| Waterman Group | | Page 1 |
|------------------------------|-------------------------|-----------|
| Pickfords Wharf | | |
| Clink Street | | |
| London, SE1 9DG | | Micro |
| Date 16/12/2022 12:47 | Designed by CSSW | Drainage |
| File CALC_CANFORDEFW_SC_100+ | Checked by | nialilade |
| Innovyze | Source Control 2020.1.3 | |
| | | |

Summary of Results for 100 year Return Period (+45%)

| | Storm Event | Max Leve (m) | l Dept | | | Max Σ Outflow (1/s) | Max Volume (m³) | Status |
|-------|----------------|--------------------|---------|-------|-----|---------------------------|-----------------------|--------|
| 15 | min Sum | nmer 42.49 | 96 0.49 | 6 4.3 | 0.0 | 4.3 | 624.7 | O K |
| 30 | min Sum | nmer 42.6 | 64 0.66 | 4 4.3 | 0.0 | 4.3 | 837.1 | O K |
| 60 | min Sum | nmer 42.84 | 47 0.84 | 7 4.3 | 0.0 | 4.3 | 1067.3 | O K |
| 120 | min Sum | nmer 43.03 | 32 1.03 | 2 4.3 | 0.0 | 4.3 | 1300.5 | O K |
| 180 | min Sum | nmer 43.15 | 51 1.15 | 1 4.3 | 0.0 | 4.3 | 1450.2 | O K |
| 240 | min Sum | nmer 43.23 | 39 1.23 | 9 4.4 | 0.0 | 4.4 | 1561.3 | O K |
| 360 | min Sum | nmer 43.3 | 67 1.36 | 7 4.6 | 0.0 | 4.6 | 1722.0 | O K |
| 480 | min Sum | nmer 43.45 | 58 1.45 | 8 4.7 | 0.0 | 4.7 | 1837.0 | O K |
| 600 | min Sum | nmer 43.52 | 26 1.52 | 6 4.8 | 0.0 | 4.8 | 1923.2 | O K |
| 720 | min Sum | nmer 43.5 | 79 1.57 | 9 4.9 | 0.0 | 4.9 | 1989.8 | O K |
| 960 | min Sum | nmer 43.65 | 53 1.65 | 3 5.0 | 0.0 | 5.0 | 2082.9 | O K |
| 1440 | min Sum | nmer 43.72 | 21 1.72 | 1 5.1 | 0.0 | 5.1 | 2168.1 | O K |
| 2160 | min Sum | nmer 43.72 | 23 1.72 | 3 5.1 | 0.0 | 5.1 | 2171.5 | O K |
| 2880 | min Sum | nmer 43.68 | 34 1.68 | 4 5.0 | 0.0 | 5.0 | 2121.6 | O K |
| 4320 | min Sum | nmer 43.5 | 73 1.57 | 3 4.9 | 0.0 | 4.9 | 1981.6 | O K |
| 5760 | min Sum | nmer 43.49 | 96 1.49 | 6 4.8 | 0.0 | 4.8 | 1885.1 | O K |
| 7200 | min Sum | nmer 43.45 | 58 1.45 | 8 4.7 | 0.0 | 4.7 | 1836.8 | O K |
| 8640 | min Sum | nmer 43.43 | 36 1.43 | 6 4.7 | 0.0 | 4.7 | 1809.4 | O K |
| 10080 | min Sum | nmer 43.42 | 25 1.42 | 5 4.7 | 0.0 | 4.7 | 1796.1 | O K |
| 15 | min Win | nter 42.55 | 56 0.55 | 6 4.3 | 0.0 | 4.3 | 700.3 | O K |
| 30 | min Win | nter 42.74 | 45 0.74 | 5 4.3 | 0.0 | 4.3 | 938.5 | O K |

| Waterman Group | | Page 2 |
|------------------------------|-------------------------|-----------|
| Pickfords Wharf | | |
| Clink Street | | |
| London, SE1 9DG | | Micro |
| Date 16/12/2022 12:47 | Designed by CSSW | Drainage |
| File CALC_CANFORDEFW_SC_100+ | Checked by | Drairiage |
| Innovvze | Source Control 2020.1.3 | |

