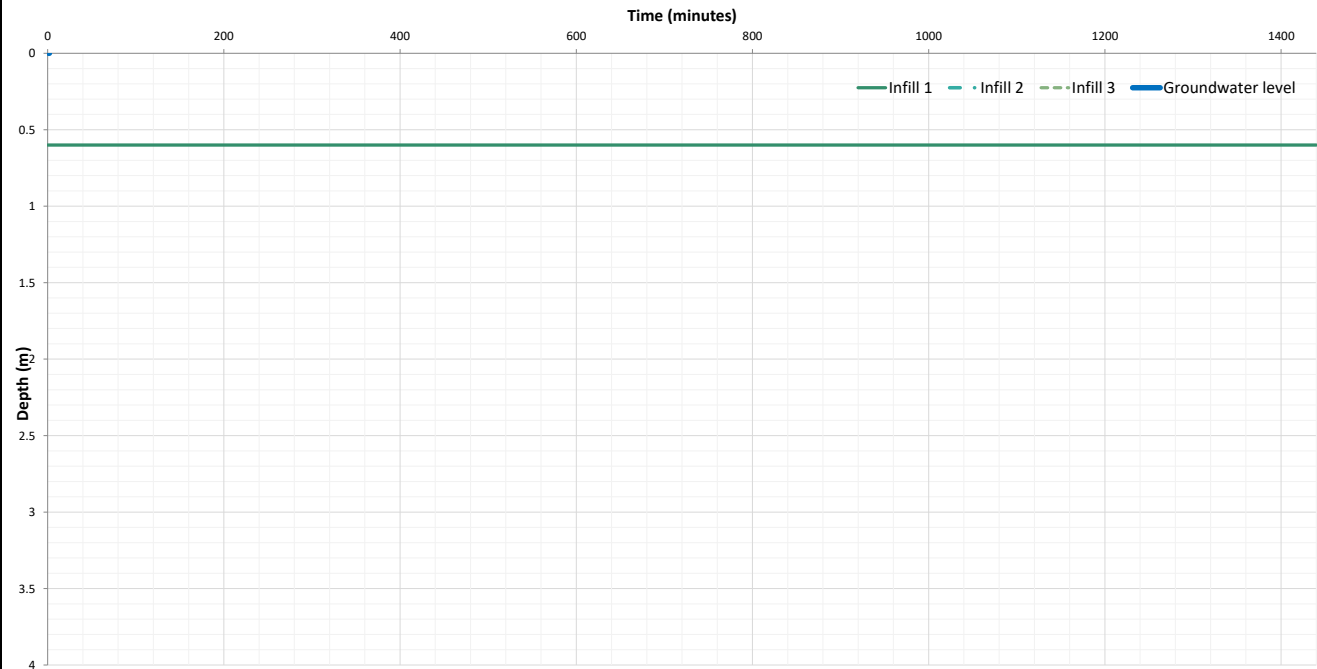
In accordance with BRE Digest 365 (2016)

DRAWN BY: CB	SCALE: Not to Scale	PROJECT NUMBER: 15-0645.05
CHECKED BY: SS	REVISION: 1	SOAKAWAY NUMBER: TR-3
DATE: 04/02/2022		

	units	Infill 1	Infill 2	Infill 3
Length	m		2.40	
Width	m		0.60	
Depth	m		3.00	
Gravel type		20mm single size		
Voids ratio		0.40		
Resting groundwater level at time of testing	m	Dry		
Depth of first reading	m	0.60	0.00	0.00
Depth of final reading	m	0.60	0.00	0.00
Did soakage test reach 25% of maximum fill depth?		No	No	No
Depth at 75% full/effective depth	m	0.60	0.00	0.00
Depth at 25% full/effective depth	m	0.60	0.00	0.00
Time at 75% full/effective depth	mins	#DIV/0!	#N/A	#N/A
Time at 25% full/effective depth	mins	#DIV/0!	#N/A	#N/A
Vp75 - 25 (volume outflowing between 75% and 25% full/effective depth)	m3	0.00	0.00	0.00
Mean surface area for outflow (50% full/effective depth)	m2	1.44	1.44	1.44
tp75 (time for the water level to fall from 75% to 25% full/effective depth)	mins	#DIV/0!	#N/A	#N/A
Soil infiltration rate, f =	m/s	#DIV/0!	#N/A	#N/A
or	m/s	#DIV/0!	#N/A	#N/A

Recommended soil infiltration rate	
#DIV/0!	m/s

**Note:**  
**Where water level did not fall below the 25% of the maximum fill level, soil infiltration rate is based on effective drainage achieved only.**

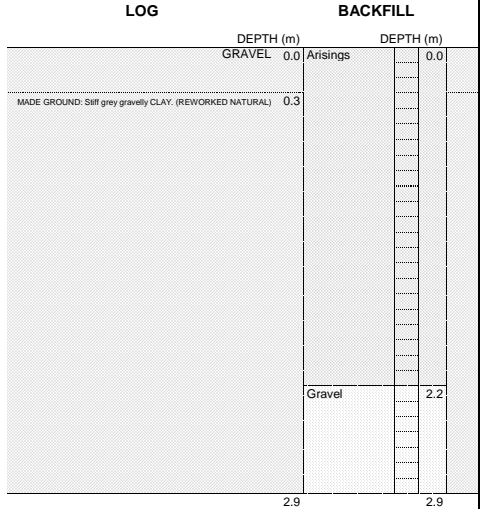
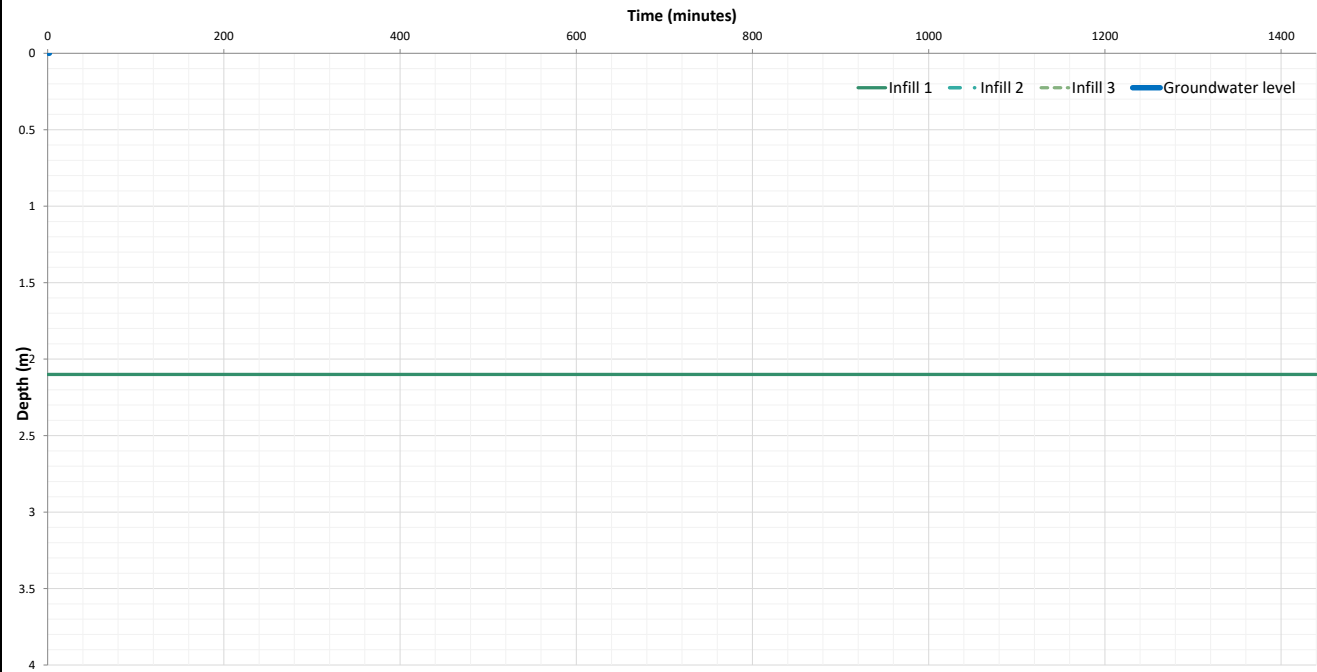


	TITLE: Soakaway Test Results Corby Mytilineous	<i>In accordance with BRE Digest 365 (2016)</i>	DRAWN BY: CB	SCALE: Not to Scale	PROJECT NUMBER: 15-0645.05
	CHECKED BY: SS		REVISION: 1	SOAKAWAY NUMBER: TR-4	
	DATE: 04/02/2022				

	units	Infill 1	Infill 2	Infill 3
Length	m		2.00	
Width	m		0.60	
Depth	m		2.90	
Gravel type		20mm single size		
Voids ratio		0.40		
Resting groundwater level at time of testing	m	Dry		
Depth of first reading	m	2.10	0.00	0.00
Depth of final reading	m	2.10	0.00	0.00
Did soakage test reach 25% of maximum fill depth?		No	No	No
Depth at 75% full/effective depth	m	2.10	0.00	0.00
Depth at 25% full/effective depth	m	2.10	0.00	0.00
Time at 75% full/effective depth	mins	#DIV/0!	#N/A	#N/A
Time at 25% full/effective depth	mins	#DIV/0!	#N/A	#N/A
Vp75 - 25 (volume outflowing between 75% and 25% full/effective depth)	m3	0.00	0.00	0.00
Mean surface area for outflow (50% full/effective depth)	m2	1.20	1.20	1.20
tp75 (time for the water level to fall from 75% to 25% full/effective depth)	mins	#DIV/0!	#N/A	#N/A
Soil infiltration rate, f =	m/s	#DIV/0!	#N/A	#N/A
or	m/s	#DIV/0!	#N/A	#N/A