Summary of Results for 100 year Return Period (+45%)

| | Stori Even | | Max Level (m) | Max Depth (m) | Max Control (1/s) | Max Overflow (1/s) | Σ | Max Outflow (1/s) | Max Volume (m³) | Status | ; |
|------|---------------|--------|---------------------|---------------------|-------------------------|--------------------------|---|-------------------------|-----------------------|--------|---|
| 60 | min | Winter | 42.950 | 0.950 | 4.3 | 0.0 | | 4.3 | 1196.9 | O K | (|
| 120 | min | Winter | 43.158 | 1.158 | 4.3 | 0.0 | | 4.3 | 1459.7 | OK | (|
| 180 | min | Winter | 43.293 | 1.293 | 4.5 | 0.0 | | 4.5 | 1629.5 | O K | (|
| 240 | min | Winter | 43.393 | 1.393 | 4.7 | 0.0 | | 4.7 | 1755.8 | O K | (|
| 360 | min | Winter | 43.539 | 1.539 | 4.9 | 0.0 | | 4.9 | 1939.3 | O K | (|
| 480 | min | Winter | 43.644 | 1.644 | 5.0 | 0.0 | | 5.0 | 2071.9 | O K | (|
| 600 | min | Winter | 43.724 | 1.724 | 5.1 | 0.0 | | 5.1 | 2172.4 | O K | (|
| 720 | min | Winter | 43.786 | 1.786 | 5.2 | 0.0 | | 5.2 | 2250.8 | O K | (|
| 960 | min | Winter | 43.875 | 1.875 | 5.3 | 0.0 | | 5.3 | 2362.9 | O K | (|
| 1440 | min | Winter | 43.964 | 1.964 | 5.4 | 0.0 | | 5.4 | 2474.3 | O K | (|
| 2160 | min | Winter | 43.987 | 1.987 | 5.4 | 0.0 | | 5.4 | 2503.7 | O K | (|
| 2880 | min | Winter | 43.963 | 1.963 | 5.4 | 0.0 | | 5.4 | 2474.0 | O K | (|
| 4320 | min | Winter | 43.862 | 1.862 | 5.3 | 0.0 | | 5.3 | 2346.5 | O K | (|
| 5760 | min | Winter | 43.765 | 1.765 | 5.1 | 0.0 | | 5.1 | 2223.4 | O K | (|
| 7200 | min | Winter | 43.706 | 1.706 | 5.1 | 0.0 | | 5.1 | 2149.3 | O K | 7 |
| 8640 | min | Winter | 43.672 | 1.672 | 5.0 | 0.0 | | 5.0 | 2107.0 | OK | (|
| 0800 | min | Winter | 43.650 | 1.650 | 5.0 | 0.0 | | 5.0 | 2078.6 | O K | 7 |

| | Storm Event | | Rain (mm/hr) | Volume | | Volume | Time-Peak (mins) |
|-------|----------------|--------|-----------------|--------|--------|--------|------------------|
| | | | | (m³) | (m³) | (m³) | |
| 60 | min W | Winter | 60.630 | 0.0 | 655.5 | 0.0 | 64 |
| 120 | min V | Winter | 37.271 | 0.0 | 675.7 | 0.0 | 122 |
| 180 | min V | Winter | 27.931 | 0.0 | 710.7 | 0.0 | 182 |
| 240 | min V | Winter | 22.724 | 0.0 | 735.4 | 0.0 | 242 |
| 360 | min V | Winter | 16.947 | 0.0 | 769.6 | 0.0 | 360 |
| 480 | min V | Winter | 13.743 | 0.0 | 792.4 | 0.0 | 478 |
| 600 | min V | Winter | 11.660 | 0.0 | 808.4 | 0.0 | 596 |
| 720 | min V | Winter | 10.181 | 0.0 | 819.9 | 0.0 | 714 |
| 960 | min V | Winter | 8.193 | 0.0 | 833.7 | 0.0 | 950 |
| 1440 | min W | Winter | 5.968 | 0.0 | 839.4 | 0.0 | 1414 |
| 2160 | min V | Winter | 4.289 | 0.0 | 1641.1 | 0.0 | 2100 |
| 2880 | min V | Winter | 3.382 | 0.0 | 1639.4 | 0.0 | 2768 |
| 4320 | min V | Winter | 2.414 | 0.0 | 1596.5 | 0.0 | 4060 |
| 5760 | min V | Winter | 1.911 | 0.0 | 2979.5 | 0.0 | 4608 |
| 7200 | min V | Winter | 1.612 | 0.0 | 2971.2 | 0.0 | 5544 |
| 8640 | min V | Winter | 1.413 | 0.0 | 2938.5 | 0.0 | 6480 |
| 10080 | min V | Vinter | 1.271 | 0.0 | 2880.8 | 0.0 | 7368 |

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| Waterman Group | | Page 3 |
|------------------------------|-------------------------|-----------|
| Pickfords Wharf | | |
| Clink Street | | |
| London, SE1 9DG | | Micro |
| Date 16/12/2022 12:47 | Designed by CSSW | Drainage |
| File CALC_CANFORDEFW_SC_100+ | Checked by | Dialilade |
| Innovyze | Source Control 2020.1.3 | |

Rainfall Details

Rainfall Model FEH Return Period (years) 100 FEH Rainfall Version 2013 Site Location GB 403424 96712 SZ 03424 96712 Data Type Point Summer Storms Yes Winter Storms Yes Cv (Summer) 0.750 Cv (Winter) 0.840 Shortest Storm (mins) 15 Longest Storm (mins) 10080 Climate Change % +45

Time Area Diagram

Total Area (ha) 2.380

Time (mins) Area From: To: (ha)

| Waterman Group | | Page 4 |
|------------------------------|-------------------------|-----------|
| Pickfords Wharf | | |
| Clink Street | | |
| London, SE1 9DG | | Micro |
| Date 16/12/2022 12:47 | Designed by CSSW | Drainage |
| File CALC_CANFORDEFW_SC_100+ | Checked by | Dialilade |
| Innovyze | Source Control 2020.1.3 | |

Model Details

Storage is Online Cover Level (m) 44.525

Tank or Pond Structure

Invert Level (m) 42.000

| Depth | (m) | Area | (m²) | Depth | (m) | Area | (m²) | Depth | (m) | Area | (m²) |
|-------|-----|------|-------|-------|------|------|-------|-------|-----|------|------|
| 0. | 000 | 12 | 260.0 | 2. | .000 | 12 | 260.0 | 2. | 001 | | 0.0 |

Hydro-Brake® Optimum Outflow Control

Unit Reference MD-SHE-0093-5200-2000-5200 Design Head (m) 2.000 Design Flow (1/s) 5.2 Flush-Flo™ Calculated Objective Minimise upstream storage Application Sump Available Diameter (mm) 93 Invert Level (m) 41.810 Minimum Outlet Pipe Diameter (mm) 150 Suggested Manhole Diameter (mm) 1200

Control Points Head (m) Flow (1/s) Design Point (Calculated) 2.000 5.2 Flush-Flo $^{\text{m}}$ 0.405 4.3 Kick-Flo $^{\text{m}}$ 0.832 3.5 Mean Flow over Head Range - 4.1

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake® Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

| Depth (m) | Flow (1/s) | Depth (m) Flo | ow (1/s) | Depth (m) Flow | (1/s) | Depth (m) | Flow (1/s) |
|-----------|------------|---------------|----------|----------------|-------|-----------|------------|
| | | | | | | | |
| 0.100 | 3.0 | 1.200 | 4.1 | 3.000 | 6.3 | 7.000 | 9.4 |
| 0.200 | 4.0 | 1.400 | 4.4 | 3.500 | 6.8 | 7.500 | 9.7 |
| 0.300 | 4.3 | 1.600 | 4.7 | 4.000 | 7.2 | 8.000 | 10.0 |
| 0.400 | 4.3 | 1.800 | 4.9 | 4.500 | 7.6 | 8.500 | 10.3 |
| 0.500 | 4.3 | 2.000 | 5.2 | 5.000 | 8.0 | 9.000 | 10.6 |
| 0.600 | 4.2 | 2.200 | 5.4 | 5.500 | 8.4 | 9.500 | 10.8 |
| 0.800 | 3.6 | 2.400 | 5.7 | 6.000 | 8.7 | | |
| 1.000 | 3.8 | 2.600 | 5.9 | 6.500 | 9.1 | | |