Recommended soil infiltration rate	
#DIV/0!	m/s

**Note:**  
**Where water level did not fall below the 25% of the maximum fill level, soil infiltration rate is based on effective drainage achieved only.**



TITLE: Soakaway Test Results  
 Corby  
 Mytilineous

In accordance with BRE Digest 365 (2016)

DRAWN BY: CB	SCALE: Not to Scale	PROJECT NUMBER: 15-0645.05
CHECKED BY: SS	REVISION: 1	SOAKAWAY NUMBER: TR-5
DATE: 04/02/2022		

## Appendix G - Risk Definitions

## Contaminated Land Risk Definitions

The following methodology is based on the methodology presented in CIRIA C552 Contaminated Land Risk Assessment: A Guide to Good Practice 2001. It requires the classification of the:

- ▲ Magnitude of the potential consequence (severity) of the Risk occurring: and
- ▲ Magnitude of the Probability (likelihood) of the Risk occurring.

The classifications are then compared to indicate the risk presented by each pollutant linkage.

### Consequence to Receptor Definition Matrix

	Human Health	Controlled Waters	Buildings/Services
Severe Consequence	Acute or chronic permanent impact on human health.	Sensitive controlled water pollution ongoing, or just about to occur.	Catastrophic collapse
Medium Consequence	Chronic permanent impact on human health	Gradual pollution of sensitive controlled water	Degradation of materials
Mild Consequence	Chronic temporary impact on human health	Gradual pollution of non-sensitive controlled water	Damage to building rendering it unsafe to occupy (eg foundation damage resulting in instability).
Minor Consequence	Non-permanent health effects to human health (easily prevented by means such as personal protective clothing etc).	Slight discoloration of water	Easily repairable effects of damage to buildings, structures and services, i.e discoloration of concrete

### Probability Definitions

Probability	Definition in Context
Higher	There is a pollution linkage and an event that either appears very likely in the short term and almost inevitable over the long term, or there is evidence at the receptor of harm or pollution. Positive evidence of source, pathway and receptor.
Likely	There is a pollution linkage and all the elements are present and in the right place, which means that it is probable that an event will occur. Circumstances are such that an event is not inevitable, but possible in the short term and likely over the long term. Suspect source, pathway, and receptor
Low Likelihood	There is a pollution linkage and circumstances are possible under which an event could occur. However, it is by no means certain that even over a longer period such event would take place, and is less likely in the shorter term.
Unlikely	There is a pollution linkage but circumstances are such that it is improbable that an event would occur even in the very long term No evidence of hazard, pathway, and receptor

## Standard Risk Matrix

		Consequence/Magnitude of impact			
		Severe	Medium	Mild	Minor
Probability	High	Very High	High	Moderate	Moderate/Low
	Likely	High	Moderate	Moderate/low	Low
	Low Likelihood	Moderate	Moderate/low	Low	Very Low
	Unlikely	Moderate/low	Low	Very Low	Very Low

## Classified risks and likely action

Significance Level	Definition/Comments
<b>Very High Risk</b>	<p>There is a high probability that severe harm could arise to a designated receptor from an identified hazard, OR, there is evidence that severe harm to a designated receptor is currently happening.</p> <p>This risk, if realised, is likely to result in a substantial liability. Urgent investigation (if not undertaken already) and remediation are likely to be required.</p> <p>Demonstrable contaminated land situation, highest threat &amp; liability level, urgent action recommended.</p>
<b>High Risk</b>	<p>Harm is likely to arise to a designated receptor from an identified hazard.</p> <p>Realisation of the risk is likely to present a substantial liability. Urgent investigation (if not undertaken already) is required and remedial works may be necessary in the short term and are likely over the longer term.</p> <p>Likely contaminated land situation, risk assessment and action recommended.</p>
<b>Moderate</b>	<p>It is possible that harm could arise to a designated receptor from an identified hazard. However, if is either relatively unlikely that any such harm would be severe, or if any harm were to occur it is more likely that the harm would be relatively mild</p> <p>Investigation (if not already undertaken) is normally required to clarify the risk and to determine the potential liability. Some remedial works may be required in the longer term.</p> <p>Plausible contaminated land situation, risk assessment and possible action recommended.</p>
<b>Low Risk</b>	<p>It is possible that harm could arise to a designated receptor from an identified hazard, but it is likely that this harm, if realised, would at worst normally be mild.</p> <p>Unlikely contaminated land situation, possible risk assessment and possible action.</p>
<b>Very Low Risk</b>	<p>There is a low possibility that harm could arise to a receptor. In the event of such harm being realised it is not likely to be severe.</p> <p>Negligible risk, no action recommended except vigilance for changes in conditions.</p>