Weir Overflow Control

Discharge Coef 0.544 Width (m) 1.000 Invert Level (m) 44.300

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Print

Close Report



Growth curve factor 200 years:

Sean Whelan

Calculated by:

Greenfield runoff rate estimation for sites

50.77017° N

1.95232° W

2657742111

Nov 10 2022 13:37

Site Details

Latitude:

www.uksuds.com | Greenfield runoff tool

| Site name: | Canfo | rd EfW | | | | | Landa. | |
|--|-----------|--------------|---------|-------------|----------------------|---|------------------|----|
| | Carno | I G LIVV | | | | | Longitude: | |
| Site location: | Wimbo | orne | | | | | | |
| guidance "Rainfall run | off manag | gement for | develo | opments", S | C030219 (2013), | meet normal best practice criteria in line with Environment Agency 219 (2013), the SuDS Manual C753 (Ciria, 2015) and the non-statutory unoff rates may be the basis for setting consents for the drainage of | | |
| standards for SuDS (E surface water runoff fr | | 5). This inf | formati | on on green | field runoff rates n | nay be the basis for setting consents for the drainage of | Date: | |
| Runoff estimation | on appı | roach | IH12 | 4 | | | | |
| Site characteris | tics | | | | | Notes | | |
| Total site area (ha) | : 1 | | | | | (1) Is Q _{BAR} < 2.0 I/s/ha? | | |
| Methodology | | | | | | (1) 10 GBAN 1 IIO II O/MAI | | |
| Q _{BAR} estimation m | nethod: | Calcu | late fr | om SPR a | and SAAR | When Q_{BAR} is < 2.0 l/s/ha then limiting discha | rge rates are se | et |
| SPR estimation m | ethod: | Calcu | late fr | om SOIL 1 | type | at 2.0 l/s/ha. | | |
| Soil characteris | tics | Defaul | t | Edite | d | | | |
| SOIL type: | : | 2 | | 2 | | (2) Are flow rates < 5.0 l/s? | | |
| HOST class: | | N/A | | N/A | | Where flow rates are less than 5.0 l/s consent | for discharge in | |
| SPR/SPRHOST: | (| 0.3 | | 0.3 | | usually set at 5.0 l/s if blockage from vegetation | O | 5 |
| Hydrological ch | aracter | ristics | D | efault | Edited | materials is possible. Lower consent flow rates where the blockage risk is addressed by using | - | |
| SAAR (mm): | | | 823 | | 823 | drainage elements. | , appropriate | |
| Hydrological regio | n: | | 7 | | 7 | (3) Is SPR/SPRHOST ≤ 0.3? | | |
| Growth curve fact | or 1 yea | r: | 0.85 | 5 | 0.85 | (6,18 61 10 61 11 10 61 2 6.61 | | |
| Growth curve fact | or 30 ye | ars: | 2.3 | | 2.3 | Where groundwater levels are low enough the | | |
| Growth curve fact | or 100 y | ears: | 3.19 | 9 | 3.19 | soakaways to avoid discharge offsite would no preferred for disposal of surface water runoff. | ormally be | |

3.74

3.74

| Greenfield runoff rates | Default | Edited |
|-------------------------|---------|--------|
| Q _{BAR} (I/s): | 2.2 | 2.2 |
| 1 in 1 year (l/s): | 1.87 | 1.87 |
| 1 in 30 years (l/s): | 5.07 | 5.07 |
| 1 in 100 year (l/s): | 7.03 | 7.03 |
| 1 in 200 years (l/s): | 8.24 | 8.24 |

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at www.uksuds.com/terms-and-conditions.htm. The outputs from this tool are estimates of greenfield runoff rates. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of this data in the design or operational characteristics of any drainage scheme.



CALCULATIONS

Company: WIE Office: London

 Sheet No:
 1 of 3
 Project No:
 WIE18278

 By
 S Whelan
 Date
 09/12/2022

Checked: B McCarthy Date 09/12/2022

Project Title Canford EfW CHP Facility

Calculations Title Summary of surface water strategy

| LOCATION | CALCULATIONS | | | | | | | | | | |
|----------|---|-----------------------------------|-----------|--------------------|---------------|----------------------------------|-----|--|--|--|--|
| | Surface water at the | Site will be mana | ged in | accord | ance with th | he Local Authority requirement | ts, | | | | |
| | | scharge restricted | to the | greenfi | eld runoff ra | ate, including for the impacts o | f | | | | |
| | climate change. | | | | | | | | | | |
| | | | | | | | | | | | |
| | Existing surface w | ater discharge fr | om Ef | W CHP | Facility: | | | | | | |
| | | Area (ha) | Calc | ulation | method | Discharge Rate | | | | | |
| | Site Area | 2.380 | Wal | ingford | (Page 2) | 265.2 l/s | | | | | |
| | (calculated w | vith PIMP of ## % |) | | | | | | | | |
| | | | | | | | | | | | |
| | Existing dischar | ge rate for 1 in 10 | 0 year | storm (| PIMP = 100 | 0%) = 265.2 l/s | | | | | |
| | | | | | | | | | | | |
| | Proposed discharg | | | | | | | | | | |
| | Greenfield runo | | | /s/ha | | 16.7 l/s | | | | | |
| | | l/s/ha l/ | | | | | | | | | |
| | Q _{BAR} | | .2 | | | | | | | | |
| | 1 in 1 year | 1.87 4. | | | | | | | | | |
| | 1 in 30 year | 5.07 12 | | | | | | | | | |
| | 1 in 100 year | | 5.7 | | | | | | | | |
| | 1 in 200 year | 8.24 19 | 0.6 | | | | | | | | |
| | | f (1 0:1 : | | | 6 11 | 55 1 - 0 1/ | | | | | |
| | Proposed discha | arge for the Site is | at the | Q _{BAR} g | reentield ru | inoff rate = 5.2 l/s | | | | | |
| | | | | 000/ | | 1 (1) | | | | | |
| | The proposed d | ischarge rate resu | ilts in a | 98% | reduction in | n peak runoff from the Site. | | | | | |
| | 04 | 4 | | | | | | | | | |
| | Storage requireme | | 2505 | 3 boo | hoon colou | ulated for the Cita vaina | | | | | |
| | A required storage volume of 2505 m³ has been calculated for the Site using | | | | | | | | | | |
| | MicroDrainage Source Control. Runoff from the Site was limited 5.2 l/s and storage been represented within a single feature to identify to total storage required for the Site. | | | | | | | | | | |
| | represented with | iii a sirigie leature | e to lue | illily to | lolal Sloray | ge required for the Site. | | | | | |
| | Storage provide | $d = 2,511 \text{ m}^3, \text{s}$ | ee stro | ane de | taile on che | act 3 | | | | | |
| | Otorage provide | u - 2,311 ,3 | 500 | age de | talis on sile | Set 0 | | | | | |
| | | | | | | | | | | | |
| | | | | | | | | | | | |
| | | | | | | | | | | | |
| | | | | | | | | | | | |
| | | | | | | | | | | | |
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| | | | | | | | | | | | |