## Geotechnical Risk Classification

The geohazards listed in the report within Section 4 follow guidance presented in Clayton, C.R.I. (2001) *Managing Geotechnical Risk*, Thomas Telford and the Highways Agency document CD622 '*Managing Geotechnical Risk*' (2008) which aims to identify and manage the geotechnical risks associated with a scheme throughout its lifespan, from planning to construction to maintenance.

For each geohazard the probability of the hazard occurring (P) has been considered together with the impact it would have (I) if it were to happen to calculate the risk rating between 1 and 25.

Risks that fall within Moderate, Significant and Severe categories below are considered to be **substantial** and are therefore listed within the report.

<table border="1" style="border-collapse: collapse; width: 100%;"> <thead> <tr> <th style="padding: 5px;">Probability</th> <th style="padding: 5px;">(P)</th> </tr> </thead> <tbody> <tr> <td style="padding: 5px;">Very Likely (VLk)</td> <td style="padding: 5px;">5</td> </tr> <tr> <td style="padding: 5px;">Likely (Lk)</td> <td style="padding: 5px;">4</td> </tr> <tr> <td style="padding: 5px;">Plausible (P)</td> <td style="padding: 5px;">3</td> </tr> <tr> <td style="padding: 5px;">Unlikely (U)</td> <td style="padding: 5px;">2</td> </tr> <tr> <td style="padding: 5px;">Very Unlikely (VU)</td> <td style="padding: 5px;">1</td> </tr> </tbody> </table>	Probability	(P)	Very Likely (VLk)	5	Likely (Lk)	4	Plausible (P)	3	Unlikely (U)	2	Very Unlikely (VU)	1	X	<table border="1" style="border-collapse: collapse; width: 100%;"> <thead> <tr> <th style="padding: 5px;">Impact</th> <th style="padding: 5px;">(I)</th> </tr> </thead> <tbody> <tr> <td style="padding: 5px;">Very High (VH)</td> <td style="padding: 5px;">5</td> </tr> <tr> <td style="padding: 5px;">High (H)</td> <td style="padding: 5px;">4</td> </tr> <tr> <td style="padding: 5px;">Medium (M)</td> <td style="padding: 5px;">3</td> </tr> <tr> <td style="padding: 5px;">Low (L)</td> <td style="padding: 5px;">2</td> </tr> <tr> <td style="padding: 5px;">Very Low (VL)</td> <td style="padding: 5px;">1</td> </tr> </tbody> </table>	Impact	(I)	Very High (VH)	5	High (H)	4	Medium (M)	3	Low (L)	2	Very Low (VL)	1	=	<table border="1" style="border-collapse: collapse; width: 100%;"> <thead> <tr> <th style="padding: 5px;">(R)</th> <th style="padding: 5px;">Risk</th> </tr> </thead> <tbody> <tr> <td style="padding: 5px;">20 – 25</td> <td style="padding: 5px; background-color: red;">Severe</td> </tr> <tr> <td style="padding: 5px;">15 – 19</td> <td style="padding: 5px; background-color: orange;">Substantial</td> </tr> <tr> <td style="padding: 5px;">10 – 14</td> <td style="padding: 5px; background-color: yellow;">Moderate</td> </tr> <tr> <td style="padding: 5px;">5 – 9</td> <td style="padding: 5px; background-color: lightgrey;">Minor</td> </tr> <tr> <td style="padding: 5px;">1 – 4</td> <td style="padding: 5px;">Negligible</td> </tr> </tbody> </table>	(R)	Risk	20 – 25	Severe	15 – 19	Substantial	10 – 14	Moderate	5 – 9	Minor	1 – 4	Negligible
Probability	(P)																																							
Very Likely (VLk)	5																																							
Likely (Lk)	4																																							
Plausible (P)	3																																							
Unlikely (U)	2																																							
Very Unlikely (VU)	1																																							
Impact	(I)																																							
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Medium (M)	3																																							
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Very Low (VL)	1																																							
(R)	Risk																																							
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10 – 14	Moderate																																							
5 – 9	Minor																																							
1 – 4	Negligible																																							