CALCULATIONS

Company: WIE Office: London

 Sheet No:
 2 of 3
 Project No:
 WIE18278

 By
 S Whelan
 Date
 09/12/2022

Checked: B McCarthy Date 09/12/2022

Project Title Canford EfW CHP Facility

Calculations Title Existing Discharge Rate - Modified Rational Method

| LOCATION | CALCULATIONS | | | | | | | | | | OP. | TIONS | | | | | | |
|-------------|--|---|------------------------|-----------|--------|------------|------------|--------|------|------|-----|----------|------|-------|-------|---|--|-----|
| | Calculation | s based | on: Design | and Ana | lysis | of urba | n storm o | draina | age | . Th | e W | allingfo | rd P | roce | dure, | | | |
| | Volume 1 F | Principles | methods a | and pract | ice. | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | User Input | Data | | | | | | | | | | | | | | | | |
| | Total site a | | | | | | | | | | | | 2.38 | ha | | | | |
| | SAAR (Fro | m FEH) | | | | | | | | | | | 575 | | | | | |
| | · · · · · · · · · · · · · · · · · · · | | rom FEH) | | | | | | | | | 4 | 1.81 | | | | | |
| | Rainfall Intensity (From FEH) PIMP (% impervious) | | | | | | | | | | | 100 % | | | | | | |
| | Soil Type | | | | | | | | | | | (| 0.30 | | | | | |
| | | Very Low Runoff (well drained sandy, loamy or earthy peat soils | | | | | | | | | | (| 0.15 | | | | | |
| | Low Runof | Low Runoff (Very permeable soils (e.g. gravel, sand) | | | | | | | | | | (| 0.30 | | | | | |
| | _ | Moderate (Very fine sands, silts and sedimentary clays) | | | | | | | | | | (| 0.40 | | | | | |
| | ` | | Clayey or loamy soils) | | | | | | 0.45 | | | | | | | | | |
| | | | oils of the | | nds) | | | | | | | (| 0.50 | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| Fig. 9.7 | UCWI (Fro | m Figure | 9.7 of Wa | llingford | Metho | od) | | | | | | | 52 | | | | | |
| | | | | | | | | | | | | | | | | | | |
| Eqn. 13 | Qp (peak c | lischarge |) = 2.78 Cv | CRIA | | | | | | | | | | | | | | |
| | Where: | Qp (Pea | ak Dischar | ge) | i = ra | ainfall ir | ntensity | | | | A = | Total A | rea | | | | | |
| | | | | | | | | | | | | | | | | | | |
| From FEH | Average rainfall Intensity (i) | | | | | | | | | | | | | | | | | |
| | M100_60 is: 41.81 mm | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| Eqn 7.20 | Cv = PR/10 | 00 | | | | | | | | | | | | | | | | |
| Eqn 7.3 | PR = (| 0.829 PIN | MP) + (25.0 | SOIL) + | (0.0 | 78 UCV | VI) - 20.7 | | | | | | | | | | | |
| | PIMP (Percentage of catchment which is impervious) | | | | | | | | | 100 | % | | | | | | | |
| Page 52 | Note: PIMP can not be less than 4 | | | | | | | , | | | 40 | % | | | | | | |
| | | Thus va | lue of PIM | P to be u | sed | | | | | | 100 | % | | | | | | |
| | | Soil: | 0.30 | | WI: | 52 | | | | | | | | | | | | |
| | PR = | | | | | | | | | | 1 | 73.76 | | | | | | |
| | Thus Cv = | | | | | | | | | | | 0.74 | | | | | | |
| Sec 7.10 | CR (Recommended for simulation and design) | | | | | | | | | | | 1.3 | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | Qp for 1 in | 100 yea | r 60 minut | e duratio | n = | | | 26 | 5.2 | I/s | or | 1 | 11.4 | l/s/h | a | | | |
| | | , | | | | | | | | | | | | | | | | +++ |
| | | | | | | | | | | | | | | | | | | +++ |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | _ | | + |



CALCULATIONS

WIE Office: London Company: 3of 3 Project No: WIE18278 Sheet No: Ву S Whelan Date 09/12/2022 Date 09/12/2022

B McCarthy

Checked:

Project Title Canford Energy from Waste Facility

Calculations Title Proposed surface water storage

| CATION | 1 | | | CALCUL | , | | | | OPTIONS |
|--------|---|--------------------------------------|------------|-----------------------|---------------|-----------|--------------------|---------------------|---------|
| | Countries and the | o Cita | | | حالة حالة بين | / | | | |
| | Surface water at the water discharge re | etricted t | n the aree | aged in accordance | e with the | for the i | numority requireme | change | |
| | water disoriarge re | Stricted t | o are gree | rincia ranon rate, ii | loidailig | 101 110 1 | impacts of climate | oriango. | |
| | | | | | | | | | |
| | Outfall details | | | | | | | | |
| | | | | | | | | | |
| | Invert Level = | 41.81 | mAOD | No. outgoing pip | nes = | 2 | | | |
| | Ground Level : | | mAOD | Outgoing diame | | | mm | | |
| | | 2.72 | | Outgoing diame | lei – | 100 | 111111 | | |
| | Depth bgl = | 2.12 | m | | | | | | |
| | | | | | | | | | |
| | Storage details | 8 | | | | | | | |
| | | | | | | | | | |
| | Tank 1: | | | | | | | | |
| | run length = | 46 | m | Invert Level = | 42.00 | mAOD | Cover = | 0.53 m | |
| | gradient = | 245 | (1:X) | Ground Level = | 44.53 | mAOD | Area = | 137 m ² | |
| | Backdrop = | 0 | mm | Tank Depth = | 2.00 | m | Volume = | 260 m ³ | |
| | | | | | | | | | |
| | Tank 2: | | | | | | | | |
| | run length = | 91 | m | Invert Level = | 42.18 | mAOD | Cover = | 0.54 m | |
| | gradient = | 245 | (1:X) | Ground Level = | | | Area = | 90 m ² | |
| | Backdrop = | 0 | mm | Tank Depth = | | m | Volume = | 154 m ³ | |
| | Баскигор – | 0 | 111111 | rank Deptii - | 1.00 | 111 | voluitle – | 104 ([] | |
| | TI- 0- | | | | | | | | |
| | Tank 3: | 445 | | | 40.00 | | | 0.50 | |
| | run length = | 115 | m | Invert Level = | | mAOD | Cover = | 0.50 m | |
| | gradient = | 245 | (1:X) | Ground Level = | | mAOD | Area = | 840 m ² | |
| | Backdrop = | 0 | mm | Tank Depth = | 1.75 | m | Volume = | 1397 m ³ | |
| | | | | | | | | | |
| | Paving 01 | | | | | | | | |
| | run length = | 158 | m | Invert Level = | 42.45 | mAOD | Cover = | 0.57 m | |
| | gradient = | 245 | (1:X) | Ground Level = | 44.53 | mAOD | Area = | 163 m ² | |
| | Backdrop = | 0 | mm | Storage Depth : | 1.50 | m | Volume = | 73 m ³ | |
| | | | | | | | | | |
| | Paving 02 | | | | | | | | |
| | run length = | 215 | m | Invert Level = | 42 69 | mAOD | Cover = | 1.11 m | |
| | gradient = | 245 | (1:X) | Ground Level = | | | Area = | 126 m ² | |
| | Backdrop = | 0 | ` ' | | | | Volume = | 76 m ³ | |
| | Баскогор – | U | mm | Storage Depth : | 2.00 | m | volume – | 70 m ³ | |
| | David 00 | | | | | | | | |
| | Paving 03 | 40- | | | 10.00 | | | 10.50 | |
| | run length = | 125 | m | Invert Level = | | mAOD | Cover = | 0.50 m | |
| | gradient = | 245 | (1:X) | Ground Level = | | | Area = | 1082 m ² | |
| | Backdrop = | 0 | mm | Storage Depth : | 1.70 | m | Volume = | 552 m ³ | |
| | | | | | | | | | |
| | | | | | | | | | |
| | Storage volum | e summa | ary | | | | | | |
| | | | | | | | | | |
| | Tank 1: | 260 m ³ | | | | | | | |
| | Tank 2: | 154 m ³ | | | | | | | |
| | | 1397 m ³ | | | | | | | |
| | Paving 01 | 73 m ³ | | | | | | | |
| | Paving 01 Paving 02 | 75 m ³ | | | | | | | |
| | | 76 m ³ 552 m ³ | | | | | | | |
| | Paving 03 | | | | | | | | |
| | Total 2 | 2511 m ³ | | | | | | | |